

**U.S. DEPARTMENT OF COMMERCE**

NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION  
NATIONAL OCEAN SERVICE

# DATA ACQUISITION AND PROCESSING REPORT

*Type of Survey*

**Hydrographic**

*Project No.*

**M-I907-NF-13**

*Registry No.*

**W00246, W00247**

## LOCALITY

*State*

**Puerto Rico**

*General Locality*

**North Atlantic Ocean**

**2013**

**CHIEF OF PARTY**

**Timothy Battista, Mike Stecher**

## LIBRARY & ARCHIVES

**DATE**

**March 2013**

## HYDROGRAPHIC STYLE SHEET

**INSTRUCTIONS** — The Hydrographic Sheet should be accompanied by this form, filled in as completely as possible, when the sheet is forwarded to the Office.

**FIELD No**  
NOAA Ship Nancy Foster

State	Puerto Rico
General Locality	North Atlantic Ocean
Sub-Locality	Pta. Miquillo to Cabo San Juan, 10 nm W of Isla De Culebra
Scale	1:20,000
Date of Survey	March 5, 2013 to March 29, 2013
Instructions dated	February 20, 2013    Project No.    M-I907-NF-13
Vessel	NOAA Ship Nancy Foster
Chief of party	Timothy Battista
Surveyed by	NOAA Center for Coastal Monitoring and Assessment
Soundings by	Reson 7125 SV, Kongsberg EM1002
Graphic record scaled by	N/A
Graphic record checked by	N/A
Automated Plot	N/A
Verification by	N/A
Soundings in	Meters at MLLW
Remarks	All times are UTC.

## ACRONYMS AND ABBREVIATIONS

AWOIS	Automated Wreck and Obstruction Information System
BAG	Bathymetric Attributed Grid
BASE	Bathymetry Associated with Statistical Error
CCMA	Center for Coastal Monitoring and Assessment
CO-OPS	Center for Operational Oceanographic Products and Services
CTD	Conductivity Temperature Depth
CUBE	Combined Uncertainty and Bathymetry Estimator
DGPS	Differential Global Positioning System
FPM	Field Procedures Manual (April 2012)
GAMS	GPS Azimuth Measurement Subsystem
GPS	Global Positioning System
HIPS	Hydrographic Information Processing System
HSSD	Hydrographic Survey Specifications and Deliverables Manual (April 2012)
HSTP	Hydrographic Systems Technology Programs
HSX	Hypack Hysweep File Format
HTD	Hydrographic Surveys Technical Directives
HVF	HIPS Vessel File
IHO	International Hydrographic Organization
IMU	Inertial Motion Unit
MLLW	Mean Lower Low Water
NMEA	National Marine Electronics Association
NOAA	National Oceanic and Atmospheric Administration
NOS	National Ocean Service
OMAO	Office of Marine and Aviation Operations (NOAA)
POS/MV	Position and Orientation System for Marine Vessels
PPS	Pulse per second
ROV	Remotely Operated Vehicle
R/V	Research Vessel
SAT	Sea Acceptance Test
SBE	Smooth Best Estimate
SBET	Smooth Best Estimate and Trajectory
SVP	Sound Velocity Profiler
TPE	Total Propagated Error
TPU	Total Propagated Uncertainty
TSG	Thermosalinograph
USCRTF	U.S. Coral Reef Task Force
ZDA	Global Positioning System timing message
ZDF	Tide Zone Definition File

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**M-I907-NF-13**  
**Data Acquisition and Processing Report**  
**Caribbean Sea, USVI**  
**March 2013**  
**NOAA Ship Nancy Foster**  
**Center for Coastal Monitoring & Assessment**  
**Biogeography Branch**  
**Lead Hydrographer, Mike Stecher**  
**Lead Scientist, Timothy Battista**

## **INTRODUCTION**

In June 1998, the U.S. Coral Reef Task Force (USCRTF) was established by Presidential Executive Order 13089. The USCRTF mission is to lead, coordinate, and strengthen U.S. government actions to better preserve and protect coral reef ecosystems. The National Oceanic and Atmospheric Administration's (NOAA) Center for Coastal Monitoring and Assessment (CCMA) Biogeography Team is supporting the USCRTF mandate. The Biogeography Team has completed its tenth year of an ongoing scientific research mission on board the NOAA Ship Nancy Foster from March 5<sup>th</sup> to March 29<sup>th</sup>, 2013.

The objective of this project was to collect a multibeam bathymetric dataset with 100 percent seafloor ensonification, along with multibeam backscatter suitable for seafloor characterization in a high-priority conservation area. This report applies to surveys W00246 and W00247 that took place near the west coast of the island of Puerto Rico. Unless otherwise noted, the acquisition and processing procedures used, and deliverables produced are in accordance with the NOAA Hydrographic Survey Specifications and Deliverables Manual (HSSD) of April 2012, Field Procedures Manual (FPM) of April 2012, and all active Hydrographic Surveys Technical Directives (HTD). The project instructions required complete multibeam coverage in water depths greater than ten meters for both survey sites. The multibeam data was collected to conform to IHO Order 1 (<100m) and Order 2 (>100m) accuracy standards. The strategies developed for each survey area took into account the minimum depths, general bathymetry, and time allotment. The delineation and identification of seafloor habitats within areas mapped during the mission was assisted by the use of an ROV with video and camera capabilities. All references to equipment, software, or data acquisition and processing methods were valid at the time of document preparation

## A. EQUIPMENT

Detailed descriptions of the equipment and systems, including hardware and software, used for bathymetric data acquisition and processing appear below.

**Table 1.** NOAA Ship Nancy Foster Hardware

Hydrographic Systems Inventory Cruise# M-I907-NF-13				HARDWARE
Equipment type	Manufacturer	Model	Serial #	Firmware
Transducer	Kongsberg/Simrad	EM1002	288	N/A
Transceiver Unit	Kongsberg/Simrad	EM1002	303	N/A
Reson	Reson	7125SV	1812025	MR 7.1.1
Reson Projector Unit	Reson	TC 2160	2308096	N/A
Reson Projector Unit	Reson	TC 2163	4408349	N/A
Reson Receiver Unit	Reson	EM 7200	2908034	N/A
Inertial GPS PCS	Applanix	POS/MV 320 V4	2249	3.2
IMU	Applanix	LN 200	447	N/A
DGPS	Trimble	DSM 132	224096283	3.0
SVP	SBE	SBE 19	0355	N/A
SVP	SBE	SBE 19	1448	N/A
SVP	Reson	SVP 71	2008048	N/A

**Table 2.** Acquisition & Processing Software

Hydrographic Systems Inventory Cruise# M-I907-NF-13			SOFTWARE
Equipment type	Manufacturer	Model	Software Version
Inertial GPS PCS	Applanix	POS/MV 320 V4	5.03
Navigation	Coastal Oceanographics	Survey	2012
Acquisition	Coastal Oceanographics	Hysweep	2012
Acquisition	Kongsberg/Simrad	MERLIN	v5.2.2
Acquisition	Sun Microsystems	TT32220431	Solaris 8
Processing	NOAA	Velocwin	8.85
Processing	CARIS	HIPS & SIPS	7.1.2
7k Control Center 7125	Reson	7125	FP1.3.2
7k Control Center 7125	Reson	7K UI	3.12.7.3
7k Control Center 7125	Reson	7K Center	3.7.11.11
7k Control Center 7125	Reson	7K IO	3.4.1.11



## **A1. SURVEY VESSEL**

The NOAA Ship Nancy Foster (R352) is fifty-seven meters in length, has a beam of twelve meters, and draws approximately three meters of water. During the Charleston, South Carolina drydock period in November of 2005, numerous survey hardware and software installations were implemented by NOAA's Office of Marine and Aviation Operations (OMAO) to make multibeam data acquisition a more integral component of the ship's research support. OMAO funded the permanent installation of a Simrad EM1002 multibeam sonar, an Applanix POS/MV positioning system, ancillary sensors, and support equipment. The Nancy Foster was also permanently mobilized with a dual frequency Reson 7125 SV multibeam system during a dry dock period in February of 2011.

**Fig. 1: NOAA Ship *Nancy Foster***



## A2. MULTIBEAM SYSTEMS

### A2.a Kongsberg EM1002

A Simrad EM1002 multibeam echosounder is permanently hull-mounted between two fiberglass hydrodynamic fittings starboard of the keel line, aft of the bow. The EM1002 is a 95-kHz system with a 150° swath consisting of 111 individually formed, electronically roll-stabilized 2° beams, with a maximum ping rate of 10Hz, depending on water depth. The EM1002 has three different automatically adjusted pulse lengths to maximize coverage in deeper waters at 0.2, 0.7 and 2 milliseconds respectively. A combination of phase and amplitude detection was used, resulting in measurement accuracy practically independent of beam angle. The system is compensated in real-time for sound velocity changes at the transducer array, to assist the electronic beam steering capabilities.



**Fig 2: EM1002 transducer fairing**



**Fig 3: EM1002 transducer**

The EM1002 sonar system is controlled with a UNIX-based operator system (SUN Solaris 8) that utilizes the Common Desktop Environment and Kongsberg's MERLIN v5.2.2 acquisition and control program. Before surveying began, and periodically thereafter, the EM1002 system self-test (BIST test) was performed to confirm the sonar's operating status. No sonar errors were observed during the survey. As per advice from the Kongsberg representative during the SAT, the automatic and default parameters were used to control the sonar during data acquisition. The EM1002 backscatter default options were verified with Adel Sterling and the Hawaii Mapping Resource Group, who have extensive experience acquiring backscatter imagery with the EM1002 system onboard the R/V *Kilo Moana*. The equidistant beam-spacing mode was chosen to give a uniform distribution of soundings on the seafloor. The ping rate was set by the system and was automatically adjusted according to the depth below the transducer. Only limited runtime parameters changed during the survey including the maximum port and starboard angles, which did not exceed 60°.

## A2.b Reson 7125 SV

A Reson SeaBat 7125 SV dual-frequency multibeam sonar with an integrated SVP-71 sound velocity profiler (SVP) was mounted onto the hull of the Nancy Foster during a dry dock period in February, 2011. Due to the poor performance encountered with the 7125 SV during the 2011 field season, the original receiver array was replaced for the 2012 field season with a refurbished unit.

The sonar is mounted on the hull, and is located port of the keel, and forward of the reference point of the vessel. The Reson 7125 SV operates at a selectable 400 kHz or 200 kHz frequency, producing a 140° swath of 512 0.5° x 1.0° uniform beams. All of the multibeam data collected for these surveys were acquired with the 400 kHz frequency. The performance of the 200 kHz was determined to be sub-par during the 2012 field season.

**Fig 4:** Reson 7125 mounted onto the hull of the Nancy Foster



### **A3. POSITION, HEADING and MOTION REFERENCE UNITS**

#### **A3.a Applanix Position & Orientation System for Marine Vessels 320 Version 4 (POS/MV)**

The Nancy Foster is outfitted with an Applanix POS/MV 320 V4 and is augmented by a Trimble DSM132 Differential Global Positioning System (DGPS). The POS/MV system comprises of an inertial motion unit (IMU), dual Global Positioning System (GPS) antennas, and a data processor.

The POS/MV system provided attitude, heading, and position for the sonar data. The POS/MV also provided time synchronization for the sonar's acquisition systems using the ZDA GPS message and PPS strobe.

The POS/MV was configured to log TrueHeave and POSpac data packets at 50Hz for post-processing with Caris and POSpac MMS if needed. Under typical survey conditions several POSpac file were logged each survey day.

#### **A3.b Trimble DSM132 Differential GPS Receiver**

A Trimble DSM132 acquired corrections from the U.S. Coast Guard beacon located at Isabel, Puerto Rico (295 kHz). The DSM132 was also configured to receive satellite correctors from Omnistar when the vessel was out of range of the Isabel station.

The DSM132 provided differential corrections to the POS/MV. The DSM132 also acted as a redundant positioning system onboard for quality control purposes. A pre-cruise comparison between the POS/MV and DSM132 positioning systems was conducted while the vessel was stationary in port in San Juan with satisfactory results.

### **A4. SOUND SPEED MEASUREMENT SYSTEMS**

The Sea-Bird Electronics (SBE) sound velocity profilers were factory calibrated prior to the start of acquisition. The calibration results are included in the Separates II section of the Descriptive Reports (DR) for W00246 and W00247.

#### **A4.a SBE Thermosalinograph**

The vessel is equipped with a hull-mounted SBE 45 thermosalinograph (TSG) near the EM1002 transducer. The TSG measures near-surface conductivity and temperature to calculate sound velocity in real time. The data from the TSG was streamed to the EM1002's MERLIN acquisition-and-control software to aid in electronic beam steering.

#### **A4.b SBE 19Plus**

The primary Conductivity Temperature Depth CTDs for determining sound velocity throughout the water column was a SBE 19Plus. Sound velocity casts were deployed approximately every

four hours during survey operations. Sound velocity casts were processed with Velocwin V8.9.0.2 software and converted to Simrad & Caris formats. The vessel's hydraulic winch was rigged through the block of the port J-Frame davit, which provided a consistent rate of descent for acquisition of the sound velocity data.

#### **A4.c Reson SVP-71**

The SVP-71 measures the speed of sound near the Reson 7125 transducers to provide real-time surface sound-speed values. The sound speed is output to the Reson 7125's processing unit. The sonar requires sound velocity information for beam-forming and cannot be used to acquire data without the real-time sound velocity information.

### **A5. ACQUISITION AND PROCESSING SYSTEMS**

#### **A5.a Hypack Hysweep, Geocoder and Fledermaus**

Coastal Oceanographics Hypack/Hysweep 2012 was used for 7125 SV data acquisition and vessel navigation. The system provided precise time tagging of the sensor data and real-time data displays for quality control. Data was acquired in three formats: .RAW, .HSX and .S7K.

A combination of the Geocoder implementation included with Hypack and Fledermaus were used to process the backscatter acquired by the 7125 SV and EM1002.

#### **A5.b Kongsberg MERLIN v5.2.2**

Kongsberg's MERLIN v5.2.2 multibeam control and data acquisition software was used for EM1002 multibeam data collection. The software operates on a SOLARIS-based Sun Microstation workstation.

#### **A5.c Hydrographic Systems Technology Programs (HSTP) Software**

The Velocwin software created by NOAA's Hydrographic Systems and Technology Programs (HSTP) was used to process the SBE data. Velocwin creates and archives sound velocity profiles, performs quality assurance, and processes pressure-based depth data.

#### **A5.d CARIS**

Bathymetric survey data was converted and processed in Caris HIPS v7.1.2 with modifications to the default CUBE (Combined Uncertainty Bathymetric Estimator) Parameters.XML. The default CUBE Parameters.XML was replaced with the new file issued to all NOAA hydrographic field units included with the FPM. Processing methodology followed the standard Caris HIPS CUBE workflow. These steps include data conversion, filtering, sound velocity correction, tide correction, Total Propagated Error calculation, TrueHeave application, merging, and editing.





### **A6.c Multibeam Sonar Operations**

Full multibeam coverage was a requirement for this survey. Multibeam operations utilized the techniques defined by the HSSD. The sonar systems were tuned to simultaneously maximize bathymetric and backscatter data quality by not over-saturating sonar returns by using the SATMON utility. The multibeam sonar was operated at different range scales throughout the survey by adjusting the depth range to obtain the best coverage in varying depths of water.

### **A7. Quality Assurance**

Acquisition and processing methods followed systematic and standardized workflows as defined by the FPM.

## **B. QUALITY CONTROL**

### **B1. Data Acquisition**

#### **B1.a Multibeam**

Incremental adjustments to the sonar including changes in range and gain were made during acquisition to ensure acquisition of the best quality bathymetric and backscatter data. Vessel speed was adjusted in accordance with the HSSD to ensure required along-track coverage. Typical windows for monitoring raw sensor information included timing synchronization, surface-sound velocity, vessel motion, GPS quality, intensity, and satellite coverage.

Pre-cruise position confidence checks and multibeam lead line checks were conducted to confirm horizontal and vertical positioning accuracies. An SVP comparison check was performed by lashing the two SBE 19*Plus* units together and lowering them simultaneously to the seafloor. The sound speed profiles were computed for each of the sensors and compared to confirm that instrumentation was functioning within survey tolerances.

### **B2. Data Processing**

#### **B2.a Uncertainty Modeling**

Error values for the multibeam and positioning systems were compiled from manufacturer specification sheets for each sensor and from values set forth in Table 4-10 of the FPM.

Uncertainty values relating to the vessel's two survey systems were entered into the HVF's. The estimated tidal error budget in the vicinity of the project area was not computed by CO-OPS due to a lack of available water level time series data. The measured tidal error budget in the vicinity of W00246 and W00247 was therefore estimated to be 0.025 meters at the 95% confidence level. The tidal zoning error budget in the vicinity of W00246 and W00247 was also estimated to be 0.15 meters at the 95% confidence level. Sound speed uncertainties for the survey were based on the defaults as listed in Table 4-10 of the FPM.

#### **B2.b Vessel Files**

Two HVF files were created to correspond to each sonar configuration used during the survey. The vessel file contains all offsets and system biases for the survey vessels and its systems, as well as error estimates for latency, sensor offset measurements, attitude and navigation measurements, and draft measurements. Sensor offsets values were calculated from the vessel surveys, which were conducted prior to the start of field operations.

The dynamic draft survey was performed during the Sea Acceptance Test (SAT) offshore of Charleston, S.C. in March 2006. OMAO representatives performed the survey and evaluated the results. The dynamic draft was determined using the reference surface method as per the FPM. Results of the dynamic draft survey were also entered into the vessel configuration files. The



Nancy Foster HVF reports that include TPU values are located in Appendix I.

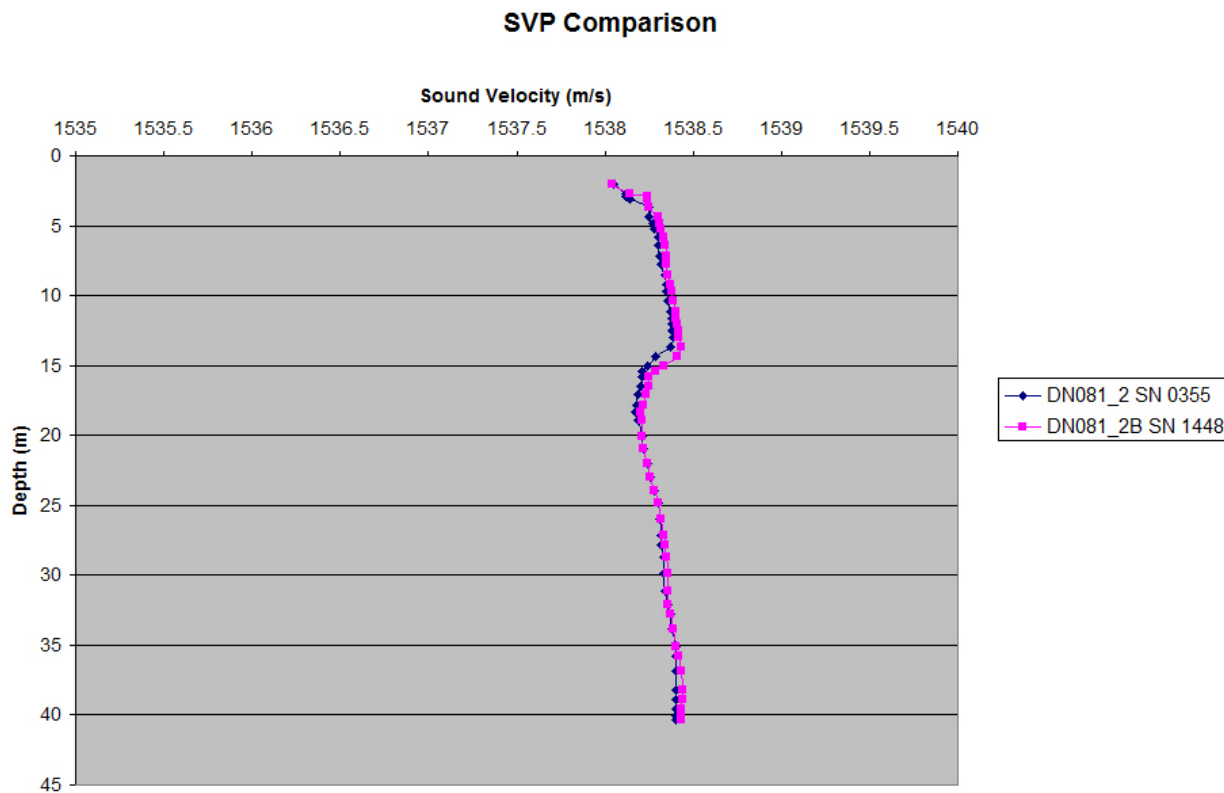
### B2.c Static Draft

Draft was measured pre- and-post cruise from draft marks on the port side of the vessel's hull for the EM1002 and the 7125 SV. The total draft change for the 7125 SV and the EM1002 draft change was negligible.

### B2.d Sound Velocity

Sound-speed profiles were applied to each line using the “nearest-in-distance-within-time” option in the Caris SVP correction routine. Velocity casts were taken at approximately four-hour frequency intervals with the SBE 19*Plus*. The online surveyors made periodic comparisons and verifications of sound-velocity measurements that were made during survey operations between the SVP-71 and the SBE 19*Plus*. In addition, the two SBE 19*Plus* units were combined, deployed, and processed to confirm SBE calibration coefficients.

Fig 6: SVP comparison



### B3. CARIS Data Processing

Multibeam data processing followed the standard HIPS workflow for CUBE editing except that the hypothesis surface was not edited. Instead, fliers influencing the CUBE surface were rejected and critical soundings not incorporated in the CUBE surface were designated.

The list of correctors and filters applied to the bathymetric data in HIPS appears below. Several of the steps are interim processes and were re-applied as needed.

1. Apply True Heave
2. Load Delta Draft
3. Load Tide
4. Apply sheet-wide concatenated sound-speed profiles
  - Nearest in distance within time
5. Merge
6. Compute TPU
7. Filters applied based on the following criteria:
  - Reject soundings with poor quality flags (0 and 1 for Reson)
  - Add data to CUBE surface
    - Resolution dependent on depth
    - Density & Local Disambiguation method
    - Advanced NOAA settings specific to surface resolution

Each survey area was subdivided by creating three separate field sheets; W00246, W00247 and Vieques. CUBE surfaces were created using the algorithm and parameters contained in the NOAA Cubeparams.xml file as provided with FPM. CUBE surfaces were created over the survey areas using grid-resolution thresholds and resolution-dependent maximum propagation distances for complete coverage surveys as specified in the HSSD. The NOAA parameter configurations for resolutions used are listed in Table 3.

**Table 3.** Surface Resolutions

Surface Resolutions		CUBE Parameters
Depth Range	Grid Resolution	Configuration Name
18 to 40 meters	2 meter	NOAA_2m
36 to 80 meters	4 meter	NOAA_4m
72 to 160 meters	8 meter	NOAA_8m
144+ meters	16 meter	NOAA_16m

The CUBE workflow included the review and focused editing of multiple CUBE child layers including Density, Hypothesis Count & Strength, Node Standard Deviation, and Uncertainty. Survey coverage was reviewed to ensure that there were no substantial holidays and that there were no data gaps present over significant features. The HIPS density layer of each grid was

reviewed to ensure that the minimum sounding density of three soundings per node was achieved for 95 percent of nodes populated by mainscheme survey lines and that significant features had a designated sounding overlying the least depth. Some areas where ping drops occurred from the 7125 SV do result in some areas of low sounding density on each sheet.

#### **B4. Final Bathymetric Processing**

The finalized CUBE surfaces were generated using the “greater of the two” option for the final uncertainty value. Resolution dependent depth thresholds were also applied as defined in the HSSD.

Finalized surfaces were then reviewed in the HIPS 3D graphics window with an extreme vertical exaggeration to verify that all fliers have been removed from the surfaces. The BASE Surface to BAG (Bathymetric Attributed Grid) function was then used on each CUBE Depth surface and exported from HIPS for submittal.

### **C. CORRECTIONS TO ECHO SOUNDINGS**

#### **C1. Vessel HVFs**

Caris HIPS HVF's were created to define the vessel's offsets and sounding uncertainties. The HVFs were used for converting and processing multibeam data collected both sonar systems. The HVFs used for this project are included with the digital data submitted with the survey.

#### **C2. Vessel Offsets**

On February 7, 2006 the NOAA Ship Nancy Foster had her sensor offsets surveyed by the Power & Control Systems Group of L3 Communications. The IMU, GPS antennas, EM1002 transducer and the center of rotation were surveyed with respect to the reference point, which is slightly aft of the IMU in the forepeak of the vessel. An additional survey to locate the newly mounted 7125 was performed on February 28, 2011 by The IMTEC Group, Ltd.

These offsets were entered into the MERLIN acquisition software, POS/MV software, and the appropriate areas of the Caris HVF files. The vessel survey reports are included in Appendix I.

#### **C3. Patch Tests**

Multibeam patch tests were conducted for each sonar system. The purpose of the patch test is to measure alignment offsets between the IMU sensor and the multibeam transducer, while also determining time delays between the time-tagged sensor data. Each patch test consisted of a series of lines run in a specific pattern, which were then used in pairs to analyze roll, pitch, and heading alignment bias angles.

Roll alignment was determined by evaluating the reciprocal lines run over a flat bottom. The pitch tests consisted of set of reciprocal lines located on a steep slope. The yaw error was determined by running parallel lines over the same area. All lines were run at approximately three knots to six knots. Patch tests were run in the local survey area.

Selected pairs of lines were then analyzed in HIPS Calibration editor to measure the angular sensor bias values. Visual inspection of the data confirmed each adjustment. Patch test values for both sonar systems are listed in Table 4.

**Table 4. Patch Test Values**

<b>M-I907-NF-13 Patch Test Values</b>				
	<b>Pitch</b>	<b>Roll</b>	<b>Yaw</b>	<b>Latency</b>
<b>EM1002</b>	0.14	0.00	-0.10	0.00
<b>7125-SV</b>	0.00	0.09	-0.46	0.00

#### **C4. Static and Dynamic Draft**

Static draft values were obtained from visual observations of the projection draft marks on the starboard side of the Nancy Foster for the EM1002 and the 7125 SV. The static draft recorded on March 4<sup>th</sup>, 2013 was 3.74m while tied up in San Juan, Puerto Rico. Subtracting the initial draft value of 3.74m from the fixed offset (1.68m) for the Reference Point to the EM1002 gives the final draft reading of -2.06m. A draft value of -2.053m was determined for the 7125. The draft values were entered into the MERLIN software for the EM1002 and into the HVF for the 7125 SV and confirmed with leadline readings. The final EM1002 and 7125 SV draft reading at the end of the cruise (March 30<sup>th</sup>, 2013) was negligible.

The dynamic draft survey was performed during the Sea Acceptance Test (SAT) offshore of Charleston, South Carolina in March of 2006. Representatives from the OMAO performed the survey and evaluated the results. The dynamic draft was determined using the reference surface method as per the FPM. Results of the dynamic draft survey were entered into the vessel configuration files.

#### **C5. Attitude**

All attitude corrections are generated by the POS/MV using data from the IMU-200 Inertial Measurement Unit. The 7125 had roll stabilization applied in real-time. The EM1002 had heave, pitch and roll applied in real-time, therefore attitude was not applied for the EM1002 data in post-processing.

#### **C6. True Heave**

The Nancy Foster is equipped with the POS/MV TrueHeave (TH) option. True Heave is a “delayed” heave corrector as opposed to “real-time” heave corrector and is fully described in

Section 6 of the POS/MV Version 4 Installation and Operation Manual. TH is logged along with other POSpac data in the daily POS files through the Ethernet Logging function in the POS/MV controller software. To ensure proper calculation of TH, files are logged for at least three minutes prior to the beginning of acquisition and three minutes past the end of each day's survey operations. TH was applied to only the 7125 SV data for both surveys W00246 and W00247.

## **C7. Tide and Water Level Corrections**

Existing water level stations were used in conjunction with height and time correctors in a Caris tide zone definition file (ZDF). Predicted tides, adjusted to Mean Lower Low Water (MLLW), and ZDFs were supplied by NOAA CO-OPS prior to the commencement of survey operations. Verified six-minute-interval water level and final tide-zone correctors were applied while post-processing the data. During the computation of the TPE, survey-specific parameters including the estimated tidal errors were applied. The estimated tidal-error contribution to the total survey error budget was not determined by CO-OPS due to a lack of available water level time series data, therefore estimated values were used. The primary and subordinate stations experienced no downtime during periods of hydrographic survey.

## **C8. Sound Velocity Correction**

After each cast the sound speed data was reviewed for outliers or anomalies that could impact data quality. Additionally, the sound speed measured by the SBE 19*Plus* at the surface was compared to the Reson 7125 SV and EM1002 surface velocities for agreement, to ensure that both systems were working properly. In addition to these periodic comparisons, a comparison check was performed by lashing two SBE 19*Plus* units together and simultaneously lowering them to the bottom. All comparisons were well within survey specification.

For each survey all casts were concatenated into a master SVP file that included time, position, depth, and sound speed. The sound-speed correction was applied to each line using the nearest-in-distance- within-time option in the HIPS SVP correction routine.

## **C9. Lead Line Comparisons**

Lead line checks were performed against both of the multibeam echosounders prior to data acquisition. While the vessel was tied up alongside the pier, lead lines were taken starboard of each of the multibeam systems. Digital data was logged simultaneously during the lead line procedure for each system. The multibeam data was then converted and queried in Caris HIPS to confirm that the acoustic depths matched the lead lines. No bias was detected as each of the lead line readings agreed with the multibeam soundings.

**D. Letter of approval**

As Lead Hydrographer, I have ensured that standard field surveying and processing procedures were followed during this project in accordance with the Hydrographic Manual, Fourth Edition; Hydrographic Survey Guidelines; Field Procedures Manual, and the NOS Hydrographic Surveys Specifications and Deliverables Manual, as updated for 2012.

I acknowledge that all of the information contained in this report is complete and accurate to the best of my knowledge.



Approved and Forwarded: \_\_\_\_\_

Michael Stecher  
NOAA Contractor  
CCMA Biogeography Branch

ACSM Certified Hydrographer #237

## **APPENDIX I**

### **VESSEL REPORTS AND SURVEYS**

Vessel Name: NF7125\_400khz\_512\_2013.hvf

Depth Sensor:

Sensor Class: Swath  
Time Stamp: 2012-093 00:00

Comments:  
Time Correction(s) 0.000

Transducer #1:

-----  
Pitch Offset: 0.000  
Roll Offset: 0.150  
Azimuth Offset: 0.000

DeltaX: 0.538  
DeltaY: -2.179  
DeltaZ: 1.084

Manufacturer:  
Model: sb7125d  
Serial Number:

Depth Sensor:

Sensor Class: Swath  
Time Stamp: 2013-065 00:00

Comments:  
Time Correction(s) 0.000

Transducer #1:

-----  
Pitch Offset: 0.000  
Roll Offset: 0.090  
Azimuth Offset: -0.460

DeltaX: 0.538  
DeltaY: -2.179  
DeltaZ: 1.084

Manufacturer:  
Model: sb7125d  
Serial Number:

---

Navigation Sensor:

Time Stamp: 2012-093 00:00

Comments: (null)  
Time Correction(s) 0.000  
DeltaX: 0.000



DeltaY: 0.000  
DeltaZ: 0.000

Manufacturer: (null)  
Model: (null)  
Serial Number: (null)

---

Gyro Sensor:

Time Stamp: 2012-093 00:00

Comments:  
Time Correction(s) 0.000

---

Heave Sensor:

Time Stamp: 2012-093 00:00

Comments: (null)  
Apply Yes  
Time Correction(s) 0.000  
DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000  
Offset: 0.000

Manufacturer: (null)  
Model: (null)  
Serial Number: (null)

---

Pitch Sensor:

Time Stamp: 2012-093 00:00

Comments:  
Apply Yes  
Time Correction(s) 0.000  
Pitch offset: 0.000

Manufacturer: (null)  
Model: (null)  
Serial Number: (null)

---

Draft Sensor:

Time Stamp: 2012-093 00:00

Apply Yes  
Comments:  
Time Correction(s) 0.000

Entry 1)	Draft: 0.007	Speed: 5.054
Entry 2)	Draft: 0.041	Speed: 6.143
Entry 3)	Draft: 0.002	Speed: 7.911
Entry 4)	Draft: 0.032	Speed: 9.778

---

TPU

Time Stamp: 2012-094 00:00

Comments:  
Offsets

Motion sensing unit to the transducer 1  
X Head 1 -0.537  
Y Head 1 -2.178  
Z Head 1 1.084

Motion sensing unit to the transducer 2  
X Head 2 0.000  
Y Head 2 0.000  
Z Head 2 0.000

Navigation antenna to the transducer 1  
X Head 1 5.280  
Y Head 1 -8.755  
Z Head 1 17.377

Navigation antenna to the transducer 2  
X Head 2 0.000  
Y Head 2 0.000  
Z Head 2 0.000

Roll offset of transducer number 1 0.000  
Roll offset of transducer number 2 0.000

Heave Error: 0.050 or 5.000'' of heave amplitude.

Measurement errors: 0.002

Motion sensing unit alignment errors

Gyro:0.000 Pitch:0.000 Roll:0.000

Gyro measurement error: 0.020

Roll measurement error: 0.020

Pitch measurement error: 0.020

Navigation measurement error: 1.000

Transducer timing error: 0.010

Navigation timing error: 0.010

Gyro timing error: 0.010

Heave timing error: 0.010

PitchTimingStdDev: 0.010

Roll timing error: 0.010

Sound Velocity speed measurement error: 0.000

Surface sound speed measurement error: 0.000

Tide measurement error: 0.000

Tide zoning error: 0.000

Speed over ground measurement error: 0.015

Dynamic loading measurement error: 0.150

Static draft measurement error: 0.150

Delta draft measurement error: 0.030  
StDev Comment: (null)

---

Svp Sensor:

Time Stamp: 2012-093 00:00

Comments:

Time Correction(s) 0.000

Svp #1:

-----

Pitch Offset: 0.000  
Roll Offset: 0.000  
Azimuth Offset: 0.000

DeltaX: 0.538  
DeltaY: -2.179  
DeltaZ: 1.084

SVP #2:

-----

Pitch Offset: 0.000  
Roll Offset: 0.000  
Azimuth Offset: 0.000

DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000

Time Stamp: 2013-065 00:00

Comments:

Time Correction(s) 0.000

Svp #1:

-----

Pitch Offset: 0.000  
Roll Offset: 0.000  
Azimuth Offset: 0.000

DeltaX: 0.538  
DeltaY: -2.179  
DeltaZ: 1.084

SVP #2:

-----

Pitch Offset: 0.000  
Roll Offset: 0.000  
Azimuth Offset: 0.000

DeltaX: 0.000  
DeltaY: 0.000

DeltaZ: 0.000

---

WaterLine:

Time Stamp: 2012-093 00:00

Comments: (null)

Apply Yes

WaterLine -2.053

---

DeltaX: 0.000

DeltaY: 0.000

DeltaZ: 0.000

---

WaterLine:

Time Stamp: 2012-093 00:00

Comments: (null)

Apply Yes

WaterLine -2.053

---

**Vessel Name: NF\_EM1002\_USVI.hvf**

Depth Sensor:

Sensor Class: Swath  
Time Stamp: 2006-064 00:00

Comments: SAT  
Time Correction(s) 0.000

Transducer #1:

-----

Pitch Offset: 0.900  
Roll Offset: -0.110  
Azimuth Offset: -0.200

DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000

Manufacturer:  
Model: em1002  
Serial Number:

Depth Sensor:

Sensor Class: Swath  
Time Stamp: 2007-044 00:00

Comments: 2007\_Patch  
Time Correction(s) 0.000

Transducer #1:

-----

Pitch Offset: 1.490  
Roll Offset: 0.040  
Azimuth Offset: 0.500

DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000

Manufacturer:  
Model: em1002  
Serial Number:

Depth Sensor:

Sensor Class: Swath  
Time Stamp: 2008-051 00:00

Comments: USVI\_patch  
Time Correction(s) 0.000

Transducer #1:  
-----  
Pitch Offset: 0.140  
Roll Offset: -0.080  
Azimuth Offset: -0.400

DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000

Manufacturer:  
Model: em1002  
Serial Number:

Depth Sensor:

Sensor Class: Swath  
Time Stamp: 2013-064 00:00

Comments: USVI 2013  
Time Correction(s) 0.000

Transducer #1:  
-----  
Pitch Offset: 0.140  
Roll Offset: 0.000  
Azimuth Offset: -0.100

DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000

Manufacturer:  
Model: em1002  
Serial Number:

---

Navigation Sensor:

Time Stamp: 2006-064 00:00

Comments:  
Time Correction(s) 0.000  
DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000

Manufacturer:  
Model:  
Serial Number:

---

Gyro Sensor:

Time Stamp: 2006-064 00:00

Comments: (null)  
Time Correction(s) 0.000

Entry 0) Draft: 0.000 Speed: 0.000

---

Heave Sensor:

Time Stamp: 2006-064 00:00

Comments: Caris TechNote - SV Corrections for Simrad.pdf 072303  
Apply No  
Time Correction(s) 0.000  
DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000  
Offset: 0.000

Manufacturer: (null)  
Model: (null)  
Serial Number: (null)

---

Pitch Sensor:

Time Stamp: 2003-111 00:00

Comments: Caris TechNote - SV Corrections for Simrad.pdf 072303  
Apply No  
Time Correction(s) 0.000  
Pitch offset: 0.000

Manufacturer: (null)  
Model: (null)  
Serial Number: (null)

---

Roll Sensor:

Time Stamp: 2006-064 00:00

Comments: Caris TechNote - SV Corrections for Simrad.pdf 072303  
Apply No  
Time Correction(s) 0.000  
Roll offset: 0.000

Manufacturer: (null)  
Model: (null)  
Serial Number: (null)

---

Draft Sensor:

Time Stamp: 2006-064 00:00

Apply Yes

Comments: (null)

Time Correction(s) 0.000

Entry 1) Draft: 0.007 Speed: 5.054

Entry 2) Draft: 0.041 Speed: 6.143

Entry 3) Draft: 0.002 Speed: 7.911

Entry 4) Draft: 0.032 Speed: 9.778

---

TPU

Time Stamp: 2006-064 00:01

Comments:

Offsets

Motion sensing unit to the transducer 1

X Head 1 1.856

Y Head 1 0.074

Z Head 1 1.800

Motion sensing unit to the transducer 2

X Head 2 0.000

Y Head 2 0.000

Z Head 2 0.000

Navigation antenna to the transducer 1

X Head 1 6.596

Y Head 1 5.760

Z Head 1 17.984

Navigation antenna to the transducer 2

X Head 2 0.000

Y Head 2 0.000

Z Head 2 0.000

Roll offset of transducer number 1 -0.014

Roll offset of transducer number 2 0.000

Heave Error: 0.050 or 5.000'' of heave amplitude.

Measurement errors: 0.020

Motion sensing unit alignment errors

Gyro:0.000 Pitch:0.000 Roll:0.000

Gyro measurement error: 0.020

Roll measurement error: 0.020

Pitch measurement error: 0.020

Navigation measurement error: 2.000

Transducer timing error: 0.000

Navigation timing error: 0.010

Gyro timing error: 0.010

Heave timing error: 0.010

PitchTimingStdDev: 0.010

Roll timing error: 0.010

Sound Velocity speed measurement error: 0.600



Surface sound speed measurement error: 0.500  
Tide measurement error: 0.010  
Tide zoning error: 0.100  
Speed over ground measurement error: 0.250  
Dynamic loading measurement error: 0.000  
Static draft measurement error: 0.100  
Delta draft measurement error: 0.150  
StDev Comment: (null)

---

Svp Sensor:

Time Stamp: 2006-064 00:00

Comments: (null)  
Time Correction(s) 0.000

Svp #1:

-----  
Pitch Offset: 0.000  
Roll Offset: 0.000  
Azimuth Offset: 0.000

DeltaX: 1.856  
DeltaY: 0.811  
DeltaZ: 1.676

SVP #2:

-----  
Pitch Offset: 0.000  
Roll Offset: 0.000  
Azimuth Offset: 0.000

DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000

Time Stamp: 2007-044 00:00

Comments: (null)  
Time Correction(s) 0.000

Svp #1:

-----  
Pitch Offset: 0.000  
Roll Offset: 0.000  
Azimuth Offset: 0.000

DeltaX: 1.856  
DeltaY: 0.811  
DeltaZ: 1.676

SVP #2:

-----

Pitch Offset: 0.000  
Roll Offset: 0.000  
Azimuth Offset: 0.000

DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000

Time Stamp: 2008-051 00:00

Comments: (null)  
Time Correction(s) 0.000

Svp #1:

-----  
Pitch Offset: 0.000  
Roll Offset: 0.000  
Azimuth Offset: 0.000

DeltaX: 1.856  
DeltaY: 0.811  
DeltaZ: 1.676

SVP #2:

-----  
Pitch Offset: 0.000  
Roll Offset: 0.000  
Azimuth Offset: 0.000

DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000

Time Stamp: 2013-064 00:00

Comments:  
Time Correction(s) 0.000

Svp #1:

-----  
Pitch Offset: 0.000  
Roll Offset: 0.000  
Azimuth Offset: 0.000

DeltaX: 0.000  
DeltaY: 0.000  
DeltaZ: 0.000

SVP #2:

-----  
Pitch Offset: 0.000  
Roll Offset: 0.000

Azimuth Offset: 0.000

DeltaX: 0.000

DeltaY: 0.000

DeltaZ: 0.000

---

WaterLine:

Time Stamp: 2006-064 00:00

Comments:

Apply No

WaterLine 0.000

---



2/8/2006

Subj : NOAA SHIP Nancy Foster Survey

Ref: (a) SW225-AO-MMA-010/OP762/ALIGN THEORY, Theory of Combat System Alignment  
(b) Table 1 of ITEM NO. 501

Encl: (1) Foundation Leveling Data Sheets

PacOrd personnel accomplished the survey of the equipment listed in table 1 of work item # 501 on board the NOAA SHIP Nancy Foster.

The granite blocks Roll and Pitch planes were set to the ship's gravity plane. The granite block was then used as the reference for all readings requiring a comparison to the ship's gravity plane.

The ship's centerline was transferred up from the keel, to the granite block 0°-180° reference line through an access cut into the hull of the ship. The granite block reference lines were then used as the reference for all readings requiring centerline reference.

The IMU foundation had to be removed, drilled and tapped for the new style IMU and reset.

The 12KHZ Transducer pitch angle exceeds the  $\pm 0.25^\circ$  allowed by four minutes (reading is  $+0.3166^\circ$ ), a waiver was received from NOAA for this condition.

All other readings are within tolerance.

The final survey data is summarized in enclosure (1).

Byron K. Dunn  
CSA Engineer

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NOAA Ship Nancy Foster, R-352  
Orthogonal Survey & Sonar Installation  
February 2011

**FINAL REPORT**

February 28, 2011



Prepared By:

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Industrial Measurement Technology Engineering Consultants

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### **REVISIONS:**

Rev. 0 – Initial Release February 28, 2011

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## **PROJECT OVERVIEW**

### **Purpose**

The purpose of this commentary is to summarize the procedures and analytical methods employed to perform the 3-D coordinate total station inspection that produced the data in this report for those unfamiliar with the equipment and process.

Dimensional data resulting from the inspection is included with the report.

### **General Comments**

This report summarizes coordinate measurement data taken on the NOAA vessel Nancy Foster February 8 through 23, 2011. The vessel was located in a floating dry dock at Detyens Shipyard, Charleston, SC.

Coordinate measurements were taken to characterize the vessel and create the required reference coordinate system for reporting azimuth, pitch, roll and coordinate data.

Coordinate measurements were made to define elements as described in WI507 Rev 1.

### **3-D Coordinate Measurement Equipment**

A Sokkia NET 1200 enhanced electronic total station operated through a notebook computer running New River Kinematics Spatial Analyzer™ measurement and analysis software was utilized. This system measures 3-D spherical coordinates by recording an azimuth and zenith angle simultaneously with the near infrared distance coaxial with the telescope line of sight for each observation. Spatial Analyzer measurement and analysis software converts the spherical coordinate data to a Cartesian coordinate system that can be defined by the user. Measurements are made to either adhesive or kinematic targets that have a retro-reflective target face.

Temporary "benchmarks" or reference points were placed throughout the dry-dock area and on the vessel as required to allow for re-locating the instrument to a new position or "Station" and tie all of the data to the common coordinate system for comparison.

The measuring system used for this final inspection report is one of several owned by The IMTEC Group, Ltd. The NET 1200 total station, S/N 110350 was calibrated, traceable to N.I.S.T. and in accordance with A.N.S.I. Z-540-1, at the Sokkia USA Factory Service Center June 14, 2010.



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### Nomenclature

In order to communicate in the language of large-scale metrology, Key terms used in this report are presented.

- ◆ **Benchmark-** A mark on a stable object of predetermined position and elevation used as a reference point.
- ◆ **Best-Fit-**The condition whereby the values of the parameters of a mathematical model (such as a shape like a rectangle) are derived by computing the model values to a set of measured targets. When the result is optimized, it is also referred to as a least-squares adjusted fit.
- ◆ **Buck In-To** align to or set a line of sight to a predetermined axis
- ◆ **Coordinate system-**A 3-dimensional space defined by mutually orthogonal lines to which points are referenced
- ◆ **Observation-**The distance and horizontal and zenith angles obtained from a single pointing of a total station to a point of interest or target.
- ◆ **Target-** A *Target* is defined as a point that is determined directly from measurements
- ◆ **Transformation-**The mathematical relationship between targets and/or points in different systems. When a transformation is computed, the values of the parameters that define the mathematical model are solved for.
- ◆ **Transform-**To compute the orientation of a Station, Group, System or Frame relative to another Station, System, Group or Frame.

### Reference Coordinate System

The following parameters were used to define the reference coordinate system for reporting the survey data:

Origin:	Top Dead Center of the Granite Block, X=0.000, Y=0.000, Z=0.000
X-Axis:	Line faired through the centerline of the keel from Frames 10 to 82 at ~10 frame intervals
Y-Axis:	Orthogonal to X-Axis
Z-Axis:	Perpendicular to Keel Plane, orthogonal to X-Axis
Rotation:	Pitch set by Keel Plane, Roll set by Fantail plane
System:	X+ Fwd, Y+ Stbd, Z+ Down (towards keel)

### Measurement Procedure

Adhesive targets with retro reflective target face were used throughout the survey as temporary benchmarks for relocating the instrument to new stations. Kinematic (a target with a known offset) retro reflective targets such as the RT-50M swivel targets used to measure some of the features defining the specified elements to be reported. The RT-50M was also frequently used as a temporary benchmark. Where possible, a retro reflective surface target was used to eliminate any offsets.

The Sokkia NET 1200 total station operated through a notebook computer running Spatial Analyzer™ industrial measurement software was used to measure the targets and record observations.

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### Vessel Features

- ◆ The Granite Block was surveyed and used as the Origin for this survey. This required an access hole to be cut in the hull on the port side of the vessel just above the keel.
- ◆ The location of the POS MV GPS antennae.
- ◆ Request was made to survey the existing IMU. As-found survey data showed it to be 11' 33" to Stbd which confirmed what shipboard personnel suspected. Decision was made to adjust it back to zero azimuth. Due to the mounting configuration, inclination was disturbed while adjusting the azimuth and was also reset as close as achievable to the ship's pitch and roll planes.
- ◆ Request was made to survey the location of the existing EM 1002 transducer in the Stbd side fairing.

The alignment team assisted with the installation of the following components:

- ◆ Reson Seachest – Verified installation met azimuth and inclination requirements of 1° Heading, 1° 2" Pitch & 1° Roll.
- ◆ Reson 7125 Multibeam system – Derived final coordinates to the Main, 200 KHz & 400 KHz transducers. Heading, Pitch and Roll values not required by Reson.
- ◆ New Port Fairing – Assisted shipyard personnel with proper fit-up of fairing to hull by providing a cut line around the perimeter where it would meet the hull. During installation, the fairing was set to < .5 degree Azimuth and Inclination relative to the vessel.
- ◆ Original ADCP 150 KHz and Knudsen 12 KHz transducers were reinstalled in the new fairing. The mounting rings were set to within the azimuth and inclination specification from WI507 Rev 1, page 507-10, Table 1 and monitored during the welding process to ensure they remained within the required specification.
- ◆ A new Simrad EK60 Echo Sounder system consisting of 4 transducers was also installed in the new port fairing. The mounting rings for this system were verified for required azimuth and inclination as well and coordinates were obtained to the center of each.
- ◆ A Valeport SVS was installed on the Stbd side of the hull aft of frame 31 and coordinates obtained to the center of the probe face in the extended position.

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### **3-D X, Y, Z coordinates, Post Processing**

In some cases, the features or targets defining the elements required by the survey were made to a kinematic target with a known offset orthogonal to the vessel's final reference coordinate system. After the each survey was complete, these offsets were applied to report the final X, Y, Z value of the element.

The pitch and roll values for the planer elements were processed mathematically in the Spatial Analyzer software. The azimuths were also processed mathematically from data points recorded during the survey.

#### **Data files**

One measurement file was used to perform the survey.

All measurement files were backed up at the completion of a set of observations from a particular station and on a daily basis.

The measurements were performed from different instrument locations referred to as "Stations", e.g. Sta 0, Sta 1, Sta N, etc.

Station transformations are used to bring a new instrument location into the current vessel coordinate system (see measurement procedure). The result produces some residuals.

#### **Measurement Precision and Uncertainty**

Based on a sample analysis of the results of the observations taken during the performance of this inspection, the Spatial Analyzer software reports a maximum standard deviation of slightly less than 1 mm for all observations.

Based on 125 sample observations:

Ux Ave = 0.8mm  
Uy Ave = 0.8mm  
Uz Ave = 1.0mm  
Umax = 1.2 mm

Uncertainties are reported to be:

Point to Point, any element or target within the vessel survey to another element or feature in the survey

$X, Y, \& Z \leq 2.0 \text{ mm}$

Region to Region, i.e., GPS antenna to Reason Sea Chest :

$X \leq 3.0 \text{ mm}$

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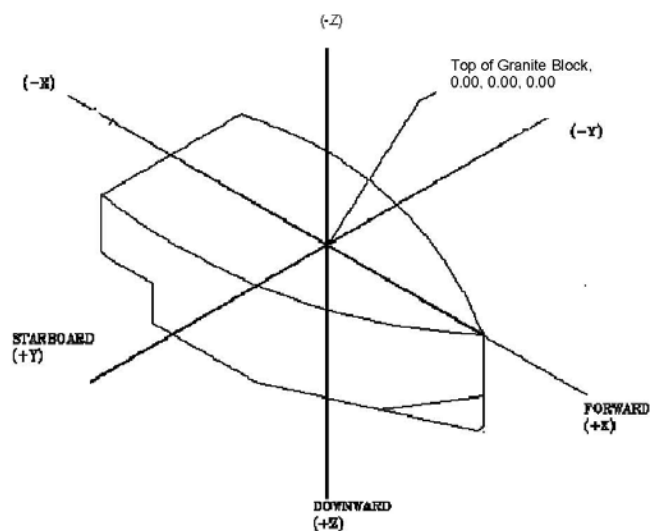
$$Y \leq 3.0 \text{ mm}$$
$$Z \leq 3.0 \text{ mm}$$

Angular precision is based on analysis of features measured and calculation of the mathematical relationship of these features.

The angular measurement precision of the NET1200 is  $< 1$  arc second in azimuth and zenith. There can be some error introduced by targeting. Random and systematic errors can be introduced by the working environment.

The expected angular precision is analyzed to be:

Azimuth:  $\leq 00^{\circ}00' 30''$   
Pitch:  $\leq 00^{\circ}01' 30''$   
Roll:  $\leq 00^{\circ}01' 30''$



Vessel Coordinate System, Nancy Foster

NOAA Ship Nancy Foster  
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**Table 1 - NOAA Nancy Foster Element Coordinate Summary - February 2011  
(Dimensions in Centimeters)**

Ship Elements	X	Y	Z
GRANITE BLOCK <sup>(1)</sup>	0.0	0.0	0.0
IMU <sup>(2)</sup>	73.9	-0.2	-12.0
FWD POS/MV ANTENNA	657.7	-475.0	-1629.3
AFT POS/MV ANTENNA	431.7	-473.4	-1627.9
ADCP 150 KHZ	-603.7	-156.3	155.1
KNUDSEN 12 KHZ TRANSDUCER	-721.9	-155.7	154.8
EM 1002 MULTIBEAM	82.4	182.3	169.7
EK60 - ES120-7C <sup>(3)</sup>	-559.3	-156.4	154.9
EK60 - ES38-B <sup>(3)</sup>	-661.1	-156.0	154.6
EK60 - ES70-C <sup>(3)</sup>	-775.7	-155.5	153.2
EK60 - ES200-7C <sup>(3)</sup>	-810.4	-155.4	153.3
RESON 7125 - MAIN	-173.3	54.7	108.4
RESON 7125 - 200KHZ	-217.8	67.8	109.9
RESON 7125 - 400KHZ	-217.9	39.7	109.9
VALEPORT SVS	-357.5	155.2	110.6

Benchmarks	X	Y	Z
IMU FWD	339.3	23.5	-19.6
IMU AFT	-146.7	23.9	-19.5
IMU ALIGNMENT CUBE TOP CENTER	161.5	178.5	-7.5
AFT DECK PORT	-3783.5	-527.0	-384.3
AFT DECK STBD	-3782.7	525.2	-385.1
AFT DECK ALIGNMENT CUBE TOP CENTER	-3592.3	583.2	-469.3
FLYING BRIDGE PORT	468.9	-562.4	-1421.9
FLYING BRIDGE STBD	469.3	558.6	-1420.5
FLYING BRIDGE ALIGNMENT CUBE TOP	648.4	0.0	-1431.0
KEEL FWD	279.4	-1.5	110.9
KEEL AFT	-171.6	-1.4	110.2

Notes:

- (1) Granite Block grouted in place.
- (2) IMU was repositioned to ship's Heading, Pitch and Roll
- (3) Measurements are to the center of mounting face. Additional offset to transducer face has not been applied.

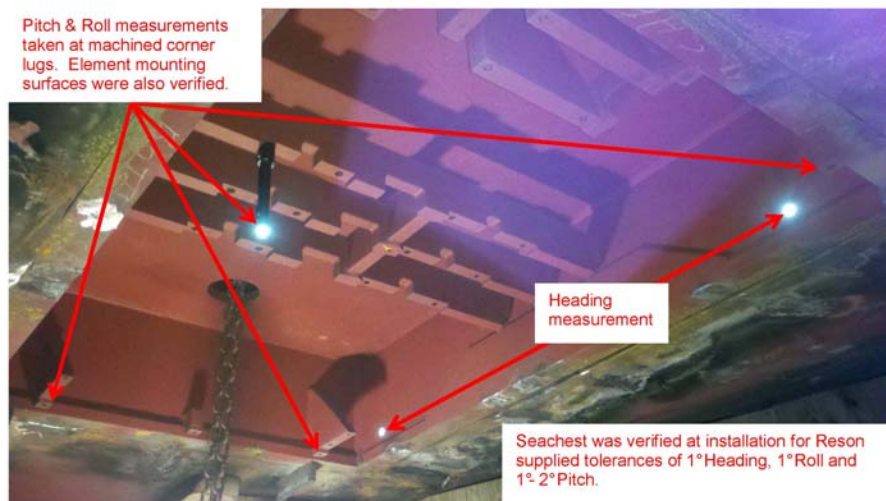
NOAA Ship Nancy Foster  
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**Table 2 - NOAA Nancy Foster Pitch, Roll & Heading Summary - February 2011  
Decimal Degrees**

Ship Elements	Azimuth	Rotation	Pitch	Rotation	Roll	Rotation
GRANITE BLOCK	-0.0442	PORT	0.0698	Bow Up	-0.0025	Stbd Up
IMU	-0.0006	PORT	0.0075	Bow Up	-0.0169	Stbd Up
FWD POS/MV ANTENNA	N/A		N/A		N/A	
AFT POS/MV ANTENNA	N/A		N/A		N/A	
ADCP 150 KHZ	-0.2284	PORT	-0.0938	Bow Dn	-0.0146	Stbd Up
KNUDSEN 12 KHZ TRANSDUCER	0.0319	STBD	-0.0147	Bow Dn	-0.0818	Stbd Up
EM 1002 MULTIBEAM	N/A		N/A		N/A	
EK60 - ES120-7C	0.7459	STBD	0.4399	Bow Up	-0.8502	Stbd Up
EK60 - ES38-B	-1.1866	PORT	-0.2496	Bow Dn	-0.4000	Stbd Up
EK60 - ES70-C	-0.6582	PORT	-0.1178	Bow Dn	-0.3949	Stbd Up
EK60 - ES200-7C	-0.7286	PORT	-0.2808	Bow Dn	0.3034	Stbd Dn
RESON SEACHEST	-0.0369	PORT	0.3439	Bow Up	0.3027	Stbd Dn

NOAA Ship Nancy Foster  
Orthogonal Survey February 2011  
Final Report- Rev "0"

### Reson 7125 Sea Chest



### Reson 7125 Elements

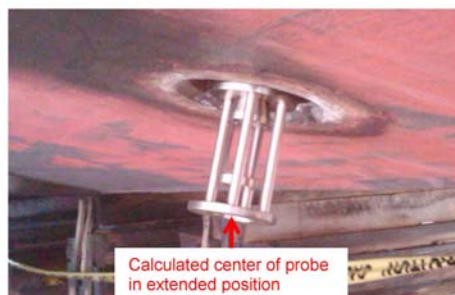


NOAA Ship Nancy Foster  
Orthogonal Survey February 2011  
Final Report- Rev "0"

**New Port Fairing Transducer Rings**



**Valeport SVS**



**POS MV ANTENNA**





**APPENDIX II**  
**POS/MV 320 V4 CONFIGURATION REPORTS**

Extract POS COnfig Version 1.0  
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October 29 2013 01:18 pm

Source Name: POS\_EM1002\_Config.nvm  
Output File: C:\Users\bfrancis\Desktop\EM1002\302\_posconfig

#### Message 37 - Base GPS 1 Setup

Input Data Type Port 1 - Accept RTCM 1/9

#### Message 38 - Base GPS 2 Setup

Input Data Type Port 2 - Accept RTCM 1/9

#### Message 34 - COM Port Setup

Number of COM ports = 5

COM1 - Protocol: 19200,No Parity,8 data,1 stop,None

Input Selection: No Input

Output Selection: NMEA Message

COM2 - Protocol: 19200,No Parity,8 data,1 stop,None

Input Selection: No Input

Output Selection: Real-time Binary

COM3 - Protocol: 9600,No Parity,8 data,1 stop,None

Input Selection: Base GPS 1

Output Selection: NMEA Message

COM4 - Protocol: 115200,No Parity,8 data,1 stop,None

Input Selection: No Input

Output Selection: Real-time Binary

COM5 - Protocol: 19200,No Parity,8 data,1 stop,None

Input Selection: No Input

Output Selection: NMEA Message

xx

#### Message 51 - Display Port Control

Number of groups selected for Display Port = 25

1 2 3 4 5 6 7 8 9 10 11 12

13 14 17 20 23 24 99 102 103 104 105 110  
20000

Message 53 - Logging Port Control

Number of groups selected for Logging Port = 0  
Logging Port Output Rate 1 Hz  
AutoLog Select Disabled

Message 135 - NMEA Message Select

Number of Port 3  
Assigned port number COM1  
Update Rate Selection 1 Hz  
Output Selection GGA ZDA VTG  
talker ID \$IN  
Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Heave Up  
Assigned port number COM3  
Update Rate Selection 1 Hz  
Output Selection GGA HDT ZDA VTG SHR UTC  
talker ID \$IN  
Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Heave Up  
Assigned port number COM5  
Update Rate Selection 1 Hz  
Output Selection ZDA  
talker ID \$IN  
Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Heave Up

Message 136 - Binary Message Select

Number of Port 2  
Assigned port number COM2  
Update Rate Selection 100 Hz  
Output Selection SIMRAD-1000(TB)  
Selected frame Sensor1  
Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Heave Up

Assigned port number COM4  
Update Rate Selection 50 Hz  
Output Selection TSS  
Selected frame Sensor1  
Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Heave Up

Message 33 - Event Discrete Setup

Event 1 Trigger Positive edge  
Event 2 Trigger Positive edge

Message 30 - Primary GPS Setup

GPS AutoConfig True

Message 31 - Secondary GPS Setup

GPS AutoConfig True

Message 24 - User Accuracy Specifications

User Attitude Accuracy 0.05  
User Heading Accuracy 0.05  
User Position Accuracy 2  
User Velocity Accuracy 0.5

Message 52 - Real-time Data Port Control

Number of groups selected for Real-time Data Port = 5  
3 7 20 102 111  
Data Port Output Rate 50 Hz

Message 61 - Data Port Control

Number of groups selected for Data Port = 15  
1 2 4 5 9 10 99 102 110  
Ref to IMU Lever Arm 0.738 0.001 -0.125 [Wavemaster User => 0.730 -0.021 -  
0.052]  
Ref to Pri GPS Lever Arm 6.571 -4.740 -16.308  
Ref to Aux1 GPS Lever Arm 5.371 -4.740 -16.308  
Ref to Aux2 GPS Lever Arm 0.000 0.000 0.000

IMU to Ref Mounting Angle      0.000   111    113    10001 10009 10011 10012  
Data Port Output Rate 20 Hz

Message 20 - General Installation Parameters

0.000 0.000  
AutoStart Enabled  
Multipath Low

Message 120 - Sensor Parameter Set-up

Sensor1 Ref Mount Angle 0.000 0.000 0.000  
Sensor2 Ref Mount Angle 0.000 0.000 0.000  
Ref Sensor1 Lever Arm    0.000 0.000 0.000  
Ref Sensor1 Lever Arm    0.000 0.000 0.000  
Ref to CoR Lever Arm    -12.295 0.000 -1.965

Message 121 - Vessel Installation Parameter Set-up

Ref to Vessel Lever Arm   0.000 0.000 0.000

Message 106 - Heave Filter Set-up

Heave Bandwidth 12.000  
Heave Damping Ratio 0.707

Message 105 - Analog Port Set-up

Roll Scale 1.00  
Pitch Scale 1.00  
Heave Scale 1.00  
Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Clockwise  
Formula Select - TSS Trig  
Analog Port Enabled True  
Output Frame Sensor 1

Message 21 - GAMS Installation Parameters

Two Antenna Separation 2.253  
Baseline Vector            -2.253 0.027 0.011  
Heading Calibration Threshold 0.700  
Heading Correction    0.000

Extract POS Config Version 1.0  
Copyright (C) 2006 Applanix - A Trimble Company

October 20 2010 04:11 pm

Source Name: POS\_7125\_Config.nvm  
Output File: C:\Users\bfrancis\Desktop\7125\7125\_posconfig

Message 37 - Base GPS 1 Setup

Input Data Type Port 1 - Accept RTCM 1/9

Message 38 - Base GPS 2 Setup

Input Data Type Port 2 - Accept RTCM 1/9

Message 34 - COM Port Setup

Number of COM ports = 5

COM1 - Protocol: 19200, No Parity, 8 data, 1 stop, None

Input Selection: No Input

Output Selection: NMEA Message

COM2 - Protocol: 19200, No Parity, 8 data, 1 stop, None

Input Selection: No Input

Output Selection: Real-time Binary

COM3 - Protocol: 9600, No Parity, 8 data, 1 stop, None

Input Selection: Base GPS 1

Output Selection: NMEA Message

COM4 - Protocol: 115200, No Parity, 8 data, 1 stop, None

Input Selection: No Input

Output Selection: Real-time Binary

COM5 - Protocol: 19200, No Parity, 8 data, 1 stop, None

Input Selection: No Input

Output Selection: NMEA Message

Message 51 - Display Port Control

Number of groups selected for Display Port = 25  
1 2 3 4 5 6 7 8 9 10 11 12  
13 14 17 20 23 24 99 102 103 104 105 110  
20000

#### Message 53 - Logging Port Control

Number of groups selected for Logging Port = 0  
Logging Port Output Rate 1 Hz  
AutoLog Select Disabled

#### Message 135 - NMEA Message Select

Number of Port 3  
Assigned port number COM1  
Update Rate Selection 1 Hz  
Output Selection GGA ZDA VTG  
talker ID \$IN  
Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Heave Up  
Assigned port number COM3  
Update Rate Selection 1 Hz  
Output Selection GGA HDT ZDA VTG SHR UTC  
talker ID \$IN  
Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Heave Up  
Assigned port number COM5  
Update Rate Selection 1 Hz  
Output Selection ZDA  
talker ID \$IN  
Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Heave Up

#### Message 136 - Binary Message Select

Number of Port 2  
Assigned port number COM2  
Update Rate Selection 100 Hz  
Output Selection SIMRAD-1000(TB)  
Selected frame Sensor1

Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Heave Up

Assigned port number COM4  
Update Rate Selection 50 Hz  
Output Selection TSS  
Selected frame Sensor1  
Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Heave Up

#### Message 33 - Event Discrete Setup

Event 1 Trigger Positive edge  
Event 2 Trigger Positive edge

#### Message 30 - Primary GPS Setup

GPS AutoConfig True

#### Message 31 - Secondary GPS Setup

GPS AutoConfig True

#### Message 24 - User Accuracy Specifications

User Attitude Accuracy 0.05  
User Heading Accuracy 0.05  
User Position Accuracy 2  
User Velocity Accuracy 0.5

#### Message 52 - Real-time Data Port Control

Number of groups selected for Real-time Data Port = 5  
3 7 20 102 111

Data Port Output Rate 50 Hz

#### Message 61 - Data Port Control

Number of groups selected for Data Port = 15  
1 2 4 5 9 10 99 102 110 111 113 10001  
10009 10011 10012  
Data Port Output Rate 20 Hz



#### Message 20 - General Installation Parameters

Ref to IMU Lever Arm     -0.000 -0.000 0.000 [Wavemaster User => -0.008 -0.022  
0.073]  
Ref to Pri GPS Lever Arm     5.833 -4.470 -16.183  
Ref to Aux1 GPS Lever Arm     5.371 -4.740 -16.308  
Ref to Aux2 GPS Lever Arm     0.000 0.000 0.000  
IMU to Ref Mounting Angle     0.000 0.000 0.000  
AutoStart Enabled  
Multipath Low

#### Message 120 - Sensor Parameter Set-up

Sensor1 Ref Mount Angle 0.000 0.000 0.000  
Sensor2 Ref Mount Angle 0.000 0.000 0.000  
Ref Sensor1 Lever Arm     0.000 0.000 0.000  
Ref Sensor1 Lever Arm     0.000 0.000 0.000  
Ref to CoR Lever Arm     0.000 0.000 0.000

#### Message 121 - Vessel Installation Parameter Set-up

Ref to Vessel Lever Arm     0.000 0.000 0.000

#### Message 106 - Heave Filter Set-up

Heave Bandwidth 12.000  
Heave Damping Ratio 0.707

#### Message 105 - Analog Port Set-up

Roll Scale 1.00  
Pitch Scale 1.00  
Heave Scale 1.00  
Roll Sense Port Up  
Pitch Sense Bow Up  
Heave Sense Clockwise  
Formula Select - TSS Trig  
Analog Port Enabled True  
Output Frame Sensor 1

#### Message 21 - GAMS Installation Parameters

Two Antenna Separation 2.253

Baseline Vector -2.253 0.027 0.011  
Heading Calibration Threshold 0.700  
Heading Correction 0.000