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DATA ACQUISITION & PROCESSING REPORT

OPR-A375-NRT-10 NOAA Navigation Response Team 5 LTJG Matthew Nardi, Team Lead, Processing and Submittal PS Nicholas Forfinski, Planning and Acquisition

A. EQUIPMENT

A.1. Vessels

A.1.1. S3002

NRT5 operated a single vessel, S3002 (see Fig. 1), a 30-foot (overall), gray, aluminum-hull SeaArk Commander. NOAA Survey Vessel S3002 was powered by dual 130-horse power Honda outboards. A Kohler 7.5e generator supplied AC power. A rack-mount APC Smart-UPS (uninterruptable power supply) provided battery backup for the survey-system electronics.

Figure 1: NOAA S3002 (NRT5)

A.1.1.1. Calibration & Configuration

See section C.1.1 for a description of the full vessel survey.

A.2. Depth Measurement Equipment

A.2.1. Kongsberg Simrad EM3002 Multibeam Echosounder

S3002 is equipped with a hull-mounted Kongsberg EM3002 multibeam, which is located directly beneath the IMU. The EM3002 is a 300 kHz (nominal) system with a characteristic operating depth range of 1 to 150 meters water depth. Under ideal, cold water conditions, the range may extend to 200 meters. The swath width is 130° , and the nadir beam is 1.5° x 1.5° . The system has a maximum ping rate of 40 Hz. The processing unit (PU) performs beam forming and bottom detection and automatically controls transmit power, gain, and ping rate. The sonar processor incorporates real time surface sound speed measurements for initial beam forming and steering. SVP correction is also performed in real time. The Seafloor Information System (SIS) application, designed to run under Microsoft Windows, provides control and monitoring of the EM3002.

A.2.1.1. Calibration & Configuration

The installation and runtime parameter configuration files are included in Appendix IV (Electronic Appendix). See section C.1.3 for a description of the calibration patch test.

A.3. Vessel Position and Orientation Equipment

A.3.1. TSS POS/MV Position & Orientation Sensor

S3002 is equipped with an Applanix POS/MV 320 version 4. The POS/MV consists of dual Trimble BD950 GPS receivers (with corresponding Zephyr antennas), an inertial motion unit (IMU), and a POS computer system (PCS). The two antennas are mounted approximately 1.5 meters apart atop the launch cabin (see Fig. 2). The primary receiver (on the port side) is used for position and velocity, and the secondary receiver is used to provide heading information as part of the GPS azimuthal measurement sub-system (GAMS).

Figure 2: POS/MV Antenna Installation

The IMU contains three solid-state linear accelerometers and three solid state gyros, which together provide a full position and orientation solution. The IMU is mounted on the top of the sonar housing, beneath a removable deck plate (see Fig. 3).

Figure 3: IMU Installation

A.3.1.1. Calibration & Configuration

A GAMS calibration was not performed specifically for OPR-A375-NRT5-10. No changes had been made to the POS/MV system which necessitated a GAMS calibration after the previous GAMS calibration in 2009. The 2009 GAMS calibration report is included in Appendix II.

The POS/MV is configured, operated, and monitored via the POS/MV controller software, which is installed on the S3002 acquisition computer. The primary GPS-to-reference point lever arm was accounted for in the POS/MV controller. A POS/MV configuration file detailing lever arms, input/output settings, and operational settings is contained in Appendix IV (Electronic Appendix).

The controller software was also used to initiate Ethernet logging of the POSPac datagram bundle, which was used in post-processed kinematic (PPK) processing (See ERS SOP in Appendix IV - Electronic Appendix).

A.3.2. Trimble DSM212L DGPS Receiver

The POS/MV receives differential (RTCM) correctors from a Trimble DSM212L GPS receiver that includes a dual-channel low-noise MSK beacon receiver, capable of receiving U.S. Coast Guard (USCG) differential correctors. The DSM212L can also accept RTCM messages from an external source such as a user-established DGPS reference station, however, no such stations were established for OPR-A375-NRT5-10.

A.3.2.1. Calibration & Configuration

Trimble's TSIP Talker was used to configure the GPS antenna supplying Coast Guard differential correctors to the POS/MV. Due to COM port limitations, TSIP Talker was not installed on the main acquisition computer, but a separate laptop.

There are three modes of DPGS operation; Auto-Range, which locks onto the beacon nearest the vessel, Auto-Power, which locks onto the beacon with the greatest signal strength, and Manual, which allows the user to select the desired beacon. NRT5 operated in the manual mode, with the beacon set to Penobscot, ME (290 kHz). The following parameters are periodically monitored in real-time through Trimble's TSIP Talker software to ensure position data quality: 1) number of satellites used in the solution, 2) horizontal dilution of precision (HDOP), 3) latency of correctors, and 4) beacon signal strength. The DSM212L is configured to go off-line if the age of DGPS correctors exceeds 20 seconds, and to exclude satellites with an altitude below eight degrees.

A.3.3. Trimble GeoXH GPS Receiver

Geospatial data for shoreline features were collected with a Trimble GeoExplorer 2008 series GeoXH handheld outfitted with a Trimble Zephyr antenna mounted on a 2-meter, bipodequipped range pole. The Trimble GeoXH combines a Trimble L1/L2 GPS receiver with a field computer powered by Microsoft Windows Mobile version 6 operating system. The GPS field software utilized by the GeoXH to acquire data for this project was Trimble TerraSync version 4.1 while the Trimble GPS Pathfinder version 4.20 was used to post process data, and apply differential correction.

A.4. Sound Speed Equipment

S3002 is equipped with an Odom Digibar Pro surface sound speed sensor to measure sound speed at the flat-face multibeam transducer head. For water column sound speed profiles NRT5 used an Odom Digibar Pro sound speed sensor and a Seabird SBE19+ CTD profiler. Speed of sound through water is determined by a minimum of one cast every four hours, in accordance with the NOS Specifications and Deliverables for Hydrographic Surveys. Daily Quality Assurance tests (DQA) between the surface and profile sound speed probes were performed using Velociwin. Full cast comparisons were also performed periodically.

A.4.1. Odom Digibar Pro – Surface Sound Speed

Odom Digibar Pro serial# 98214 provided surface sound speed data to the flat-face EM3002 for beam steering and beam forming. The unit is mounted in a removable pole that is inserted into a bracket mounted on the transom between the two motors (see Fig. 4). The unit is configured to output an AML datagram to SIS, which is installed on the acquisition computer (see wiring diagram in Appendix II).

Figure 4: Surface Sound Speed Digibar Installation

A.4.2. Odom Digibar Pro – Profile Sound speed

Odom Digibar Pro serial #98212, which has 25 meters of cable, is used to obtain sound speed profiles in water depths up to 25 meters, or deeper if the water column is known to be well mixed beyond 25 meters. First, the Digibar profile data file is uploaded to the acquisition computer using Digibar software and processed using NOAA Velociwin software. The processing creates a series of files, including an *.asvp file, which is loaded into SIS for real-time sound speed ray tracing.

A.4.3. Seabird SBE19+ CTD Profiler

Seabird SBE19+ serial #4835 is used to obtain sound speed profiles in waters deeper than 25 meters. The raw profile data file is uploaded and processed with the acquisition computer using the NOAA Velociwin software. Velociwin generates an *.asvp file, which is loaded into SIS for real-time ray tracing.

A.4.4. Calibration & Configuration

Calibration reports for all three sound speed sensors are included in Appendix III.

A.5. Data Acquisition Software

A complete list of software and versions is included in Appendix I.

A.5.1. Hypack Hysweep

Hypack Hysweep was used for all data logging, real-time data display, and navigation. Hypack and Hysweep hardware configuration files are included in Appendix IV (Electronic Appendix).

A.5.2. Applanix PosView

The Applanix POSView software was used to configure and monitor the Applanix PosMV, and to

log PosPac files for post processing. The PosMV configuration file, which is created using POSView, is located in Appendix IV (Electronic Appendix).

A.5.3. Kongsberg SIS-Seafloor Information System

SIS was used to control the EM3002 MBES, which performed real-time motion and SVP correction.

A.5.4. Trimble TerraSync

TerraSync software was used to collect GPS data with the GeoXH handheld receiver.

A.6. Data Processing Software

A.6.1. Applanix POSPac MMS and POSGNSS

The Applanix POSPac software was used for post processing position and ellipsoidal height using the single base station PPK method.

A.6.2. Caris HIPS

Caris HIPS was used to process all MBES data including tide correction, merging with navigation data, TPU calculation, data cleaning, and CUBE BASE surface creation. The Caris HVF file, which contains offsets and correctors applied in Caris, is located in Appendix IV (Electronic Appendix).

A.6.3. Caris Bathy Database

Caris Bathy Database was used for feature management and quality assurance.

A.6.4. Velociwin

Velociwin was used to process SVP casts, and for DQA tests. The .asvp files created by Velociwin were applied to the MBES data in real-time using SIS software.

A.6.5. Pydro

Pydro was used for feature management, DTON report generation, and tides requests.

A.6.6. Trimble Pathfinder Office

Pathfinder Office was used to post process GPS data collected with GeoXH hand held receiver.

B. QUALITY CONTROL

B.1. Multibeam Echosounder Data

B.1.1. Acquisition Operations

Mainscheme multibeam data were acquired using a "paint-the-bottom," or adaptive-line-steering approach, whereby the coxswain viewed a real-time coverage map in Hysweep and accordingly adjusted line steering to ensure adequate overlap. The coxswain strove to avoid abrupt changes in direction and speed, but abrupt changes in direction and speed were unavoidable in certain areas due to current and confined areas. In areas where abrupt changes in direction were unavoidable, speed was reduced to minimize motion-related artifacts. When gaps in coverage were found, holiday line plans were created using Mapinfo and exported as Hypack line files.

The dynamic draft for a vessel of this size is typically quite small (0.5-2cm). Nonetheless, when

sea conditions allow, NRT5 follows HSTP suggestions to maintain a consistent engine trim during survey operations. The trim indicator has been marked to insure the trim is set correctly for operations.

Sound speed casts were acquired as per HSSD section 5.2.3.3. The EM3002 system is designed to apply sound speed and attitude data in real-time. Because sound speed is applied real-time, a sound speed profile must be loaded into SIS before data acquisition. Currently, post-processing sound speed data in Caris is not possible.

B.1.2. Processing Workflow

Multibeam processing for OPR-A375-NRT5-10 was based on the BASE surface/directed-editing paradigm described in FPM section 5.2, Bathymetry Processing. The multibeam processing workflow had four main components: conversion, preliminary processing, surface generation, and surface review/data cleaning (see Fig. 5). Note that the surface generation and surface review/data cleaning steps are iterative.

Figure 5: Multibeam Processing Workflow

B.1.2.1. Conversion

Raw multibeam .HSX data were converted to HDCS format in Caris HIPS. Device conversion parameters are shown in Figure 6.

Figure 6: Device Conversion Parameters

B.1.2.2. Preliminary Processing

After conversion, preliminary processing consisted of applying tide corrections and PPK navigation data, merging, and computing total propagated uncertainty (TPU). Unlike with traditional NOAA hydrographic processing schemes, the converted data for OPR-A375-NRT5- 10 were corrected for sound speed in real time, and not in Caris post processing. The only correctors that were applied in Caris were PPK navigation, dynamic draft, patch test biases, and tide.

Applying Tides

Tide correctors were applied using a zone definition file (zdf) in Caris. See section C.3 for a detailed description of the tide correctors for OPR-A375-NRT5-10.

Applying PPK SBET

Post-processed kinematic (PPK) navigation data were applied to the HDCS data using the "Load Attitude/Navigation Data" function in HIPS, as per HSD's (Hydrographic Surveys Division) Ellipsoidally Referenced Survey (ERS) SOP contained in Appendix IV (Electronic Appendix).

Merging

The merge process in Caris combines the observed depths (created during conversion) with the loaded tide file, the navigation data, the HVF draft sensor (containing dynamic draft values), and the HVF swath1 sensor (containing patch test biases) to compute the final processed depths. The "Apply refraction coefficients" and "Apply GPS tide" options were not checked, and no smoothed sensors were applied during the merge process.

Computing TPU

The TPU computation process assigns each sounding a horizontal and vertical uncertainty, or estimate of error, based on the uncertainties of the various data components, such as position, sound speed, and loading conditions. Table 1 lists the HVF TPU values used for OPR-A375-

NRT5-10.

Table 1: TPU Values

B.1.2.3. Surface Generation

The multibeam sounding data were modeled using the CUBE BASE surface algorithm implemented in Caris HIPS. CUBE BASE surfaces were generated using the parameters outlined in Hydrographic Surveys Technical Directive 2009-02 (CUBE Parameters). The resolutions of the finalized surfaces were based on the complete MBES coverage resolution requirements specified in the Specs and Deliverables (5.2.2.2). The deeper limit of certain ranges was extended to avoid gaps between surfaces on particularly steep slopes.

B.1.2.4. Surface Review/Data Cleaning

Rather than a traditional line-by-line review and a full subset-cleaning, the data cleaning/quality review process for OPR-A375-NRT5-10 consisted of a combination of the directed-editing approach described in FPM section 5.2 and a full subset-review (not full subset-cleaning). All the sounding data were viewed in subset, but unlike in the traditional workflow, where every sounding deemed to be "noise" is rejected, only the soundings that negatively impacted the CUBE surface were rejected. Surface review also consisted of evaluating achieved coverage and sounding density, checking for systematic errors, and designating soundings. Sounding designation was in accordance with Specs and Deliverable section 5.2.1.2.

B.2. Feature Data

Feature management consisted of two main workflows (see Fig. 7): hydrography features and shoreline features. The distinction between the hydrography and shoreline workflow is due to (1) the acquisition method and (2) the inability to edit/export S-57 line features in/from Pydro. Whereas the hydrography features were derived from the bathymetry data or vessel navigation data, the shoreline features were acquired using a Trimble GeoXH GPS, digitized from an orthophoto, or acquired as a DP in Hypack, and processed using Caris BDB.

Figure 7: Feature Management Workflow

B.2.1. Hydrography Features

B.2.1.1. Bottom Samples

Bottom sample features were created in Caris Bathy Database. SBDARE point features were created at the position of each bottom sample and then attributed with the appropriate NATSUR/NATQUA attributes. The SBDARE features were then exported to a .000 file and imported into PYDRO for inclusion in the survey area feature file deliverable.

B.2.1.2. Designated Soundings

The least depth of charted features and significant uncharted features were flagged "designated" in Caris HIPS to ensure that the depth was portrayed in the final BASE surface. Soundings that were flagged designated were then imported into PYDRO as bathymetric features. Once in PYDRO, these bathymetric features were correlated with ENC GPs, and given the appropriate S-57 attribution.

B.2.1.3. Detached Positions (DPs)

Features for which the least depth or position could not be derived from the bathymetry data were defined based on a range and bearing, or detached position (DP), relative to the vessel position. DPs were created as Hypack targets and then imported into Pydro.

B.2.2. Shoreline Features

B.2.2.1. GPS Features

Acquisition: All GPS shoreline features were collected using an S-57 data dictionary installed on the GeoXH handheld. The data were acquired using the appropriate feature categories, which were primarily "shoreline construction" and "mooring facility". At the beginning of each feature survey, the GPS unit was allowed to acquire a minimum of 10 minutes of carrier-phase lock on the initial point, followed by a minimum 2-minute observation on each subsequent vertex of the structure while maintaining the initial lock. A GPS position was collected once every 5 seconds throughout each observation.

Processing: Data were held for a minimum 24-hour period before post-processing, to allow adequate time for the National Geodetic Survey (NGS) website to contain the necessary data. Data were processed using the recommended Automatic Carrier and Code Processing, with the H-Star Processing routine set to use the Eastport CORS station (EPRT) as the single base provider. Once the GPS shoreline feature data were post-processed, the feature data were exported from Pathfinder as a shapefile and then imported into the Pydro PSS as a reference layer.

Uncertainties: Raw data, as acquired, generally fell within a 1-meter accuracy range at a 68% confidence level. The GeoXH used H-Star technology to provide sub-foot (30cm) accuracy after post processing for the vast majority of positions acquired. A total of 4774 positions were collected over the course of shoreline feature geospatial data acquisition. The H-Star processing routine first attempts to process each position with code and carrier corrections, and then chooses the highest-quality solution. Table 2 summarizes the percentage of code- and carrier-corrected positions, and Table 3 summarizes the estimated accuracies for all positions collected.

Table 2: Code versus Carrier Corrections

Table 3: Shoreline-Features Position Uncertainty

B.2.2.2. Digitized Features

In three (3) special instances in H11257, shoreline features were digitized in Caris Bathy Database from orthophotos downloaded from the U.S. Geological Survey (USGS) Seamless Data website.

Refer to section D.1.4 of the H12257 descriptive report (DR) for a detailed discussion of these special instances.

C. CORRECTIONS TO ECHO SOUNDINGS

The following section describes the determination and evaluation of the three main categories of corrections to echosoundings: vessel, sound speed, and water level correctors.

C.1. Vessel Correctors

Vessel correctors include static offsets, dynamic offsets, and patch test biases. The various correctors are applied to echo soundings at different points throughout the data pipeline, which is detailed in the sections below.

C.1.1. Static Offsets

C.1.1.1. Vessel Lever-Arms

The National Geodetic Survey conducted a full vessel survey on 8/4-8/5/09 in Newport, RI (see Appendix II for the NGS report). The primary-GPS-to-Reference-Point lever arm is accounted for in the POS/MV controller. The Reference-Point-to-Multibeam-Transducer lever arm is accounted for in SIS.

C.1.1.2. Static Draft

A static draft measurement was performed in May 2010 in Newport, RI. To determine the static draft (i.e., the height of the waterline above/below the reference point), two new reference marks and an easily repeatable method were established. A reference mark was established on the port and starboard gunwales, closely aligned with the RP (the middle of the top surface of the IMU), in the along-ship dimension (see Figs. $8 \& 9$). The static draft was calculated by subtracting the waterline-to-gunwale vertical distance (0.658 m) from the RP-to-gunwale vertical distance (0.680 m) for each benchmark and then taking the average.

Figure 8: Waterline Offset

The vertical positions of the newly established reference marks were tied into the vessel coordinate frame by running a string taut athwartship over the RP (top mark on IMU). This athwartship string, orthogonal to the z-axis of the vessel coordinate frame, provided a convenient point, nearly directly over the IMU, at which to indirectly measure the RP-to-gunwale vertical

distance. To account for the slight slope of the gunwale, a wedge was placed over both reference marks (see Fig 5).

Figure 9: Waterline Reference Marks

C.1.2. Dynamic Offsets

Dynamic draft measurements were not performed specifically for OPR-A375-NRT5-10; however, no significant changes had been made to the vessel since the previous dynamic draft calculation in 2009. The 2009 dynamic correctors are summarized in Table 5. A negative draft corrector implies that the boat moved down.

Table 4: 2010 Dynamic Draft Values

C.1.3. Patch Test Biases

A patch test was performed on 8/30/10 (DN 242), in Friar Roads, just offshore of Eastport, ME (see Fig. 10). Distinct sandwaves were used as the calibration target. The timing offset was determined using the conventional method, rather than the "precise timing" method. The derived biases (summarized in Table 5), were entered into the Swath1 sensor of the Caris HVF and therefore were applied to the data during the merge step of post-processing.

Figure 10: Patch Test Location (Charted depths are in meters)

C.2. Sound Speed

Sound speed corrections were performed in real-time by the EM3002 controller software, SIS. Casts were taken, at a minimum, every four hours as per NOS Specifications and Deliverables for Hydrographic Surveys.

C.3. Water Level Corrections

Tide corrections for OPR-A375-NRT5-10 were applied using the zone definition file A375NRT52010CORP.zdf.

Tide data were downloaded from the Center for Operational Oceanographic Products and Services (CO-OPS) website (http://tidesandcurrents.noaa.gov/olddata/) and applied using the zone definition file (*.zdf) provided by CO-OPS for this project. Approved final tides were applied by field personnel upon receipt.

APPROVAL SHEET

Data Acquisition & Processing Report Navigation Response Team 5

As Chief of Party, I have ensured that surveying and processing procedures were conducted in accordance with the Field Procedures Manual and that the submitted data meet the standards contained in the 2010 Hydrographic Surveys Specifications and Deliverables.

I acknowledge that all of the information contained in this report is complete and accurate to the best of my knowledge.

Respectfully,

Matthew Nardi I am approving this document 2011.05.10 13:47:29 -04'00'

LTJG Matthew Nardi Team Lead, NOAA NRT-5

Appendices

Appendix I – System Tracking

Appendix II - Vessel Reports, Offsets, and Diagrams

U.S. Department of Commerce National Oceanic & Atmospheric Administration National Ocean Service National Geodetic Survey Field Operations Branch

NOAA Boat – S 3002 IMU and MULTI-BEAM Component Spatial Relationship Survey Field Report

Kevin Jordan August, 2009

NOAA Boat $- S 3002$ IMU and MULTI-BEAM Survey

PURPOSE

The intention of this survey was to accurately position the Inertial Measuring Unit (IMU) and MULTI-BEAM (MBES) components that have been installed onboard the NOAA Boat S 3002.

PROJECT DETAILS

This survey was conducted on August 4 & 5, 2009 near the Naval Education and Training Center in Middletown, RI. The Boat was on a trailer and attached to a towing vehicle. The weather was clear and sunny on the day of the survey. Reconnaissance was conducted, and control marks CL 1, BM 1, BM 2, and BM 3 were found as described. CL 2 and BM 4 were searched for, but were not recovered.

INSTRUMENTATION

The TOPCON GPT 3000 Series Total Station was used to make all measurements.

A SECO 25 mm Mini Prism System configured to have a zero mm offset was used as target sighting and distance measurements.

SOFTWARE AND DATA COLLECTION

ADL Ver. 2.0.11 was used for data collection

ForeSight DXM Ver. 3.2.2 was used for post processing.

PERSONNEL

Kevin Jordan NOAA/NOS/NGS/Field Operations Branch 757-441-3603

Steve Holdorff NOAA/NOS/NGS/Field Operations Branch 757-441-3603

 $NOAA$ Boat – S 3002 IMU and MULTI-BEAM Survey

SURVEY PROCEDURES

Establishing the Centerline

To conduct this survey a local coordinate reference frame was established, where the X axis runs along the centerline of the boat and is positive from the primary reference point towards the bow of the boat. The Y axis is perpendicular to the centerline of the boat (X axis), and is positive from the primary reference point towards the right, when looking at the boat from the stern. The Z axis is positive in an upward direction from the primary reference point.

A temporary centerline mark (TCL) was established to align horizontally with CL 1. This was performed by measuring between the two benchmarks at the stern (BM 2 and BM 3) and placing a single punch mark on the deck halfway between them. An assumed distance of 3 meters was entered into NGS Program FORWARD.exe to produce a coordinate along the X axis to enter into the data collector to start the survey (initial azimuth). The instrument was setup on TCL and an assumed elevation of 100 ft was entered into the data collector. A prism was set above CL 1 and an azimuth of 0° 00' 00" was entered into the data collector while aimed at CL 1. From this station, temporary control points (TP 1 and TP 2) were set off the boat on steady ground.

Setup 1

TP 1 – While occupying TP 1 the instrument was set to initialize on TCL. After initialization was conducted, angular and distance measurements were taken to collect the following points: VBES (SINGLE-BEAM center point), GPS STAR (Starboard GPS Receiver), GPS PORT (Port GPS Receiver), DGPS (Differential GPS Receiver), BM 1, IMU, and BM 3.

Setup 2

TP 2 – Occupying TP 2 the instrument was set to initialize on TCL. After initialization was conducted, angular and distance measurements were taken to collect the following points: MBES (MULTI-BEAM center point), BM 2, and SSS TP (SIDE SCAN SONAR TOW POINT), and CL 1 OBS^{*}. Coordinate checks were made to the following previously established points:

* CL 1 OBS was positioned, but was determined later to have a bad elevation after review of field work later that day. Survey operations were conducted on the following day to correct this bad elevation.

Setup 3

Occupying TP 1 the instrument was set to initialize on TCL. After initialization was conducted, angular and distance measurements were taken to collect the following point: TP 4

During this observation, a coordinate check was made to: BM 2 $X, Y = 0.002(m)$ $Z = 0.002(m)$

Setup 4

TP 4 – Occupying TP 1 the instrument was set to initialize on TCL. After initialization was conducted, angular and distance measurements were taken to collect the following point: CL 1 OBS

During this observation, a coordinate check was made to: TP 1

 $X, Y = 0.001(m)$ $Z = 0.009(m)$

POST PROCESSING

Since the project was initialized using assumed positions and elevations, the collected points needed to be translated to a referenced coordinate system. Using ForeSight DXM, our observed CL 1 OBS was translated N 0.000(m), E 0.000(m), and Elev 0.000(m). See table 1

The same adjustment was made for the IMU as the reference point of N 0.000(m), E 0.000(m), and Elev 0.000(m). See table 1

DISCUSSION

All sensor/benchmark coordinates are contained in spreadsheet "S3002 2009.xls."

The positions given for all GPS antenna are to the top center of the antenna. As stated from the previous 2005 survey by Kendall L. Fancher:

"To correct the Z value contained in the spreadsheet for each antenna to the electronic phase center, I recommend the following steps be taken;

> 1) Measure the total height of each antenna type. This information is probably located on the antenna or with equipment documentation.

2) Investigate to find the electronic phase center offset of the antenna. This information is probably located on the antenna or with equipment documentation. This value may also be available at the NGS website for antenna modeling.

3) Subtract the total height of the antenna from the spreadsheet Z value for each antenna. This will give you a Z value for the ARP (antenna reference point) 4) Then add to this value the electronic phase center offset value."

Table 1. - NRT S 3002 survey August 2009

Table 2. – NRT S 3002 Control network inverse comparison.

S3002 Dynamic Draft Test 13 April 2009

LT(jg) Matthew Jaskoski

Background:

NRT-5 is capable of acquiring both bathymetry data and side scan sonar imagery. Accuracy in data processing is in part dependent on the determination of the change in vessel draft in relation to vessel speed through the water. This test empirically determines the dynamic draft of S3002 using the multibeam echosounder method.

Location, Date, and Personnel:

Sonar data were acquired at Gravesend Bay, New York Harbor, NY (Figure 1) on April 13 2009 (DN 103) by LT(jg) Matthew Jaskoski (OIC), PST Bert Ho (data recorder), and PST John Doroba (launch coxswain).

Figure 1: Work Site

Equipment:

TSS POS/MV version 4 + Precise Timing Aero Antenna DSM 212L DGPS receiver Kongsberg Simrad EM 3002 Odom Digibar Pro Sound Velocimeter

Procedure:

Data Acquisition:

Data were acquired over a flat relatively shallow area (appx. 8m water depth) of the Gravesend Bay anchorage. The survey area is located as close as is practicable to the Battery Park Harmonic water level station. The survey time was planned to coincide as closely as practicable to slack water. To account for any current S3002 made repeated passes at various speed intervals over the survey line in both directions. The survey line was approximately 1000m in length, however due to a barge anchoring on the northern end of the survey line during data acquisition, dead in the water (DIW) data were acquired at positions 250m, 375m and 500m along the line instead of the usual 250m, 500m and 750m positions. A sound velocity cast was taken near the survey area and applied in SIS during data acquisition.

Data Processing:

Data were converted and processed in accordance with established protocols with the following exceptions; 1) True heave was not applied as long period heave may bias dynamic draft calculations – random short period heave will be canceled out by using the median reference surface depth, and 2) a dummy dynamic draft table was created in the HVF to ensure that historic dynamic draft measurements would not be applied to the dataset. Subsets were cleaned of fliers and Uncertainly weighted surfaces were generated at 0.50m resolution. Surfaces were queried for depth and standard deviation these values were entered into an Excel spreadsheet where the median was calculated for depth and the mean was calculated for standard deviation. Vessel speed was queried in the subsets, entered in the Excel spread sheet and averaged for all subsets. The dynamic draft offset was calculated for each reference area by subtracting the median reference surface depth from median depths for each RPM/speed interval. The mean dynamic draft was calculated by averaging the median values for the subsets at $\frac{1}{4}$ and $\frac{3}{4}$ the length of the line (subsets A and C).

These values are tabulated below.

Table 1: Dynamic Draft Offset Data

Figure 2: Dynamic Draft Offset Data

Figure 3: Historical Dynamic Draft Offset Data for S3002

Conclusions:

The multibeam echosounder method of determining the dynamic draft has yielded acceptable results, current dynamic draft numbers fall within the range of previous years' results.

* POS/MV COM 1 Position Data: 9600,N,8,1,NONE; GGA, HDT, ZDA, VTG; 1Hz ** POS/MV COM 2 Attitude Data: SIMRAD 1000 Tate-Bryant, 25Hz

Appendix III – Calibration

SEA-BIRD ELECTRONICS, INC. 13431 NE 20th Street, Bellevue, Washington, 98005-2010 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4835 CALIBRATION DATE: 26-May-10

SBE19plus TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

ITS-90 COEFFICIENTS

- $a0 = 1.266560e-003$ $a1 = 2.595838e-004$
- $a2 = 4.741769e-007$
- $a3 = 1.352598e-007$

$MV = (n - 524288) / 1.6e+007$

 $R = (MV * 2.900e+009 + 1.024e+008) / (2.048e+004 - MV * 2.0e+005)$ Temperature ITS-90 = $1/\{a0 + a1[h(R)] + a2[h^2(R)] + a3[h^3(R)]\}$ - 273.15 (°C)

Residual = instrument temperature - bath temperature

Date, Delta T (mdeg C)

Temperature Calibration Report

Temperature sensors are normally calibrated 'as received', without adjustments, allowing a determination sensor drift. If the calibration identifies a problem, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or non-functional, or by customer request.

An 'as received' calibration certificate is provided, listing coefficients to convert sensor frequency to temperature. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'offset' allows a small correction for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair apply only to subsequent data.

'AS RECEIVED CALIBRATION' Performed Not Performed Date: 5/26/2010 Drift since last cal: $+0.00021$ Degrees Celsius/year Comments:

Comments:

SEA-BIRD ELECTRONICS, INC.

13431 NE 20th Street, Bellevue, Washington, 98005-2010 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4835 CALIBRATION DATE: 26-May-10

SBE19plus CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

COEFFICIENTS:

- $g = -1.018451e+000$ $h = 1.321073e-001$
- $i = -2.285564e-004$
- $\dot{1} = 3.350235e-005$

 $CPCor = -9.5700e-008$ $CTcor = 3.2500e-006$

 $f =$ INST FREQ / 1000.0

Conductivity = $(g + hf^2 + if^3 + if^4) / (1 + \delta t + \epsilon p)$ Siemens/meter

t = temperature[°C)]; p = pressure[decibars]; δ = CTcor; ϵ = CPcor;

Residual = instrument conductivity - bath conductivity

Date, Slope Correction

SEA-BIRD ELECTRONICS, INC.
13431 NE 20th Street Bellevue, Washington 98005 USA

raaaar Phone: (425) 643-9866 Fax: (425) 643-9954 www.seabird.com

Conductivity Calibration Report

Conductivity sensors are normally calibrated 'as received', without cleaning or adjustments, allowing a determination of sensor drift. If the calibration identifies a problem or indicates cell cleaning is necessary, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or nonfunctional, or by customer request.

An 'as received' calibration certificate is provided, listing the coefficients used to convert sensor frequency to conductivity. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'slope' allows small corrections for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair or cleaning apply only to subsequent data.

*Measured at 3.0 S/m

Cell cleaning and electrode replatinizing tend to 'reset' the conductivity sensor to its original condition. Lack of drift in post-cleaning-calibration indicates geometric stability of the cell and electrical stability of the sensor circuit.

SEA-BIRD ELECTRONICS, INC. 13431 NE 20th Street, Bellevue, Washington, 98005-2010 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4835 CALIBRATION DATE: 25-May-10 SBE19plus PRESSURE CALIBRATION DATA 160 psia S/N 7813

COEFFICIENTS:

y = thermistor output; t = PTEMPA0 + PTEMPA1 * y + PTEMPA2 * y^2 x = pressure output - PTCA0 - PTCA1 * t - PTCA2 * t^2

* PTCPA / (PTCPA + PTCR1 * t + PTCR2 * t²)

$$
n = x * PICB0 / (PICB0 + PICB1 * t + PICB2 * t)
$$

pressure (psia) = PA0 + PA1 * n + PA2 * n^2

Date, Avg Delta P%FS

 \bullet 25-May-10 -0.00

Date: Sep 25, 2009

DIGIBAR CALIBRATION REPORT

version 1.0 (c) 2004

ODOM HYDROGRAPHIC SYSTEMS, Inc.

Serial #: 98214-092509

STANDARD DEL GROSSO H2O

Odom Hydrographic Systems, Inc.
1450 SeaBoard Avenue, Baton Rouge, Louisiana 70810-6261, USA
Telephone: (225)-769-3051, Facsimile: (225)-766-5122
E-mail: email@odomhydrographic.com, HTTP: www.odomhydrographic.com

The instruments used in this calibration have been calibrated to the published manufacturer specifications using standards traceable to NIST, to consensus standards, to ratio methods, or to acceptable values of natural physical constants that meets the requirements of ANSI/NCSL Z540-1, ISO 9001, ISO 10012 and ISO 17025. Certificate/traceability numbers: 0002-2655.00-23491-001, 0002-2655.00-23491-002. ID#'s:294,295,762,172,56

Date Serial #

SW Version

Cable Length

Zero Voltage

Span Volage

 $R5$

 $R9$

Gradient

Intercept

Max psi:

Press Transduce

Mid-Scale Voltage

9/28/2009

98214

 1.08

100m

58649

 $.17$

 2.67

 1.42

 $3.9K$

 $10K$

3342

227

200psi

Digibar

Pressure Transducer Linearity

Date: May 13, 2010

DIGIBAR CALIBRATION REPORT version 1.0 (c) 2004

ODOM HYDROGRAPHIC SYSTEMS, Inc.

Serial #: 98212-051310

STANDARD DEL GROSSO H2O

 $\textit{Odom Hydrographic Systems, Inc.}\footnote{To see Board Avenue, Baton Rouge, Louisiana 70810-6261, USA-} \begin{minipage}{0.9\textwidth} \begin{tabular}{l} \textbf{70810-6261, USA}\\ \textbf{70810-6261, Fabphone: (225)-769-3051, Fascimile: (225)-766-5122\\ \textbf{E-mail: email@odomhydrographic.com, HTTP: www.odomhydrographic.com \end{tabular}} \end{minipage}$

The instruments used in this calibration have been calibrated to the published manufacturer specifications using standards traceable to NIST, to consensus standards, to ratio methods, or to acceptable values of natural physical constants that meets the requirements of ANSI/NCSL Z540-1, ISO 9001, ISO 10012 and ISO 17025. Certificate/traceability numbers: 0002-2655.00-23491-001, 0002-2655.00-23491-002. ID#'s:294,295,762,172,56

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Date Serial #

SW Version

Cable Length

Zero Voltage

Span Volage

 $R5$ $\overline{R9}$

Gradient Intercept

Max psi:

Velocity Check:

Communications:

External Power:

Depth Check:

Press Transducer

Mid-Scale Voltage

5/20/2010

98212

 1.11

20 meter

58649

 $.18$

2.68

 1.43 $3.9K$

 $10K$ 3378

405

200 psi

 $\sqrt{}$

 $\sqrt{}$

 $\sqrt{ }$

NA

Digibar

DVM @ L1

Appendix IV – Electronic Appendix

The Electronic Appendix contains digital files meant to accompany the report body. It is submitted as a .zip file located in the *Appendix4-ElectronicAppendix* folder.