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### *Ferdinand R. Hassler* Chief of Party: LCDR Benjamin K. Evans, NOAA Year: 2011 Version: 1.0 Publish Date: 2012-04-27

### **ent**

### **e essels**

# **e** nan assle







*Figure 1: NOAA Ship Ferdinand R. Hassler, Starboard View*



*Figure 2: NOAA Ship Ferdinand R. Hassler, Bow and Hull View*

# **A.2 Echo Sounding Equipment**

# **A.2.1 Side Scan Sonars**

### **A.2.1.1 Klein 5000**







*Figure 3: Klien 5500 configured for towing*

# **A.2.2** ulti eam Echosounders

### **A.2.2.1 eson 125**







*Figure 4: 7125 Housing flush mounted on hull*



*Figure 5: Histogram of depth differences from reference surface comparison between port and starboard 7125. Depths from port system average 0.04 meters shallower than starboard with a standard deviation of 0.03 meters.* 

### **A.2.2.2 eson 125**







### **A.2.2. eson 111**







*Figure 5: 7111 mount and fairing. Sonar is located forward on staboard hull.* 



*Figure 6: Histogram of depth differences from reference surface comparison with dual-head 7125. Depths from the 7111 are 0.4 meters deeper than the depths from the 7125s with a 0.4 meter standard deviation.* 

# **A.2. Single eam Echosounders**

#### **A.2..1 dom 200**





*Figure 6: Hull mounted Odom Vertical Beam Echosounder*

# A.2. hase easuring ath metric Sonars

No phase measuring bathymetric sonars were utilized for data acquisition.

# **A.2.5 ther Echosounders**

No additional echosounders were utilized for data acquisition.

# **A. anual Sounding Equipment**

# **A..1 ier epth auges**

No diver depth gauges were utilized for data acquisition.

### **A..2 ead ines**







*Figure 7: Leadline with removable "mud-shoe"*

# **A.. Sounding oles**

No sounding poles were utilized for data acquisition.

# **A.. ther anual Sounding Equipment**

No additional manual sounding equipment was utilized for data acquisition.

# **A. ositioning and Attitude Equipment**

# **A..1 Applani S**









## **A..2 S**



# **A.. rimle acpacs**

Trimble backpack equipment was not utilized for data acquisition.

# **A.. aser angeinders**

No laser rangefinders were utilized for data acquisition.

# **A..5 ther ositioning and Attitude Equipment**

No additional positioning and attitude equipment was utilized for data acquisition.

# **A.5 Sound Speed Equipment**

# **A.5.1 Sound Speed roiles**

**A.5.1.1 roilers**

## **A.5.1.1.1 Sea** ird Sea at 1





*Figure 8: SBE 19 CTD cast in protective cage*

### **A.5.1.2 Sound Speed roilers**

### **A.5.1.2.1 rooe cean 0**





*Figure 9: MVP control station & winch*



*Figure 10: MVP single sensor free fall fish* 

**A.5.2 Surace Sound Speed**

### **A.5.2.1 Sea** ird 5 icro S



# A. ori ontal and ertical ontrol Equipment

# **A..1 oriontal ontrol Equipment**

No horizontal control equipment was utilized for data acquisition.

# **A..2 ertical ontrol Equipment**

No vertical control equipment was utilized for data acquisition.

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# A. .1 omputer ard are





# **A..2 omputer Sotare**































# **A. ottom Sampling Equipment**

# **A..1 ottom Samplers**

# **A..1.1 onar ildco 12**



*Description* Grab sampler triggered by contact with sea floor.



*Figure 11: Ponar Grab Sampler*

 **ualit ontrol**

### **B.1 Data Acquisition**

### **B.1.1 Bathymetry**

#### **B.1.1.1 Multibeam Echosounder**

Multibeam data are acquired in through Hypack/Hysweep in HSX format for bathymetry. Multibeam data and are also logged locally on the Reson topside machines in s7k format. The HSX format includes sounding solutions, navigation, and attitude data. The s7k format includes sounding solutions, navigation, attitude and backscatter snippet data. This record included Reson datagrams: 1003, 1012, 1012, 7000, 7004, 7006, 7008, 7011, 7503. The Hypack logged .7k snippet backscatter record is not available for the dual head 7125 configuration. Ship navigation and survey line monitoring are performed with Hypack/ Hysweep.

The Reson units are interfaced with the acquisition machines through UDP LAN connections over a dedicated network switch (Netgear ProSafe Gigabit Switch). Position and attitude data is passed from the POS-MV to both the Reson machines and to the acquisition computers through dedicated network switches (NetGear ProSafe Gigabit switch). There is a decicated switch for the port and starbord POS systems. Time is passed from the POS to the Reson machines via a RS232 serial connection. The starboard POS is interfaced with the starboard 7125 and the 7111, which is located in the starboard hull. The port POS is interfaced to the port 7125.

Surface sound speed from the starboard TSG-45 is fed into all Reson machines via RS232 serial connections.

In the dual head 7125 configuration, the port 7125 is configured as the master and the starboard unit the slave. Pinging is alternated between the two heads to avoid interference. The Hypack logged HSX file in this configuration contains sounding data from both heads with the navigation and attitude data from the starboard POS-MV.

### **B.1.1.** in le Beam Echosounder

Single beam echosounder bathymetry was not acquired.

### **B.1.1. hase Measurin Bathymetric onar**

Phase measuring bathymetric sonar bathymetry was not acquired.

### **B.1.** ma ery

### **B.1..1 ide can onar**

The side scan fish is towed from a block suspended from the A-frame on the stern of the vessel . The height of the fish above the sea floor is actively managed through use of the remote winch control. Side scan imagery is monitored and logged using SonarPro. Tow cable offset values are entered into SonarPro to account for cable out in the docked tow position. This position has 12 m of cable between the tow point and the fish.

Survey lines are pre-planned to achieve coverage required by the project instruction. These lines are planned in MapInfo and exported to Hypack. Hypack is used for ship navigation and for survey line tracking.

### **B.1.. hase Measurin Bathymetric onar**

Phase measuring bathymetric sonar imagery was not acquired.

### **B.1. ound eed**

#### **B.1..1 ound eed roiles**

Seabird SBE 19 and MVP sound speed profilers are used regularly to collect sound speed data for ray tracing corrections for the multibeam sonar systems. In shallow water, the SBE 19 is hand deployed from the stern. In deeper water the oceanographic winch is used. Data is retrieved from the SBE 19 with a serial connection to an acquisition computer. Data from both the SBE 19 and MVP are processed through the NOAA in-house program Velocipy to give Caris .SVP formatted sound velocity profiles. All svp profiles for a survey sheet are concatenated to one master file for a survey.

Casts are taken at least every four hours. Cast frequency is increased in areas with strong sound speed gradients or anticipated sound speed variability. Cast locations are spread through the survey area to best capture the variability and are typically oversampled when using the MVP.



*Figure 12: Example of sound speed samples taken in a survey area*

#### **B.1.. urace ound eed**

The starboard Seabird TSG 45 thermosalinograph is used for determination of surface sound speed. This unit is located in the starboard main engine room and draws water from the raw water cooling line of the main engine. The port TSG-45 data is not used because the unit is uninsulated and reads erroneously high seawater temperatures. The starboard TSG and associated plumbing is insulated This device calculates the sound speed from the measured salinity and temperature (using the Chen-Millero equation) of the sampled water. A serial broadcast device sends the sound speed message from the SBE-45 to the port and starboard 7125 systems and the 7111. Other than the records in the logged multibeam data files, the surface sound speed is not logged.

### **B.1.** oriontal and ertical ontrol

#### **B.1..1 oriontal ontrol**

During acquisition, the port and starboard POS-MV units output position and attitude data through dedicated network switches (Netgear ProSafe Gigabit Switch) to both the acquisition computers and the sonar systems.

Applanix POS/MV .000 files are logged to the acquisition machine which contain attitude, heading, position and velocity data compliant with section 3.4.1 of the FPM. During acquisition, the navigation solution status status is constantly monitored by the acquisition watch stander.

Real-time USCG DGPS correctors are used for all acquisition. Specific DGPS stations are noted in the Descriptive Reports accompanying each survey.

#### **B.1.. ertical ontrol**

Preliminary, observed and verified water levels are downloaded using FetchTides and applied to the data using CARIS HIPS Load Tide function. Refer to individual survey Descriptive Reports for detail.

## **B.1.** eature eri ication

Feature verification followed guidelines set forth in section 3.5.5 of the FPM. Refer to individual sheet DRs for additional information if differing from previously stated.

# **B.1. Bottom am lin**

Bottom Sampling followed guidelines set forth in sections 7.1 of the HSSD and 2.5.4.2.1 of the FPM. Refer to individual sheet DRs for additional information if differing from previously stated.

### **B.1. Bac scatter**

Backscatter is acquired in the 7008 record logged in the .s7k files directly from the Reson 7125 processors. For processing, this record is paired with a GSF file exported from CARIS containing processed depth information. The paired files are imported into QPS Fledermaus Geocoder Toolbox for mosaic processing.

# **B.1. ther**

No additional data were acquired.

### **Additional Discussion**

Ferdinand Hassler maintains a continuous manned survey watch during all survey acquisition. The watch stander is in constant communication with the bridge and monitors the performance of all systems. Thresholds set in Hypack/Hysweep, POS view, Reson and Sonar Pro alert the watch stander by displaying alarm messages when error thresholds or tolerances are exceeded. Alarm conditions that may compromise survey data quality are corrected and then noted in acquisition log. Warning messages such as the temporary loss of differential GPS, excessive cross track error, or vessel speed approaching the maximum allowable survey speed are addressed by the watch stander and corrected before further data acquisition occurs.

# **B. Data rocessin**

# **B..1 Bathymetry**

### **B..1.1 Multibeam Echosounder**

Bathymetry processing followed section 4.2 of the FPM unless otherwise noted.

Raw .hsx multibeam data are converted to CARIS HIPS HDCS format. TrueHeave, sound speed and water level correctors are applied to all lines and the data is merged. Total Propagated Uncertainty (TPU) is computed using settings documented for each survey in the descriptive report.

The general resolution, depth ranges, and Combined Uncertainty and Bathymetric Estimator (CUBE) parameter settings outlined in section 5.2.2.2 of the HSSD and section 4.2.1.1.1.1 of the FPM are used for surface creation and analysis. A detailed listing of the resolutions and the actual depth ranges used during the processing of each survey, along with the corresponding fieldsheet(s), is provided in the Descriptive Report of each survey.

BASE surfaces are created using the CUBE algorithm and parameters contained in the NOAA CUBEParams\_NOAA.xml file as provided in Appendix 4 of the FPM. The CUBEParams\_NOAA.xml file will be included with the HIPS Vessel Files with the individual survey data. The NOAA parameter configurations for resolutions 0.5-32 meters are used.

Multibeam data are reviewed and edited in HIPS swath editor and in subset mode as necessary. The finalized BASE surfaces and CUBE hypotheses are used for directed data editing at the appropriate depth  range in subset editor. The surfaces and subset editor view are also used to demonstrate coverage and to check for errors due to tides, sound speed, attitude and timing.

Vessel heading, attitude, and navigation data are reviewed in HIPS navigation editor and attitude editor if deemed necessary upon review of surfaces. Where necessary, fliers or gaps in heading, attitude, or navigation data are manually rejected or interpolated for small periods of time. Any such editing is detailed in the survey Descriptive Report.

The Density method for hypothesis disambiguation is used.

The surface filtering function in CARIS HIPS is not utilized routinely.

In depths less than 20 meters and deeper in areas of navigational significance where the BASE surface does not depict the desired depth for the given area, a designated sounding is selected. Designated soundings are selected as outlined in section 5.2.1.2 of the HSSD.

IHO child layers are created using the following two formulas for IHO\_1 and IHO\_2, respectively; - Uncertainty/((0.5^2 +((Depth\*0.013)^2))^0.5) and -Uncertainty/((1.0^2 +((Depth\*0.023)^2))^0.5). IHO\_1 is created for all soundings less than 100 meters while IHO\_2 is for 100 meters and deeper. This layer is then exported and run through an application which computes statistics. The results are reported and analyzed in each sheets individual DR.

Additionally, a combined surface is reviewed in 3-D mode using one of the following programs; CARIS HIPS, CARIS Base Editor or IVS Fledermaus, to ensure that the data are reasonable models of the sea floor and do not contain any fliers.



*Figure 13: MBES flow diagram*

### **B..1. inle Beam Echosounder**

Single beam echosounders were not utilized during the 2011 field season other than for testing purposes.



*Figure 14: VBES flow diagram*

### **B..1. hase Measurin Bathymetric onar**

Phase measuring bathymetric sonar bathymetry was not processed.

### **B..1. eciic Data rocessin Methods**

### **B.** .1. . Methods sed to Maintain Data nte rity

The use of processing logs to record and communicate problems from acquisition to final processing.

#### **B..1.. Methods sed to enerate Bathymetric rids**

All methods used to generate final bathymetric grids are followed as put forth in section 4.2 and all relevant subsections of the FPM.

#### **B.** .1. . Methods sed to Derie inal De ths



### **B.** ma ery

#### **B...1 ide can onar**

Side scan sonar data are converted from .sdf (Sonarpro raw format) to CARIS HDCS lines. Fish height, vessel heading, and vessel navigation records are reviewed for each file and edited as necessary. Tow point offsets (A-Frame and cable out), fish depth, fish attitude and water depth are used to calculate horizontal lay back. Fish navigation is recalculated using CARIS SIPS.

After towfish navigation is recalculated, side scan imagery data are slant-range corrected and closely examined for targets. Targets are selected and saved as contacts to a contact file for each line of SSS data. Contact selection includes measuring apparent height and width, selecting contact position and creating a contact snapshot image. Targets are exported to Pydro for correlation and processing. Significant targets are surveyed with MBES to obtain least depths.

Side scan sonar coverage is determined by creating mosaics using Mosaic Editor in CARIS SIPS. This processed imagery data is stored in SIPS as Georeferenced Backscatter Rasters, or GeoBaRs. From GeoBaRs, mosaics are created which can be examined and edited in Mosaic Editor.



*Figure 15: SSS flow diagram*

### **B... hase Measurin Bathymetric onar**

Phase measuring bathymetric sonar imagery was not processed.

#### **B... eciic Data rocessin Methods**
#### **B.** . . Methods sed to Maintain Data nte rity

The use of processing logs to record and communicate problems from acquisition to final processing.

#### **B.** . . Methods sed to Achie e b ect Detection and Accuracy equirements

Range of the SSS, XTE, speed of vessel collecting data and repetitious processing examinations are all used to ensure that object detection and accuracy requirements are met.

#### **B....** Methods sed to eriy ath oerae

Swath coverage is verified through construction of side scan mosaics. During acquisition, the outer portions of the swath are monitored for refraction artifacts. If an apparent refraction artifact impacts objects detection ability and cannot be eliminated through adjustment of fish height, the range scale is reduced.

#### **B.... riteria sed or ontact election**

Contacts are selected it the apparent shadow measures greater than 1.0 meters or if the contact might otherwise be navigationally significant.

#### **B.... omression Methods sed or eiein maery**

No compression methods were used for reviewing imagery.

#### **B.. ound eed**

**B...1 ound eed roiles**

CTD profiles from both the Seabird SBE 19 and the AML Micro-CTD installed in the MVP system are processed using the NOAA developed program Velocipy. From each system, sound speed profiles are extracted and archived as both individual and concatenated Caris SVP files.

#### **B...1.1 eciic Data rocessin Methods**

**B...1.1.1 aris ile oncatenation Methods**

All sound speed profiles for a survey sheet are concatenated into one master file.

*Figure 99: no figure*

#### **B... urace ound eed**

Surface sound speed data were not processed.

### **B.. oriontal and ertical ontrol**

**B...1 oriontal ontrol**

Fixed USCG DGPS stations are used for all real time horizontal control. If post-processed GPS techniques are used to improve horizontal control, specific information is included in the Descriptive Report.

*Figure 99: no figure*

#### **B... ertical ontrol**

CO-OPS zoned water levels utilizing water level observations from fixed, continuously operating NOAA tide gages are used for reduction of data to MLLW. Predicted water levels are applied during preliminary processing. Before submission, verified water levels are applied to all tidally corrected data. If postprocessed GPS techniques are used to improve horizontal control, specific information is included in the Descriptive Report.

*Figure 99: no figure*

#### **B.** . eature eri ication

Features are processed using NOAA's Pydro software and are included with submitted processed data in the survey's final feature file (FFF). The FFF includes all features; buoys, rocks, wrecks, bottom samples, etc., addressed within the limits of each individual sheet.

*Figure 99: no figure*

## **B.. Bacscatter**

All backscatter was processed from acquired Reson .s7k files. Processed bathymetry is exported from Caris in GSF format, paired with the .s7k file in the raw data directory, and imported into QPS Fledermaus Geocoder Toolbox. A mosaic is processed with default processing parameters. Reson TVG plugins are used for all processing steps.

*Figure 99: no figure*

## **B.. ther**

No additional data were processed.

## **B.** uality Mana ement

Standard operating procedures (SOPs) and checklists are followed by personnel throughout the survey to ensure consistent high quality data and products.

Data is constantly reviewed for quality during acquisition and processing by all personnel. Before any data is to be submitted it is reviewed independently by at least three experienced persons who are signatories to the Descriptive Report.

## **B.** ncertainty and Error Mana ement

Error values for the multibeam and positioning systems were compiled from manufacturer specifications sheets for each sensor and from values set forth in section 4.2.3.8 and Appendix 4 - CARIS HVF Uncertainty Values of the 2011 FPM.

Regardless of this document stating that TPU was not calculated, TPU was calculated, but individual uncertainty values are not included here to reduce duplication. Refer to individually submitted HVF files for Uncertainty values used.

#### **B.** .1 otal ro a ated ncertainty

Total propagated uncertainty was not calculated.

## **B.. Deiations**

There were no deviations from the requirement to compute total propagated uncertainty.

**orrections o** Echo **oundin s** 

- **.1 essel sets and aybac**
- **.1.1 essel sets**

**.1.1.1 Descrition of prectors** 

#### **.1.1. Methods and rocedures**

Sensor offsets are measured with respect to the vessel's reference point. These offsets are derived from the full survey performed in the shipyard, a partial survey performed by NGS and measurements / verifications performed by Ferdinand R. Hassler personnel. All necessary offsets are tracked and updated as needed on a spreadsheet to be submitted with the appendices of this report.

The port IMU serves as the reference point for the port-only 7125 configuration and the side scan sonar. For all other vessel configurations the starboard IMU is the reference point.

#### **.1.1. essel set orrectors**









## **.1. aybac**

#### **.1. .1 Descrition of prectors**

Layback is calculated in Caris from the cable-out and fish depth. Cable-out is output from a cable counter and recorded in the .sdf file. A 12 meter offset is applied in Sonar Pro to account for the amount of cable out when the towfish is in the docked position. The side scan cable is marked at 12 meters and is deployed to this position on launching. The cable counter is reset to zero at this position and the 12 meter offset applied in SonarPro. Thus the cable out value in the .sdf file is the correct value for the cable between the tow point and the towfish. The port POS system is used for positioning of the side scan. The port IMU is the reference point for offsets.

#### **.1.. Methods and rocedures**

Layback was calculated from the side scan calibration performed prior of obtaining data.



#### **.1.. aybac orrectors**

## **. tatic and Dynamic Drat**

## **..1 tatic Drat**

#### **...1.1 Descrition o** orrectors

Because of her SWATH design HASSLER is particularly susceptible to loading and trim. While underway, the ballast is actively managed to maintain the draft at the design draft of 3.85 meters. During typical survey operations, HASSLER burns approximately 4,000 liters of diesel per day. At a density of 0.83 kilograms/ liter this is approximately 3.3 metric tons of fuel per day. At design draft of 3.85 meters, 1.3 metric tons is required to submerge an additional 0.01 meters of the hull in salt water. The daily fuel burn would thus account for 0.03 meters of variation in the draft. Ballast is adjusted daily to account for fuel burn and the levels in other tanks. Uncertainty is conservatively estimated at 0.05 meters.

#### **..1. Methods and rocedures**

The waterline to reference point is calculated from the vessel offset survey and the vessel draft marks.

## **Dynamic Dra** t

#### **...1 Descrition o orrectors**

#### **... Methods and rocedures**

An ellipsoidally referenced DDM was performed following guidelines put forth in the field procedures manual.

For a complete list of the dynamic draft please refer to attached ERDDM\_Summary or appropriate HVF.

#### **... Dynamic Drat orrectors**



## **ystem Ali nment**

#### **.** .1 Descrition o orrectors

#### **.. Methods and rocedures**

Methods and Procedures used follow recommendations given in section 1.5 of the 2011 FPM.

## .. ystem Ali nment orrectors





## **. ositionin and Attitude**

#### **.** .1 Descrition o orrectors

#### **.. Methods and rocedures**

Vessel attitude is measured by the POS/MV and recorded in the Hysweep .hsx file. The Reson 7111 is patch stabilized in real time, otherwise, attitude measurements not applied in real time are applied during post processing in CARIS HIPS using the raw POS/MV attitude data recorded in the Hysweep .hsx file. When available, post processed kinematic (PPK) position and attitude solutions from the POS/MV .000 file are applied to MBES data in CARIS HIPS in the form of SBET files.

The POS/MV TrueHeave data is logged within the POS/MV .000 files and applied in CARIS HIPS during post processing using the "Apply TrueHeave" function. TrueHeave is a forward-backward filtered heave corrector as opposed to the real time heave corrector, and is fully described in section 6 of the POS/MV V4 User Guide 2009.

PPK data in the form of Single Best Estimate of Trajectory (SBET) files are applied to soundings to increase the accuracy of the kinematic vessel corrections and to allow the ability to reference soundings to the ellipsoid. Standard daily data processing procedures include post processing of POS/MV kinematic .000 files using Applanix POSPac MMS and POSGNSS software using either IN-Fusion SmartBase or IN-Fusion SingleBase processing modes. After processing and quality control analysis of the post-processed SBET files is complete. the SBET and SMRMSG files are applied to the HDCS data in CARIS HIPS using the "Load Attitude/Navigation Data" and "Load Error Data" processing tools.

- **ides and ater eels**
- **.** .1 Descrition o orrectors
- **.. Methods and rocedures**

Unless otherwise noted in the survey Descriptive Report (DR) and/or project Horizontal and Vertical Control Report (HVCR), the vertical datum for all soundings and heights is Mean Lower Low Water (MLLW). Predicted, preliminary, and/or verified water level correctors from the primary tide station(s) listed in the Project Instructions may be downloaded from the CO-OPS website and used for water level corrections during the course of the project. These tide station files are collated to include the appropriate days of acquisition and then converted to CARIS .tid file format using FetchTides.

Water level data in the .tid files are applied to HDCS data in CARIS HIPS using the zone definition file (.zdf) or a Tidal Constituent and Residual Interpolation (TCARI) model supplied by CO-OPS. Upon receiving final approved water level data, all data are reduced to MLLW using the final approved water levels as noted in the individual surveys DR.

A complete description of vertical control utilized for a given project can be found in the project specific HVCR, submitted for each project under separate cover when necessary as outlined in section 5.2.3.2.3 of the FPM.

Newer methods for handling vertical control are being developed and, if utilized, will be explained in more detail in the project wide HVCR or survey descriptive report.

- **. ound eed**
- **..1 ound eed roiles**
- **.** .1.1 Descrition o orrectors

#### **..1. Methods and rocedures**

Seabird .cnv and MVP .bot files are collected when necessary and converted to .svp files using Velocipy. These .svp files are concatenated into one vessel specific master file which is then applied to HDCS data using a specified method. This method of applying sound speed to data is listed in the processing log included in the Separates submitted with the individual survey.

#### **.. urace ound eed**

**...1 Descrition o** orrectors

Surface sound speed output by the starboard TSG is fed to all multibeam systems via serial connections.

**... Methods and rocedures**

The sound speed is monitored by the acquisition watch stander and periodically compared with the CTD or MVP derived values.

#### **D. A A EE**

This Data Acquisition and Processing Report for project OPR-D304-FH-11, Approaches to Chesapeake Bay and M-H712-FH-11, Florida to North Carolina Trackline is respectfully submitted.

As Chief of Party, I have ensured that standard field surveying and processing procedures were adhered to during these projects in accordance with the Hydrographic Surveys Specifications and Deliverables (4/2011), Hydrographic Survey Technical Directive HTD 2010-2, and the Field Procedures Manual for Hydrographic Surveying (5/2011).

I acknowledge that all of the information contained in this report is complete and accurate to the best of my knowledge.

This DAPR applies to surveys F00607, H12346 which was completed in 2011 for Project D304 and survey D00158 which was completed in 2011 for Project H712.

Approved and Forwarded:

Samuel Greenaway

Digitally signed by Samuel Greenaway DN: cn=Samuel Greenaway, o=NOAA Office of Marine and Aviation Operations, ou=Ferdinand R. Hassler,

LT Samuel F. Greenaway, NOAA LCDR Benjamin K. Evans, NOAA Field Operations Officer Chief of Party

\_ \_ email=samuel.greenaway@noaa.gov, c=US Date: 2012.07.30 13:09:53 Z Benjamin K. Evans  $\mu_{\rm m}$  /  $\ell_{\rm m}$  2012.07.30 09:20:37 -04'00'

**Appendix I**

**Vessel Reports** 

Final report

## **SURVEY REPORT**

#### **SHIP: M286 SWATH FERDINAND R. HASSLER**

## **LOCATION: PASCAGOULA, MS**

**DATE: 7/18-7/26, 2009**  And **11/4, 2009**

#### **PURPOSE:**

Determine the ship's centerline, roll, and pitch. Install benchmarks, install the master reference plane in the same planes as the measured roll, pitch, and azimuth of the ship. Assist the shipyard to install the IMUs parallel to the centerline, and in the same plane as the ship's roll and pitch. Assist the shipyard in installing the transducers in the same plane as roll, pitch and azimuth of the ship. Measure and spot the draft marks.

#### **PERSONNEL:**

 Eric Kostelak Brian Kloter Raymond Impastado John Miskimmin

### **EQUIPMENT LIST:**

WILD T2 THEODOLITE SN: 169786 Calibration Expiration Date; 12/19/09

WILD T2 THEODOLITE SN: 155062 Calibration Expiration Date; 12/19/09

 WYLER CLINO 2000 CLINOMETER SN: M4416 Calibration Expiration Date; 07/10/10

 TOPCON GTS-301 One Second Electronic Total Station, Serial number GU1193 Calibration Expiration Date; 07/12/09

WILD NA1 AUTO LEVEL: SN 472810 Calibration Expiration Date; 07/12/09

## Procedures:

- **1**. Establish a baseline in relation to the centerline of both pontoons.
	- A. Locate points on each of the pontoons to determine centerline
	- B. Measure the elevation differences of the points. Take the average of these to determine the pitch and roll of each pontoon.
- **2.** Take the average of the measurements of the two pontoons for roll, pitch, and centerline. The result can then be used as the Master reference.
- **3.** Create a traverse, in a level plane, around the ship using the established baseline as a reference. Set various points that will be used to locate the master reference block, IMUs, bench marks, transducers, and antennas.
- **4.** Locate, set and secure the master reference block to within 9 arc seconds of the calculated roll, pitch, and centerline values.
- 5. Once the MRB has set for a day, confirm the measurements relative to the results of step 2. If the measurements are within the two values used in Step 2, these values will become the Final Master Reference, which all further measurements will be referenced to.
- **6**. Locate IMU foundations, adjust to be level with roll and pitch, and aligned with centerline.
- **7**. Establish bench marks that are aligned to the centerline in any areas that require future measurements.
- **8**. For transducers, on the bottom of the hull, establish punch marks aligned to the centerline that can be used to align the transducers to the centerline.
- **9**. Run a closed level loop from the master reference block to all bench marks, Transducers, antennas, and sensors to determine their elevation values relative to the reference. (Z axis).
- **10**. Using established elevation points within the traverse, determine the correct locations for all draft marks.

**11**. Work with the shipyard to determine the correct alignment of the transducers.

#### **METHODS**

All angles at intersections were turned 4 times, 2 in regular, and 2 in inverted position. All other angles were turned 2 times, once in regular, and once in inverted position.

 Slope distances were measured with a zenith angle in the regular and inverted Position.

The Traverse was closed and computed for accuracy.

## **Results**

## **MRB**

After the MRB has set up for 24 hours, it was found the chock fast had caused an 18 second movement in roll. As this small value was well within the average of the two pontoons, the final reference was shifted to the MRB values.

## **IMU**

During measurements of the IMUs, we discovered it was impossible to meet the specification to be level to the roll and pitch within 90 arc seconds using the existing mounts. The shipyard manufactured a double plate separated by three threaded rods, which allowed fine adjustment in two planes (roll and pitch). The IMUs were aligned to zero measurable azimuth error, and to within 5 arc seconds in roll and pitch relative to the MRB.

## **TRANSDUCERS**

## **7125**

During measurements it became apparent that it was impossible to meet the roll and pitch specification on the multibeam transducer mounts. There was no measurable azimuth error on either 7125 transducer mount, when the welding was finished. The shipyard came up with the roll and pitch solution of machining the surfaces in place once the mounting plates were completely welded out. We attended for the machine work on 8/19/09. A portable milling machine was put in place, leveled to within 5 arc seconds of the MRB plus 4.5 degrees of roll to Give the transducer mounting surfaces the specified 4.5 degree outward roll angle. See attached photo. It was agreed by all that if the milling machine was positioned correctly, the surfaces had to be correct, but as a check to confirm the process, we measured the machined surface on the port unit, and found the pitch error was zero, and the roll error was 15 seconds. This was well within the required 90 seconds.

Milling machine set up on 7125 transducer housing



## **7111**

Like the 7125s, it was impossible to meet the roll and pitch specification on this transducer mounting plate. It too, was machined by the portable milling machine. The machine was set up to be within 5 seconds of the MRB Pitch and Roll values.

# XYZ COORDINATES TABLE











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 $\omega$






 $\label{eq:zeta} \begin{array}{c} \vspace{2mm} \vspace{2mm} \\ \vspace{2mm} \vspace{2mm} \end{array} \hspace{2mm} \begin{array}{c} \vspace{2mm} \\ \vspace{2mm} \end{array} \$ 









 $\omega^{(0)}$ 





 $\left\langle \hat{\mathbf{e}}_{i}\right\rangle$ 

























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# U.S. Department of Commerce National Oceanic & Atmospheric Administration National Ocean Service National Geodetic Survey Field Operations Branch

## NOAA SHIP HASSLER POS ANTENNA and Component Spatial Relationship Survey Field Report

Kevin Jordan March, 2011



## NOAA Ship Hassler POS Antenna and Spatial Relationship Survey

## **PURPOSE**

The intention of this survey was to accurately position the relocated POS Antennas and Side Scan Sonar tow point.

#### PROJECT DETAILS

This survey was conducted on March 29, 2011 on Spring River Island in Pascagoula, MS. NGS was provided data from a previous survey that contained a complete point listing of all components as well as recoverable bench mark stations. The NOAA Ferdinand Hassler was in water causing some instability of the instrument and target reflectors. The tilt compensator had to be bypassed in order to take measurements.

#### INSTRUMENTATION

The TOPCON GPT 3000 Series Total Station was used to make all measurements.

A SECO 25 mm Mini Prism System configured to have a zero mm offset was used as target sighting and distance measurements.

## SOFTWARE AND DATA COLLECTION

TDS Survey Pro Ver. 4.7.1

ForeSight DXM Ver. 3.2.2 was used for post processing.

**PERSONNEL** 

Kevin Jordan NOAA/NOS/NGS/Field Operations Branch 757-441-5478

Doug Adams NOAA/NOS/NGS/Field Operations Branch 757-441-5480

NOAA Ship Hassler POS Antenna and Spatial Relationship Survey

## **SURVEY PROCEDURES**

#### **RECOVERED STATIONS**

## MID BENCH MARK TOP WHEEL HOUSE



## PORT BENCH MARK TOP WHEEL HOUSE



STARBOARD BENCH MARK TOP WHEEL HOUSE



AFT MID BENCH MARK BACK DECK



PORT BENCH MARK BACK DECK



STARBOARD BENCH MARK BACK DECK



## PORT BENCH MARK BRIDGE WING -NO PHOTOS OF THIS STATION

## **NEW FEATURES**



# STARBOARD POS ANTENNA MOUNT



SIDE SCAN SONAR TOW POINT -Horizontal Survey Point (HSP) -Vertical Survey Point (VSP)



#### **Setup #1**

Using the coordinates from the previous survey, the field crew setup the theodolite on the MID BENCH MARK TOP WHEEL HOUSE and initialized on PORT BENCH MARK BRIDGE WING to obtain a starting azimuth. From this setup, we collected the four POS antenna mount locations:

PORT FWD ANTENNA PORT AFT ANTENNA STARBOARD FWD ANTENNA STARBOARD AFT ANTENNA

Positional checks were made to bench mark stations (see attached comparison report):

PORT BENCH MARK TOP WHEEL HOUSE STARBOARD BENCH MARK TOP WHEEL HOUSE PORT BENCH MARK BRIDGE WING

A temporary point (TP1) was established on the flying bridge near the stairs in order to collect the location of the SIDE SCAN SONAR TOW POINT.

#### **Setup #2**

The field crew setup on TP1 and initialized on the MID BENCH MARK TOP WHEEL HOUSE. From this setup, we collected:

SIDE SCAN SONAR TOW POINT

Positional checks were made to bench mark stations (see attached comparison report):

MID BENCH MARK TOP WHEEL HOUSE AFT MID BENCH MARK BACK DECK

#### **Setup #3**

The field crew setup on AFT MID BENCH MARK BACK DECK and initialized on TP1. Positional checks were made to bench mark stations (see attached comparison report):

PORT BENCH MARK BACK DECK STARBOARD BENCH MARK BACK DECK
### **DISCUSSION**

All sensor/benchmark coordinates are contained in spreadsheets "NOAA SHIP HASSLER.xls"

The following table includes stations that were observed from more than one setup and for each, an inverse was computed to identify possible setup errors. Each station checked with favorable results.





POSMV offsets are derived from Impasato Centerline Survey (2010) and NGS POS Antenna Survey (April 2011), and measurements by FH personnel.



center

(in POSMV) phase center (in POSMV)

phase center





Measurement	<b>IMU to 7111 (MRU to Trans)</b>		Fwd Port Ant to 7111 (Nav to Trans)			<b>Hysweep Offsets</b>		
Coord. Sys.	Caris			Caris				<b>Hypack</b>
x	1.203			12.402		<b>Stbd IMU to</b> 7111 RP	Stbd	1.203
v	11.678			9.749			Fwd	11.678
z	1.180			13.920			Vertical	3.460
*Top of IMU is RP (Reference Pt)				(Hypack vertical is positive down from waterline.)				

Vessel Offsets for S250 7111 are derived from Impasato Centerline Survey (2010) and NGS POS Antenna Survey (April 2011), and measurements by FH personnel.







Vessel Offsets for S250 Stbd 7125 are derived from Impasato Centerline Survey (2010) and NGS POS Antenna Survey (April 2011), and measurements by FH personnel















**Waterline to Stbd 7125 RP**





Tilted up 4.5 degrees up on both sides

(Hypack vertical is positive down from waterline.)

Vessel Offsets for dual 7125 are derived from Impasato Centerline Survey (2010) and NGS POS Antenna Survey (April 2011), and measurements by FH personnel. **Calculations**





**Note: For dual acquisition 7125, the HSX file contains data from both 7125s but only POSMV data from the stbd POSMV. The port 7125 is swath 1 (beams 1-512) and the stbd 7125 is swath 2 (beams 513 to 1024).** 

























PORT STBD Notes Average 2.27475 2.286643 Waterline<br>SD 0.0413 0.042215 Loading U 0.0413 0.042215 Loading Uncertainty **Appendix II**

**Echosounder Reports** 

#### **Hassler Multibeam Echosounder Calibration**





HEADING/YAW view parallel to track, offset lines (outerbeams) [opposite direction, same speed]





## **Processing Log**



**PATCH TEST RESULTS/CORRECTORS**



**HVF Hydrographic Vessel File created or updated with current offsets**

**Name: Date:**

### **FERDINAND R. HASSLER Multibeam Echosounder Calibration**

**Please choose a vessel**

Vessel



## **Acquisition Log**



2011\_1881611 345 8.0





## **Processing Log**



#### **PATCH TEST RESULTS/CORRECTORS**



#### **NARRATIVE**

PS Wilson values (2nd attempt): latency and pitch were both no change. Roll value -0.08, yaw value -0.35 LT Greenaway, 2nd attemp - roll -0.08

Not sure the casue.

**HVF Hydrographic Vessel File created or updated with current offsets**

**Name:** <u>**Date: Date: Date</u>** 

## **FERDINAND R. HASSLER Multibeam Echosounder Calibration**

 $\overline{V}$ **Please choose a vessel**





# **Acquisition Log**







#### **Processing Log**



#### **PATCH TEST RESULTS/CORRECTORS**



#### **NARRATIVE**

Both HSX and S7K processed and SBETs and Error Files applied from POSPAC.

**HVF Hydrographic Vessel File created or updated with current offsets**

**Name:** Date: **Date: Date: Date:**

S250‐Dual Head Worksheet



#### **FH 2011 Sidescan Calibration Side Scan run on Dn279, 2011. MBES run on Dn277, 2011 Contact is conspicuous point on debris field off Cape Charles City**

#### **MBES Position of Contact**

Lat (DD) Long (DD) 37.2338 ‐76.0775



Criteria: 95% Confidence that any future measurement will not give <sup>a</sup> positional error greater than 10 meters.

Assuming x and y errors are goverened by the same normal distribution, the square of the distance error is governed by Chi‐squared statistics.

So:

 $=$   $\alpha$ σ  $\sigma$   $\chi$ <sub>n; $\alpha$ </sub>  $P\left[ d^{-2} > \frac{\sigma^2 \chi^2_{n;\alpha}}{n} \right]$ 

Setting the distance error equal to 10 meters and using the Chi‐squared value for one degree of freedom and alpha <sup>=</sup> 0.05, solve for the maximum value for the standard deviation of the <sup>x</sup> or y error.



The sample estimate of the standard deviation will also be Chi‐squared distributed

At a 95% confidence interval the standard deviation range is:




**Appendix III**

**Positioning and Attitude System Reports** 

# **POSMV 320 INSTALLATION REPORT**



Prepared for NOAA Ferdinand Hassler S250 SWATH May, 2011 By

> Bruce A. Francis Applanix Houston, TX











During the period of May16th to May 18th, 2011 two POSMV systems were commissioned aboard NOAA vessel *Ferdinand Hassler*. The following is a summary of the events and final observations.

#### **Chronology:**

May 16th-

Travel from Houston TX to New Orleans LA. Overnight in Gulfport MS with the intention of meeting the ship in the morning to conduct dockside testing in the morning before the ship sets sail in the afternoon. Informed by Steve Laverty there has been a change in plan and the CO wants to depart the dock at 0900 tomorrow instead.

#### May 17th-

 Arrive ship 0730. Brief review of POSMV installation with Briana Welton followed by cursory inspection. Both POSMV systems are up and running with no errors. Collected a set of dockside POSMV data from both systems for processing in POSPAC later today. Plan is to meet at the NOAA facility in Pascagoula at 0630 and transit out to ship in small boat.

May 18<sup>th</sup>- 0630- Depart Pascagoula for Ferdinand Hassler. Upon arrival commenced system inspection and diagnostics. No faults found. Conducted two GAMS calibrations on both POSMV systems and completed system acceptance testing.

#### **Calibration and testing results:**

1. The GAMS calibration was completed on May  $18<sup>th</sup>$  and checked against the calculations derived from the survey report. Further comparisons are required but it appears that the survey calculations differ somewhat from the GAMS measured values.

#### **Notes:**

 As a result of post processing the data set collected during commissioning, it was discovered that the POSMV IMU's were actually reversed at the back of the POSMV PCS units. Because of the symmetry in the two systems, these errors were not immediately obvious during the trials; however the lever arm errors were apparent in the data set. After physically changing the IMU inputs the processed calibration data was now reasonable when compared to the measured survey results. A new GAMS calibration was performed by the NOAA personnel after the IMU cables were returned to the correct orientation and the information below is based upon the correct orientation.





#### **Recommendations:**

While the large separation between the GPS antennas across decks will improve heading accuracy, there is a possibility that flexure in the ship will cause poor GAMS performance as the baseline vectors may become unstable. We were unable to fully test this configuration in a calm sea but if this turns out to be the case after the ship experiences a modest increase in sea state, the solution might be to extend the separation between the antennas on the individual mounts and switch the antenna input to the POS from cross decks to using the pairs from each side to their corresponding POS unit. The minimum separation should be 1 meter whereas now the distance is only about 0.6m and slightly too short to expect normal GAMS performance.

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Submitted By: Bruce A. Francis Customer Support Engineer Marine Products 713-896-9900 bfrancis@applanix.com









#### **Port System Lever Arms: (Units are in Meters)**







**General System information:** 

**Options included- RTK (RTK-0); True Heave (THV-0); (DPW-0) Password protection Disabled** 

#### **Port POSMV**



#### **Basic installation geometry:**







POSRT Data Extraction Utility [Jun 15 2011] Copyright (c) 2008-2011 Applanix Corporation. All rights reserved. Date : 07/25/11 Time : 15:12:36 -- -- First POS file : E:\Clients config, IP, & test results\NOAA\NOAA Swath\Final\_Data\_IMUcorrect\For Bruce Frances\2011\_152\_S250\_Port\_A\_GAMS.000 Last POS file : E:\Clients config, IP, & test results\NOAA\NOAA Swath\Final\_Data\_IMUcorrect\For Bruce Frances\2011\_152\_S250\_Port\_A\_GAMS.000 Output path : C:\Documents and Settings\bfrancis\My Documents\POSPac MMS\Unnamed(1)\Swath Port IMU\Extract Output kernel : Swath Port IMU Start time : 0.000 End time : 999999.000 VNAV output modulus : 1 -- -- 307750.275 : The First Group 99: Versions & Statistics System Version: Product-Model: MV-320; Version: VER4; Serial Number: S/N3187; Hardware Version: HW3.3-7; Software Release Version-Date: SW05.03-Mar10/10; ICD release version: ICD04.02; Operating System Version: OS425B14; IMU Type: IMU2; Primary GPS Type: PGPS13; Secondary GPS Type: SGPS13; Option mnemonic-Expiry Time: DMI0; Option mnemonic-Expiry Time: GIM0; Option mnemonic-Expiry Time: RTK-0; Option mnemonic-Expiry Time: THV-0; Option mnemonic-Expiry Time: DPW-0; Primary GPS Version: BD950 SN:4814A14457, v.00232, channels:24; Secondary GPS Version: BD950 SN:4814A14447, v.00232, channels:24; Total Hours : 561.4; Number of Runs: 53 Average Length of Run: 10.6; Longest Run: 126.2; Current Run: 12.1; -- 307750.275 : Diffcorr2 time1 gap: start 0.0, end 307750.2749 307750.280 : IMU type: IMU2 Data rate = 200 Hz 307750.280 : Extracting Group 4 : Time-tag data 307750.290 : SNV status changed to 0 (Full Nav) 307751.070 : Primary GNSS receiver type is GNSS13. 307751.090 : Secondary GNSS receiver type is GNSS13. 307755.275 : GenB( 9): GAMS solution in use CLEARED. 307756.275 : GenB( 9): GAMS solution in use SET. 307758.275 : GenB( 9): GAMS solution in use CLEARED. -- 307759.275 : Message 50: Transition to NAVIGATE mode. -- -- 307759.275 : Message 37: Base 1 setup Input data type expected: RTCM 1 or 9 Datum Type: NAD83 -- -- 307759.275 : Message 38: Base 2 setup Input data type expected: RTCM 1 or 9 Datum Type: WGS84 -- -- 307759.275 : Message 20: General parameters Time and distance tag types: 2 1 Autostart selection: ENABLED Reference-IMU lever arm: -0.008 -0.031 0.130 Reference-primary GPS lever arm: 1.395 1.050 -13.084 Reference-auxiliary 1 GPS lever arm: 0.000 0.000 0.000













GAMS heading calibration threshold : 0.500<br>GAMS heading correction : 0.000 GAMS heading correction











#### **Observed GAMS values derived from the field calibration:**

Port GAMS Cal #1









## **Primary GPS data observed from internal Trimble BD950 receivers.**<br>**<b>REGPS Data**

#### **Secondary embedded GPS data:**







#### **Com port #1 settings as installed: DGPS input from Trimble SPS Receiver.**



#### **Com port #2 settings as installed**



#### **Com port #3 settings as installed:**







#### **Com port #4 settings as installed:**



### **Com port #5 settings as installed**



**Heave data plot:** 



The heave plot above shows the relationship between the Real-time (RT) heave and the True (or delayed TH) heave measurements. The green line relates to quality control (QC) and represents the difference between the two values. When the delta between the RT and TH exceeds 5cm or 5% of total heave (pink line) then the radio light on the main controller screen will turn from green to red but does not affect the real-time heave data being collected. Quite often this occurs after the vessel makes a turn or an abrupt change in speed and is not necessarily cause for alarm. The heave filter has a 105 second buffer so the event which may have caused the impulse happened in the past. A red light merely calls the users attention to the difference and may also suggest that the filter settings need to be refined if the QC value is continually out of bounds.

Note: The TrueHeave data filter is delayed about 3 minutes from the TH value. Also, Group 111 & 113 must be enabled in the Ethernet Real-time logging page. In addition, this filter should be adjusted as required for changes in the local swell conditions. Su do require a for hoth POSMV systems.





# **NOAA**



## Ferdinand Hassler

**The main controller screens below shows normal POSMV operation. POS Mode is FULL indicating that all user accuracy settings have been satisfied. Note, when using RTK the position threshold should be set to a smaller value i.e. 0.100m or whatever is specified in the survey parameters. Exceeding any of the limits below will cause one of the radio lights to turn red and the POS mode will no longer report "Full Navigation" This however only affects the flag in the GGA or GGK message and not the performance.** 



#### Port POSMV Final Navigation







Port side antenna and IMU mounting:















#### **Port System Lever Arms: (Units are in Meters)**







#### **STRB POSMV**









POSRT Data Extraction Utility [Jun 15 2011] Copyright (c) 2008-2011 Applanix Corporation. All rights reserved. Date : 07/25/11 Time : 15:12:36 -- -- First POS file : E:\Clients config, IP, & test results\Swath 250 Testing\Final Report Files\Final\_Data\_IMUcorrect\For Bruce Frances\2011\_152\_S250\_Stbd\_GAMS.000 Last POS file : E:\Clients config, IP, & test results\Swath 250 Testing\Final Report Files\Final\_Data\_IMUcorrect\For Bruce Frances\2011\_152\_S250\_Stbd\_GAMS.003 Output path : C:\Documents and Settings\bfrancis\My Documents\POSPac MMS\Unnamed(2)\Mission 1\Extract Output kernel : Mission 1 Start time : 0.000 End time : 999999.000 VNAV output modulus : 1 -- Opening file: E:\Clients config, IP, & test results\Swath 250 Testing\Final Report Files\Final\_Data\_IMUcorrect\For Bruce Frances\2011\_152\_S250\_Stbd\_GAMS.000 307625.639 : Output time 1 is in UTC time 307625.639 : Output time 2 is in POS time 307625.639 : Output distances are in POS distance 307625.639 : IMU type: IMU2 Data rate = 200 Hz 307625.639 : Extracting Group 4 : Time-tag data 307625.649 : SNV status changed to 0 (Full Nav) 307626.069 : Primary GPS receiver type is GPS13. 307626.094 : Secondary GPS receiver type is GPS13. 307626.144 : Extracting Group 10: The General Status & FDIR data. 307626.144 : GenA( 2): IIN quadrant resolved SET. 307626.144 : GenA( 3): IIN fine align active SET. 307626.144 : GenA( 4): IIN navigator initialized SET. 307626.144 : GenA( 5): IIN navigator alignment active SET. 307626.144 : GenA( 7): IIN full navigation solution SET. 307626.144 : GenA( 8): IIN initial position valid SET. 307626.144 : GenA(16): RAM config != NVM SET. 307626.144 : GenB( 0): IIN user attitude performance SET. 307626.144 : GenB( 1): IIN user heading performance SET. 307626.144 : GenB( 2): IIN user position performance SET. 307626.144 : GenB( 3): IIN user velocity performance SET. 307626.144 : GenB( 8): GAMS installation parameters valid SET. 307626.144 : GenB( 9): GAMS solution in use SET. 307626.144 : GenB(10): GAMS solution OK SET. 307626.144 : GenB(16): Primary GPS configuration file sent SET. 307626.144 : GenB(18): Primary GPS in CA mode SET. 307626.144 : GenB(23): Primary GPS observables in use SET. 307626.144 : GenB(24): GAMS secondary GPS observables in use SET. 307626.144 : GenC( 6): RTCM Type 1 or 9 in use SET. 307626.144 : GenC(13): IIN in RTCM DGPS aided mode SET. 307626.144 : FDIR1(13): Ephemeris missing SET. -- 307626.144 : The First Group 99: Versions & Statistics System Version: Product-Model: MV-320; Version: VER4; Serial Number: S/N3189; Hardware Version: HW3.3-7; Software Release Version-Date: SW05.03-Mar10/10; ICD release version: ICD04.02; Operating System Version: OS425B14; IMU Type: IMU2; Primary GPS Type: PGPS13; Secondary GPS Type: SGPS13; Option mnemonic-Expiry Time: DMI0; Option mnemonic-Expiry Time: GIM0; Option mnemonic-Expiry Time: RTK-0; Option mnemonic-Expiry Time: THV-0; Option mnemonic-Expiry Time: DPW-0; Primary GPS Version: BD950 SN:4808A98939, v.00232, channels:24; Secondary GPS Version: BD950 SN:4642A73565, v.00232, channels:24; Total Hours : 789.9; Number of Runs: 66 Average Length of Run: 12.0; Longest Run: 84.0; Current Run: 12.2; -- 307626.144 : Diffcorr2 time1 gap: start 0.0, end 307626.1439

**Page 18 of 26** 







-- 307633.139 : Message 50: Transition to NAVIGATE mode. -- -- 307633.139 : Message 37: Base 1 setup Input data type expected: RTCM 1 or 9 Datum Type: NAD83 -- -- 307633.139 : Message 38: Base 2 setup Input data type expected: RTCM 1 or 9 Datum Type: WGS84 -- -- 307633.139 : Message 20: General parameters Time and distance tag types: 2 1 Autostart selection: ENABLED Reference-IMU lever arm: -0.008 -0.031 0.130 Reference-primary GPS lever arm: 1.929 -11.199 -13.076 Reference-auxiliary 1 GPS lever arm: 0.000 0.000 0.000 Reference-auxiliary 2 GPS lever arm: 0.000 0.000 0.000 Reference-IMU mounting angles: 0.000 0.000 0.000 Reference-vehicle mounting angles: 0.000 0.000 0.000 Multipath environment: LOW -- -- 307633.139 : Message 24: User accuracy parameters User position accuracy: 2.00 User velocity accuracy: 0.50 User attitude accuracy: 0.05 User heading accuracy: 0.05 -- -- 307633.139 : Message 106: Heave ratios Heave Bandwidth (sec): 12.000 Heave Damping Ratio: 0.707 -- -- 307633.139 : Message 120: Heave and sensor 1&2 install parameters Reference-Sensor1 alignment angles (R,P,Y) in degrees: 0.000 0.000 0.000 Reference-Sensor2 alignment angles (R,P,Y) in degrees: 0.000 0.000 0.000 Reference-Sensor1 lever arm in meters:  $0.000 \t 0.000 \t 0.000 \t 0.000$ <br>Reference-Sensor2 lever arm in meters:  $0.000 \t 0.000 \t 0.000$ Reference-Sensor2 lever arm in meters: Reference-Centre of Rotation in meters:  $0.000 \t 0.000 \t 0.000$ -- -- 307633.139 : Message 121: Vessel Installation Parameters Reference-Vessel in meters: 0.00 0.00 0.00 -- -- 307633.139 : Message 32: PCS IP address IP Address (Network part 1): 129 IP Address (Network part 2): 100 IP Address (Host part 1): 1 IP Address (Host part 2): 231 -- -- 307633.139 : Message 56: General data Initial status: COARSE\_LEVEL Initial position: 30.339738973 -88.576114608 -17.526 Initial distance: 0.00 Initial attitude: 0.000 0.000 0.000 -- -- 307633.139 : Message 21: GAMS install parameters A-B antenna separation: 8.122 A-B baseline vector: 0.170 8.120 -0.003 Heading error for calibration: 0.50 A-B azimuth correction: 0.000 --













#### **Observed GAMS values derived from the field calibration:**  STRB GAMS Cal #1









#### **Primary GPS data observed from internal Trimble BD950 receivers.**

#### **Secondary embedded GPS data:**







### **Com port #1 settings as installed: DGPS input from Trimble SPS Receiver.**



### **Com port #2 settings as installed**



#### **Com port #3 settings as installed:**







#### **Com port #4 settings as installed:**



### **Com port #5 settings as installed**







### **STRB POSMV Final Navigation**







STRB side antenna and IMU mounting:



STRB IMU Mount





## **NOAA POS/MV Calibration Report**





### **POS/MV Calibration**

#### **Calibration Procedure:** (Refer to POS MV V4 Installation and Operation Guide, 4-25)



#### **Calibration Results:**



**Save POS Settings on PC** (Use File > Store POS Settings on PC)

File Name: POSConfig\_DATE (saved in GNSS folder on C drive)



#### **SETTINGS**





**Lever Arms and Mounting Angles** (Use Settings > Installation > Lever Arms and Offsets)



**Tags, Multipath and Auto Start (Use Settings > Installation > Tags, Multipath and Auto Start)** 



**Sensor Mounting** (Use Settings > Installation > Sensor Mounting)





**GPS Receiver Configuration** (Use Settings> Installation> GPS Receiver Configuration)







### **NOAA POS/MV Calibration Report**



**Satellite Constellation** (Use View> GPS Data)

**Secondary GPS**

#### **Primary GPS**




### **POS/MV Calibration**



c) Roll rotation - apply a right-hand screw rotation θx about the

twice-rotated x-axis to align one frame with the other.

**Calibration Procedure:** (Refer to POS MV V4 Installation and Operation Guide, 4-25)

### **SETTINGS**



**COM2** ZDA and PPS for Reson 7125 and 7111



**COM3** TSS motion string for Reson 7111



**COM4** GGA and VTG for Side Scan









**Frame Control** (Use Tools > Config)



User Frame **Primary GPS Measurement** IMU Frame Auxiliary GPS Measurement

**Use GAMS enabled**

### **Primary GPS Receiver**



### **Secondary GPS Receiver**



**Appendix IV**

**Sound Speed Sensor Reports** 



13431 NE 20th Street, Bellevue, Washington, 98005-2010 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

**SENSOR SERIAL NUMBER: 1060 CALIBRATION DATE: 26-Feb-11** 

**GHIJ COEFFICIENTS** 

SBE19 CONDUCTIVITY CALIBRATION DATA PSS 1978:  $C(35.15.0) = 4.2914$  Seimens/meter

### **ABCDM COEFFICIENTS**



 $a = 4.50284488e-002$  $b = 4.31069500e-001$  $c = -4.00398956e+000$  $d = -1.50222338e-004$  $m = 2.1$  $CPCor = -9.5700e-008 (nominal)$ 



Conductivity =  $(g + hf^2 + if^3 + if^4)/10(1 + \delta t + \epsilon p)$  Siemens/meter Conductivity =  $(a f^m + b f^2 + c + dt) / [10 (1 + \epsilon p)$  Siemens/meter

t = temperature[°C)]; p = pressure[decibars];  $\delta$  = CTcor;  $\epsilon$  = CPcor;

Residual = (instrument conductivity - bath conductivity) using g, h, i, j coefficients





## **Conductivity Calibration Report**



Conductivity sensors are normally calibrated 'as received', without cleaning or adjustments, allowing a determination of sensor drift. If the calibration identifies a problem or indicates cell cleaning is necessary, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or nonfunctional, or by customer request.

An 'as received' calibration certificate is provided, listing the coefficients used to convert sensor frequency to conductivity. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'slope' allows small corrections for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair or cleaning apply only to subsequent data.



\*Measured at 3.0 S/m

Cell cleaning and electrode replatinizing tend to 'reset' the conductivity sensor to its original condition. Lack of drift in post-cleaning-calibration indicates geometric stability of the cell and electrical stability of the sensor circuit.

13431 NE 20th Street, Bellevue, Washington, 98005-2010 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

### **SENSOR SERIAL NUMBER: 1060 CALIBRATION DATE: 26-Feb-11**

### SBE19 TEMPERATURE CALIBRATION DATA **ITS-90 TEMPERATURE SCALE**

### **IPTS-68 COEFFICIENTS**



**ITS-90 COEFFICIENTS** 





Temperature ITS-90 =  $1/\{g + h[ln(f_0/f)] + i[ln^2(f_0/f)] + j[ln^3(f_0/f)]\}$  - 273.15 (°C) Temperature IPTS-68 =  $1/\{a + b[ln(f_0/f)] + c[ln^2(f_0/f)] + d[ln^3(f_0/f)]\}$  - 273.15 (°C) Following the recommendation of JPOTS:  $T_{68}$  is assumed to be 1.00024 \*  $T_{90}$  (-2 to 35 °C)

Residual = instrument temperature - bath temperature

Date, Offset(mdeg C)





## **Temperature Calibration Report**



Temperature sensors are normally calibrated 'as received', without adjustments, allowing a determination sensor drift. If the calibration identifies a problem, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or non-functional, or by customer request.

An 'as received' calibration certificate is provided, listing coefficients to convert sensor frequency to temperature. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'offset' allows a small correction for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair apply only to subsequent data.



 $\overbrace{63283}^{1060}$  SEA-BIRD ELECTRONICS, INC.<br> $\overbrace{632333333336652 \times (425)643 \times 9866}^{20 \text{th Street, Bellevue, Washington, } 98005-2010 USA}$ 425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

**UMBER: 1060** CALIDRATION DATE: 09-Mar-11

### SBE19 PRESSURE CALIBRATION DATA 300 psia S/N 195086 TCV: 218

### STRAIGHT LINE FIT:



**OUADRATIC COEFFICIENTS:** 





Straight Line Fit:

Pressure (psia) =  $M * N + B (N = binary output)$ 

Quadratic Fit:

pressure (psia) = PA0 + PA1 \* N + PA2 \*  $N^2$ 

Residual = (instrument pressure - true pressure) \* 100 / Full Scale Range



### AML Calibration Equipment

### Temperature Calibrations

Performed using either of two Hart Scientific "Black Stack" Model 1560 Power Bases with attached Hart Scientific Model 2563 Thermistor Modules connected to a Thermometrics AS125 4 Wire Thermistor Standard

1: Hart Scientfic Power Base 1560 S/N 79263 / Thermistor Module 2563 S/N 79039 / Thermometrics AS125 4 Wire Thermistor Standard S/N 2131 2: Hart Scientfic power Base 1560 S/N A05690 / Thermistor Module 2563 S/N A05693 / Thermometrics AS125 4 Wire Thermistor Standard S/N 2128

Temperature calibration equipment is calibrated yearly and verified bi-monthly as per Applied Microsystems Ltd. Calibration Schedule T11.2 utilizing a Hart Scientific Model 5901 Triple Point of Water Cell. All temperature calibrations and verifications are ITS-90 and NIST traceable

### Pressure Calibrations

Performed using a Budenburg Model 380D S/N 18564 Range 0-8000 psi Deadweight Tester. Calibrations and verifications are implemented as per Applied Microsystems Ltd. Calibration Schedule T11.2. All pressure calibrations and verifications are NIST traceable.

### Conductivity Calibrations

Performed using either of two Guildline 8400B S/N 59251 or Guildline 8400 S/N 43385 Autosals. Both Conductivity Calibrators are calibrated and verified using Ocean Scientific International IAPSO Standard Seawater as per Applied Microsystems ltd. Calibration Schedule T11.2. All Conductivity Calibrations and verifications are NIST traceable

### Battery Channel Calibrations

Performed using a Precision Fluke Model 45 Multimeter S/N 4720162. Calibrations and verifications are implemented as per Applied Microsystems Ltd. Calibration Schedule T11.2 All calibrations and verifications are NIST traceable.

### Sound Velocity Calibrations

Performed using an Applied Microsystems Ltd Temperature Standard S/N 9998 in distilled water, <5 ppm TDS, and sound velocity reference is Del Grosso and Mader's Pure Water Equation. Calibrations and verifications are implemented as per Applied Microsystems Ltd. Calibration Schedule T11.2 All temperature calibrations and verifications are ITS-90 and NIST traceable.

# Conductivity Calibration





mS/cm=A+B\*Nte+C\*Nte^2+D\*Nte^3+(E+F\*Nte+G\*Nte^2+H\*Nte^2)\*Raw

A=-1.152428E-2 G=1.893281E-11 B=9.157882E-7 H=-5.385734E-14  $C=-8.103243E-9$   $I=0.000000E+00$ D=2.305094E-11 J=0.000000E+00 E=2.692588E-5 K=0.000000E+00 F=-2.139692E-9 L=0.000000E+00



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# Pressure Calibration





dBar=A+B\*T+C\*T^2+D\*T^3+(E+F\*T+G\*T^2+H\*T^3)\*Raw+(I+J\*T+K\*T^2+L\*T^3)\*Raw^2





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# Temperature Calibration





Deg C=A+B\*Raw+C\*Raw^2+D\*Raw^3+E\*Raw^4+F\*Raw^5+G\*Raw^6





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## 1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

### SENSOR SERIAL NUMBER: 0276 CALIBRATION DATE: 15-Feb-09

SBE 45 TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

### ITS-90 COEFFICIENTS

- $a0 = 4.876460e 006$
- $a1 = 2.820307e-004$
- $a2 = -3.073148e 006$
- a3 <sup>=</sup> 1.663229e-007



Temperature ITS-90 =  $1/{a0 + a1}$ [ $ln(n)$ ] +  $a2$ [ $ln^2(n)$ ] +  $a3$ [ $ln^3(n)$ ]} - 273.15 (°C)

Residual <sup>=</sup> instrument temperature - bath temperature



Date, Delta T (mdeg C)

## 1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

### SENSOR SERIAL NUMBER: 0276 CALIBRATION DATE: 15-Feb-09

SBE 45 CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) <sup>=</sup> 4.2914 Siemens/meter

### COEFFICIENTS:

- $g = -1.000413e+000$
- h <sup>=</sup> 1.568807e-001
- i <sup>=</sup> -2.349823e-004
- $j = 4.488494e-005$





f <sup>=</sup> INST FREQ \* sqrt(1.0 <sup>+</sup> WBOTC \* t) / 1000.0

Conductivity =  $(g + hf^2 + if^3 + if^4) / (1 + \delta t + \epsilon p)$  Siemens/meter

t = temperature<sup>[°</sup>C)]; p = pressure[decibars];  $\delta$  = CTcor;  $\varepsilon$  = CPcor;

Residual <sup>=</sup> instrument conductivity - bath conductivity



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SBE 45 TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

### ITS-90 COEFFICIENTS

- $a0 = 1.268100e-005$
- $a1 = 2.854515e-004$
- $a2 = -3.347123e-006$
- a3 <sup>=</sup> 1.747491e-007



Temperature ITS-90 =  $1/{a0 + a1}$ [ $ln(n)$ ] +  $a2$ [ $ln^2(n)$ ] +  $a3$ [ $ln^3(n)$ ]} - 273.15 (°C)

Residual <sup>=</sup> instrument temperature - bath temperature



Date, Delta T (mdeg C)

## 1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

### SENSOR SERIAL NUMBER: 0277 CALIBRATION DATE: 15-Feb-09

SBE 45 CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) <sup>=</sup> 4.2914 Siemens/meter

### COEFFICIENTS:

- $g = -9.768655e-001$
- h <sup>=</sup> 1.532775e-001
- i <sup>=</sup> -2.703518e-004
- $j = 4.580328e-005$





f <sup>=</sup> INST FREQ \* sqrt(1.0 <sup>+</sup> WBOTC \* t) / 1000.0

Conductivity =  $(g + hf^2 + if^3 + if^4) / (1 + \delta t + \epsilon p)$  Siemens/meter

t = temperature<sup>[°C</sup>)]; p = pressure[decibars];  $\delta$  = CTcor;  $\varepsilon$  = CPcor;

Residual <sup>=</sup> instrument conductivity - bath conductivity

