Table of Contents

A Equipment	<u>1</u>
A.1 Survey Vessels	
A.1.1 NOAA Ship FERDINAND R. HASSLER	<u>1</u>
<u>A.1.2 FH Launch 2702</u>	<u>5</u>
A.2 Echo Sounding Equipment	
A.2.1 Side Scan Sonars	
A.2.1.1 Klein 5000 V2 Bathymetry	
A.2.2 Multibeam Echosounders	
<u>A.2.2.1 RESON 7125</u>	
<u>A.2.2.2 RESON 7125</u>	
<u>A.2.2.3 R2Sonic 2022</u>	
A.2.3 Single Beam Echosounders	
A.2.4 Phase Measuring Bathymetric Sonars	
A.2.5 Other Echosounders	<u>17</u>
A 2 M	17
A.3 Manual Sounding Equipment	
A.3.1 Diver Depth Gauges	
A.3.2 Lead Lines	
A.3.3 Sounding Poles	
A.3.4 Other Manuar Sounding Equipment	<u>19</u>
A.4 Positioning and Attitude Equipment	19
A.4.1 Applanix POS/MV	
A.4.2 DGPS	
A.4.3 Trimble Backpacks	
A.4.4 Laser Rangefinders	
A.4.5 Other Positioning and Attitude Equipment	
A.5 Sound Speed Equipment	<u>25</u>
A.5.1 Sound Speed Profiles	
A.5.1.1 CTD Profilers	<u>26</u>
A.5.1.1.1 Sea-Bird SeaCat 19plus 350 meter and 3500 meter	<u>26</u>
A.5.1.2 Sound Speed Profilers	
A.5.1.2.1 Rolls-Royce Brooke-Ocean MVP200	<u>28</u>
A.5.2 Surface Sound Speed	<u>30</u>
A.5.2.1 Sea-Bird 45 MicroTSG	<u>30</u>
<u>A.5.2.2 RESON SVP-70</u>	<u>31</u>
A.5.2.3 Valeport miniSVS	<u>31</u>
A.6 Horizontal and Vertical Control Equipment	
A.6.1 Horizontal Control Equipment	
A.6.1.1 Base Station Equipment	<u>32</u>

A.6.1.2 Rover Equipment	<u>33</u>
A.6.2 Vertical Control Equipment	<u>33</u>
A.7 Computer Hardware and Software	
A.7.1 Computer Hardware	
A.7.2 Computer Software	<u>34</u>
A.8 Bottom Sampling Equipment	37
A.8.1 Bottom Samplers	
A.8.1.1 Ponar Wildco 1728	
<u>A.8.1.2 Go Pro Hero 3</u>	<u>39</u>
B Quality Control	<u>39</u>
B.1 Data Acquisition	39
B.1.1 Bathymetry	
B.1.2 Imagery	
B.1.3 Sound Speed	
B.1.4 Horizontal and Vertical Control	
B.1.5 Feature Verification	
B.1.6 Bottom Sampling	
B.1.7 Backscatter	
B.1.8 Other	
B.2 Data Processing	16
B.2.1 Bathymetry	
B.2.2 Imagery	
B.2.3 Sound Speed B.2.4 Horizontal and Vertical Control	
B.2.5 Feature Verification	
B.2.6 Backscatter	
<u>B.2.7 Other</u>	<u>51</u>
B.3 Quality Management	<u>52</u>
B.4 Uncertainty and Error Management	<u>52</u>
B.4.1 Total Propagated Uncertainty (TPU)	<u>52</u>
B.4.2 Deviations	
C Corrections To Echo Soundings	<u>57</u>
C.1 Vessel Offsets and Layback	57
C.1.1 Vessel Offsets	
C.1.2 Layback	
C.2 Static and Dynamic Draft	61
C.2.1 Static Draft	<u></u>

C.3 System Alignment 66 C.4 Positioning and Attitude 69 C.5 Tides and Water Levels 70 C.6 Sound Speed 70 C.6.1 Sound Speed Profiles 70 C.6.2 Surface Sound Speed 71 List of Figures
C.5 Tides and Water Levels 70 C.6 Sound Speed 70 C.6.1 Sound Speed Profiles 70 C.6.2 Surface Sound Speed 71 List of Figures
C.6 Sound Speed 70 C.6.1 Sound Speed Profiles 70 C.6.2 Surface Sound Speed 71 List of Figures
C.6.1 Sound Speed Profiles 70 C.6.2 Surface Sound Speed 71 List of Figures
C.6.2 Surface Sound Speed
List of Figures
T
Figure 1: NOAA Ship FERDINAND R. HASSLER, Starboard View
Figure 2: NOAA Ship FERDINAND R. HASSLER, Bow and Stern View
Figure 3: Launch 2702 profiles
Figure 4: Klien 5000 V2 configured for towing
Figure 5: 7125 Housing flush-mounted on hull
Figure 6: Location of the patch test and reference surface performed in Rhode Island Sound13
Figure 7: A difference surface showing the difference in the Port 400kHz and Stbd 400kHz systems 13
Figure 8: Statistics derived from the difference surface between the Port 400kHz and Stbd 400kHz
<u>systems.</u>
Figure 9: R2Sonic 2022 flush-mounted on hull
Figure 10: Leadline fitted with custom mud-shoe to limit penetration of soft bottoms
Figure 11: TruPulse 360R Laser Rangefinder
Figure 15: Ponar grab sampler.
Figure 16: Camera with custom mount allowing for high quality video of the seafloor
Figure 17: Go Pro video camera
Figure 18: Ship survey systems wiring diagram41
Figure 19: 2702 survey systems wiring diagram.
Figure 20: Example of sound speed samples taken in a survey area44
Figure 21: MBES flow diagram.
Figure 22: S250 dynamic draft derived from ERDDM methods. Positive values are displacements of the
IMU towards the sea floor. Thin lines are results from port and starboard head for third and fourth order
polynomial fits. Black bold line is dynamic draft value used for both hulls
Figure 23: S250 dynamic draft derived from ERDDM methods comparison from years 2011 - 201664
Figure 24: 2702 dynamic draft derived from ERDDM methods. Positive values are displacements of the
IMU towards the sea floor. Thin lines are results from port and starboard head for third and fourth order
polynomial fits

Data Acquisition and Processing Report

NOAA Ship Ferdinand R. Hassler

Chief of Party: LCDR Matthew J. Jaskoski, NOAA

Year: 2016 Version: 1.1

Publish Date: 2017-04-20

A Equipment

A.1 Survey Vessels

A.1.1 NOAA Ship FERDINAND R. HASSLER

Name	NOAA Ship FERDINAND R. HASSLER			
Hull Number	S250			
Description	FERDINAND R. coastal mapping		nall Waterplane Area, Twin-Hull (SWATH)	
Utilization	Survey			
	LOA	37.7 meters		
Dimensions	Beam	18.5 meters		
	Max Draft	3.85 meters		
	Date		2009-11-04	
Most Recent Full Static Survey	Performed By		Raymond C. Impastato, Professional Land Surveyor	
	Discussion		This survey was provided by the shipbuilder, V.T. Halter Marine, and performed in the shippard prior to delivery.	
	Date		2012-06-12	
	Performed By		Kevin Jordan, NGS	
Most Recent Partial Static Survey	Discussion		This survey was performed after the POS/MV antenna mounts were reconfigured to newly fabricated mounts and ties the POS antennae into benchmarks on the 03 deck.	

Most Recent Full Offset Verification	Full offset verification was not performed.			
	Date	2013-04-07		
	Method Used	Optical level run while ship was out of the water in drydock		
Most Recent Partial Offset Verification	Discussion	A level loop was run from the POS antenna to each sensor mounted on the ship's hull. In addition, measurements were made to both IMU base plates through the 7125 cable passage. The resulting offsets from this survey were used to verify and update Z offsets between all sensors.		
	Date	2011-07-12		
Most Recent Static Draft Determination	Method Used	Calculation from design waterline and measured offsets		
	Discussion	Assumed design waterline of 3.8 meters and measured offsets to IMU were used to determine static draft of the reference point. The ship's draft is operationally managed with daily ballast to achieve a true waterline of 3.77 meters. Draft uncertainty is estimated at 0.05 meters. See Section C.2.1.1 for additional discussion.		
	Date	2016-02-21		
	Method Used	Ellipsoid referenced dynamic draft measurement (ERDDM)		
Most Recent Dynamic Draft Determination	Discussion	Data were acquired with canards at zero trim angle. During all survey operations, the canards are set to zero trim angle. Averages are being calculated from all ERDDM tests since the installation of the buoyancy appendages in 2013. This will help filter out errors located in individual tests.		

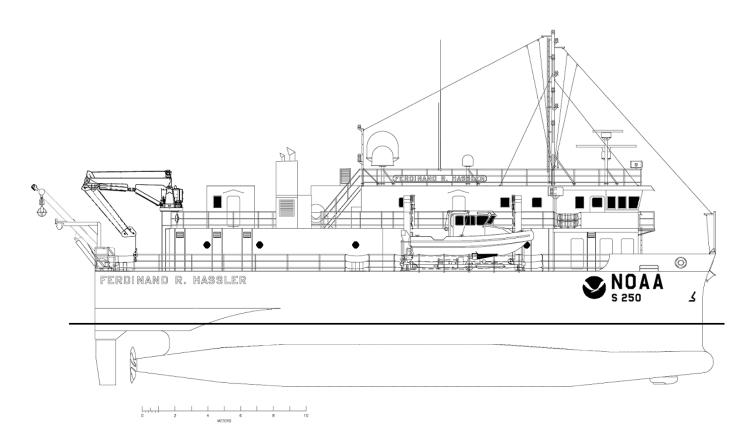


Figure 1: NOAA Ship FERDINAND R. HASSLER, Starboard View

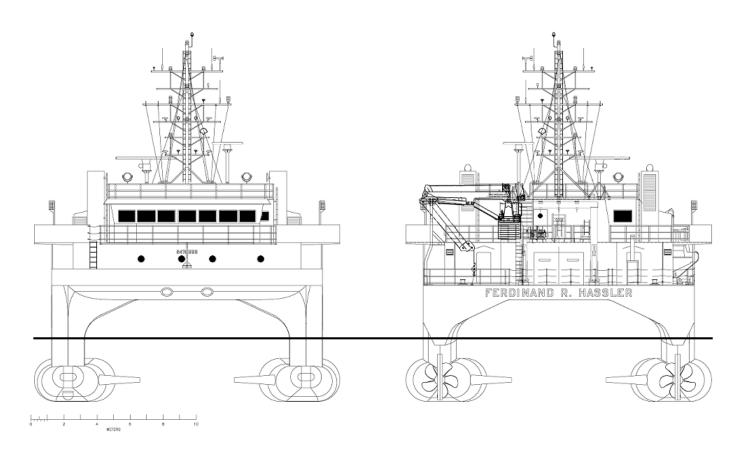
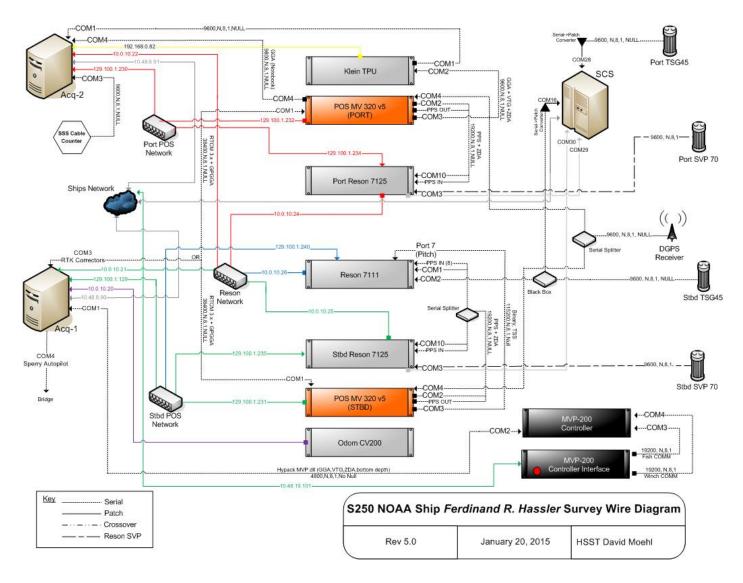


Figure 2: NOAA Ship FERDINAND R. HASSLER, Bow and Stern View



A.1.2 FH Launch 2702

Name	FH Launch 2702			
Hull Number	2702			
Description		25ft enclosed cabin survey launch made by North River, outfitted with jet drive propulsion and Yanmar diesel engine.		
Utilization	Near shore shallo	Near shore shallow water hydrographic survey vessel.		
	LOA	7.62 meters		
Dimensions	3.05 meters			
	0.76 meters			

	Date	2015-06-16	
	Performed By	Kevin Jordan, NGS	
Most Recent Full Static Survey	Discussion	The intention of this survey was to accurately position the POS/MV IMU, GPS Antennas, Sonar Equipment, benchmarks, and reference marks located on the 2702 Launch.	
Most Recent Partial Static Survey	Partial static survey was not performed.		
Most Recent Full Offset Verification	Full offset verification was not performed		
Most Recent Partial Offset Verification	Partial offset verification was not performed.		
	Date	2016-08-14	
	Method Used Bubble level and tape measure		
Most Recent Static Draft Determination	Discussion	The waterline was measured using a bubble level and tape measure to measure the vertical distance from the benchmarks to the waterline. The static draft was calculated using those values.	
	Date	2016-03-03	
Most Recent	Method Used	Ellipsoid referenced dynamic draft measurement (ERDDM)	
Dynamic Draft Determination	Discussion	This was the first dynamic draft measurement performed on Launch 2702. Dynamic draft measurements will be performed on an annual basis and averaged to aid in filtering outliers.	

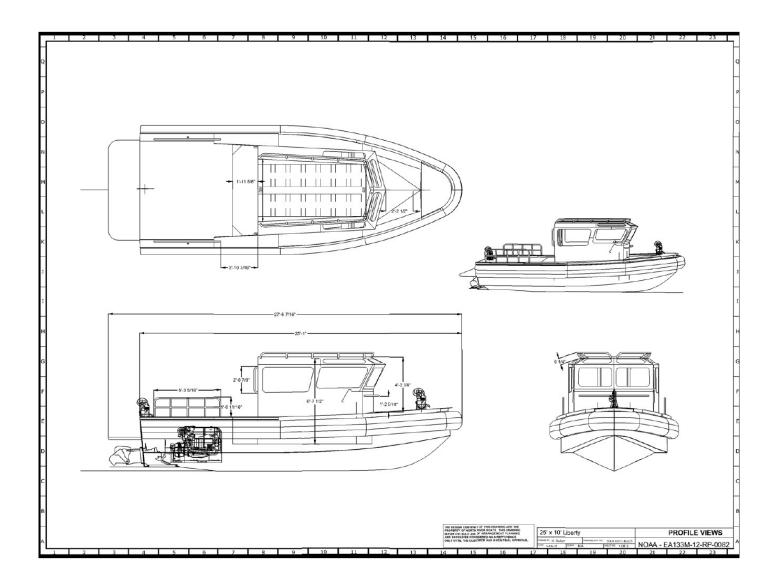
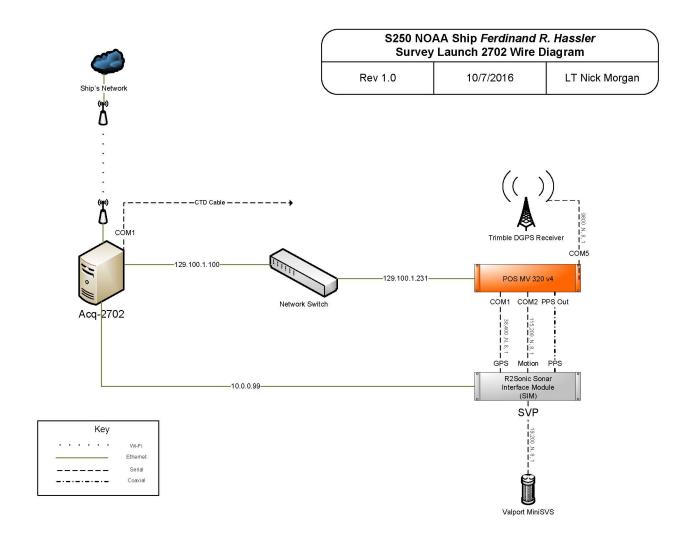


Figure 3: Launch 2702 profiles



A.2 Echo Sounding Equipment

A.2.1 Side Scan Sonars

A.2.1.1 Klein 5000 V2 Bathymetry

Manufacturer	Klein
Model	5000 V2 Bathymetry
Description	High-speed high-resolution towed side-scan sonar (SSS) system. This system is a beamforming acoustic imagery device with an operating frequency of 455 kHz and vertical beam width of 40°. The Klein 5000 V2 system consists of a 5250 V2 towfish and a 5105

V2 Transceiver Processing Unit (TPU). The towfish is towed via 3/8" armored coaxial cable connected to a DT marine electro-hydraulic winch (s/n 1271 302 OEHLW3R) equipped with a Klein slip ring model: (14103033, s/n 1802003). The towfish is fitted with a Klein K-wing depressor wing. The winch is controllable from the sonar operator's station. Cable out is measured with a 3PS cable counter integrated with a General Oceanics model 4042 sheave. The sheave is mounted on the A-frame and is the tow point for offsets measurements. Cable counter accuracy was verified on August 3, 2012 using a known length of line.

The SSS cable was re-terminated on July 27, 2012 and a new 12 meter cable mark for the docked and zero measurement was marked and verified on March 3, 2014.

A side scan calibration was conducted on March 8, 2016(Dn068) on a buoy block offshore of Duck, NC with towfish SN: 386. In this test a number of lines were run adjacent to known buoy block. The side scan positions are compared with the multibeam positions in the attached report. The 95% confidence interval of the positioning error is 10.0 meters. The calculated error in the report is within the positioning error threshold established in the 2014 Field Procedures Manual.

Serial	Vessel Installed On	S250					
Numbers	TPU s/n	777	77				
	Towfish s/n	386	86				
	Frequency	455 kilohertz					
		Resolution	10 centimeters	20 centimeters	36 centimeters	61 centimeters	
Specifications	Along Track Resolution	Min Range	38 meters	75 meters	150 meters	250 meters	
		Max Range	meters	meters	meters	meters	
	Across Track Resolution	3.75 centimeters					
	Max Range Scale	250 meters					
Manufacturer	Vessel Installed On	S250					
Calibrations	Calibration Date	2016-03-08					



Figure 4: Klien 5000 V2 configured for towing

A.2.2 Multibeam Echosounders

A.2.2.1 RESON 7125

Manufacturer	RESON
Model	7125
Description	The RESON 7125 is a dual head, dual frequency system configured to work as a unit. While the particulars of the port system are specified in this section and the starboard head in the following section, this description and following quality control address the two heads as an integrated system.

The port and starboard sonars are mounted in their respective hulls with a 4.5 degree outboard tilt. The sonars can be operated independently, but are typically operated together as a dual-head system using frequency modulated (FM) pulses combined with center frequency separation to enable simultaneous pinging between the heads. When operated as a dual head system, the starboard system acts as the master and the port system the slave. The range scale, ping rate, surface sound speed, and time varied gain (TVG) parameters are controlled by the master.

Patch Tests -

Due to installation of two new receivers during the 2016 April-June drydock period, a new patch test for the Starboard 400kHz and 200kHz modes was conducted on July 9, 2016 (Dn191) in the southern approaches of Rhode Island Sound.

Reference Surfaces -

In conjunction with the new patch test noted above, a reference surface for both Port and Starboard, in both 400kHz and 200kHz modes was conducted on July 11, 2016 (Dn193) in the southern approaches of Rhode Island Sound.

	Vessel Installed On	S250	S250		same	
	Processor s/n	18210412051	18210412051		same	
	Transceiver s/n	212036		same	same	
Serial Numbers	Transducer s/n	n/a		n/a	n/a	
	Receiver s/n	0214074		same		
	Projector 1 s/n	2611093		same		
	Projector 2 s/n	n/a		n/a		
	Frequency	400 kilohertz	400 kilohertz		200 kilohertz	
	Beamwidth	Along Track	1.0 degrees	Along Track	2 degrees	
	Beamwiain	Across Track	0.5 degrees	Across Track	1 degrees	
Specifications	Max Ping Rate	50 hertz	50 hertz		50 hertz	
	Beam Spacing	Beam Spacing Mode	Equidistant	Beam Spacing Mode	Equidistant	
		Number of Beams	512	Number of Beams	512	
	Max Swath Width	140 degrees	140 degrees		140 degrees	
	Depth Resolution	6 millimeters	6 millimeters		6 millimeters	
	Depth Rating	Manufacturer Specified	150 meters	Manufacturer Specified	400 meters	
		Ship Usage	100 meters	Ship Usage	250 meters	

Manufacturer Calibrations

Manufacturer calibration was not performed.

	Vessel Installed On	S250	S250
	Methods	Reference surface comparison	Ellipsoidal Referenced Lead Line and Water Line
System Accuracy Tests	Results	Reference surfaces were performed in the vicinity of Rhode Island Sound on July 9, 2016 (DN191). The 7125 200kHz and 400kHz sonars were operated in single head FM and differenced with the opposite side sonar of the same frequency. The distribution of depth differences, port minus starboard 400kHz for DN191 reference surface. Depths from starboard are on average -0.04 meters deeper than depths from port system with a standard deviation of -0.05 meters.	On March 5, 2014 a static lead line comparison was performed relative to the ellipsoid for the port 7125 system. Ellipsoid height was obtained on a fixed mark ashore using static GPS observations. While the ship was pierside at Judd Gregg Marine Research Complex, a lead-line was lowered to the sea floor in the port 7125 field of view while logging sounding data. Observed ellipsoid height was transferred to the suspended lead-line using differential leveling, and the distance from the lead to the mark measured with a steel survey tape. Logged sonar data was processed through CARIS using standard ERS methods to yield an ellipsoid referenced measurement. Results of this test show the sonar measured depth to be 0.03 meters shallower than the lead-line derived depths with a propagated uncertainty of 0.03 meters. In addition to the ellipsoid measurement, the lead-line was marked at the waterline and the distance from the lead to the mark measured with a steel survey tape. Logged sonar data was processed through CARIS using a zero-tide file to yield a waterline referenced measurement. Sonar depths were an average of 0.04 meters deeper than lead-line derived depths with a propagated error of 0.06 meters. The uncertainty of the measurement is dominated by the uncertainty in reading ship draft marks. This test was repeated for the starboard 7125 system. Results show the sonar depth 0.01 meters deeper than lead-line derived depths with a propagated uncertainty of 0.03 meters. For the waterline; sonar measured depths were an average of 0.15 meters shallower than the lead-line derived depths with a propagated uncertainty of 0.03 meters. For the waterline; sonar measured depths were an average of 0.15 meters shallower than the lead-line derived depths with a propagated uncertainty of 0.03 meters. For the waterline; sonar measured depths were an average of 0.15 meters shallower than the lead-line derived depths with a propagated error of 0.06 meters. There is still uncertainty of the measurement, mainly dominated by the uncer

Snippets	Sonar has snippets logging capability.
----------	--



Figure 5: 7125 Housing flush-mounted on hull.

Figure 6: Location of the patch test and reference surface performed in Rhode Island Sound.

Figure 7: A difference surface showing the difference in the Port 400kHz and Stbd 400kHz systems.

Figure 8: Statistics derived from the difference surface between the Port 400kHz and Stbd 400kHz systems.

A.2.2.2 RESON 7125

Manufacturer	RESON
Model	7125
Description	Starboard system of a dual head configuration. For a description of this system and associated quality control tests, see entry for port 7125.

	Vessel Installed On	S250		same				
	Processor s/n	18215011048		same				
	Transceiver s/n	212035		same				
Serial Numbers	Transducer s/n	n/a		n/a				
	Receiver s/n	1215068		same				
	Projector 1 s/n	1111236		same				
	Projector 2 s/n	n/a		n/a				
	Frequency	400 kilohertz		200 kilohertz				
	D : 1.1	Along Track	0.5 degrees	Along Track	2 degrees			
	Beamwidth	Across Track	1 degrees	Across Track	1 degrees			
	Max Ping Rate	50 hertz	50 hertz					
	Beam Spacing	Beam Spacing Mode	Equidistant	Beam Spacing Mode	Equidistant			
Specifications		Number of Beams	512	Number of Beams	512			
	Max Swath Width	140 degrees		140 degrees				
	Depth Resolution	6 millimeters		6 millimeters				
	Depth Rating	Manufacturer Specified	150 meters	Manufacturer Specified	400 meters			
		Ship Usage	100 meters	Ship Usage	250 meters			
Manufacturer Calibrations	Manufacturer calibr	Manufacturer calibration was not performed.						
System Accuracy Tests	System accuracy test was not performed.							
Snippets	Sonar has snippets logging capability.							

A.2.2.3 R2Sonic 2022

Manufacturer	R2Sonic
Model	2022
Description	The Sonic MBES works on a user selectable frequency range of 200 kHz to 400 kHz so it is adaptable to a wide range of survey depths and conditions. The user can adjust the operating frequency, via the Sonic Control GUI, on the fly, without having to shut down the sonar system or change hardware or halt recording data. The Sonic MBES have a user selectable sector angle, from 10° to 160°, using all 256 beams; the desired sector angle can be selected on the fly without a halt to data recording.

	The selected swath direct the highly co	_	-		st recording, to		
	Vessel Installed On	2702					
	Processor s/n	103297					
	Transceiver s/n	N/A					
Serial Numbers	Transducer s/n	800148					
	Receiver s/n	N/A					
	Projector 1 s/n	N/A					
	Projector 2 s/n	N/A					
	Frequency	200 kilohertz		400 hertz			
	D	Along Track	1.0 degrees	Along Track	2.0 degrees		
	Beamwidth	Across Track	1.0 degrees	Across Track	2.0 degrees		
	Max Ping Rate	60 hertz		60 hertz	·		
	Dogue Cogoino	Beam Spacing Mode	Equidistant	Beam Spacing Mode	Equidistant		
Specifications	Beam Spacing	Number of Beams	256	Number of Beams	256		
	Max Swath Width	160 degrees		160 degrees			
	Depth Resolution	12.5 millimeters		12.5 millimeters	3		
	Depth Rating	Manufacturer Specified	100 meters	Manufacturer Specified	100 meters		
		Ship Usage	100 meters	Ship Usage	100 meters		
Manufacturer	Vessel Installed On	2702					
Calibrations	Calibration Date	2015-11-16					
	Vessel Installed On	2702					
	Methods	Reference Surfa	ce				
System Accuracy Tests	Results	Reference surfaces were performed in the vicinity of Cape Henry VA in Anchorage B on March 17, 2016 (DN077). The 7125 400kHz sonars were operated in dual head FM mode and compared to Launch 2702's R2Sonic. Results are shown in the text and images below. The distribution of depth differences (Launch 2702's R2Sonic 2022 minus S250's Dual Reson 7125's): Depths from the R2sonic are on average 0.055 meters shallower than depths from the Dual Reson 7125 system with a standard deviation of 0.037 meters.					
Snippets	Sonar has snippets l	ogging capabilit	у.				



Figure 9: R2Sonic 2022 flush-mounted on hull.

A.2.3 Single Beam Echosounders

No single beam echosounders were utilized for data acquisition.

A.2.4 Phase Measuring Bathymetric Sonars

No phase measuring bathymetric sonars were utilized for data acquisition.

A.2.5 Other Echosounders

No additional echosounders were utilized for data acquisition.

Additional Discussion

A.3 Manual Sounding Equipment

A.3.1 Diver Depth Gauges

Manufacturer	In-Situ Inc.	In-Situ Inc.				
Model	Rugged TROLL 1	Rugged TROLL 100 / Rugged BaroTROLL				
Description	records changes in with an accompan objects can be obt and record barome level due to baron	The Rugged TROLL 100 is a non-vented (absolute) data logger that measures and records changes in water level, pressure, and temperature. When post-processed with an accompanying CTD cast and tide value, accurate least depths on submerged objects can be obtained. The Rugged BaroTROLL is a data logger used to measure and record barometric pressure, which is used to compensate for changes in water level due to barometric fluctuations. Typically the BaroTROLL is not used for dive operations but may prove to be beneficial for least depth investigations in the future.				
Serial Numbers	349000 - Rugged TRO	349000 - Rugged TROLL 100				
	349047 - Rugged Bar	349047 - Rugged BaroTROLL				
Calibrations	No calibrations we	ere performed.				
	Serial Number	349000				
	Date	2014-04-15				
Accuracy Checks	Procedures	Sounding System Comparison - The DLDG was taped to the leadline while recording and submerged to the seafloor for a measurement. A cast was taken during the comparison and the data gathered were processed using Velocipy. The DLDG results were 0.13 meters deeper than the leadline measurement, 0.13 and 0.23 meters shallower than the port and starboard 7125 values, respectively.				
Correctors	Correctors were no	Correctors were not determined.				
Non-Standard Procedures	Non-standard proc	Non-standard procedures were not utilized.				

A.3.2 Lead Lines

Manufacturer	Unknown					
Model	Traditional	Traditional				
Description		FERDINAND R. HASSLER is equipped with one lead line. Lead lines are used for measurements near shore over submerged shoals and for echosounder depth comparisons.				
Serial Numbers	RA6S					
Calibrations	No calibrations were p	performed.				
	Serial Number	RA6S				
	Date	2016-03-13				
Accuracy Checks	Procedures The wet lead line was stretched with an amount of force equal to the weight, on relatively flat ground and compared with a steel survey tape. Values were recorded of true measurements at lead line markings.					
Correctors	From the table of values obtained during the accuracy checks a table of correctors was calculated. This table is stored locally aboard the FERDINAND R. HASSLER and referenced when appropriate.					
Non-Standard Procedures	Non-standard procedu	ares were not utilized.				



Figure 10: Leadline fitted with custom mud-shoe to limit penetration of soft bottoms.

A.3.3 Sounding Poles

No sounding poles were utilized for data acquisition.

A.3.4 Other Manual Sounding Equipment

No additional manual sounding equipment was utilized for data acquisition.

A.4 Positioning and Attitude Equipment

A.4.1 Applanix POS/MV

Manufacturer	Applanix						
Model	POS/MV 320 V5	POS/MV 320 V5					
Description	Tightly coupled GPS and inertial positioning and attitude sensing system for port hull. Inertial motion unit (IMU) is located below water line close to the port side 7125 wet end. GPS antennae are located on flying bridge of S250. The V5 system was installed on July 29, 2013.						
	Manufacturer	Applanix					
	Model	POS/MV 320 V5					
	Description	Rack mounted PO	OS control system l	ocated in charting	lab.		
PCS	Firmware Version	8.15					
	Software Version	8.15					
	Serial Numbers	Vessel Installed On	S250 Port				
		PCS s/n	5806				
	Manufacturer	Applanix					
	Model	Type 36					
	Description	Inertial measurement system consisting of three orthogonal accelerometers and three orthogonal fiber-optic gyroscopes. Located in port hull near 7125 wet end.					
<i>IMU</i>	Serial Numbers	Vessel Installed On S250 Port hull					
		IMU s/n 2423					
		IMU s/n 2423					
	Certification			2013-06-26			
	Manufacturer	Trimble					
	Model	GA830 GNSS/M	SS				
Antennas	Description	GNSS/MSS antennae are used for position input as well as aiding the heading solution. The antennae pair for the port system is the forward a aft pair on the port side. The separation distance between the antennae is approximately 2 meters. These new Trimble GA830 antennas were installed on September 30th, 2015.					
	G	Vessel Installed On	Antenna s/n	Port or Starboard	Primary or Secondary		
	Serial Numbers	S250 Port (forward)	6997	Port	Primary		

		Vessel Installed On	Antenna s/n	Port or Starboard	Primary or Secondary		
		S250 Port (aft)	5401	Port	Secondary		
	Vessel	S250					
GAMS Calibration	Calibration Date	2016-02-11					
Configuration Reports	POS/MV configura	tion reports were r	not produced.				
Manufacturer	Applanix						
Model	POS/MV 320 V5						
Description	starboard hull. Ine starboard side 7125	pled GPS and inertial positioning and attitude sensing system for ull. Inertial motion unit (IMU) is located below water line close to the ide 7125 wet end. GPS antennae are located on flying bridge of S250. Item was installed on July 29, 2013.					
	Manufacturer	Applanix					
	Model	POS/MV 320 V5					
	Description	Rack mounted POS control system located in charting lab.					
	Firmware Version	8.15					
PCS	Software Version	8.15					
	Serial Numbers	Vessel Installed On S250 Starboard					
		PCS s/n	PCS s/n 5807				
	Manufacturer	Applanix					
	Model	Type 36					
	Description	Inertial measurem	d three orthogon	•	nogonal oscopes. Located in		
<i>IMU</i>	Serial Numbers	Vessel Installed On	S250 Starboard	hull S250 top h	Starboard hull new		
		IMU s/n	2424	2672			

Certification Date

2424

2013-06-26

IMU s/n

Trimble

Certification

Manufacturer

Antennas

	Model	GA830 GNSS/MSS GNSS/MSS antennae are used for position input as well as aiding the heading solution. The antennae pair for the port system is the forward and aft pair on the port side. The separation distance between the antennae is approximately 2 meters. These new Trimble GA830 antennas were installed on, September 30th, 2015.				
	Description					
		Vessel Installed On	Antenna s/n	Port or Starboard	Primary or Secondary	
		S250 Starboard (forward)	7000	Starboard	Primary	
		S250 Starboard (aft)	5415	Starboard	Secondary	
GAMS Calibration	Vessel	S250				
Omis Calibration	Calibration Date	2016-02-11				
Configuration Reports	POS/MV configuration reports were not produced.					

Manufacturer	Applanix	Applanix					
Model	POS MV 320 v4	POS MV 320 v4					
Description	2702. Inertial moti	Tightly coupled GPS and inertial positioning and attitude sensing system for launch 2702. Inertial motion unit (IMU) is located underneath the false floor in the bilge compartment next to the coxswain station. GPS antennae are located on cabin-top of 2702.					
	Manufacturer	Applanix					
	Model	MV 320 v4	MV 320 v4				
	Description	The POS Computer System (PCS) comprises the processor, GPS receiver and interface cards necessary to communicate with and process the IMU and GPS data. Rack mounted system located in the survey rack underneath the survey station counter in launch 2702.					
PCS	Firmware Version	5.03					
	Software Version	5.8					
	Serial Numbers	Vessel Installed On	2702				
		PCS s/n	3189				

	Manufacturer	Applanix					
	Model	Type 2					
	Description						
 IMU	Serial Numbers	Vessel Installed On					
		IMU s/n	803				
	Certification	IMU certificati	on report was	not produced.			
	Manufacturer	Trimble					
	Model	382AP GNSS	382AP GNSS				
	Description	GNSS antennae are used for position input as well as aiding the heading solution. The antennae pair for the POS MV are located forward and aft on the starboard side. The separation distance between the antennae is approximately 2 meters.					
Antennas	Serial Numbers	Vessel Installed On	Antenna s/n	Port or Starboard	Primary or Secondary		
		2702 Starboard (aft)	60243869	Starboard	Primary		
		2702 Port (fwd)	60243047	Port	Secondary		
GAMS Calibration	Vessel	2702					
Ginib Cantitation	Calibration Date	2016-03-03					
Configuration Reports	POS/MV configura	ntion reports were not produced.					

A.4.2 DGPS

Description	Hemisphere PGS	Hemisphere PGS MBX Kit		
	Manufacturer	Hemisphere		
	Model	MBX-4		
Antennas	Description			
	Serial Numbers	Vessel Installed On	S250	
		Antenna s/n	1113139440044	

	Manufacturer	Hemisphere		
	Model	MBX-4		
	Description			
Receivers	Firmware Version	1.0		
	Serial Numbers	Vessel Installed On	S250	
	Seriai Numbers	Antenna s/n	1118144550001	
Description	Trimble DGPS Kit			
1	Manufacturer	Trimble		
	Model	SPS361		
Antennas	Description			
Antennas	Serial Numbers	Vessel Installed On	2702	
		Antenna s/n	8838	
	Manufacturer	Trimble		
	Model	SPS361		
	Description	Auxillary DGPS Receiver		
Receivers	Firmware Version	N/A		
	C · IN I	Vessel Installed On	2702	
	Serial Numbers	Antenna s/n	5449R80011	

A.4.3 Trimble Backpacks

Trimble backpack equipment was not utilized for data acquisition.

A.4.4 Laser Rangefinders

Manufacturer	Laser Technology Inc	
Model	TruPulse 360R	
Description	Rugged and waterproof laser rangefinder which provides full measurement capabilities of distances, heights and azimuths.	
Serial Numbers 2557		
DQA Tests DQA test was not performed.		



Figure 11: TruPulse 360R Laser Rangefinder

A.4.5 Other Positioning and Attitude Equipment

No additional positioning and attitude equipment was utilized for data acquisition.

A.5 Sound Speed Equipment

A.5.1 Sound Speed Profiles

A.5.1.1 CTD Profilers

A.5.1.1.1 Sea-Bird SeaCat 19plus 350 meter and 3500 meter

Sea-Bird			
SeaCat 19plus 350 meter and 3500 meter			
Internal logging conductivity, temperature, and depth measuring devices.			
Vessel Installed On CTD s/n	S250 19P65591-6918	S250 19P32914-4480	S250 19P36399-4642
CTD s/n Date Procedures	6918 2016-01-22 Routine calibration	4480 2016-01-22 Routine calibration	4642 2016-01-22 Routine calibration service
	SeaCat 19plus 350 n Internal logging cor Vessel Installed On CTD s/n CTD s/n Date	SeaCat 19plus 350 meter and 3500 meter Internal logging conductivity, temperature Vessel Installed On S250 CTD s/n 19P65591-6918 CTD s/n 6918 Date 2016-01-22 Routine calibration	SeaCat 19plus 350 meter and 3500 meter Internal logging conductivity, temperature, and depth measuring Vessel Installed On \$250 \$250 CTD s/n 19P65591-6918 19P32914-4480 CTD s/n 6918 4480 Date 2016-01-22 2016-01-22 Procedures Routine calibration Routine calibration



Figure 12: Ferdinand R. Hassler CTD inventory

A.5.1.2 Sound Speed Profilers

A.5.1.2.1 Rolls-Royce Brooke-Ocean MVP200

Manufacturer	Rolls-Royce Brooke-Ocean		
Model	MVP200		
Description	The cable was outfitted on August 18, 2014. Towfish with AML Micro-CTD sensor SN-8609 was lost at sea on September 10, 2016 after the cable parted while the towfish was in the docked position. The ship did not have a known spare on hand and performed manual CTDs for the remainder of the year.		
Serial Numbers	Vessel Installed On Sound Speed Profiler s/n	S250 8609	S250 8615
Calibrations	Sound Speed Profiler s/n Date Procedures	8609 2016-01-14 Routine calibration service	8615 2013-08-10 Certificate of Conformity

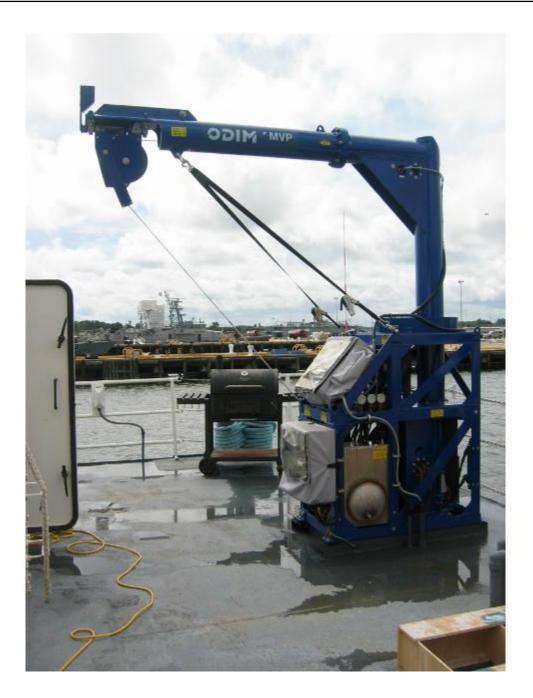


Figure 13: MVP control station & winch



Figure 14: MVP single sensor free fall fish.

A.5.2 Surface Sound Speed

A.5.2.1 Sea-Bird 45 MicroTSG

Manufacturer

Model	45 MicroTSG		
Description	Two SBE-45 thermosalinographs are installed to determine the sound velocity of the water at the sonar transducers. This data is used to aid beam steering of the multibeam 7111 sonar system, and as a backup sound speed input available for beam steering of the multibeam 7125 sonar systems. One is located in the starboard engine room, the other in the port. Both units draw sampling water from the main cooling water line of the respective main engine. The SBE-45s are configured to use their internal temperature sensors. Both units are insulated with foam to ensure accurate temperature readings. These devices calculate the sound speed from the measured salinity and temperature (using the Chen-Millero equation) of the sampled water. A serial broadcast device sends the sound speed message from the SBE-45 to the RESON 7111 and SCS acquisition server.		
Serial Numbers	Vessel Installed On	S250 Port	S250 Starboard
Seriai Ivanibers	Sound Speed Sensor s/n	4553332-0276	4553332-0277
	Sound Speed Sensor s/n	4553332-0276	4553332-0277
Calibrations	Date	2015-04-02	2015-04-02
	Procedures	Routine calibration service	Routine calibration service

A.5.2.2 RESON SVP-70

Manufacturer	RESON		
Model	SVP-70		
Description	Sound velocity probe developed for fixed-mount installation near RESON 7125 transducer heads which uses a direct path echosounding technique that instantly compensates for temperature and pressure with internal sensors, providing accurate surface sound velocity measurements for beam steering. During the April-June 2016 drydock period, the port SVP-70 (S/N 2011276) was reinstalled. In August of 2016, the starboard SVP-70 sensor (S/N 2011278) began malfunctioning. The port SVP-70 was then fed to the starboard RESON 7125. The STBD SVP-70 was removed from the hull in December 2016 and sent to the manufacturer for repair.		
Serial Numbers	Vessel Installed On	S250 Starboard hull	S250 Port hull
Serial Numbers	Sound Speed Sensor s/n	2011278	2011276
	Sound Speed Sensor s/n	2011278	2011276
Calibrations	Date	2014-03-12	2015-03-24
	Procedures	Routine calibration service	Routine calibration service

A.5.2.3 Valeport miniSVS

Manufacturer	Valeport	
Model	miniSVS	
Description	The miniSVS consists of a single circuit board controlling all sampling, processing and communications functions, and a sensor comprising a ceramic transducer, a signal reflector, and spacer rods to control the path length. The two are connected by a single coaxial cable. A titanium housing may be fitted, which provides waterproof protection to a depth in excess of 6000m.	
Serial Numbers	Vessel Installed On	2702
Seriai Ivambers	Sound Speed Sensor s/n	48002
	Sound Speed Sensor s/n	48002
Calibrations	Date	2016-01-21
	Procedures	Routine calibration service

Additional Discussion

When in the deployed and docked position, the MVP sensor is towed at approximately the same height as the surface sound speed sensor. As part of the system start up and watch turnover procedures as well as periodically through a survey watch, these values are verified to be in agreement. Comparison casts between a SeaCat 19+ and the MVP are conducted once a project or if any issues with the MVP sensor are suspected. The results of these tests are included in the Separates section of each survey.

A.6 Horizontal and Vertical Control Equipment

A.6.1 Horizontal Control Equipment

A.6.1.1 Base Station Equipment

Descript	ion	Trimble NetR5 receiver used for long-term GPS base observations and correctors.
----------	-----	---

	Manufacturer	Trimble	
	Model	Zephyr Geodetic Model 2	
GPS Antennas	Description	The Zephyr Geodetic 2 is the antenna component for the NetR5 system which incorporates a large Trimble Stealth TM Ground Plane, which reduces multipath interference using technology similar to that used by Stealth aircraft to hide from radar. The antenna is made with weather-resistant materials and a low profile design, so the antenna can be used for many years of continuous operation on a permanent installation.	
	Serial Numbers	1440921338	
		m	
	Manufacturer	Trimble	
	Model	NetR5 GNSS	
GPS Receivers	Description	The Trimble NetR5 Reference Station is a multi-channel, multi-frequency GNSS receiver designed for use as a stand-alone reference station or as part of a GNSS infrastructure solution.	
	Firmware Version	4.03	
	Serial Numbers	4934K63376	
UHF Antennas	No UHF antennas were installed.		
UHF Radios	No UHF antennas were installed.		
Solar Panels	No solar panels were installed.		
Solar Chargers	No solar chargers were installed.		
DQA Tests	No DQA tests were performed.		

A.6.1.2 Rover Equipment

No rover equipment was utilized for data acquisition.

A.6.2 Vertical Control Equipment

No vertical control equipment was utilized for data acquisition.

A.7 Computer Hardware and Software

A.7.1 Computer Hardware

Manufacturer	Dell		
Model	T5500		
Description	Processing Computers		
	Computer s/n	Operating System	Use
Serial Numbers	FH-PROC1 Service Tag # GFTQ8V1	Windows 7	Processing
	FH-PROC2 Service Tag # GFTR8V1	Windows 7	Processing
	FH-PROC3 Service Tag # GFTN8V1	Windows 7	Processing
	FH-PROC4 Service Tag # GFTM8V1	Windows 7	Processing

Manufacturer	Dell			
Model	Precision Tower 7810	Precision Tower 7810		
Description	Acquisition Computers	Acquisition Computers		
Serial Numbers	Computer s/n	Operating System	Use	
	FH-ACQ3 Service Tag # 84WYV52	Windows 7	Acquisition	
	FH-ACQ4 Service Tag # 84WXV52	Windows 7	Acquisition	

Manufacturer	Cybertron PC		
Model	Generic		
Description	Processing Computer		
Serial Numbers	Computer s/n	Operating System	Use
	FH-PROC5 Service Tag # FQC-00765	Windows 7	Processing

A.7.2 Computer Software

Manufacturer	CARIS
Software Name	HIPS/SIPS
Version	9.1

Service Pack	N/A
Hotfix	24
Installation Date	2016-05-01
Use	Processing
Description	Data Processing (FH used Caris 9.0.21 for initial processing. Surveys from project OPR-D304-FH-16 were transferred to the TJ for final processing and reporting where 9.1.4 was used)

Manufacturer	CARIS
Software Name	Bathy BASE Editor
Version	4.1
Service Pack	N/A
Hotfix	21
Installation Date	2016-05-01
Use	Processing
Description	Data analysis and feature management

Manufacturer	CARIS
Software Name	Plot Composer
Version	5.3
Service Pack	N/A
Hotfix	N/A
Installation Date	2015-02-18
Use	Processing
Description	Mapping and plotting software

Manufacturer	Applanix
Software Name	POSPac
Version	7.2
Service Pack	N/A
Hotfix	N/A
Installation Date	2016-06-01
Use	Processing
Description	Position and Attitude processing software

Manufacturer	NOAA
"	

Software Name	Pydro
Version	16
Service Pack	N/A
Hotfix	N/A
Installation Date	2016-05-01
Use	Processing
Description	Feature management, correlation, and report generator. Pydro automatically updates throughout the project.

Manufacturer	NOAA
Software Name	Velocipy
Version	16
Service Pack	N/A
Hotfix	N/A
Installation Date	2015-02-16
Use	Processing
Description	Feature management, correlation, and report generator, software update installed for bug fixes and schema changes. Velocipy automatically updates with Pydro throughout the project.

Manufacturer	IVS 3D
Software Name	Fledermaus
Version	7
Service Pack	5
Hotfix	3
Installation Date	2016-04-01
Use	Processing
Description	Data modeling

Manufacturer	Hypack
Software Name	Hypack/Hysweep
Version	2014
Service Pack	0
Hotfix	16
Installation Date	2014-02-18
Use	Acquisition

Description	Data logging			
Manufacturer	Applanix			
Software Name	POSView			
Version	8.46			
Service Pack	N/A			
Hotfix	N/A			
Installation Date	2015-12-14			
Use	Acquisition			
Description	Positioning			
Manufacturer	Synergy			
Software Name	Synergy			
Version	1.4.14			
Service Pack	N/A			
Hotfix	N/A			
Installation Date	2014-02-17			
Use	Acquisition			
Description	Shared mouse and keyboard between acquisition systems			

A.8 Bottom Sampling Equipment

A.8.1 Bottom Samplers

A.8.1.1 Ponar Wildco 1728

Manufacturer	onar Wildco			
Model	1728			
Description	Grab sampler triggered by contact with sea floor. A custom mount equipped with camera and light was designed for the acquisition of video of the seafloor.			



Figure 15: Ponar grab sampler

Figure 16: Camera with custom mount allowing for high quality video of the seafloor

A.8.1.2 Go Pro Hero 3

Manufacturer	Go Pro
Model	Hero 3
Description	Video camera rigged as a drop camera to function along with grab sampler. The camera contains a 12 MP sensor capable of 1440p at 48fps. This camera supplements the data gathered with the grab sampler, and allows the field unit to provide data from null samples from the sediment sampler.



Figure 17: Go Pro video camera.

B Quality Control

B.1 Data Acquisition

B.1.1 Bathymetry

B.1.1.1 Multibeam Echosounder

Multibeam data on S250 are logged locally on the RESON topside machines in s7k format. Multibeam data are also acquired through Hypack/Hysweep in HSX format for bathymetry, though these files are only used in the event of errors in the s7k file and are otherwise discarded. The HSX format includes sounding solutions, navigation and attitude data. Ship navigation and survey line monitoring are performed with Hypack/Hysweep. The s7k format includes sounding solutions, navigation, attitude, and backscatter snippet data. This record is configured to include the following RESON datagrams: 1003: Position; 1012: Roll, Pitch, Heave; 1013: Heading; 7000: 7k Sonar Settings; 7004: 7k Beam Geometry; 7006: 7k Bathymetric Data; 7008: Bathymetry (For UI Display Only); 7017: Bathymetry (RAW for hydrography); 7027: 7k Generic Watercolumn Data (used for snippets backscatter) and 7503: Remote Control Sonar Settings.

All multibeam sonars are configured in equidistant ("Best Coverage" in newest RESON version) beam steering mode. The opening angle of the 7125 systems is configured based on analysis of coverage, speed, and expected sound speed refraction errors for each survey. This angle typically varies between 120 and 140 degrees. Power, gain, and TVG parameters are typically set for a particular project and changes during acquisition are minimal.

The RESON units are interfaced with the acquisition machines through UDP LAN connections over a dedicated network switch (NetGear ProSafe Gigabit Switch). Position and attitude data is passed from the POS-MV to both the RESON machines and to the acquisition computers through dedicated network switches (NetGear ProSafe Gigabit Switch). There is a dedicated switch for the port and starboard POS systems. Time is passed from the POS to the RESON machines via an RS232 serial connection and a PPS pulse via a coaxial cable with BNC connectors. The starboard POS is interfaced with the starboard 7125 and the 7111, which is located in the starboard hull. The port POS is interfaced to the port 7125. A diagram of this configuration is included with the support files to this report and illustrated in Figure 20.

Data acquired on Launch 2702 is processed by the Sonar Interface Module and delivered to the acquisition machine through a direct ethernet connection and logged using Hypack 2015 in the .HSX and R2Sonic .R2S formats. A swath angle of 120 degrees with the sector rotated 20 degrees to counteract the mounting angle on the hull is used as standard procedure. Bottom sampling is set to equidistant quad which distributes soundings evenly in the x and y directions. Roll stabilization is used and frequency can be adjusted on the fly from 200-400kHz. The sonar has the ability to log TruePix (similar to sidescan with 3D relief), Snippets, and Water Column data.

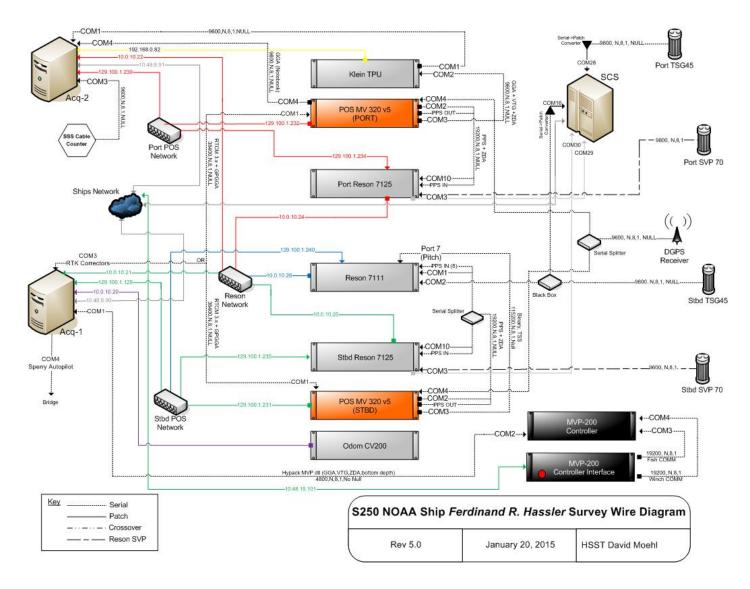


Figure 18: Ship survey systems wiring diagram

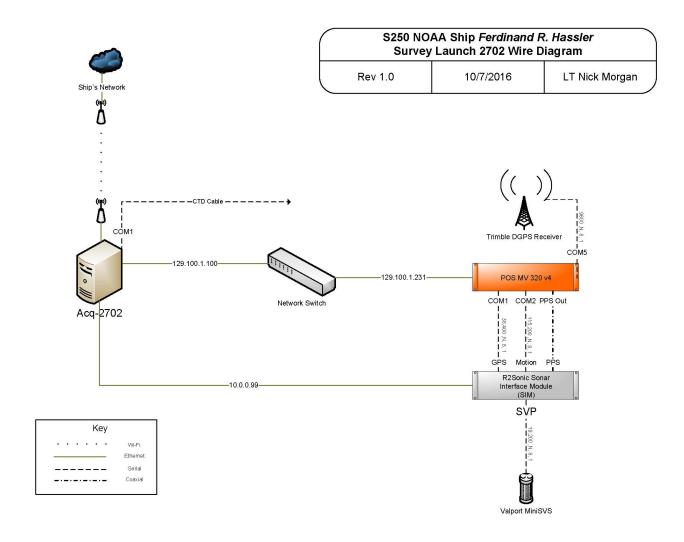


Figure 19: 2702 survey systems wiring diagram

B.1.1.2 Single Beam Echosounder

Single beam echosounder bathymetry was not acquired.

B.1.1.3 Phase Measuring Bathymetric Sonar

Phase measuring bathymetric sonar bathymetry was not acquired.

B.1.2 Imagery

B.1.2.1 Side Scan Sonar

Side scan sonar imagery was not acquired.

B.1.2.2 Phase Measuring Bathymetric Sonar

Phase measuring bathymetric sonar imagery was not acquired.

B.1.3 Sound Speed

B.1.3.1 Sound Speed Profiles

Seabird SBE 19plus and MVP sound speed profilers are used regularly to collect sound speed data for ray tracing corrections for the multibeam sonar systems. The MVP is the primary method of sound speed profiling unless fishing gear or other potential dangers are deemed high enough risk that the MVP could be lost. To mitigate the risk of loss "running" casts are performed, where the ship recovers the MVP immediately upon a successful cast. If it is deemed that a "running" cast is too high risk a "static" cast will be performed, where the ship will stop all way and manually winch out to the desired depth before recovering the towfish. CTD casts are performed if there is not an MVP qualified operator available on watch. Data is retrieved from the Seabird CTDs with a serial connection to a processing computer. Data from both the Seabirds and MVP are processed through the NOAA in-house program Velocipy to give CARIS .svp formatted sound velocity profiles. All .svp profiles for a survey sheet are concatenated to one master file for a survey.

Casts are taken at least every four hours, but typically far more frequently. The interval between casts is typically between ten minutes and four hours based on the observed variability between casts and is discussed in the Descriptive Report of each survey.

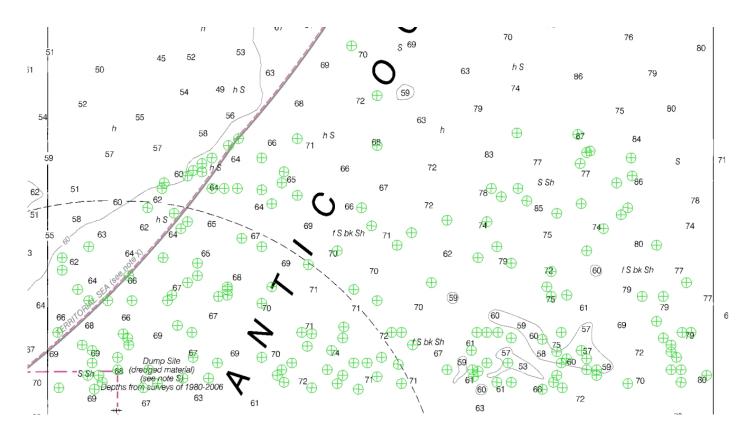


Figure 20: Example of sound speed samples taken in a survey area

B.1.3.2 Surface Sound Speed

Surface sound speed for both RESON 7125 systems is fed from individual SVP-70 sound velocity sensors mounted near each transducer. While operating in dual-head mode the starboard SVP-70 feeds both the master and slave. Seabird TSG 45 thermosalinograph measures sea surface conductivity and temperature and then calculates surface sound speed for the RESON 7111. Surface sound speed is typically compared daily between the real time MVP output and the starboard SVP-70 sensor by the acquisition watch. Data from all surface sound speed sensors can be fed into SCS for real time comparison and are recorded during MVP or CTD casts to perform surface sound speed DQAs.

The R2Sonic 2022 uses a surface sound speed input from the Valeport miniSV that is mounted in the sonar void along with the sonar receiver and transmitter. During regular launch operations, periodic DQAs with the CTDs along with visual comparisons cast to cast by the acquisition operator.

B.1.4 Horizontal and Vertical Control

B.1.4.1 Horizontal Control

Applanix POS/MV files are logged using both the USB logging function and Ethernet logging function. Both files contain the same data records including attitude, heading, position, and velocity data as stated in section 3.4.1 of the FPM. During acquisition, the navigation solution status is constantly monitored by the acquisition watch stander.

The internal (USB) logged files are size limited, therefore files submitted typically start with the .000 extension and increment upwards (e.g. .001, .002, .003, ...). There are approximately 240 files generated during 24 hours of acquisition. The Ethernet logged files are typically broken at approximately UTC noon and midnight each day to yield two files per hull for a survey day.

Real-time USCG DGPS correctors are used for all acquisition. Specific DGPS stations are noted in the DR accompanying each survey.

B.1.4.2 Vertical Control

Preliminary, observed, and verified water levels are downloaded using FetchTides and applied to the data using CARIS HIPS Load Tide function. For data submission, depth data are reduced to MLLW either through application of Verified Water levels and Verified Tidal Zoning or using GPS derived vertical positions and the VDatum model. Refer to individual sheet DRs for detailed methods and additional information.

B.1.5 Feature Verification

Feature verification data were not acquired.

B.1.6 Bottom Sampling

Bottom Sampling followed guidelines set forth in sections 7.1 of the HSSD and 2.5.4.2.1 of the FPM. Unless specified otherwise in the DR, bottom sample locations are guided by analysis of the backscatter and bathymetry of the survey area. Refer to individual sheet DR for additional information.

B.1.7 Backscatter

Backscatter is acquired in the 7008 record logged in the .s7k files directly from the RESON 7125 processors. For the 7125 400kHz systems, snippet size is set to 25 samples in water depths less than 50 meters and to 50 samples in depth greater than 50 meters. The 7125 200kHz system has snippets size set to 100 in depths less than 100 meters and 200 in all depths greater than 100 meters. 7111 snippet size is set to 40 samples in depths less than 80 meters, 80 samples in depths between 150 and 300 meters, and 120 samples in deeper depths. All processing of backscatter is done using the FMGT module of the QPS Fledermaus package.

B.1.8 Other

No additional data were acquired.

Additional Discussion

FERDINAND R. HASSLER maintains a continuous manned survey watch during all survey acquisition. The watch stander is in constant communication with the bridge and monitors the performance of all systems. Thresholds set in Hypack/Hysweep, POSview, RESON, and SonarPro alert the watch stander by displaying alarm messages when error thresholds or tolerances are exceeded. Alarm conditions that may compromise survey data quality are corrected and then noted in acquisition log. Warning messages such as the temporary loss of differential GPS, excessive cross track error, or vessel speed approaching the maximum allowable survey speed are addressed by the watch stander and corrected before further data acquisition occurs.

B.2 Data Processing

B.2.1 Bathymetry

B.2.1.1 Multibeam Echosounder

Bathymetry processing followed section 4.2 of the FPM unless otherwise noted.

Raw .s7k (Reson 7125s) and .HSX/.R2S (R2Sonic 2022) multibeam data were converted to CARIS HIPS HDCS format using established and internally documented settings. After TrueHeave, sound speed, water level correctors, and SBETS are applied to all lines, GPS Tides are calculated using the HSD Operations Branch provided VDatum separation model and the lines are merged. Once lines are merged, Total Propagated Uncertainty (TPU) is computed using settings documented for each survey in the Descriptive Report. Default CARIS device models (devicemodels.xml) are used during processing.

The general resolution, depth ranges, and Combined Uncertainty and Bathymetric Estimator (CUBE) parameter settings outlined in section 5.2.2.2 of the HSSD and section 4.2.1.1.1.1 of the FPM are used for surface creation and analysis. If these depth range values for specific resolutions require adjustment for analysis and submission of individual surveys then the required waiver from NOAA HSD Operations is requested. A detailed listing of the resolutions and the actual depth ranges used during the processing of each survey, along with the corresponding fieldsheet(s), is provided in the Descriptive Report of each survey.

BASE surfaces were created using the CUBE algorithm and parameters contained in the NOAA CUBEParams_NOAA.xml file as provided in Appendix 4 of the FPM. The CUBEParams_NOAA.xml file is included with the HIPS Vessel Files with the individual survey data. The NOAA parameter configurations for resolutions 0.5-16 meters are used.

Multibeam data were reviewed and edited in HIPS Subset Editor as necessary. The finalized BASE surfaces and CUBE hypotheses guided directed data editing at the appropriate depth range in subset editor. The surfaces and subset editor views were also used to demonstrate coverage and to check for errors due to tides, sound speed, attitude and timing.

Vessel heading, attitude, and navigation data were reviewed with the HIPS navigation editor and attitude editor as deemed necessary upon review of surfaces. Where necessary, fliers or gaps in heading, attitude, or navigation data were manually rejected or interpolated for small periods of time. Any editing of this nature is outlined in the Descriptive Report for the particular survey.

Either the Density or the Density & Locale method for hypothesis disambiguation is typically used. This follows section 4.2.1.1.1 of the FPM as available disambiguation methods. The disambiguation method can be seen in each individual layers properties and can be modified if desired.

The surface filtering function in CARIS HIPS is not utilized routinely. If utilized, the individual Descriptive Report lists the confidence level settings for standard deviation used and discuss the particular way the surface filter was applied.

Designated soundings were selected as outlined in section 5.2.1.2 of the HSSD.

IHO child layers were created using the following two formulas for IHO_1 and IHO_2, respectively; - Uncertainty/((0.5^2 +((Depth*0.013)^2))^0.5) and -Uncertainty/((1.0^2 +((Depth*0.023)^2))^0.5). IHO_1 is created for all soundings less than 100 meters while IHO_2 is for 100 meters and deeper. This layer is then exported and run through an application which computes statistics. The results are reported and analyzed in each sheets' individual DR, but the layers are not submitted with the survey.

Additionally, a combined resolution surface was created and reviewed in 3-D mode using one of the following programs; CARIS HIPS, CARIS Base Editor or IVS Fledermaus, to ensure that the data are sufficiently free of artifacts and is a reasonable model of the sea floor.

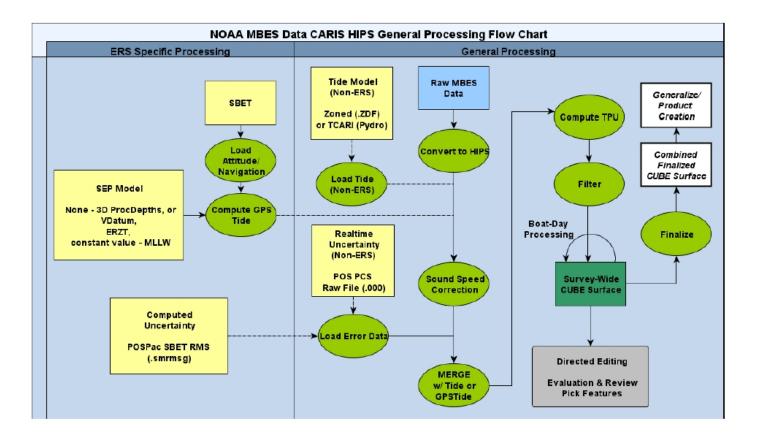


Figure 21: MBES flow diagram

B.2.1.2 Single Beam Echosounder

Single beam echosounder bathymetry was not processed.

B.2.1.3 Phase Measuring Bathymetric Sonar

Phase measuring bathymetric sonar bathymetry was not processed.

B.2.1.4 Specific Data Processing Methods

B.2.1.4.1 Methods Used to Maintain Data Integrity

Quality control logs were used to track and communicate problems during processing.

B.2.1.4.2 Methods Used to Generate Bathymetric Grids

All methods used to generate final bathymetric grids are followed as put forth in section 4.2 and all relevant subsections of the FPM.

B.2.1.4.3 Methods Used to Derive Final Depths

	Cleaning Filters		
Methods Used	Gridding Parameters		
	Surface Computation Algorithms		
Description	Filters were used on a case by case basis as determined by the hydrographer, refer to individual sheet DRs for more information.		

B.2.2 Imagery

B.2.2.1 Side Scan Sonar

Side scan sonar imagery was not processed.

B.2.2.2 Phase Measuring Bathymetric Sonar

Phase measuring bathymetric sonar imagery was not processed.

B.2.2.3 Specific Data Processing Methods

B.2.2.3.1 Methods Used to Maintain Data Integrity

Processing logs were used to record and communicate problems from acquisition to final processing.

B.2.2.3.2 Methods Used to Achieve Object Detection and Accuracy Requirements

Range of the SSS, XTE, speed of vessel collecting data, and repetitious processing examinations were all used

to ensure that object detection and accuracy requirements are met.

B.2.2.3.3 Methods Used to Verify Swath Coverage

Swath coverage is verified through construction of side scan mosaics. During acquisition, the outer portions of the swath are monitored for refraction artifacts. If an apparent refraction artifact impacts object detection ability and cannot be eliminated through adjustment of fish height, the range scale is reduced.

B.2.2.3.4 Criteria Used for Contact Selection

In CARIS SIPS, if an apparent shadow measures greater than 1.0 meters a contact is chosen for development by MBES.

B.2.2.3.5 Compression Methods Used for Reviewing Imagery

No compression methods were used for reviewing imagery.

B.2.3 Sound Speed

B.2.3.1 Sound Speed Profiles

Daily sound speed profiles from the SBE and MVP profilers were processed with Velocipy after acquisition.

Project OPR-G309-FH-16 Note:

Based on feedback from the Atlantic Hydrographic Branch (AHB), the Ferdinand R. Hassler discovered that one element of the recommended Caris processing workflow was not followed throughout project OPR-G309-FH-16. The Caris Sound Velocity Correction (SVC) process was conducted before but not after loading Smoothed Best Estimates of Trajectory (SBETs). It is recommended to perform the SVC process after loading SBETs in order for the ray tracing to account for the updated motion and attitude information. A copy of survey H12932 was re-processed to assess the effect of not applying SVC after loading SBETs. As viewed in Caris Subset Editor, the vertical difference between processing methods ranged from 0.005 -0.010 meters in all sampled areas, including two wrecks. The SVC processing methods were also compared using 2 meter and 4 meter difference surfaces. In the 2 meter difference surface, the depths differ by -8.17 to 3.07 meters, with a mean difference of 0.00 meters and a standard deviation of 0.00 meters, and 95% of nodes exhibit a depth difference of ± 0.01 meters. In the 4 meter difference surface, the depths differ by -0.74 to 0.62 meters, with a mean difference of 0.00 meters and a standard deviation of 0.00 meters, and 95% of nodes exhibit a depth difference of ± 0.01 meters. The high values in the difference surfaces are isolated and limited to features and steep slopes. A detailed review confirmed that the high values in the difference surfaces are entirely the result of CUBE gridding inconsistencies and small horizontal shifts in the grid node structure rather than actual vertical differences in the sounding data. The results of this testing were discussed with HSD Operations and AHB. Based on the limited magnitude of the error, it was concluded that re-processing the entire project was unnecessary. The ship's Caris processing SOP has been updated to reflect the recommended SVC workflow. Details on the analysis can be found in the Appendix.

B.2.3.1.1 Specific Data Processing Methods

B.2.3.1.1.1 Caris SVP File Concatenation Methods

CTD profiles from the Seabird SBE 19-plus and AML Micro-CTD were processed using the NOAA developed program Velocipy. From each system, sound speed profiles are extracted and archived as both individual and concatenated CARIS SVP files.

B.2.3.2 Surface Sound Speed

The SBE-45s were configured to average four samples and report the result once a second. No additional filters are applied.

B.2.4 Horizontal and Vertical Control

B.2.4.1 Horizontal Control

Fixed USCG DGPS stations were used for all real-time horizontal control. If post-processed GPS techniques were used to improve horizontal and vertical control, specific information is included in the Descriptive Report and/or the project's Horizontal and Vertical Control Report.

If USB logged TrueHeave files contained IMU data gaps or other errors apparent during post processing, the Ethernet-logged files may be examined and used if free from gaps. If this is the case both files will be submitted with the GNSS data.

B.2.4.2 Vertical Control

CO-OPS zoned water levels utilizing water level observations from fixed, continuously operating NOAA tide gages are used for reduction of data to MLLW. Predicted water levels are applied during preliminary processing. Before submission, verified water levels are applied to all tidally corrected data. If post-processed GPS techniques are used to improve vertical control, specific information is included in the Descriptive Report and/or the project's Horizontal and Vertical Control Report.

B.2.5 Feature Verification

Features were processed using CARIS BASE Editor software and were included with submitted in the survey's final feature file (FFF) in S-57 .000 format. The FFF includes all features; buoys, rocks, wrecks, bottom samples, etc., addressed within the limits of each individual sheet.

B.2.6 Backscatter

All backscatter was processed from acquired RESON .s7k or Hypack .7k files. All backscatter processing was performed with QPS Fledermaus Geocoder Toolbox and a mosaic calculated with default processing parameters. RESON TVG plugins were used for all processing steps.

B.2.7 Other

No additional data were processed.

B.3 Quality Management

Standard Operating Procedures (SOPs) and checklists are followed by personnel throughout the survey to ensure consistent high quality data and products.

Data are reviewed for artifacts and errors during daily processing, and also reviewed by the Field Operations Officer and/or Hydrographic Senior Survey Technician daily. Before any data is to be submitted it is reviewed independently by at least three experienced hydrographers who are signatories to the Descriptive Report.

B.4 Uncertainty and Error Management

TPU is processed using the following settings.

B.4.1 Total Propagated Uncertainty (TPU)

B.4.1.1 TPU Calculation Methods

TPU is calculated in CARIS HIPS using the Compute TPU tool. Project specific values for tide and sound speed are entered and used over the duration of each project.

B.4.1.2 Source of TPU Values

Error values for the multibeam and positioning systems were compiled from manufacturer specifications sheets for each sensor and from values set forth in section 4.2.3.8 of the 2014 FPM.

B.4.1.3 TPU Values

Vessel	S250 (Port)	S250 (Port)		
Echosounder	RESON 712	RESON 7125 200 kilohertz		
TPU Standard Deviation Values		Gyro	0.020 degrees	
		П	5 % Amplitude	
	Motion	Heave	0.050 meters	
		Pitch	0.020 degrees	
		Roll	0.020 degrees	

	Navigation Position	0.500 meters		
		Transducer	0.005 seconds	
	Timing	Navigation	0.005 seconds	
		Gyro	0.005 seconds	
		Heave	0.005 seconds	
		Pitch	0.005 seconds	
		Roll	0.005 seconds	
		x	0.050 meters	
	Offsets	у	0.050 meters	
		z	0.050 meters	
		Gyro	0.100 degrees	
	MRU Alignment	Pitch	0.020 degrees	
		Roll	0.020 degrees	
		Speed	0.050 meters/second	
	 Vessel	Loading	0.050 meters	
	Vessei	Draft	0.050 meters	
		Delta Draft	0.050 meters	
Vessel	S250 (Port)	(Port)		
Echosounder	RESON 7125	400 kilohertz		
		Gyro	0.020 degrees	
		Heave	5.000 % Amplitude	
	Motion		0.050 meters	
		Pitch	0.020 degrees	
		Roll	0.020 degrees	
	Navigation Position	0.500 meters		
TPU Standard		Transducer	0.005 seconds	
Deviation Values		Navigation	0.005 seconds	
	T ::	Gyro	0.005 seconds	
	Timing	Heave	0.005 seconds	
		Pitch	0.005 seconds	
		Roll	0.005 seconds	
		x	0.050 meters	
	Offsets	у	0.050 meters	
		z	0.050 meters	

		Cumo	0.027 degrees
	MRU Alignment	Gyro	
		Pitch	0.04 degrees
		Roll	0.04 degrees
		Speed	0.050 meters/second
	Vessel	Loading	0.050 meters
	Vesset	Draft	0.050 meters
		Delta Draft	0.050 meters
Vessel	S250 (Starboar	d)	
Echosounder	RESON 7111 1	100 kilohertz	
		Gyro	0.020 degrees
		77	5.000 % Amplitude
	Motion	Heave	0.050 meters
		Pitch	0.020 degrees
		Roll	0.020 degrees
	Navigation Position	1.000 meters	
		Transducer	0.005 seconds
		Navigation	0.005 seconds
	Timing	Gyro	0.005 seconds
	Timing	Heave	0.005 seconds
TPU Standard		Pitch	0.005 seconds
Deviation Values		Roll	0.005 seconds
	Offsets	x	0.100 meters
		у	0.100 meters
		z	0.100 meters
		Gyro	0.130 degrees
	MRU Alignment	Pitch	0.030 degrees
		Roll	0.030 degrees
	Vessel	Speed	0.030 meters/second
		Loading	0.040 meters
		Draft	0.050 meters
		Delta Draft	0.050 meters
Vessel	S250 (Starboard)		
Echosounder	RESON 7125 200 kilohertz		

		Gyro	0.020 degrees	
		 Heave	5 % Amplitude	
	Motion		0.050 meters	
		Pitch	0.020 degrees	
		Roll	0.020 degrees	
	Navigation Position	1.000 meters		
		Transducer	0.005 seconds	
		Navigation	0.005 seconds	
	Timing	Gyro	0.005 seconds	
	Timing	Heave	0.005 seconds	
TPU Standard		Pitch	0.005 seconds	
Deviation Values		Roll	0.005 seconds	
		x	0.050 meters	
	Offsets	у	0.050 meters	
		z	0.050 meters	
		Gyro	0.080 degrees	
	MRU Alignment	Pitch	0.010 degrees	
		Roll	0.010 degrees	
	Vessel	Speed	0.050 meters/second	
		Loading	0.050 meters	
		Draft	0.050 meters	
		Delta Draft	0.050 meters	
Vessel	S250 (Starboar	S250 (Starboard)		
Echosounder	RESON 7125 400 kilohertz			
		Gyro	0.020 degrees	
TPU Standard		77	5 % Amplitude	
	Motion	Heave	0.050 meters	
Deviation Values		Pitch	0.020 degrees	
		Roll	0.020 degrees	
	Navigation Position	1.000 meters		

	Transducer	0.005 seconds	
	Navigation	0.005 seconds	
T:	Gyro	0.005 seconds	
Timing	Heave	0.005 seconds	
	Pitch	0.005 seconds	
	Roll	0.005 seconds	
	x	0.050 meters	
Offsets	у	0.050 meters	
	z	0.050 meters	
	Gyro	0.090 degrees	
MRU Alignment	Pitch	0.030 degrees	
	Roll	0.030 degrees	
	Speed	0.050 meters/second	
V1	Loading	0.050 meters	
Vessel	Draft	0.050 meters	
	Delta Draft	0.050 meters	

B.4.2 Deviations

There were no deviations from the requirement to compute total propagated uncertainty.

Additional Discussion

MRU Align StdDev gyro and MRU Align StdDev Roll/Pitch were derived during patch test processing. Typically several individuals come up with five values for timing, pitch, roll, and yaw. A standard deviation is computed from the different values obtained by each individual. The standard deviation from each individual is then averaged and used as the MRU alignment error (standard deviation of all the independent measurements divided by the square root of the number of measurements).

S250:	MRU Align StdDev gyro	MRU Align StdDev Roll/Pitch
Port 7125 400kHz: Port 7125 200kHz: Stbd 7125 400kHz: Stbd 7125 200kHz:	0.070m 0.060m 0.090m 0.120m	0.080m 0.060m 0.060m 0.020m
2702:		
R2Sonic:	0.090m	0.020m

C Corrections To Echo Soundings

C.1 Vessel Offsets and Layback

C.1.1 Vessel Offsets

C.1.1.1 Description of Correctors

No description was provided.

C.1.1.2 Methods and Procedures

Sensor offsets are measured with respect to the vessel's reference point. These offsets are derived from the full survey performed in the shipyard, a partial survey performed by NGS personnel and measurements/ verifications performed by FERDINAND R. HASSLER personnel. All offsets are tracked and updated as needed on a spreadsheet submitted with the appendices of this report.

The port IMU serves as the reference point for the port-only 7125 HSX configuration, the port 7125 s7k configuration and the side scan sonar. For all other vessel configurations the starboard IMU is the reference point.

POS GPS antennae pairs are mounted to a 2 meter length of channel extrusion in a fore and aft orientation.

C.1.1.3 Vessel Offset Correctors

Vessel	S250 Port	S250 Port		
Echosounder	RESON 7125 400 kg	RESON 7125 400 kilohertz		
Date	2013-07-01	2013-07-01		
		x	-1.244 meters	
		у	0.362 meters	
Officials	MRU to Transducer	z	1.349 meters	
Offsets	WIKO to Transaucer	x2	N/A	
		y2	N/A	
		z2	N/A	

		x x	-2.246 meters
		у	-2.351 meters
	Nav to Transducer	z	14.269 meters
	Nav to Transaucer	x2	N/A
		y2	N/A
		z2	N/A
	Transducer Roll	Roll	4.500 degrees
	Transaucer Kon	Roll2	N/A
Vessel	S250 Port (For use w	with STBD POS data)	
Echosounder	RESON 7125 400 he	rtz	
Date	2013-07-01		
		x	-13.490 meters
		у	0.338 meters
		z	4.311 meters
	MRU to Transducer	x2	N/A
		y2	N/A
		z2	N/A
Offsets	Nav to Transducer	x	-10.386 meters
Ojjseis		у	-2.362 meters
		z	46.699 meters
	Traisancer	x2	N/A
		y2	N/A
		z2	N/A
	Transducer Roll	Roll	4.5 degrees
		Roll2	N/A
Vessel	S250 Starboard		
Echosounder	RESON 7125 400 kilohertz		
Date	2013-07-01		
	MDV. T. I	x	1.424 meters
		у	0.380 meters
Officials		z	1.358 meters
Offsets	MRU to Transducer	x2	N/A
		y2	N/A
		32	17/1

I				
		x	4.528 meters	
		У	-2.320 meters	
	 Nav to Transducer	z	14.278 meters	
	Trav to Transaucer	x2	N/A	
		y2	N/A	
		z2	N/A	
	Transducer Roll	Roll	-4.500 degrees	
	Transaction Rott	Roll2	N/A	
Vessel	S250			
Echosounder	RESON 7111 100 k	ilohertz		
Date	2013-07-01			
		x	1.203 meters	
		у	11.608 meters	
	MDII. T	z	0.977 meters	
	MRU to Transducer	x2	N/A	
		y2	N/A	
		z2	N/A	
Official		x	4.307 meters	
Offsets		У	8.908 meters	
	 Nav to Transducer	z	13.897 meters	
	Nav to Transaucer	x2	N/A	
		y2	N/A	
		z2	N/A	
	T I D II	Roll	0.000 degrees	
	Transducer Roll	Roll2	0.000 degrees	
Vessel	S250	S250		
Echosounder		Odom Echotrac CV200 - Transducer 1 = Starboard hull (200 kHz), Transducer 2 = Port hull (24 kHz) 24 kilohertz		
Date	2013-07-01			
		x	-0.455 meters	
		y	4.620 meters	
		z	1.383 meters	
Offsets	MRU to Transducer	$ x^2 $	-12.701 meters	
		y_2	4.620 meters	
		$\frac{z}{z^2}$	1.381 meters	
		الــّــــــــــــــــــــــــــــــــ		

		x	2.649 meters
		у	1.920 meters
	 Nav to Transducer	z	14.303 meters
	Nav to Transaucer	x2	-9.597 meters
		y2	1.920 meters
		z2	14.301 meters
	Transducer Roll	Roll	0.000 degrees
	Transaucer Kon	Roll2	0.000 degrees
Vessel	2702		
Echosounder	R2Sonic 2022 200 k	ilohertz	
Date	2016-09-11	2016-09-11	
		x	0.237 meters
		у	-0.833 meters
	MRU to Transducer	z	0.407 meters
	MKO to Transaucer	x2	0 meters
		y2	0 meters
		z2	0 meters
Officiato		x	0.759 meters
Offsets		у	-0.309 meters
	 Nav to Transducer	z	-2.932 meters
	Nav to Transaucer	x2	0 meters
		y2	0 meters
		z2	0 meters
	Transducer Roll	Roll	20.000 degrees
	Transaucer Ron	Roll2	N/A

C.1.2 Layback

C.1.2.1 Description of Correctors

Layback is calculated in CARIS from the cable-out and fish depth. Cable-out is output from a cable counter and recorded in the .sdf file. The side scan cable is marked at 12 meters and is deployed to this position on launching. The cable counter is reset to zero at this position and the 12 meter offset applied in SonarPro. Thus, the cable out value in the .sdf file is the correct value for the cable between the tow point and the towfish.

C.1.2.2 Methods and Procedures

No layback correctors are applied in the HVF

C.1.2.3 Layback Correctors

Vessel	S250	S250		
Echosounder	Klein 5250 455 ki	Klein 5250 455 kilohertz		
Date	2013-07-01	2013-07-01		
Layback		x	7.161 meters	
	Towpoint	У	-26.032 meters	
		z	-9.347 meters	
	Layback Error	0.00	0.00 meters	

Additional Discussion

C.2 Static and Dynamic Draft

C.2.1 Static Draft

C.2.1.1 Description of Correctors

Because of her SWATH design, FERDINAND R. HASSLER is particularly susceptible to loading and trim. While underway, the ballast is actively managed to maintain the draft at the design draft of 3.77 meters. During typical survey operations, HASSLER burns approximately 4,000 liters of diesel per day. At a density of 0.83 kilograms/liter this is approximately 3.3 metric tons of fuel per day. At design draft of 3.77 meters, 1.3 metric tons is required to submerge an additional 0.01 meters of the hull in salt water. The daily fuel burn would thus account for 0.03 meters of variation in the draft. Ballast is adjusted daily to account for fuel burn and the levels in other tanks. Uncertainty is estimated at 0.05 meters.

C.2.1.2 Methods and Procedures

The waterline to reference point is calculated from the vessel offset survey and the vessel draft marks.

C.2.2 Dynamic Draft

C.2.2.1 Description of Correctors

Dynamic draft is calculated as the dynamic height of the vessel reference point as a function of vessel speed compared to the height at rest. This correction is applied during CARIS processing.

C.2.2.2 Methods and Procedures

An ellipsoidally referenced dynamic draft measurement (ERDDM) was performed on following guidelines in the 2014 FPM on February 21, 2016 (Dn28) for vessel S250. An area was selected about 30NM off the VA/NC coast where the slope of the geoid was minimal. Speeds from 6 to 13 knots were run in one direction. The ship was then turned to the reciprocal heading, brought to a complete stop, and then the speeds from 6 to 13 knots were run in the opposite direction.

The fourth order polynomial results for the dynamic draft curves from the port and starboard side were averaged. The 2016 results and comparisons between 2011 - 2016 can be found included in the attached appendices. Results from the last three years were averaged for use as the dynamic draft corrector values for 2016.

Similar methods were used in performing the ERDDM for launch 2702 which was performed in the York River on March 3, 2016 (Dn063). This was the first ERDDM performed on the vessel, therefore no previous years values were available for averaging. The 2016 results were used for dynamic draft correctors.

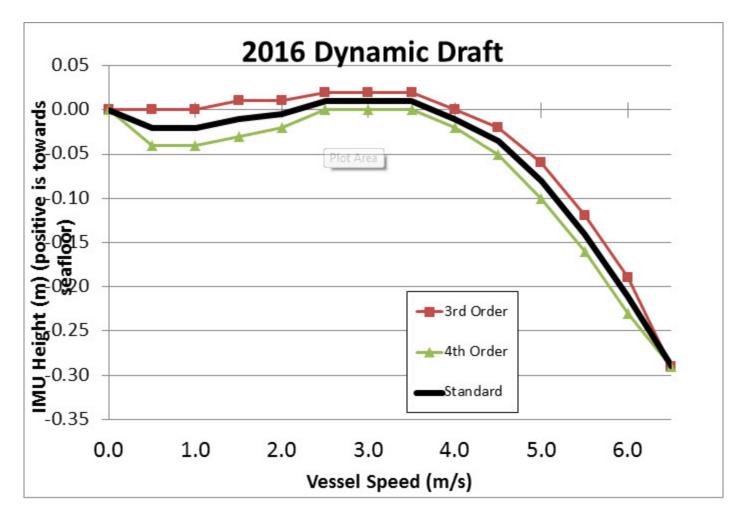


Figure 22: S250 dynamic draft derived from ERDDM methods. Positive values are displacements of the IMU towards the sea floor. Thin lines are results from port and starboard head for third and fourth order polynomial fits. Black bold line is dynamic draft value used for both hulls.

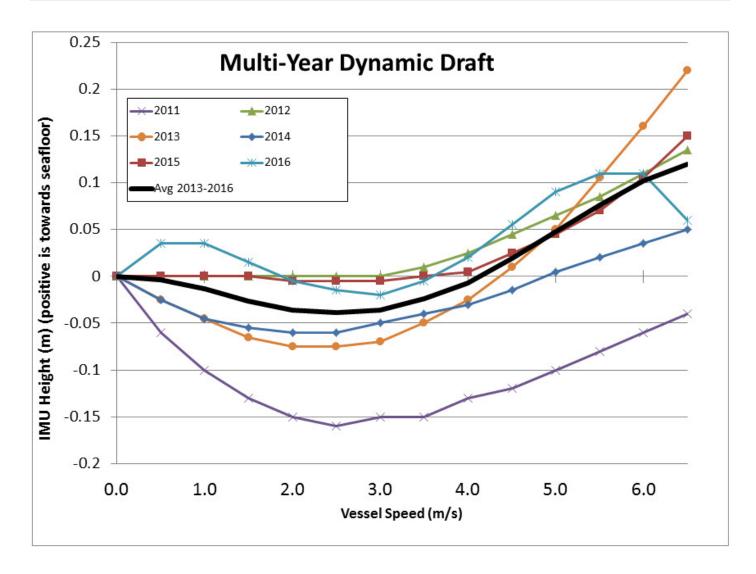


Figure 23: S250 dynamic draft derived from ERDDM methods comparison from years 2011 - 2016.

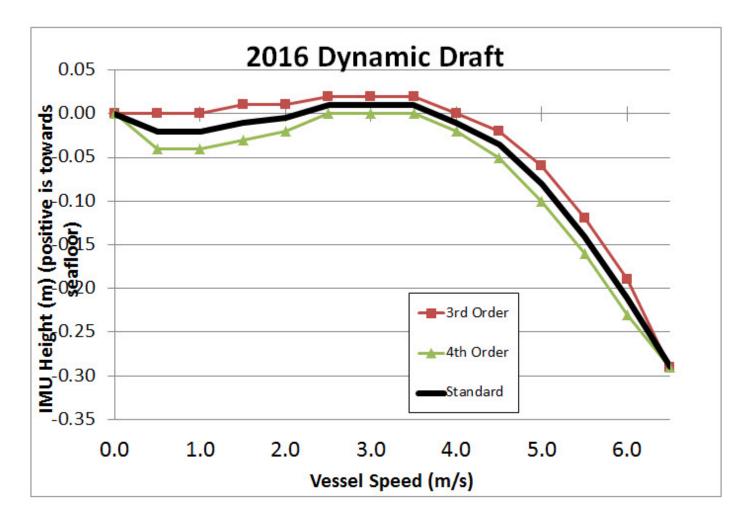


Figure 24: 2702 dynamic draft derived from ERDDM methods. Positive values are displacements of the IMU towards the sea floor. Thin lines are results from port and starboard head for third and fourth order polynomial fits.

C.2.2.3 Dynamic Draft Correctors

Vessel	S250		
Date	2016-02-21		
	Speed	Draft	
Dynamic Draft Table	0.0	0.000	
	0.5	0.00	
	1.0	-0.01	
	1.5	-0.03	
	2.0	-0.04	
	2.5	-0.04	

	Speed	Draft	
	3.0	-0.04	
	3.5	-0.02	
Vessel	S250		
Date	2015-06-14		
	Speed	Draft	
	4.0	-0.01	
	4.5	-0.02	
Dynamic Draft Table	5.0	0.05	
Dragi Tabic	5.5	0.08	
	6.0	0.10	
	6.5	0.12	
Vessel	2702		
Date	2016-03-03		
	Speed	Draft	
	0.00	0.00	
	0.5	-0.02	
	1.0	-0.02	
	1.5	-0.01	
	2.0	-0.01	
, ·	2.5	0.01	
Dynamic Draft Table	3.0	0.01	
	3.5	0.01	
	4.0	-0.01	
	4.5	-0.04	
	5.0	-0.08	
	5.5	-0.14	
	6.0	-0.21	
	6.5	-0.29	

C.3 System Alignment

C.3.1 Description of Correctors

No description was provided.

C.3.2 Methods and Procedures

Methods and Procedures used follow recommendations given in Section 1.5 of the 2014 FPM.

C.3.3 System Alignment Correctors

Vessel	S250		
Echosounder	RESON 7125 Starboard 400 megahertz		
Date	2016-07-09		
	Navigation Time Correction	0.000 seconds	
	Pitch	0.620 degrees	
	Roll	0.070 degrees	
Patch Test Values	Yaw	0.700 degrees	
	Pitch Time Correction	0.000 seconds	
	Roll Time Correction	0.000 seconds	
	Yaw Time Correction	0.000 seconds	
	Heave Time Correction	0.000 seconds	
Vessel	S250		
Echosounder	RESON 7125 Starboard 200 kilohertz		
Date	2016-07-09		
	Navigation Time Correction	0.000 seconds	
	Pitch	0.310 degrees	
	Roll	0.060 degrees	
Patch Test Values	Yaw	0.690 degrees	
	Pitch Time Correction	0.000 seconds	
	Roll Time Correction	0.000 seconds	
	Yaw Time Correction	0.000 seconds	
	Heave Time Correction	0.000 seconds	
Vessel	S250		
Echosounder	RESON 7125 Port 40	0 kilohertz	
Date	2016-07-09		

	1				
Patch Test Values	Navigation Time Correction	0.000 seconds			
	Pitch	0.380 degrees			
	Roll	-0.140 degrees			
	Yaw	-0.360 degrees			
	Pitch Time Correction	0.000 seconds			
	Roll Time Correction	0.000 seconds			
	Yaw Time Correction	0.000 seconds			
	Heave Time Correction	0.000 seconds			
Vessel	S250				
Echosounder	RESON 7125 Port 200	0 kilohertz			
Date	2016-07-09				
	Navigation Time Correction	0.000 seconds			
	Pitch	0.370 degrees			
	Roll	-0.140 degrees			
Patch Test Values	Yaw	-0.220 degrees			
	Pitch Time Correction	0.000 seconds			
	Roll Time Correction	0.000 seconds			
	Yaw Time Correction	0.000 seconds			
	Heave Time Correction	0.000 seconds			
Vessel	S250	S250			
Echosounder	RESON 7111 100 kilo	ohertz			
Date	2014-04-16				
	Navigation Time Correction	0.000 seconds			
	Pitch	-0.86 degrees			
	Roll	0.010 degrees			
Patch Test Values	Yaw	1.170 degrees			
	Pitch Time Correction	0.000 seconds			
	Roll Time Correction	0.000 seconds			
	Yaw Time Correction	0.000 seconds			
	Heave Time Correction	0.000 seconds			
Vessel	2702	2702			
Echosounder	R2Sonic 2022 400 kilohertz				
Date	2016-03-03	2016-03-03			

	Navigation Time Correction	0.000 seconds
	Pitch	-1.500 degrees
	Roll	-1.290 degrees
Patch Test Values	Yaw	-0.010 degrees
	Pitch Time Correction	0.000 seconds
	Roll Time Correction	0.000 seconds
	Yaw Time Correction	0.000 seconds
	Heave Time Correction	0.000 seconds

Additional Discussion

The RESON 7111 sonar was inoperable during the 2016 field season and was not calibrated during 2016. The 7111 patch test values are retained here from the 2014 calibration period for reference only.

C.4 Positioning and Attitude

C.4.1 Description of Correctors

No description was provided.

C.4.2 Methods and Procedures

Vessel navigation and attitude is measured by the POS/MV and recorded in the Hysweep .hsx file and the RESON .s7k file. Pitch is applied real-time to the RESON 7111. Navigation and attitude measurements not applied in real time are applied during post processing in CARIS HIPS using the attitude data recorded in the .hsx or .s7k file.

The POS/MV TrueHeave data is logged within the POS/MV .000 files and applied in CARIS HIPS during post processing using the "Apply Delayed Heave" function. TrueHeave is a forward-backward filtered heave corrector as opposed to the real time heave corrector, and is fully described in section 6 of the POS/MV V5 User Guide 2011 and V4 User Guide 2009.

In most cases the Hassler used the Fugro MarineStar satellite based corrector service to provide realtime correction to the horizontal position and ellipsoid height for all data acquisition and initial processing. The corrector signal is received on the L1 channel of the POS/MV primary GPS antenna and logged directly into the POS/MV. The POS files produced during acquisition are then processed through the POSPac MMS software to produce an SBET in the WGS84 reference frame and an RMS file containing the realtime uncertainty estimates of the position and attitude data.

Alternatively, if Marinestar service isn't available, post processing of POS/MV kinematic .000 files using Applanix POSPac MMS and POSGNSS software using either IN-Fusion SmartBase, IN-Fusion SingleBase

or Precise Point Positioning (PPP) processing modes. After processing and quality control analysis of the post-processed SBET files is complete, the SBET and SMRMSG files are applied to the HDCS data in CARIS HIPS using the "Load Attitude/Navigation Data" and "Load Error Data" processing tools, respectively.

The heave lever arms for S250 are configured to a point on the centerline of the vessel between the two POS IMUs. This was done to prevent long-term static roll angles from causing a steady state heave offset.

C.5 Tides and Water Levels

C.5.1 Description of Correctors

No description was provided.

C.5.2 Methods and Procedures

Unless otherwise noted in the survey Descriptive Report (DR) and/or project Horizontal and Vertical Control Report (HVCR), the vertical datum for all soundings and heights is Mean Lower Low Water (MLLW). Predicted, preliminary, and/or verified water level correctors from the primary tide station(s) listed in the Project Instructions may be downloaded from the CO-OPS website and used for water level corrections during the course of the project. These tide station files are collated to include the appropriate days of acquisition and then converted to CARIS .tid file format using FetchTides.

Water level data in the .tid files are applied to HDCS data in CARIS HIPS using the zone definition file (.zdf) or a Tidal Constituent and Residual Interpolation (TCARI) model supplied by CO-OPS. Upon receiving final approved water level data, all data are reduced to MLLW using the final approved water levels as noted in the individual survey's DR.

A Horizontal and Vertical Control Report (HVCR) was not created for this project.

Newer methods for handling vertical control are being developed and, if utilized, are explained in more detail in the survey DR.

C.6 Sound Speed

C.6.1 Sound Speed Profiles

C.6.1.1 Description of Correctors

No description was provided.

C.6.1.2 Methods and Procedures

Seabird .cnv and MVP .bot files are collected when necessary and converted to .svp files using NOAA's Pydro/Velocipy program. These .svp files are concatenated into one sheet specific master file per project which is then applied to HDCS data using a specified method. This method of applying sound speed to data is listed in the sheet's processing log included in the Separates submitted with the individual survey.

C.6.2 Surface Sound Speed

Surface sound speed correctors were not applied.

D. APPROVAL SHEET

This Data Acquisition and Processing Report for project OPR-G309-FH-16, Approaches to Wilmington, is respectfully submitted.

As Chief of Party, I have ensured that standard field surveying and processing procedures were adhered to during these projects in accordance with the Hydrographic Surveys Specifications and Deliverables (3/2016); Hydrographic Survey Technical Directives 2016-1, 2016-2, 2016-3; and the Field Procedures Manual for Hydrographic Surveying (4/2014).

I acknowledge that all of the information contained in this report is complete and accurate to the best of my knowledge.

This DAPR applies to surveys H12893, H12894, H12895, H12927, H12929, H12930, H12931, H12932, H12934, and F00679 which were completed in 2016.

Approved and Forwarded:

LT Nicholas C Morgan, NOAA

Thit Mayon to Mass

Field Operations Officer

LCDR Matthew J. Jaskoski, NOAA

Chief of Party

Л	-	-	~ "	Š	İΧ	

Vessel Reports

H12932 Re-SVC Process Analysis

Approaches to Wilmington (OPR-G309-FH-16) sheet H12932 assigned to Ferdinand Hassler was selected to conduct an analysis of the need to re-SVC the sheets in this project after SBET application. This sheet was chosen due to its size and the fact that it contains multiple wrecks and bottom features. The steps for the analysis are below

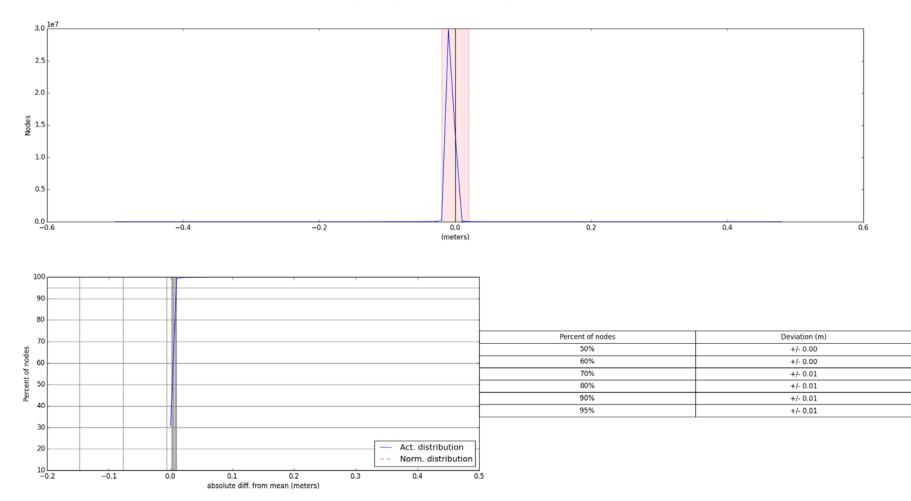
- Ensure designated soundings in the original survey were correct
- Ensure original surfaces were up to date
- Copy the original project. Rename the original project _OLD
- Re-SVC the copied project
- Re-merge the new project
- Ensure designated soundings in the new project were correct
- Create surfaces
- Difference new and old surfaces

Conclusion:

- ✓ 95% of nodes in the 2m difference surface have a value of 0.01 meters or less
- ✓ 95% of nodes in the 4m difference surface have a value of 0.01 meters or less
- ✓ Largest differences were seen over wrecks or bottom topography.
- ✓ Nodal analysis over features is not indicative of actual differences in data.

2m Difference Surface

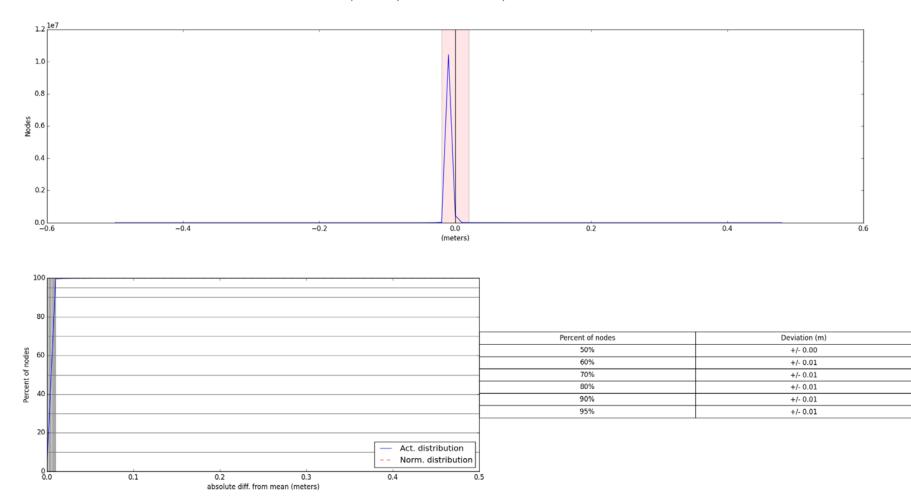
H12932_NEW_OLD_2m_MLLW_DIFF.txt
Mean: -0.00 | Mode: -0.01 | One Standard Deviation: 0.00 | Bin size: 0.01



These stats were created using the Pydro BSB Surface ASCII Export Stats tool. As is seen, 95% of all nodes in the 2 meter difference surface are +/-0.01 meters.

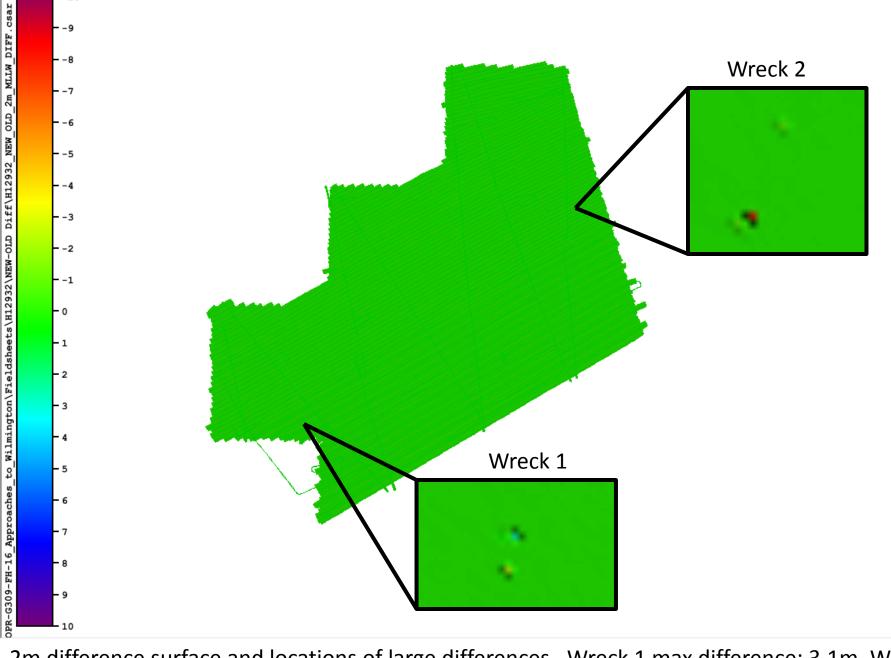
4m Difference Surface

H12932_NEW_OLD_4m_MLLW_DIFF
Mean: 0.00 | Mode: -0.01 | One Standard Deviation: 0.00 | Bin size: 0.01



These stats were created using the Pydro BSB Surface ASCII Export Stats tool. As is seen, 95% of all nodes in the 4 meter difference surface are +/-0.01 meters.

- In the 2m difference surface, 5 nodes had a difference greater than 1m with a max differences of -8.2m and 3.1m. All of these larger differences occurred over features. The 8.2m difference occurred where one surface's node referenced the feature and the other surface's node referenced the seafloor immediately next to the feature.
- In the 4m difference surface 44 nodes had a difference
 0.5m or greater with a max difference of -0.7m and 0.6m.
- A review of all non-zero difference nodes indicated the apparent vertical difference was in fact due to horizontal differences in surface node structure.
- Subset evaluations indicated typical vertical differences between SV processing methods of 1cm or less.

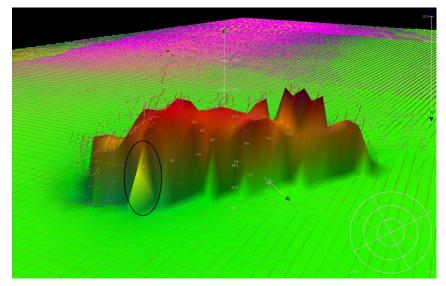


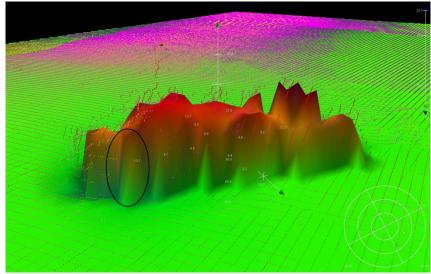
2m difference surface and locations of large differences. Wreck 1 max difference: 3.1m. Wreck 2: max difference 8.2m.

Old/New surfaces in Subset Editor

Without SVC after SBETS

With SVC after SBETS

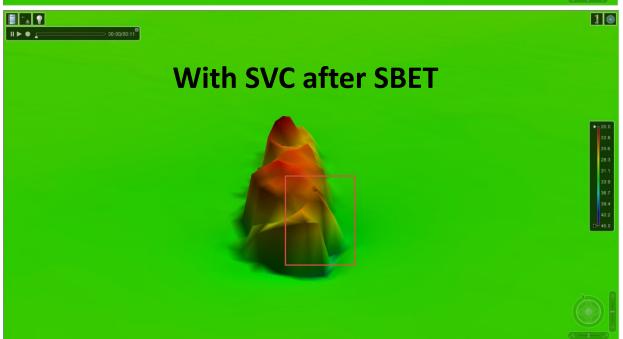


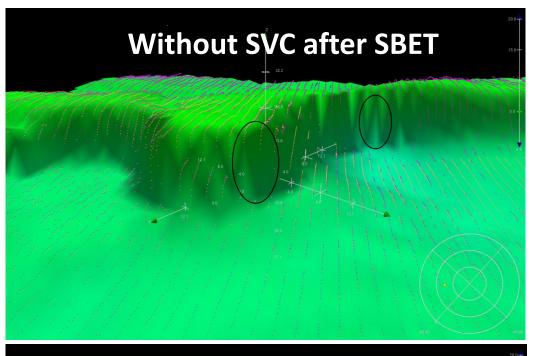


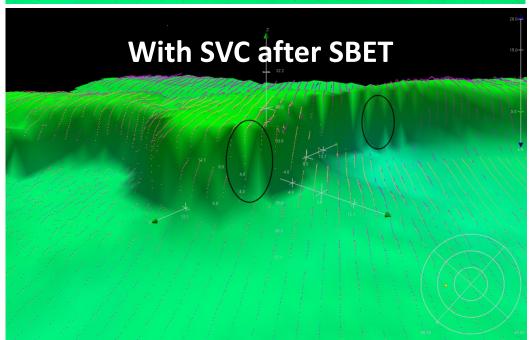
The -8.2m differenced node



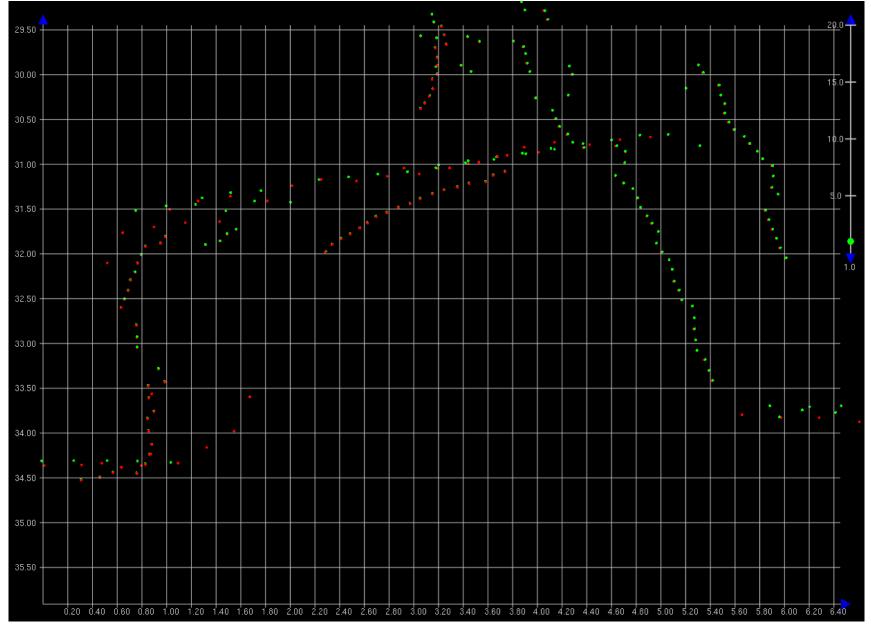




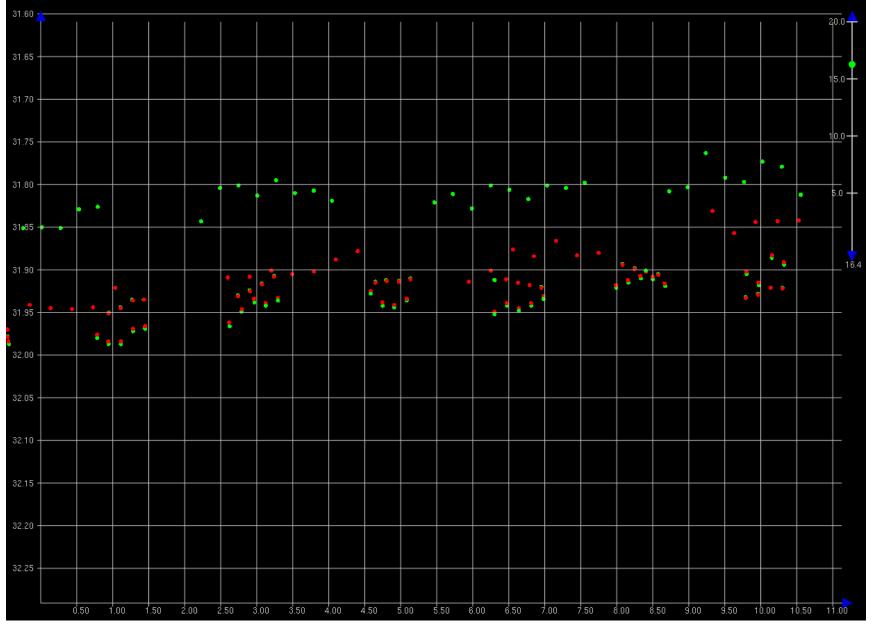




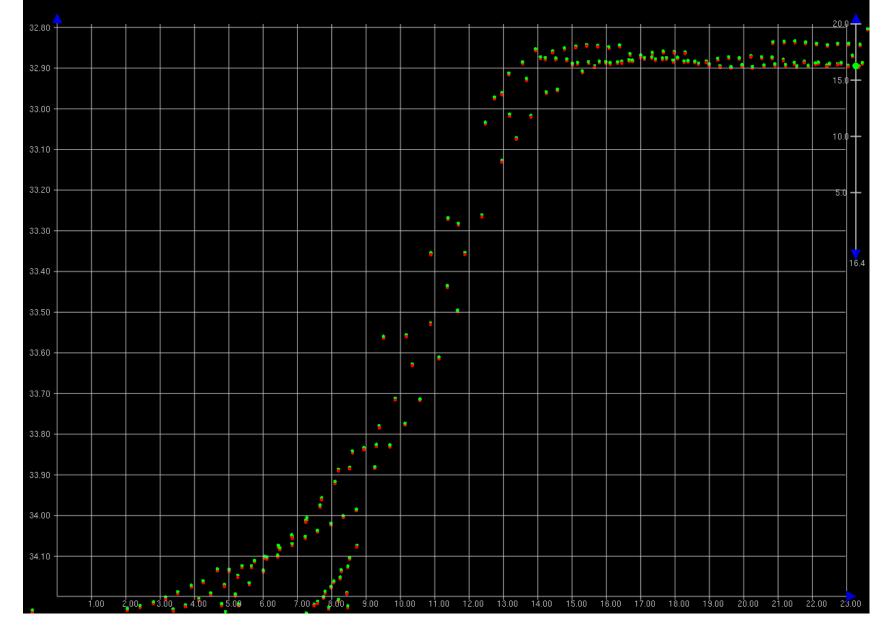




An example of sounding difference over a wreck. Green is with re-SVC, Red is old. Note that a query of soundings that appear isolated showed that they are co-located with soundings of the opposite color.



An example of sounding difference over a flat surface. Green is with re-SVC, Red is old. Note that a query of soundings that appear isolated showed that they are co-located with soundings of the opposite color.



An example of sounding difference over a steep slope. Green is with re-SVC, Red is old.

Final report

SURVEY REPORT

SHIP: M286 SWATH FERDINAND R. HASSLER

LOCATION: PASCAGOULA, MS

DATE: 7/18-7/26, 2009

And 11/4, 2009

PURPOSE:

Determine the ship's centerline, roll, and pitch. Install benchmarks, install the master reference plane in the same planes as the measured roll, pitch, and azimuth of the ship. Assist the shipyard to install the IMUs parallel to the centerline, and in the same plane as the ship's roll and pitch. Assist the shipyard in installing the transducers in the same plane as roll, pitch and azimuth of the ship. Measure and spot the draft marks.

PERSONNEL:

Eric Kostelak Brian Kloter Raymond Impastado John Miskimmin

EQUIPMENT LIST:

WILD T2 THEODOLITE SN: 169786 Calibration Expiration Date; 12/19/09

WILD T2 THEODOLITE SN: 155062 Calibration Expiration Date; 12/19/09

WYLER CLINO 2000 CLINOMETER SN: M4416 Calibration Expiration Date: 07/10/10

Date, 07/10/10

TOPCON GTS-301 One Second Electronic Total Station, Serial number GU1193 Calibration Expiration Date; 07/12/09

WILD NA1 AUTO LEVEL: SN 472810 Calibration Expiration Date; 07/12/09

Procedures:

- 1. Establish a baseline in relation to the centerline of both pontoons.
 - A. Locate points on each of the pontoons to determine centerline
 - B. Measure the elevation differences of the points. Take the average of these to determine the pitch and roll of each pontoon.
- **2.** Take the average of the measurements of the two pontoons for roll, pitch, and centerline. The result can then be used as the Master reference.
- **3.** Create a traverse, in a level plane, around the ship using the established baseline as a reference. Set various points that will be used to locate the master reference block, IMUs, bench marks, transducers, and antennas.
- **4.** Locate, set and secure the master reference block to within 9 arc seconds of the calculated roll, pitch, and centerline values.
- 5. Once the MRB has set for a day, confirm the measurements relative to the results of step 2. If the measurements are within the two values used in Step 2, these values will become the Final Master Reference, which all further measurements will be referenced to.
- **6**. Locate IMU foundations, adjust to be level with roll and pitch, and aligned with centerline.
- 7. Establish bench marks that are aligned to the centerline in any areas that require future measurements.
- **8**. For transducers, on the bottom of the hull, establish punch marks aligned to the centerline that can be used to align the transducers to the centerline.
- **9**. Run a closed level loop from the master reference block to all bench marks, Transducers, antennas, and sensors to determine their elevation values relative to the reference. (Z axis).
- **10**. Using established elevation points within the traverse, determine the correct locations for all draft marks.

11. Work with the shipyard to determine the correct alignment of the transducers.

METHODS

All angles at intersections were turned 4 times, 2 in regular, and 2 in inverted position. All other angles were turned 2 times, once in regular, and once in inverted position.

Slope distances were measured with a zenith angle in the regular and inverted Position.

The Traverse was closed and computed for accuracy.

Results

MRB

After the MRB has set up for 24 hours, it was found the chock fast had caused an 18 second movement in roll. As this small value was well within the average of the two pontoons, the final reference was shifted to the MRB values.

IMU

During measurements of the IMUs, we discovered it was impossible to meet the specification to be level to the roll and pitch within 90 arc seconds using the existing mounts. The shipyard manufactured a double plate separated by three threaded rods, which allowed fine adjustment in two planes (roll and pitch). The IMUs were aligned to zero measurable azimuth error, and to within 5 arc seconds in roll and pitch relative to the MRB.

TRANSDUCERS

7125

During measurements it became apparent that it was impossible to meet the roll and pitch specification on the multibeam transducer mounts. There was no measurable azimuth error on either 7125 transducer mount, when the welding was finished. The shipyard came up with the roll and pitch solution of machining the surfaces in place once the mounting plates were completely welded out. We attended for the machine work on 8/19/09. A portable milling machine was put in place, leveled to within 5 arc seconds of the MRB plus 4.5 degrees of roll to Give the transducer mounting surfaces the specified 4.5 degree outward roll angle. See attached photo. It was agreed by all that if the milling machine was positioned correctly, the surfaces had to be correct, but as a check to confirm the process, we measured the machined surface on the port unit, and found the pitch error was zero, and the roll error was 15 seconds. This was well within the required 90 seconds.



7111

Like the 7125s, it was impossible to meet the roll and pitch specification on this transducer mounting plate. It too, was machined by the portable milling machine.

The machine was set up to be within 5 seconds of the MRB Pitch and Roll values.

XYZ COORDINATES TABLE

POINT	X-AXIS	Y-AXIS	Z-AXIS	DESCRIPTION
5	9.264	-7.555	7.169	POINT FP
6	9.409	6.256	7.168	POINT FS
7	3.491	-7.478	7.176	POINT MP
8	3.872	6.168	7.178	POINT MS
9	-4.035	-7.561	7.168	POINT AP
10	-4.022	6.258	7.169	POINT AS
15	9.326	-0.652	7.168	CENTERLINE
18	-4.017	-0.652	7.168	CENTERLINE
19	16.343	2.530	-5.065	STARBOARD BENCH MARK TOP WHEEL HOUSE
20	16.343	-0.653	-5.064	MID BENCH MARK TOP WHEEL HOUSE
21	16.343	-3.836	-5.066	PORT BENCH MARK TOP WHEEL HOUSE
25	-1.336	0.001	0.160	AFT BENCH MARK MASTER REFERENCE PLATE
26	0.000	0.000	0.000	MASTER REFERENCE PLATE
27	-0.353	0.000	0.161	FWD BENCH MARK MASTER REFERENCE PLATE
28	13.428	-8.960	-2.496	PORT BENCH MARK BRIDGE WING
29	13.428	-5.592	-2.476	STARBOARD BENCH MARK BRIDGE WING
30	7.115	5.836	7.154	FWD PUNCH MARK ADCP
31	5.765	5.835	7.145	AFT PUNCH MARK ADCP
33	7.841	6.846	7.167	FWD PUNCH MARK RESON 7125 STARBOARD PONTOON
34	5.025	6.847	7.168	AFT PUNCH MARK RESON 7125 STARBOARD PONTOON
36	5.022	-8.169	7.157	AFT PUNCH MARK RESON 7125 PORT PONTOON
37	7.792	-8.169	7.154	FWD PUNCH MARK RESON 7125 PORT PONTOON
39	15.307	6.610	6.843	AFT PUNCH MARK RESON 7111
40	16.098	6.611	6.771	FWD PUNCH MARK RESON 7111
41	10.822	5.864	7.169	FWD PUNCH MARK MDS* STARBOARD PONTOON
42	9.818	5.863	7.172	AFT PUNCH MARK MDS* STARBOARD PONTOON
43	10.608	-7.081	7.177	FWD PUNCH MARK MDS* PORT PONTOON
44	9.762	-7.080	7.175	AFT PUNCH MARK MDS* PORT PONTOON
45	-13.926	-0.615	0.105	AFT MID BENCH MARK BACK DECK
46	-9.031	-0.615	0.125	FWD BENCH MARK BACK DECK

POINT	X-AXIS	Y-AXIS	Z-AXIS	DESCRIPTION
47	-13.926	6.471	0.114	STARBOARD BENCH MARK BACK DECK
48	-13.926	-7.697	0.093	PORT BENCH MARK BACK DECK
51	5.891	-6.878	5.839	IMU PORT PONTOON (OLD LOCATION)
52	5.923	5.428	5.840	IMU STARBOARD PONTOON (OLD LOCATION)
53	17.655	6.584	6.890	RESON 7111 CENTER OF PLATE
54	6.265	6.774	7.095	PORT EDGE RESON 7125 STARBOARD PONTOON
55	6.265	6.805	7.093	RESON 7125 STARBOARD PONTOON
56	6.223	-8.078	7.087	STARBOARD EDGE RESON 7125 PORT PONTOON
57	6.223	-8.109	7.085	RESON 7125 PORT PONTOON
58	16.039	5.417	2.563	INBOARD DRAFT MARK FRAME 4 STARBOARD
59	16.025	-6.711	2.567	INBOARD DRAFT MARK FRAME 4 PORT
60	-11.204	5.626	2.588	INBOARD DRAFT MARK FRAME 46 STARBOARD
61	-11.208	-6.870	2.562	INBOARD DRAFT MARK FRAME 46 PORT
62	16.040	7.458	2.565	OUTBOARD DRAFT MARK FRAME 4 STARBOARD
63	-11.208	7.462	2.588	OUTBOARD DRAFT MARK FRAME 46 STARBOARD
64	16.025	-8.735	2.570	OUTBOARD DRAFT MARK FRAME 4 PORT
65	-11.205	-8.711	2.555	OUTBOARD DRAFT MARK FRAME 46 PORT
66	6.273	-9.907	5.789	PORT BENCH MARK IMU PORT PONTOON
67	6.273	-5.007	5.861	STARBOARD BENCH MARK IMU PORT PONTOON
68	6.624	3.666	5.862	PORT BENCH MARK IMU STARBOARD PONTOON
69	6.624	8.571	5.798	STARBOARD BENCH MARK IMU STARBOARD PONTOON
70	5.861	-6.865	5.767	IMU PORT PONTOON
71	5.885	5.381	5.768	IMU STARBOARD PONTOON
72	-20.247	-0.609	-4.327	BOTTOM OF CENTER BLOCK "A" FRAME
73	11.205	-1.904	-7.782	BOTTOM OF GPS ANTENNAE PORT LOWER
74	10.488	-1.896	-9.774	BOTTOM OF GPS ANTENNAE PORT UPPER
75	11.180	0.594	-7.776	BOTTOM OF GPS ANTENNAE STARBOARD LOWER
76	10.455	0.589	-9.776	BOTTOM OF GPS ANTENNAE STARBOARD UPPER

JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 1-18-09 SHEET NO :- 1 SCALE: 1" = NONE 7.26-09 (1) d''c'' FWD OUTBOARD DONTOON 1.011 FRAME (2) (14) 6 (13) "F5" 154 (8) 214 i 71.056 4 (16) "81" FRAME 36 AFT

JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO: 1A SCALE: 1" - NONE INST. ON PT AVG. ¥ 2 PT. AVG. DIST 89°20'25° 89°20'30° 89°20'28' 87°41'56" 272°17'59. 87°41'59. 6.779 268°11'37" 248°11'42 268°11'40. 87°54'43' 272°05'12' 87°54'45' 7.044 "F5 " "FP" 85°25'42" 85°25'46" 85°25'44 88°45'06" 271°14'57" 88°45'05" 6.770
270°02'26' 270°02'28" 270°02'27" 88°53'12" 271°07'02" 88°53'05" 6.895 "M5 "MP" 88°39'43" 88°39'43" 88°39'43 87°52'44' 272°27'20" 87°52'42" 6.932 "A5" 269056 40 269056 48 269056 44 89054 20 272005 48 8705 4 16 6 897 "A P" RAYMOND C. IMPASTATO PROFESSIONAL LAND SURVEYOR JOB: ____FERDINAND R. HASSLER

M286 SWATH

PASCAGOULA, MISSISSIPPI

139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 FIELD CREW: R.I., E.K., J. M. & B. K.

CALCULATED BY: R. IMPASTATO

DATE: 7-18-09 SHEET NO.: 2

SCALE: 1" - NONE

STA		BS	+	HI			FS		–E	ЬE	V-						-	ÞΕ	SCI	SH	T	10	-					
	1	780		1.78	0			_	0.	00	0	(AS,	sun	160	E	LEU	ATI	ron)	PI	<u>-</u> .	"B	1"		8.	52	6
	10	100	٦	10		-0	.56	4	1.	30	14		"	AF	, ,		-			_,	7	100			-	-	-	-
			1			-0.	57	8	1.	25	8	Т	"	13	"							1.0	-				-	1
		Ť	\top			0	.81	2	- 0	2.0	32		P	-	. 4	"			-	8	. <	68	8	-			-	
	1,	017	0	.98	35										/-					_								-
						-0	36	3	1	34	8		"	M	P	"			-	7	12	9						
						-0	.37	6	/	3	61		"	M	5"				- 7	ý.	21	61	65					
						-0	37	9	1	36	4		"	FP	"				- 1	7.	16	2						
						-0	39	5	1	30	80		" 1	5	"				- 1		14	6						-
	-6	416	5 0	96	4			11																				-
		_	_		*	-0	1.40	00	1.	36	4		" /	FP	"				7		162	2						
		_	_			-0	.38	5	1.	34	9.		" 1	19	•													Ī
		_	+	-	_	-0	.39	7	1.	36	/		" 1	19	"													
	_			-	_	0,	990	0	-0	.0	32	_	"1	7	· B	"												
-	0.	807	0	.7	75						-	L																
		-	-	-	_	-0	560	3	1.	35	8		"/	95	"												+	
-		+	-	-	_	-0.	560	7	1.	34	4	_	"	P	'													_
-	-	-	-	-	-	_	200	_				_	/		2	- 4	_											_
-		-	+	-	_	Q.	77	2	0.	00	0	V	_	1	7	"	BI	′′′		_								_
	\vdash	+	-	-	-	_		\dashv	-	_	-	-	_			-			-			_	_		_			_
-			+	-		_		\dashv	-		-	_	-		-				-					_			_	_
		+	-	+	-	-	+	\dashv	-		-	-	-					-	-		_	_	_			-	_	_
			+	+	-	-	-	\dashv	-		-	_	-					\dashv	\dashv	_		_	_			_	-	_
			-	+	-	-	+	-	_	-	_	-	-		-	-		\vdash	-	_	_		_		_	-	-	_
_		+	+	\vdash	-		-			-		-	-			-		-	-		_	_		_			-	_
	\Box			+				\dashv				_	-		\dashv				+	-		-				\dashv	-	-
								7		-		-						\dashv	+	-		_	-		-	-	+	-
							\exists					-					-				-	_	-	-	-	-	-	_
									1,1			200							+				_				-	-
							1					-						3	+	-			_	-	\dashv	\dashv		-
												_												-			-	
																			+								-	-
							8																					_
												-																_
				177								-									-					-	-	_

JOB: ___ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: __R. IMPASTATO DATE: 7-18-09 SHEET NO.: 3 SCALE: 1" = NONE 7-26-09 BOTTOM OF PORT PONTOON "FP" EL=1.364 EK= 1.344 13.299 PIXCH = 0005 10" BOTTOM OF STARBOARD PONTOON EL = 1.380 A5" 0. EL = 1.358 13.430 PITCH = 0°05'38" AVERAGE = 0005'24" PITCH BOW HIGH

JOB: ____ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO : 4 SCALE: 1" = NONE 7-26-09 F5' EC = 1.380 0 EL= 1.364 13.812 KOLL = 0903 59" M5" E4 = 1.361 MP EL= 1.3485 13.651 Rock = 0°03'09" As' EL= 1,358 "AP" EL= 1.344 13.819 ROLL + 0°03'29" ROLL AVERAGE = 0°03 32" STARBOARD HIGH

RAYMOND C. IMPASTATO PROFESSIONAL LAND SURVEYOR JOB: ____FERDINAND R. HASSLER

M286 SWATH

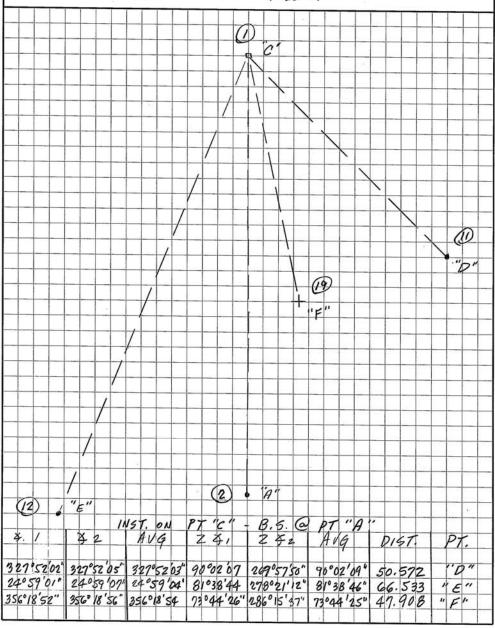
PASCAGOULA, MISSISSIPPI

139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 FIELD CREW: R.I., E.K., J. M. & B. K.

CALCULATED BY: R. IMPASTATO

SCALE: 1" - NONE

DATE: 7-18-09 SHEET NO.: 5



JOB: ____ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO.: 6 SCALE: 1" = NONE 7-26-09 (2) 0" (23) PT"E (12) 45) 1" ON POINT E' - B.S. @ PT "C" Z 4. Z 42 AVG DIS INST. "9"

FERDINAND R. HASSLER JOB: ____ RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO.: 7 SCALE: 1" = NONE 7-26-09 CLOSING ANGLES TRAVERSE 2 TRAVERSE 1 0.001 MISCUSSUE 0.001 MIGGEOSOES 120,702 LENGTH 145. 520 LENGTH PEECISION = 1: 120,702 PRECISION= 1 145,520 TRA VERSE 13 65.03311 D 24.138 110025 500 4. 86° 22 24" 42 86° 22' 22" 4, 110° 25' 51" AVG= 86° 27'23' 42 110°25' 49" AUG'= 110'25'50" ADJUSTED X'S ADJUSTED 43 40° 53' 51' 28° 40' 14 ° 110° 25' 55" 28°26' 55" 86°22' 28" 85°10' 37'' 40 53 47 28026'51" 28 40' 10" 86° 22' 23 65' 10 33' 10 25' 50" 179 59 47 180000 00" 179059147 180000 00 13 SECOND MISCLOSURE 13 SECOND MISCLOSURE

JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: <u>7-/8-09</u> SHEET NO.: 8 SCALE: 1" = NONE 7-26-09 (1) CI 650/0321 "D" 40 53 43" 33.701 F' (19) AFTER ADJUSTMENTS

JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO.: 9 SCALE: 1" - NONE 7-26-09 (1) "C" SET (21) (20) BENCH MARK 3.183 3.183 "F" (19) SET B.M. SET B.M 4, 273°02 35" 4, 213'0237" OF WHEEL HOUSE TOP

RAYMOND C. IMPASTATO PROFESSIONAL LAND SURVEYOR JOB: ____FERDINAND R. HASSLER

M286 SWATH

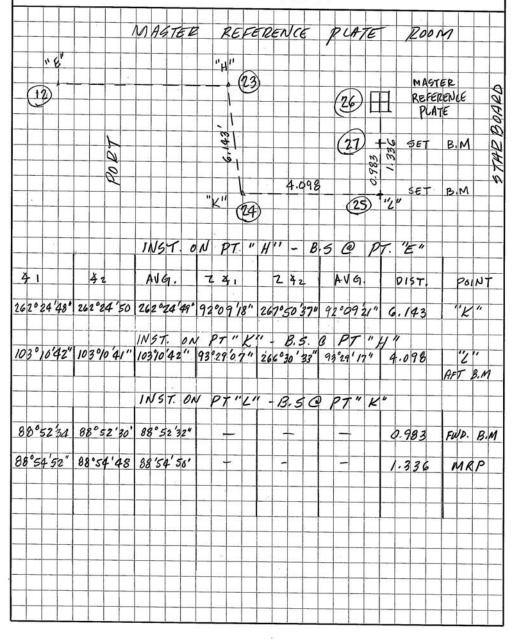
PASCAGOULA, MISSISSIPPI

139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 FIELD CREW: R.I., E.K., J. M. & B. K.

CALCULATED BY: R. IMPASTATO

DATE: 7-18-09 SHEET NO.: 10

SCALE: 1" = NONE



JOB: FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI 139 RANCH ROAD FIELD CREW: R.I., E.K., J. M. & B. K. SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO: 11 SCALE: 1" - NONE 1-26-09 STA HI ELEV DESCRIPTION 0.000 MASTER REFERENCE PLATE 1.300 1.300 1.461 -0.161 FWD B.M -0.162 1.461 -0.161 AFT B.M PT"H" -0.162 1.429 -0.129 -0.130 1.432 -0.132 T. P. 1 1.467 1.335 0.440 0.895 T. P. 2 0. 414 1.309 0.392 0.917 T.P. 3 TOP OF RAKE -8.118 -7.201 1.357 -8.558 PT"B" 1.352 -7.206 -8.122 0.916 T.P. 3 0.365 1.281 0387 0894 TP. 2 0.429 1.323 1,456 -0.133 T.R. 1.429 1.296 1.427 -0.131 1.459 -0.163 1.459 -0.163 PT "H" AFT B.M. FWD B.M. 1.297 -0.001 M. R. P.

JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO: 12 SCALE: 1" = NONE 7-26-09 STA BS-HI ELEV DESCRIPTION 0.917 T.R. 3 TOP OF RAIL 0.427 1.344 -1.207 2.551 T.P. 4 EDGE DEDECK (BRIDGE WING) 3,980 6.531 1.437 5.094 STED B.M. 1.442 5.089 MID B.M. TOP OF WHEEL HOUSE 11 11 11 1.443 5.088 PORT B.M. 1.387 6.415 1.386 5.089 MIO B.M 1.381 5.094 578D, B.M 3 923 2.552 7. P. 4 -1.228 1.324 0.406 0.918 (0.001) T.P.3

JOB: ___ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO: 13 SCALE: 1" = NONE 7-26-09 BRIDGE DECK SET B.M. 22) SET B.M. 1.491 1.877 (28) PT"E" (12)

JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO.: 14 SCALE: 1" - NONE 7-26-09 BACK DECK (46) SET B.M. (12) 2 900 4 ZIM SET B.M. 7.082 7.086 SET B.M.

JOB: ___ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI 139 RANCH ROAD FIELD CREW: R.I., E.K., J. M. & B. K. SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO.: 15 SCALE: 1" = NONE 7-26-09 STA BS HI ELEV DESCRIPTION 2.551 T.P. 4 EDGE OF DECK (BRIDGE WING) 1.385 3.936 1.445 2 491 GTARBORED B.M. BRIDGE WING (PORT SIDE) 1.429 2.507 PORT B.M. (BRIDGE WING (PORT SIDE) 1.411 3.918 1.427 2.491 STARBOARD B.M. 1.367 2551 T.P.4 0 000 MASTER PEFERENCE PLATE 1.344 1.344 1.375 -0.031 T. P. 5 1.399 1.368 1.508 -0.140 FWD. B.M BACK DECK 1.496 -0.128 AFT MID B.M. BACK DECK 1.497 -0.129 STAKBOARD B.M. BACK DECK 1.492 -0.124 PORT B.M. BACK DECK 1.466 1.342 1.471 -0.129 ST. B.M. 1.470 -0.128 AFT MID B.M. 1.482 -0.140 FWD B.M. 1.373 -0.031 T.P. S 1.383 1.352 1.352 0 000 MASTER REFERENCE PLATE

JOB: ____ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI 139 RANCH ROAD FIELD CREW: R.I., E.K., J. M. & B. K. SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO: 16 SCALE: 1" - NONE 7-26-09 c" (2) A' 7.990 M PORT (49) STARBOARD IMU IMU 50 (51) | 1NST ON PT"A" - B. S. Q PT "C" | Y. 1 | Y 2 | A VG | Z X 1 | Z X 2 | A VG | PIST | 246° 56' 46 246° 56' 42" 246° 56' 44° 91° 15 05 768 44' 45 91° 15' 10" 8.348 | 110° 36' 30" 110° 36' 38" 110° 36' 34° 90° 16' 21° 269° 43' 51" 90° 16' 15" 7.990' "M" INST. ON PY. "M" - B.S. @ PT"A" 36021'23" 36021'27" 36021'25" 91019'18" 268040'45" 91019'17" 1.395 IMU PORT INST. ON PT "N" - B.S. @ PT"A" 3/7019'00 31798 540 317018 59" 96 08 50" 2630 50 58" 96008 56" 1,624 IMU STARBORD

JOB: ___ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: __R. IMPASTATO DATE: 7-18-09 SHEET NO.: 17 SCALE: 1" = NONE 7-26-09 STA BS HI ELEV DESCRIPTION -8.558 PT"B" 1.092 -7.466 -0.357 -7.109 T.P. 6 PORT 510E -0.349 -7.458 PT "B" 1.100 -8.558 1.100 -7.458 -0.361 -7.097 T. P. 7 STARBOARD SIDE -0.346 7.443 1.116 -8.559 (0.001) T.P.7 -7.097 1.377 -5.720 0.104 -5.824 IMU STARBOARD 0.103 -5.721 1.376 7.097 T.P. 7 T.P. 6 7.109 1.341 -5.768 0.070 -5.838 IMU PORT (OLD) 0.087 -5.75/ 1.358 -7,109 T. P. 6

JOB: FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO.: 18 SCALE: 1" - NONE C" 6 (41) (43) PONCH MARK PUNCH MARK WITH WELD BEAD 6.628 WITH WELD BOAD 6.394 6.572 PUNCH MAKE PONCH MARK WITH WELD BEAD WITH WELD BEND (44) (4-2) INSTRUMENT OF PT "A" - B.S. @ PT "C" AVG. ZXI ¥ 2 AVG 742 DIST POINT 76°51'25' 89°41'15" 270°18'38" 89°41'19' 6.586 85°40'34' 89°44'20" 278°15'48' 89°44'14' 6.586 278°43'21' 89°50'54" 270°00'50' 89°59'02' 6.672 272°26'57' 90°00'48" 269°59'21" 90°00'43" 6.572 7605122" 7605128" 41 85040 36" 85040 32" 42 279°43'20" 279°43'21" 272°26'53' 272°27'01' 43 44

RAYMOND C. IMPASTATO
PROFESSIONAL
LAND SURVEYOR

JOB: FERDINAND R. HASSLER

M286 SWATH

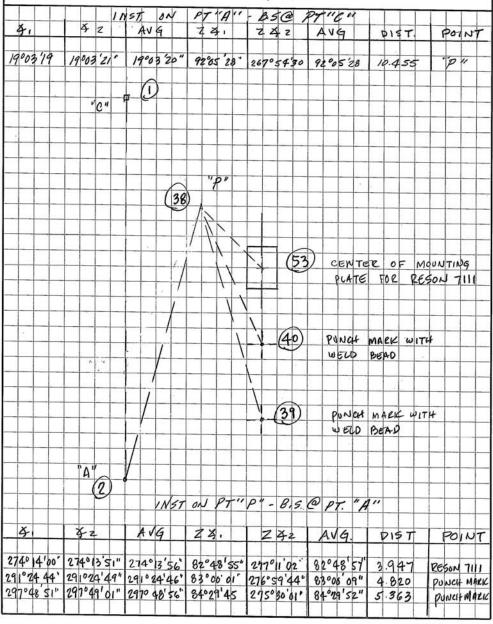
PASCAGOULA, MISSISSIPPI

139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 FIELD CREW: R.I., E.K., J. M. & B. K.

CALCULATED BY: R. IMPASTATO

SCALE: 1" - NONE

DATE: 7-18-09 SHEET NO.: 19



JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO.: 20 SCALE: 1" = NONE 7-26-09 BENCH MARKS 1MU ROOM SIDE PONTOON PORT 3.629 AZIMUTH = 90°00'00" STARBOARD B.M. 1.600 PORT B.M. 3.300 67 ×= 6.282 (66) X= 6-282 1.429 IMU Y = -5.000 (DRIGINAL LOCATION) - 9.900 X : 5.900 4=-6.871

JOB: FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO: 2/ SCALE: 1" = NONE 7-26-09 BENCH MARKS IMU ROOM STAPPONED SIDE DONTOON 3.374 1.531 1.545 PORT X=6.633 B.M. Y= 2.450 3.672 STARBOARD B.M. 3.377 X=6633 1.105 4 = 8.577 VAZIM = 90'00'00" (52) 1.612 MU (ORIGINAL LOCATION) X= 5.932 1: 5.824 5.434

JOB: FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO .: 22 SCALE: 1" = NONE 7-26-09 STA BS HI ELEV DESCRIPTION (DEIGINAL LOCATION) - 5.838 IMU PORT SIDE PONTOON 0.268 -5.570 0.220 -5.790 PORT BIM. 0,289 -5.859 STARBOARD B.M 0.296 -5.560 0.227 -5.790 PORT B.M. MU (ORIGINAL COCATION) STARBOARD SIDE B.M. -5.824 IMO 0.227 -5.597 0.250 -5.847 PORT B.M 0.200 -5.799 STARBOARD B.M. 0. 215 -5.582 0.266 -5.848 PORT B.M. 0.242 -5 824 INU

JOB: ___ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO.: 23 SCALE: 1" = NONE 7-26-09 PRESENT LOCATION OF IMU 0. M. 0.000 PORT AZIMOTH = 9000000" STARBOARD B.M. 3.322 3.323 IMU (70) 1.463 X= 6.282 X= 5.870 Y:-6.859 4 = -5.000

JOB: __ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL. LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO.: 24 SCALE: 1" = NONE 7-26-09 PRESENT COCATION OF IMU GTARBOARD SIDE PONTOON 3.371 PORT STARBOARD B.M. B.M. 3.382 0.470 X = 6.633 Y= 3.672 IMU X= 5.894 1.656 4:5.387

JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO.: 25 SCALE: 1" = NONE 7-26-09 STA HI ELEV DESCRIPTION PRESENT LOCATION PORT SIDE PONTOON INU -5.859 STACBOALD B.M. 0.184 -5.675 0.091 -5 766 INDO 0.103 -5.663 0.196 .5.859 STARBOARD B.M PRESENT LOCATION STARBOARD SIDE PONTOON IMU -5.847 PORT B.M. 0.236 -5.611 IMU 0.142 -5.753 0.158 -5.595 0-252 -5.847 BET B.M.

JOB: FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO.: 26 SCALE: 1" = NONE 7-26-09 PT. "A" - B.S. @ PT"C' INST. ON 42 AVG POINT DIST 117020'06" 117020 10" 117020'08 90054' 43" 26905 1" 90054 46" 40 " PUNCH MARK 33 WITH WELD BEAD STARBOARD PONTOON 6.758 7125 2 MACHINE SUPPACE (\$5) PUNCH MARK WITH (34) WELD BEAD INST. ON PT. "Q" + B.S. @ PT. 242 AVG AUG 124. X. DIST POINT 150°50'00" 150°50' 13" 150°50' 09 68°11'10" 291°48'44" 68°11'13" 1.426 PORT SIDE OF 7125 103°05'47" 103°04'00" 103°05'54" 77°48'15" 282°11'54 77°48'11" 2,175 PUNCH MARK PONEHMARK

JOB: ___ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO.: 27 SCALE: 1" = NONE 7-26-09 ON PT"A" - B.S. Q PT Z X1 Z X2 AVG 4. 42 AVG DIST POINT 242 20 59 242 20 59 242 20 59 242 20 59 91017 11" 268 42 49 91017 11 7.049 "E" PUNCY MARK WITH WELP BEAD -7.049 PORT POUTOON MACHINE SURFACE (57) 0.062 PONCH MARK WITH WELD BEAD INST. ON PT'R"-B.S. @ PT "A" 4.1 42 AV4 24 242 AVG DIST POINT 20704109 20704421 20704415" 64049 01 2950 023" 64049 19" 1.417 STARB, SIDE 7125 256°06'99' 256°06'49" 256°06'44 75°35'51" 294°23"58" 75°35'57" 2.165 DUNCHMARK PUNCH MARK

JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL. LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO.: 28 SCALE: 1" - NONE 7-26-09 STA BS HI ELEV DESCRIPTION PT"B" -8.558 1.234 -7.324 -0.166-7.158 AFT R.M. 7125 -0.239-7.085 7125 PORTSIDE -0.242-7.082 7125 STARB. SIDE PORT PONTOON -0.242-7.082
-0.174-7.150 FWD P.M. 7125
-0.158-7.166 AFT P.M. (-7.161) """
-0.157-7.167 FWD P.M. (-7.168) """
-0.494-6.830 RESON 7111 STARBOARD PONTOON
-0.586-6.138 FWD. P.M. 7111"
-0.513-6.811 AFT -0.178 -7.146 FWD R.M. 7125 -0.247-7.017 7125 PORT 51DE -0.251-7.073 7125 STARB. 51DE 11 11 " .. -0.172 -7.152 AFT P.M. 7125 " -0.186 -7.330 -0.265 -7.073 7/25 STACE. SIDE -0.26/-7.077 7/25 DOET SIDE -0.19/-7.147 FWD P.M 7/25 -0.188-7.150 AFT P.M. FB " 11 11 AFT P.M. FB FWO P.ND. FB " " 0.192 -7.146 1 " -0.526-6.812 AFT P.M. 7111 K FWO P.M. 7111 -0.600 -6.738 10 " RESON 7111 FAID P.M. FB AFT P.M. FB -0.507 -6.831 11 1. -0.19 -7.169 -0.170 -7.168 PORT DON TOON 11 11 -0 187 -7.151 FWD PM. 7125 10 ,, -0.256-7.082 7125 STARB. 51DE 11 " -0.252 -7.086 7/25 PORT SIDE -0.179 -7.159 AFT P.M. 7/25 1,220 -8558 PT "B" "

JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO.: 29 SCALE: 1" = NONE 7-26-09 ADCP STARBOARD DONTOON A" 6.763 (30) PUNCH MARK WITH WELD BEAD ADCP STARBOARD PONTOON DUNCH MARK WITH WELD BEAD \$ 2 | AVG | Z X , | Z X Z | AVG DIST POINT 109011 49" 189 91 59" 109 9153" 87003 07" 27205652 87003 07 6. 763 FWD POWEH MARK 119011/11" 119011/4" 119011/13" 87020 24 272 39 40 87020 22" 7.378 POWEH MARK

JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO.: 38 SCALE: 1" - NONE 7-26-09 STA BS-HI ELEV DESCRIPTION -7.152 AFT P.M. 7125 STARBOARD PONTOON 0.279 -6873 0.256 -7.129 AFT PUNCH MARK ADOP 6.263 -7.136 FWD PUNCH MARK ADOP 0.297 -6.839 0.290 -7.129 AFT RUNCH MARK ADER -7.152 AFT P.M. 7125 STAKEGARD PONTOON

JOB: FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL. LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 718-09 SHEET NO .: 31 SCALE: 1" - NONE 7-26-09 (1) NBOARD DRAFI MARKS 59 FRAME 4 FRAME 4 (2) (60) FRAME 46 (61) FRAME 46 INST. ON PT"A" - B.S. @ PT"O" 42 AVG 74. 242 AVG DIST POINT 41°11'21" 41°11'05" 41°11'13" 61°42'40" 298°1723" 61°42'49" 10.097
316°12'03" 316°12'18" 316'12'07" 62°15'60 297°45'04 62°14'58 10.240 FRAMES FRAME 4 162°46'43 162°46'44" 162°46'44 77°38 18" 292°21'40" 71°38'19" 22.023 196°29'33" 196°29'37" 196°29 30" 72°38'32" 282°21'26" 71°38'33" 22.092 FRAME 46 FRAME AL

FERDINAND R. HASSLER JOB: ____ RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 7-18-09 SHEET NO.: 32 SCALE: 1" = NONE 1-26-09 EL= -2.531 FRAME 4 STARBOARD INBOARD 102 900 4. HI = 7.316 PT'B' -8.558 EL = - 2.548. FRAME 4 PORT 242 900 PT"B" -8.558 HI=-7.316 EL= -2 601 FRAME 46 STARBOARD INBOARD 22.023 202 900 PT"B" HI = -7.3/6 -8.558 EL= - 2.588 FRAME 46 NEGARD 202 900 PT"B" HI = -7.316 - 8.558

RAYMOND C. IMPASTATO PROFESSIONAL LAND SURVEYOR

JOB: FERDINAND R. HASSLER

M286 SWATH

PASCAGOULA, MISSISSIPPI

139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955

SCALE: 1" = NONE

FIELD CREW: R.I., E.K., J. M. & B. K. CALCULATED BY: R. IMPASTATO

7-26-09

DATE: 7-18-09 SHEET NO.: 33

OUTBOARD DEAFT MARKS (64) 62) 19.862 D FRAME 4 24:196 - (65) FRAME 40 INSTRUMPENT ON PT"D"-B.S@PT"C" 2 年, AVG 2 4 2 AVG DIST POINT 292015 44 292015 53 " 2920 15 49" 76011 28" 2836 48 34 7601 27" 19,862 FRAME 4 STARBOARD 243°35'26" 243°35'34" 243°35'30" 82°33'53" 277°26'67" 82°33'53" 36. 126 FRAME 46 STARBOARD 30°38'48" 30°38'49" 30°38'49" 101°49'55" 258°10"01" 101°49'57" 24145 FRAME 4 PORT 100000 48 100000 49 10000 49 10103722" 25801242" 101037 20" 24.720 FRAME46 POPET

JOB: FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW: R.I., E.K., J. M. & B. K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 7-18-09 SHEET NO.: 34 SCALE: 1" = NONE 7-26-09 ELEU . = - 2.531 FRAME 4 STARBOADD OUTBOARD 200 ELEV = -7.146 HI= - 7.272 PT"D" EL=-2,598 FRAME 46 STARBIARD OUTBOARD el= -7.146 900 HI = 7.272 PT"D" ZX1 929805 FRANC 4 Z x 2 267042'02" PORT AVG = 92°18'01" 4.951 23.079 HI= 2.397 EC=-0,130 24.145 EL=-2.554 PT"H" PT"E" Z 4, 92°18'05° Z 42 267°42'02" FRAME 46 PORT AUG .= 92018'01 OUTBOALD 23.079 HI= 2.397 24.720 EL= -0.130 EL= 2.583

JOB: ___ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI FIELD CREW:____ R.I. & E.K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 11-4-09 SHEET NO.: 1 SCALE: 1" = NONE TOP OF WHEEL HOUSE MID B.M. PORT STB. B.M. BM INSTRUMENT ON STB. B.M B.50 PORT B.M. 2A = 103 4450 HOR > AZIMUTH BOLT A LOWER GPS ANTENNAE 3100 52 34" 3100 52 424 AVG 310° 52' 38" 2269 52 38 BOLT & UPPER GAS ANTENNAL 3070 14 02" 3070 14 23 30701413" 21701413" AVG INSTRUMENT ON MID B.M B. S @ PORT B.M. ZA - 1150 58'30" 183°53'33" AZIMUTH ZENITH & & LOWER GRS ANTENNAE 790 53 500 283053 48" AVG 283°53 43 193° 53'43" 770531354 BOLT & UPPER GP. S ANTENNAE 297028 25" 282918 38 282181 401 AUG 282 918 39 192 918 39" 62031 354 NTENNAES MOTE! O. 022 FROM BOTTOM OF BOLT TO DUTTOM

JOB: ____FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL PASCAGOULA, MISSISSIPPI LAND SURVEYOR FIELD CREW: R.I. & E.K. 139 RANCH ROAD SLIDELL, LOUISIANA 70460 CALCULATED BY: R. IMPASTATO PHONE NO: (985) 774-1955 DATE: 11-4)-09 SHEET NO.: 2 SCALE: 1" - NONE House WHEEL 700 OF (21) MID B.M. STAR BOARD PORT B.M. B.M. 20) ON PORT B.M. - B.S. @ STARBINARD B.M. INSTRUMENT HORIZ 3 AZIMOTH BOLT & LOWER GPS ANTENNAE 490 34 47. 49034 430 49034 45" 139034 45 AVG. BOUT & UPPER GRS ANTENNIE 53024'46" 53024'50" AVG. 53°24 48" 143°24 48 B.S @ PORT B.M. Z. 4 = 115958'30" INSTRUMENT ON MID B.M. AZIMUTH ZENITH \$ HORIZ. 4 BOLT & LOWER GPS ANTENMAG 17046'38" 256941'23" 282º14'00" 256941 18" 256041'21" 166 04121 77046 19" AUG 258030'00" 62024 45" BOLT & UPPER GPS ANTENNAE 2970 35'00" 258929 '51" 168929 '51" 62024 '53" AVG GTARBOARD GPS ANTENNAES

RAYMOND C. IMPASTATO PROFESSIONAL LAND SURVEYOR

JOB: ____FERDINAND R. HASSLER M286 SWATH

PASCAGOULA, MISSISSIPPI

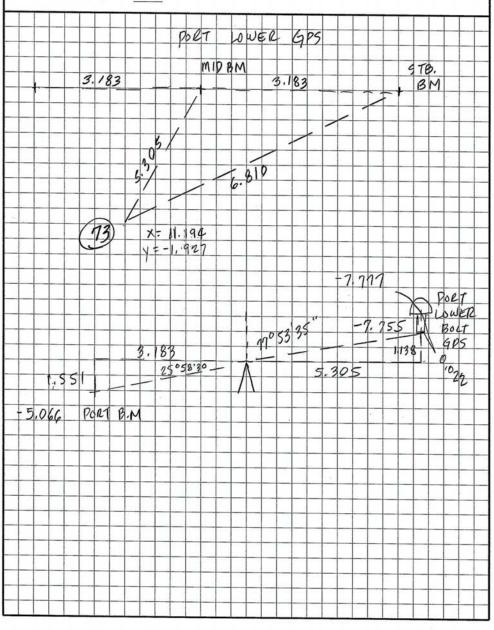
139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955

FIELD CREW:____ R.I. & E.K.

CALCULATED BY: R. IMPASTATO

DATE: 11-4-09 SHEET NO.: 3

SCALE: 1" = NONE



JOB: ____ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI 139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 FIELD CREW:____ R.I. & E.K. CALCULATED BY: R. IMPASTATO DATE: 11-4-09 SHEET NO.: 4 SCALE: 1" = NONE UPPER PORT STB MID BM BIM BM 3.183 3.183 X= 10.468 -9.766 03135 -9.744 3.183 25958'30 6.013 -5.066

RAYMOND C. IMPASTATO PROFESSIONAL LAND SURVEYOR JOB: FERDINAND R. HASSLER

M286 SWATH

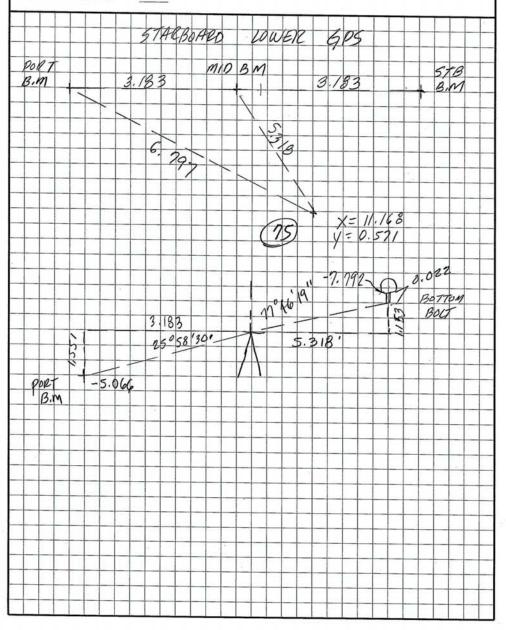
PASCAGOULA, MISSISSIPPI

139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 FIELD CREW: R.I. & E.K.

CALCULATED BY: R. IMPASTATO

DATE: 11-4-09 SHEET NO.: 5

SCALE: 1" - NONE



RAYMOND C. IMPASTATO PROFESSIONAL LAND SURVEYOR

JOB: ____FERDINAND R. HASSLER

M286 SWATH

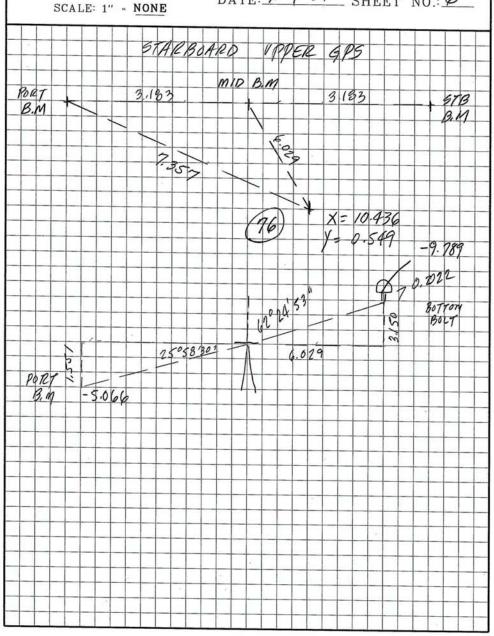
PASCAGOULA, MISSISSIPPI

139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955

FIELD CREW: R.I. & E.K.

CALCULATED BY: R. IMPASTATO

DATE: 11-4-69 SHEET NO.: 6



JOB: ___ FERDINAND R. HASSLER RAYMOND C. IMPASTATO M286 SWATH PROFESSIONAL LAND SURVEYOR PASCAGOULA, MISSISSIPPI 139 RANCH ROAD FIELD CREW: R.I. & E.K. SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 CALCULATED BY: R. IMPASTATO DATE: 11-4-09 SHEET NO.: 7 SCALE: 1" - NONE BACK DECK DORT STARBOARD B.M. B.M. INSTRUMENT ON STARBOARD B.M. BS. @ PORT B.N. Z.A: 96°53'06"

BOTTOM OF CENTER BLOCK 318°17'00"

73°49'25" 4 BOTTOM OF CENTER BLOCK 3/8'16'48" 286010 30. A16 31801654 228 1654 73 49 28" B.M. - B.S. STARBURD BIM. INSTRUMENT ON PORT & BOTTOM OF CENTER BLOCK 41°58 22" 41058 069 41058 14" 13195814 AUG. FRAME BLOCK (BOTTONA)

RAYMOND C. IMPASTATO PROFESSIONAL LAND SURVEYOR

JOB: ____FERDINAND R. HASSLER

M286 SWATH

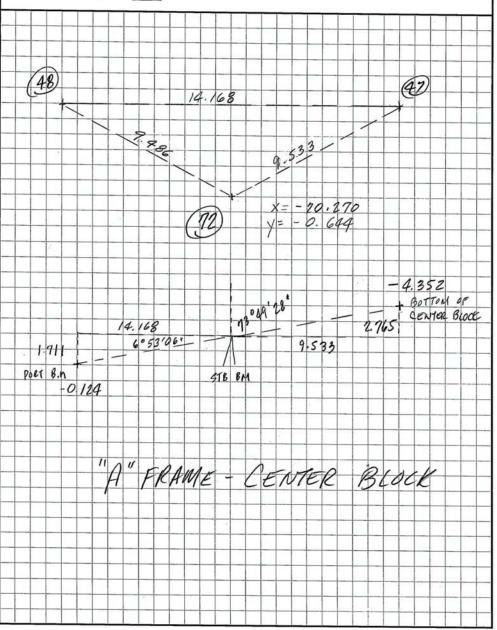
PASCAGOULA, MISSISSIPPI

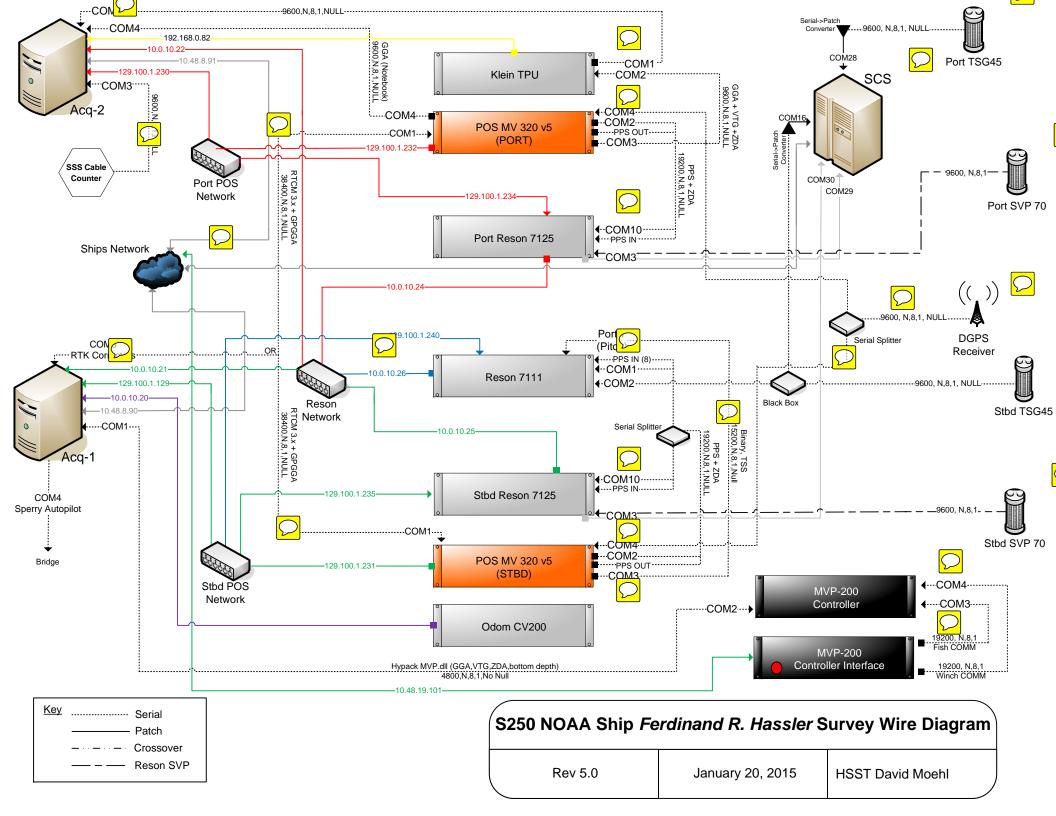
139 RANCH ROAD SLIDELL, LOUISIANA 70460 PHONE NO: (985) 774-1955 FIELD CREW: R.I. & E.K.

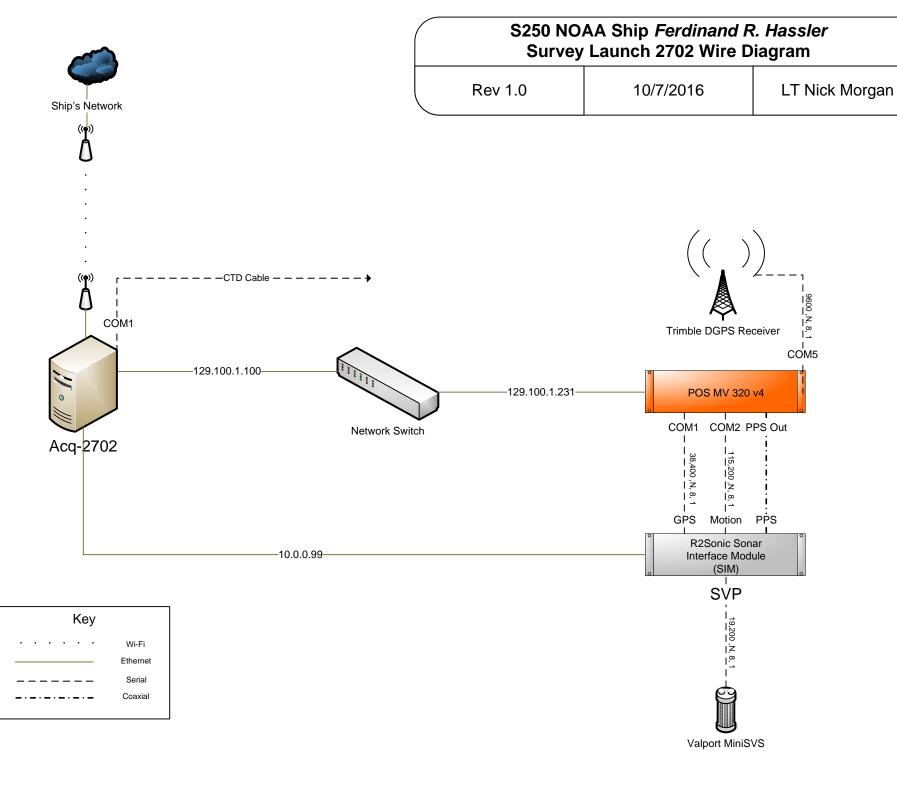
CALCULATED BY: R. IMPASTATO

DATE: 11-4-09 SHEET NO.: 8

SCALE: 1" - NONE







U.S. Department of Commerce

National Oceanic & Atmospheric Administration National Ocean Service National Geodetic Survey Field Operations Branch

NOAA SHIP HASSLER POS ANTENNA and Component Spatial Relationship Survey Field Report

Kevin Jordan March, 2011



NOAA Ship Hassler POS Antenna and Spatial Relationship Survey

PURPOSE

The intention of this survey was to accurately position the relocated POS Antennas and Side Scan Sonar tow point.

PROJECT DETAILS

This survey was conducted on March 29, 2011 on Spring River Island in Pascagoula, MS. NGS was provided data from a previous survey that contained a complete point listing of all components as well as recoverable bench mark stations. The NOAA Ferdinand Hassler was in water causing some instability of the instrument and target reflectors. The tilt compensator had to be bypassed in order to take measurements.

INSTRUMENTATION

The TOPCON GPT 3000 Series Total Station was used to make all measurements.

A SECO 25 mm Mini Prism System configured to have a zero mm offset was used as target sighting and distance measurements.

SOFTWARE AND DATA COLLECTION

TDS Survey Pro Ver. 4.7.1

ForeSight DXM Ver. 3.2.2 was used for post processing.

PERSONNEL

Kevin Jordan NOAA/NOS/NGS/Field Operations Branch 757-441-5478

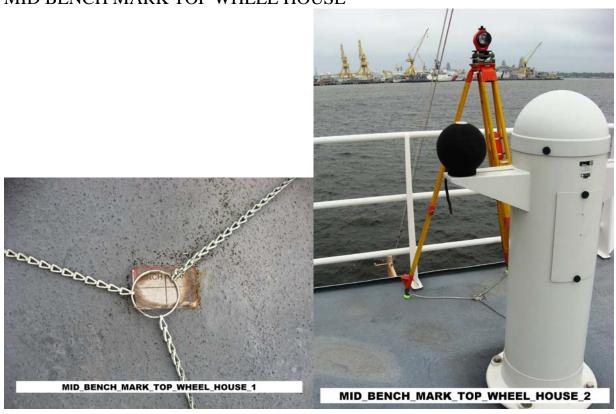
Doug Adams NOAA/NOS/NGS/Field Operations Branch 757-441-5480

NOAA Ship Hassler POS Antenna and Spatial Relationship Survey

SURVEY PROCEDURES

RECOVERED STATIONS

MID BENCH MARK TOP WHEEL HOUSE



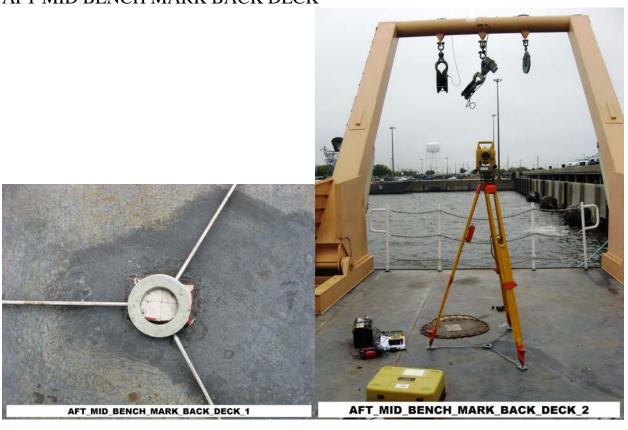
PORT BENCH MARK TOP WHEEL HOUSE



STARBOARD BENCH MARK TOP WHEEL HOUSE



AFT MID BENCH MARK BACK DECK



PORT BENCH MARK BACK DECK

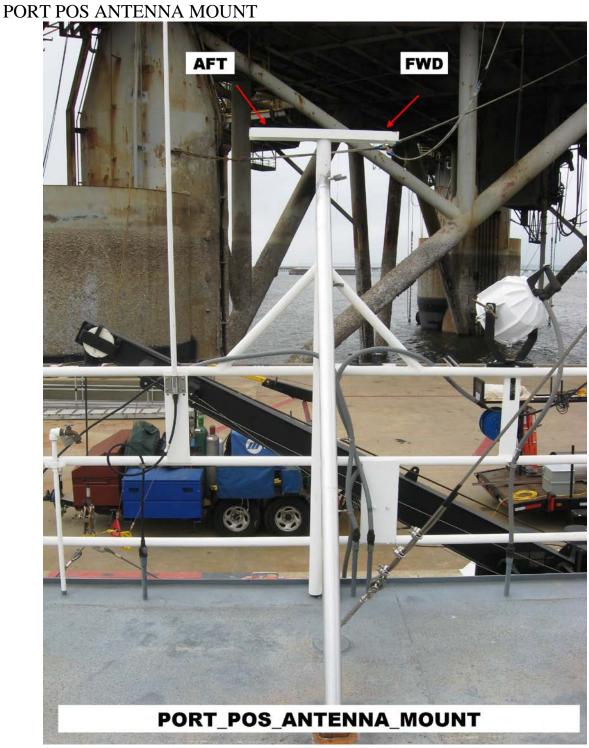


STARBOARD BENCH MARK BACK DECK



PORT BENCH MARK BRIDGE WING -NO PHOTOS OF THIS STATION

NEW FEATURES

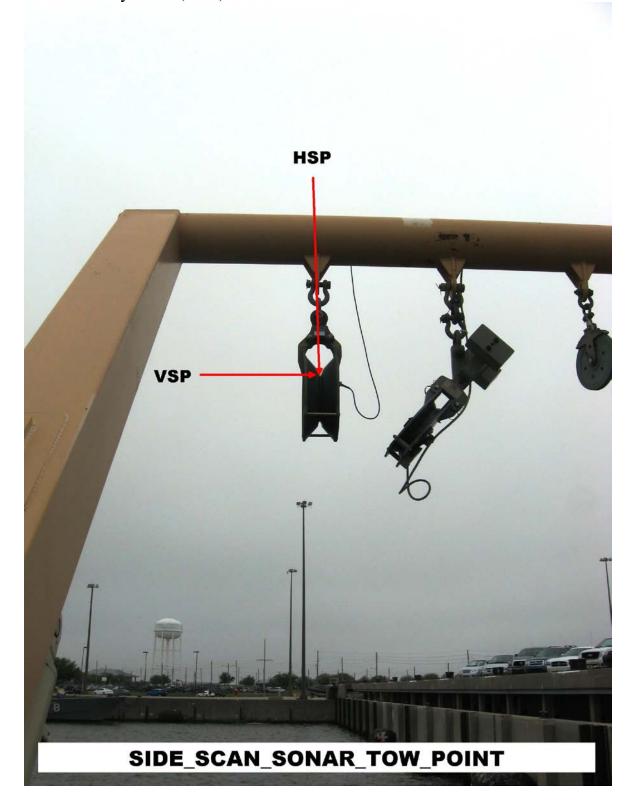


STARBOARD POS ANTENNA MOUNT



SIDE SCAN SONAR TOW POINT

- -Horizontal Survey Point (HSP)
- -Vertical Survey Point (VSP)



Setup #1

Using the coordinates from the previous survey, the field crew setup the theodolite on the MID BENCH MARK TOP WHEEL HOUSE and initialized on PORT BENCH MARK BRIDGE WING to obtain a starting azimuth. From this setup, we collected the four POS antenna mount locations:

PORT FWD ANTENNA PORT AFT ANTENNA STARBOARD FWD ANTENNA STARBOARD AFT ANTENNA

Positional checks were made to bench mark stations (see attached comparison report):

PORT BENCH MARK TOP WHEEL HOUSE STARBOARD BENCH MARK TOP WHEEL HOUSE PORT BENCH MARK BRIDGE WING

A temporary point (TP1) was established on the flying bridge near the stairs in order to collect the location of the SIDE SCAN SONAR TOW POINT.

Setup #2

The field crew setup on TP1 and initialized on the MID BENCH MARK TOP WHEEL HOUSE. From this setup, we collected:

SIDE SCAN SONAR TOW POINT

Positional checks were made to bench mark stations (see attached comparison report):

MID BENCH MARK TOP WHEEL HOUSE AFT MID BENCH MARK BACK DECK

Setup #3

The field crew setup on AFT MID BENCH MARK BACK DECK and initialized on TP1. Positional checks were made to bench mark stations (see attached comparison report):

PORT BENCH MARK BACK DECK STARBOARD BENCH MARK BACK DECK

DISCUSSION

All sensor/benchmark coordinates are contained in spreadsheets "NOAA SHIP HASSLER.xls"

The following table includes stations that were observed from more than one setup and for each, an inverse was computed to identify possible setup errors. Each station checked with favorable results.

OBSERVED to PUBLISHED COMPARISON (Units in Meters)			
NAME	Δ Northing	Δ Easting	△ Elevation
PORT BENCH MARK			
BRIDGE WING	-0.003	-0.008	0
PORT BENCH MARK			
TOP WHEEL HOUSE	0.030	-0.015	-0.003
STARBOARD BENCH			
MARK TOP WHEEL			
HOUSE	-0.026	0.010	-0.006
MID BENCH MARK			
TOP WHEEL HOUSE	0.015	0.002	-0.007
AFT MID BENCH			
MARK BACK DECK	-0.020	-0.030	0.011
PORT BENCH MARK			
BACK DECK	0.027	-0.002	-0.005
STARBOARD BENCH			
MARK BACK DECK	-0.015	0.018	-0.011

NEW GPS IMU - NGS 2012

IMU PORT				
DESCRIPTION	Χ	Υ	,	Z
STAR FWD ANT		2.722	9.162	-12.869
STAR AFT ANT		0.719	9.159	-12.895
PORT FWD ANT		2.712	1.05	-12.838
PORT AFT ANT		0.706	1.052	-12.853
STARBOARD BM TOP OF WHEEL HOUSE		10.482	9.395	-10.832
PORT BM TOP OF WHEEL HOUSE		10.482	3.034	-10.807
IMU STBD				
DESCRIPTION	Χ	Υ	,	Z
STAR FWD ANT		2.698	-3.084	-12.87
STAR AFT ANT		0.695	-3.087	-12.896
PORT FWD ANT		2.688	-11.196	-12.839
PORT AFT ANT		0.682	-11.194	-12.854
STARBOARD BM TOP OF WHEEL HOUSE		10.458	-2.851	-10.833
PORT BM TOP OF WHEEL HOUSE		10.458	-9.212	-10.808

PURPOSE

During the 2012 field season it was discovered that previously determined offsets from the original ship survey (Impastato, 2009) were in need of refinements. Results from 2012 post-processed POSPac derived offset solutions and ellipsoidally referenced leadline (ERLL) measurements showed a difference of approximately 20 centimeters in the vertical direction. This error was floating somewhere between the navigation GPS antennas, IMU and transducers. An attempt to track down this error was performed by *Ferdinand R. Hassler* personnel during the drydock period (April 2013) at Colonna's Shipyard in Norfolk, VA.

METHODS

A calibrated optical level was utilized to obtain a closed loop of elevations on important points and sensors around the ship. These elevations are with respect to gravity, in order to transform them to the ship's reference frame (SRF) an additional loop was obtained containing known benchmark elevations. From these benchmark elevations, values for pitch and roll were computed.

The primary sensor loop contained elevations from the starboard forward (primary) POS antenna on the flying bridge to a temporary benchmark (TBM) located on the drydock floor. From the TBM the loop proceeded to close by way of the port forward POS antenna and a final closing shot between the two antennas. This resulted in a closed loop with less than 5 millimeters of calculated misclosure.

The TBM on the drydock floor was utilized for spurs to survey sensors. Each individual sensor was treated separately and closed with a misclosure computed in the calculation spreadsheet. Both IMU's was measured using a level and tape measure from known point via the cable route (7125's and cables were removed for shipyard period). The 7125 elevations were computed from the averaged elevation readings on the inboard and outboard base of frame, accounting for the manufactured 4.5 degree tilt.

A total station was utilized to obtain elevations on all eight draft marks permanently fixed on the ship's hull. A reflectorless (laser) measurement device measured the vertical distance relative to a level gravimetric plane of the instrument.

To obtain results a couple of points were assumed:

- 1) The ship reference frame is accurately documented and defined from the Impastato ship survey. From the established benchmarks we are able to recreate the ship reference frame and apply pitch/roll calculations correctly.
- 2) Coordinates provided from Impastato are correct until proven otherwise. We use distances from the master reference block (MRB) for applying the pitch/roll offsets but strongly disagree with many of his z-coordinates. Also, along with #1; benchmarks utilized were crucial in recreating the ships reference frame.
- 3) Distances from the MRB for applying pitch/roll offsets is close enough to the center of gravity for the vessel to accurately apply pitch and roll.

4) The *Hassler* is located in a floating drydock which is subject to outside influences (e.g. tide, current, wind). However, the influences will affect both drydock and ship at the same rate and therefore be negligible.

RESULTS

Ship Reference Frame:

One of the primary issues with surveying a ship is orientating results obtained via outside reference frames (e.g gravity) into the SRF. During the Impastato ship survey, the surveyor defined the ship's master reference frame by measuring the pitch and roll of each pontoon and averaging these values. From this point he established various benchmarks located around the vessel; including the MRB, IMU plates, transducers and antennas. It is from this original survey benchmarks that enable us to transform coordinates relative to the SRF.

A level loop was run from a benchmark established by FH personnel on the bow of the *Hassler* to two benchmarks established by Impastato on the aft corners. From these three benchmarks we figured the difference of design slope to actual slope for both pitch and roll. The correction was corrected with the distance from the MRB, which is near but not located at the center of gravity (motion) for the vessel. This appears to be the same strategy utilized by Impastato during the original survey.

Ship Sensors:

Through careful analysis of the main level loop and the spurs to each individual sensor located on the pontoons, the following offsets were obtained.

Sensor	Corrected height from		Corrected height from	
Selisor	Antenna Base		IMU	
Port IMU (base of plate)	-12.990	Port		
Starboard IMU (base of plate)	-12.990	Starboard		
7125 Port (middle Rx)	-14.203	Port	-1.213	Port
7125 Starboard (middle Rx)	-14.212	Starboard	-1.222	Starboard
7111 (middle Rx)	-14.149	Starboard	-1.159	Starboard
Port VBES	-14.236	Starboard	-1.245	Starboard
Starboard VBES	-14.237	Starboard	-1.247	Starboard

Table 1: 2013 Sensor Offset Results

Comparisons were made from the 2013 sensor offset results with offsets used previously during the 2012 season. Two sets of z-offsets were used during the 2012 season; those obtained through Impastato ship survey coordinates and those obtained through post-processed POSPac results (supported through ERLL results). The results of the delta Z values (2013 minus 2012) are shown below in Table 2.

Sensor	Delta Z (m) (Impastato)	Delta Z (m) (Revised)	Notes and Analysis
Stbd IMU ->	0.225	-0.002	Revised measurements from POSPac and ERLL; 2013
Stbd APC	0		survey values strongly agree with revised results.
Port IMU ->	0.212	-0.019	Revised measurements from POSPac; 2013 survey values
Port APC	0.212	0.015	strongly agree with revised results.
Stbd IMU ->	-0.171	n/a	No revisions were made between the Stbd IMU and 7111
7111 Rx	0.171	11/ 4	Rx.
Stbd APC ->	0.176	n/a	No revisions were made between the Stbd APC and 7111
7111 Rx	0.170	ii/ a	Rx.
Stbd IMU ->	-0.103	-0.011	Revised measurements were never used; 2013 survey
7125S Rx	0.103	0.011	values show disagreement between IMU and sensor.
Stbd APC ->			Revised measurements from POSPac and ERLL; 2013
7125S Rx	0.244	-0.105	survey values show same disagreement between IMU and
71255 11			sensor.
Port IMU ->	-0.105	0.011	Revised measurements were never used; 2013 survey
7125P Rx	-0.103	0.011	values show disagreement between IMU and sensor.
Port APC ->	0.229	-0.123	Revised measurements from POSPac; 2013 survey values
7125P Rx	0.229	-0.123	show same disagreement between IMU and sensor.

Table 2: Delta Values between 2013 and 2012

Draft Marks:

Field elevation measurements were corrected using the same pitch and roll constants as stated earlier. For this calculation the X/Y locations of the draft marks were obtained from Impastato ship survey.

Forward Port	Forward Port	Forward Stbd	Forward Stbd
Outboard	Inboard	Inboard	Outboard
2.57	2.58	2.52	2.52
2.77	2.78	2.71	2.71
2.97	2.98	2.92	2.91
3.16	3.18	3.12	3.11
3.37	3.38	3.32	3.30
3.57	3.58	3.52	3.51
3.77	3.78	3.71	3.71
3.97	3.98	3.92	3.91
4.17	4.18	4.12	4.11
4.37	4.38	4.32	4.31
4.57	4.58	4.52	4.51

After Port	After Port	After Stbd	After Stbd
Outboard	Inboard	Inboard	Outboard
2.58	2.58	2.61	2.59
2.78	2.77	2.81	2.80
3.99	2.97	3.01	2.99
3.18	3.17	3.21	3.20
3.38	3.37	3.41	3.40
3.58	3.57	3.61	3.60
3.79	3.78	3.81	3.80
3.98	3.98	4.01	4.00
4.18	4.18	4.21	4.20
4.38	4.38	4.41	4.40
4.58	4.58	4.61	4.60

Table 3: Draft Mark Elevations relative from MRB (z is positive down)

Ship Traverse:

While in our possession the total station instrument was utilized for a ship traverse of existing benchmarks and POS antennas; as well as recreating the original SRF from the Impastato survey. Methods for this traverse were not as complete as was desired due to inadequate equipment and training of personnel. However, the calculations serve as additional checks against prior surveys and because an X/Y position was established on the TBM, help tie all previously discussed methods into a complete survey. More calculations are required on these acquired data once defined goals are obtained.

CONCLUSIONS

Vertical offsets from the level loop agree closely with offsets derived from post-processed POSPac solutions and ERLL calculations resulting in more confidence of both these methods. Hours were spent overlooking Impastato's original survey notes for any indication of possible errors or blunders but none were found. From these results it is safe to say that there were errors and possibly an overall miscommunication of exact reference points for measurement. *Ferdinand R. Hassler's* 2013 offsets will be defined from an in-depth analysis of these results and subsequent ERLL and reference surfaces to be acquired during Hydrographic Systems Readiness Review 2013.

Draft marks appear to near locations defined by Impastato as well as being generally level with respect to the ship reference frame; however, it appears that there is a disagreement with the forward starboard draft marks.

Offsets: POS MV

Measurement	Port IM	U to Fwd Por	t Ant
Coord. Sys.	Caris		POSMV
х	1.002		2.713
у	2.713		1.002
z	-12.920		-12.920
1			

Stbd IMU to Fwd Stbd Ant		
Caris		POSMV
-3.104		2.700
2.700		-3.104
-12.920		-12.920
`	,	

Stbd IMU to Heave		
Caris		POSMV
NA		NA
NA		NA
NA		NA

Stbd IMU to Heave		
Caris		POSMV
NA		NA
NA		NA
NA		NA

Stbd Ant Seperation			
(from calc)			
Scaler Distance	2.000		

Port Ant Sepera	ation
(from calc)	
Scaler Distance	2.00

Stbd Ant Seperation					
from GAMS Cal)					
caler Distance					

Port Ant Seperation (from GAMS Cal) Scaler Distance

POSMV offsets are derived from measurements by FH personnel made April 2012 after installation of new lever arm mounts and April 2013 during drydock.

Calculations

Port IMU	to Fwd Por	rt Ant	Stbd IMU	to Fwd Stb	d Ant
Adapter Plate to top of IMU	x y z	0.000 0.000 0.1236	Adapter Plate to top of IMU	x y z	0.000 0.000 0.1236
(from POSMV V5	User Guide)	(in POSMV)	(from POSMV V5	User Guide)	(in POSMV)
	x	0.000		x	0.000
Adapter Plate	y z	0.000 0.012 (in POSMV)	Adapter Plate	y z	0.000 0.012
from physical me	from physical measurement		from physical me	asurement	(in POSMV)
Center of Port IMU Plate to	x	2.713	Center of Stbd IMU Plate to	x	2.700
Fwd Port Antenna Base	y z	1.002 -12.990	Fwd Stbd Antenna Base	y z	-3.104 -12.990
(x/y from 2012 PO FH 2013 dry measurem	/dock	(in POSMV)	(x/y from 2012 PO: FH 2013 dry measureme	dock	(in POSMV)
Antenna base	x	0.000	Antenna base	x	0.000
to phase center	y z	0.000 -0.066	to phase center	y z	0.000 -0.066
(from Trimble	diagram)	(in POSMV)	(from Trimble	diagram)	(in POSMV)
Top of Port	IMU to Fwd	Port Ant	Top of Stbd	IMU to Fwd	Stbd Ant
Top of Port IMU to aft port ant phase center	y z	2.713 1.002 -12.920 (in POSMV)	Top of Stbd IMU to fwd port ant phase center	y z	2.700 -3.104 -12.920 (in POSMV)

PosPac Derived Offsets	
------------------------	--

Port IMU to Fwd Port Ant								
(from 2013 calculations)								
х	2.713							
У	1.002							
z	-12.920							

(from 2013 calculations) x 2.700	Stbd IMU to Fwd Stbd Ant						
x 2.700	(from 2013 calculations)						
	x 2.700						
у -3.104							
z -12.920							

(from PosPac calibration) average

Port	y	6.12
STBD	y	-6.12
x and z	ero	

I	Port IMU to Fwd Port Ant					
	(from PosPac calibration)					
	average					
ſ	х					
ı	У					
L	z					

^{*}calculated averages between multiple days

Ref to Center of Rotation

(Top of Stbd IMU to Center of Rotation)

-3.705 -6.033 -2.270

(from waterline) Added to Pos on DN285 2012

Offsets: Port 7125

Measurement	Port IMU to Port 7125 (MRU to Trans)		· · · · · · · · · · · · · · · · · · ·		Projector to Receiver		eiver
Coord. Sys.		Caris		Caris			Reson
Х		-1.244		-2.246			0.000
у		0.362		-2.351			-0.441
z		1.349		14.269			0.047

TILTED 4.5 degrees up to port
*Top of IMU is RP (Reference Pt)

⁽from Reson diagram, entered in Reson Hardware configuration)

Hysweep Offsets						
	Hypack					
Port IMU to Stbd	-1.244					
Port 7125 Fwd	0.362					
Vertical	3.780					

TILTED 4.5 degrees up to port (Hypack vertical is positive down from waterline.)

Offsets are derived from Impastato Centerline Survey (2010) and measurements by FH personnel made April 2012 after installation of new lever arm mounts and April 2013 during drydock.

Calculations

·	_										
Port IM	U to Po	rt 7125	Fwd Port	Ant to P	ort 7125	Reson Pr	ojector to	Receiver	Waterline	to Stbd 7	7125 RP
Top of IMU to	Х	0.000	Antenna Phase	Х	-1.002		Х	0.000	Port IMU RP	Х	-1.244
center of IMU	У	0.000	Center to IMU	У	-2.713	Tx RP	У	0.000	to Port 7125	У	0.362
Plate	Z	0.1356	Ref Pt	Z	12.920		Z	0.000	RP	Z	1.349
(from POSMV Guide)		(in CARIS)	(from POS MV ca tab)	alculation	(in CARIS)	(from Resor	n diagram)	(in Reson)	(from calcula	ations)	(in CARIS)
Port IMU	x	-1.244	D. A. HALL D.D. A.	Х	-1.244		х	0.000	T D	x	0.000
Plate to Port	у	0.362	Port IMU RP to Port 7125	у	0.362	Rx RP	у	0.441	Top Port IMU to Waterline	у	0.000
7125	Z	1.213		Z	1.349		Z	-0.047		Z	2.431
(x/y from Impa from 2013 dry		(in CARIS)	(x/y from Impastat 2013 drydo	,	(in CARIS)	(from Reson of 2013 dr	U	(in Reson)	(from waterline sp	oreadsheet)	(in Hypack)
Port IM	U to Poi	rt 7125	Fwd Port A	ant to Por	t 7125 RP	Reson Pr	ojector to	Receiver	Waterline	to Stbd 7	7125 RP
	Х	-1.244		Х	-2.246	•	Х	0.000		Х	-1.244
	У	0.362		У	-2.351		У	-0.441		У	0.362
	Z	1.349		Z	14.269		Z	0.047		Z	3.780
		(in CARIS)			(in CARIS)			(in Reson)			(in Hypack)

CALCULATION NOTES

Z calc includes 0.015 m from base to RP Impastato X/Y measurement locations unknown

0.102 from Reson diagram - Rx width

0.25 from 2013 drydock - Gap between Rx and Tx

0.28 from Reson diagram - Tx length

0.003656 4.5° tilt calculated from Tx diameter

0.046456 4.5° tilt calculated from Tx diameter

Offsets: Starboard 7125

Measurement	Stbd IMU to Stbd 7125 (MRU to Trans)		Fwd Stbd Ant to Stbd Trans)	7125 (Nav to	Reson Projector to	o Receiver
Coord. Sys.		Caris	, i	Caris	_	Reson
Х		1.424		4.528		0.000
у		0.380		-2.320		-0.437
Z		1.358		14.278		0.047
	THITCH AC January	4 411			// D !!	

TILTED 4.5 degrees up to stbd
*Top of IMU is RP (Reference Pt)

Hyswe	ep Offsets
	Hypack
Stbd IMU to Stbd	1.424
Stbd 7125 Fwd	0.380
Verti	cal 3.789

TILTED 4.5 degrees up to stbd (Hypack vertical is positive down from waterline.)

Offsets are derived from Impastato Centerline Survey (2010) and measurements by FH personnel made April 2012 after installation of new lever arm mounts and April 2013 during drydock.

Calculations

Stbd III	/IU to St	od 7125	Fwd Stbd	Ant to S	tbd 7125	Reson F	Projector to	Receiver	Waterlin	ne to Stbd	7125 RP
Top of IMU	Х	0.000	Antenna Phase	Х	3.104		Х	0.000	Stbd IMU RP	Х	1.424
to Center of	у	0.000	Center to IMU	у	-2.700	Tx RP	у	0.000	to Stbd 7125	У	0.380
IMU Plate	Z	0.1356	Ref Pt	Z	12.920		Z	0.000	RP	Z	1.358
(from POSMV Guide)		(in CARIS)	(from POS MV ca tab)	alculation	(in CARIS)	(from Resor	n diagram)	(in Reson)	(from calcul	ations)	(in CARIS)
	х	1.424	04 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	х	1.424		х	0.000	Top Stbd	Х	0.000
IMU Plate to Stbd 7125	У	0.380	Stbd IMU RP to Stbd 7125	у	0.380	Rx RP	у	0.437	IMU to	У	0.000
	Z	1.222		Z	1.358		Z	-0.047	Waterline	z	2.431
(x/y from Impa from 2013 dry	,	(in CARIS)	(x/y from Impastat 2013 drydo	,	(in CARIS)	(from Reson of 2013 dry	0	(in Reson)	(from waterline s	preadsheet)	(in Hypack)
Stbd IMU	J to Stbo	l 7125 RP	Fwd Stbd A	nt to Stb	d 7125 RP	Reson F	Projector to	Receiver	Waterlin	ne to Stbd	7125 RP
	Х	1.424		Х	4.528		Х	0.000		Χ	1.424
	У	0.380		У	-2.320		у	-0.437		у	0.380
	Z	1.358		Z	14.278		Z	0.047		Z	3.789
		(in CARIS)			(in CARIS)			(in Reson)			(in Hypack)

CALCULATION NOTES

Z calc includes 0.015 m from base to RP Impastato X/Y measurement locations unknown

0.102 from Reson diagram - Rx width

0.246 from 2013 drydock - Gap between Rx and Tx

0.28 from Reson diagram - Tx length

0.003656 4.5° tilt calculated from Tx diameter

0.046456 4.5° tilt calculated from Tx diameter

⁽from Reson diagram, entered in Reson Hardware configuration)

Offsets: Starboard 7111

Measurement	IMU to 7111 (MRU to Trans)		Fwd Stbd Ant to 7111 (Nav to Trans)		Reson Projector to	o Receiver	Hys	weep Offse	ets
Coord. Sys.	Caris			Caris			Reson			Hypack
х	1.203	3		4.307			0.000	Stbd IMU to	Stbd	1.203
у	11.60	3		8.908			-0.499	7111 RP	Fwd	11.608
z	0.97	7		13.897			-0.269		Vertical	3.408
					•	from Reson diagram,		(Hypack ve	rtical is posi	tive down

^{*}Top of IMU is RP (Reference Pt)

Reson Hardware configuration)

from waterline.)

(in Hypack)

Offsets are derived from Impastato Centerline Survey (2010) and measurements by FH personnel made April 2012 after installation of new lever arm mounts and April 2013 during drydock.

Calculation

s				•	'	•			·		
	MU to 71	11	Fwd Stb	d Ant to 7	111 RP	Reson I	Projector to	Receiver	Waterlin	e to 711	1 RP
Top of IMU to	х	0.000	Antenna Phase	х	3.104		Х	0.000		х	1.203
Center of IMU	у	0.000	Center to IMU	у	-2.700	Tx RP	у	0.000	Top Stbd IMU to 7111 RP	У	11.608
Plate	Z	0.1356	RP	Z	12.920		Z	0.000		Z	0.977
(from POSMV V5 L	Jser Guide)	(in CARIS)	(from POS MV calc	ulation tab)	(in CARIS)	(from Reso	n diagram)	(in Reson)	(from calculat	ions)	(in CARIS)
	x	1.203		х	1.203		x	0.000		х	0.000
IMU Plate to 7111 Rx Face	у	12.107	IMU RP to 7111 Acoustic RP	у	11.608	Rx RP	у	0.499	Top Stbd IMU to Waterline	У	0.000
7111 IX Tace	Z	1.159	Acoustic Ki	Z	0.977		Z	0.269	Waterinie	z	2.431
(x/y from Impasta diagram and 2013 from 2013 dry	drydock, z	(in CARIS)	(x/y from Impastato diagram, z from 201		(in CARIS)	(from Reson 2013 dr	•	(in Reson)	(from waterline spr	eadsheet)	(in Hypack)
7111 Rx Face to	X	0.000									
7111 Acoustic	у	-0.499									
RP	Z	-0.318									
(from Reson di	agram)	(in CARIS)									
Top of Stbd	IMU to 7	7111 RP	Fwd Stbd	Ant RP to	7111 RP	Reson I	Projector to	Receiver	Waterlin	e to 711	1 RP
-	Х	1.203		Х	4.307	-	Х	0.000		х	1.203
	у	11.608		У	8.908		У	-0.499		У	11.608
	Z	0.977		Z	13.897		Z	-0.269		Z	3.408

(in CARIS)

CALCULATION NOTES

1.203 from Impastato - CL IMU to CL Plate

11.77 from Impastato - CL IMU to CL Plate

0.05341 from Reson diagram - CL Plate to Mounting Bolt

0.434 from Reson diagram - Mounting Bolt to aft Tx

0.65 from Reson diagram - Tx overall length

0.125 from 2013 drydock - Gap between Tx and Rx

0.0982 from Reson diagram - Rx thickness

Sanity Check Physical measurement = 11.150 +/- 20 cm

> calc measurement = 11.228

> > -0.078

(in CARIS)

0.098 from Reson diagram - Tx diameter

(in Reson)

Offsets: Dual 7125 (HSX only)

(x/y from Impastato, Z from 2013 Drydock)

(x/y from Impastato, Z from 2013 (in CARIS) Drydock)

	Stbd IMU to Por	t 7125 (MRI	U to Trans) -	Stbd IMU t	o Stbd 7125	5 (MRU to	Fwd Stbd An	t to Port 7125	(Nav to	Fwd Stbd Ant	to Stbd 7	7125 (Nav to						
Measurement	5	Swath 1		Tra	ns) - Swath	2		Trans)			Trans)		Port 7125	Hysweep	Offsets	Stbd 7125	Hyswee	p Offsets
Coord. Sys.			Caris			Caris		(Caris			Caris			Hypack			Hypack
Х			-13.490			1.424			-10.386			4.528	Stbd IMU to S	tbd	-13.490	Stbd IMU to Stb	od	1.424
у			0.338			0.380			-2.362			-2.320	Port 7125 F	wd	0.338	Stbd 7125 Fw	d	0.380
. Z			1.314			1.358			14.234			14.278	V	ertical	3.745		rtical	3.789
	*Top of Stbd IMU	J is RP (Refe	erence Pt)										TILTED 4.5 d	egrees up	to port	TILTED 4.5 de	grees up	to stbd
	Tilted up 4.5 deg	rees up on b	ooth sides										(Hypack ver fron	tical is pos n waterline				
		Offsets a	are derived fr	om Impastato C	enterline Su	rvev (2010) and	I measurements h	v FH personne	el made An	oril 2012 after ins	tallation of	of new lever arm	mounts and Ar	oril 2013 d	uring drydocl	C .		
		0.10010 0	are derived in	om impactate c	ontonino ou		i ilioadai diliolita k					or more lover arm	mounto ana 7	7.111 E 0 1 0 G	aring aryacoi			
Calculations		0.10010	aro domed m	om impactate c		(=====	· mododromonio z	, F				01 110 W 10 V 01 U 111	mounto ana 7	J 2010 u	aring ary acci			
Calculations		IU to Port 7		'	MU to Stbd			d Ant to Port 7		Fwd Stbd			Waterline			Waterline	to Stbd	7125 RP
Calculations			125	'			Fwd Stbo		7125	Fwd Stbd					125 RP		to Stbd	7125 RP
Calculations	Stbd IM top of IMU toCenter of		125	Stbd II		7125	Fwd Stbd Ant		7125 3.104	Fwd Stbd Ant		bd 7125	Waterline Top Stbd IMU to Port	to Stbd 7	125 RP -13.490	Waterline Top Stbd IMU to Stbd		-
Calculations	Stbd IM top of IMU		0.000	Stbd III top of IMU to		7125 0.000	Fwd Stbo		7125 3.104	Fwd Stbd		3.104	Waterline Top Stbd	to Stbd 7	'125 RP -13.490	Waterline Top Stbd		1.424
Calculations	Stbd IM top of IMU toCenter of	IU to Port 7' x y z	0.000 0.000	Stbd II top of IMU to Center of IMU	MU to Stbd 7 X y z	7125 0.000 0.000	Fwd Stbd Ant	d Ant to Port 7 x y z	7125 3.104 -2.700	Fwd Stbd Ant	Ant to St x y z	3.104 -2.700	Waterline Top Stbd IMU to Port	x y z	125 RP -13.490 0.338	Waterline Top Stbd IMU to Stbd	x y z	1.424 0.380
Calculations	Stbd IMU top of IMU toCenter of Stbd IMU Plate	IU to Port 7' x y z	0.000 0.000 0.1356	Stbd III top of IMU to Center of IMU Plate (from POSMV V5	MU to Stbd 7 X y z	0.000 0.000 0.1356	Fwd Stbd Ant to Stbd IMU RP (from POS MV ca tab)	d Ant to Port 7 x y z	3.104 -2.700 12.920 n CARIS)	Fwd Stbd Ant to Stbd IMU RP (from POS MV cal tab)	Ant to St x y z	3.104 -2.700 12.920	Waterline Top Stbd IMU to Port 7125 RP	x y z	-13.490 0.338 1.314	Waterline Top Stbd IMU to Stbd 7125 RP	x y z	1.424 0.380 1.358
Calculations	Stbd IMU top of IMU toCenter of Stbd IMU Plate (from POSMV V5 U	IU to Port 7' x y z	0.000 0.000 0.1356 (in CARIS)	Stbd II top of IMU to Center of IMU Plate	MU to Stbd 7 X y z	0.000 0.000 0.1356 (in CARIS)	Fwd Stbd Ant to Stbd IMU RP	d Ant to Port 7 x y z	3.104 -2.700 12.920 n CARIS)	Fwd Stbd Ant to Stbd IMU RP	Ant to St x y z	3.104 -2.700 12.920 (in CARIS)	Waterline Top Stbd IMU to Port 7125 RP (from calculo	x y z cations)	-13.490 0.338 1.314 (in CARIS)	Waterline Top Stbd IMU to Stbd 7125 RP (from calculca	y z tions)	1.424 0.380 1.358 (in CARIS)

Stbd IMU to Port 7	125 RP	Stbd IMU to Stbd 71	25 RP	Fwd Stbd Ant to Po	rt 7125 RP	Fwd Stbd Ant to Stl	od 7125 RP	Waterline to Stbo	7125 RP	Waterline to Stb	d 7125 RP
Х	-13.490	Х	1.424	Х	-10.386	Х	4.528	Х	-13.490	х	1.424
у	0.338	у	0.380	у	-2.362	у	-2.320	у	0.338	у	0.380
Z	1.314	z	1.358	z	14.234	Z	14.278	Z	3.745	Z	3.789
	(in CARIS)		(in CARIS)		(in CARIS)		(in CARIS)		(in Hypack)		(in Hypack)

(in CARIS) (x/y from Impastato, Z from

2013 drydock)

(in CARIS)

Note: For dual acquisition 7125, the HSX file contains data from both 7125s but only POSMV data from the stbd POSMV. The port 7125 is swath 1 (beams 1-512) and the stbd 7125 is swath 2 (beams 513 to 1024).

(x/y from Impastato, Z from

2013 drydock)

(in CARIS) (x/y from Impastato, Z from 2013 (in CARIS)

Drydock)

-1.244 0.362 1.213

Offsets: ODOM Single Beam

4.620

1.383

(in CARIS)

У

Z

4.620

1.381

(in CARIS)

Measurement	Stbd II	/IU to Stb	d SB	Stbd II	MU to Po	ort SB	Fwd Stb	d Ant to S	Stbd SB	Fwd Stb	d Ant to	Port SB	Port 7125	Hyswee	p Offsets	Stbd 712	5 Hyswe	ep Offsets
Coord. Sys.			Caris			Caris			Caris			Caris			Hypack			Hypack
х			-0.455			-12.701			2.649			-9.597	Stbd IMU to S	tbd	-0.455	Stbd IMU to	Stbd	-12.701
У			4.620			4.620			1.920			1.920	Stbd SB F	wd	4.620	Port SB	wd	4.620
z			1.383			1.381			14.303			14.301	V	ertical	3.835	,	/ertical	3.861
-	(x/y from Impast		(in CARIS)	(x/y from Impast		(in CARIS)							TILTED 4.5 d	legrees	up to port	TILTED 4.5	degrees	up to stbd
Calculations	2013 dryc	lock)		2013 dryd	lock)								(Hypack vert from	tical is po n waterlii				
	Stbd II	/IU to Stb	d SB	Stbd II	MU to Po	ort SB	Fwd Stb	d Ant to S	Stbd SB	Fwd Stb	d Ant to	Port SB	Waterline	e to Stb	d SB RP	Waterli	ne to Po	t SB RP
_	top of IMU	Х	0.000	top of IMU	х	0.000	Fwd Stbd	Х	3.104	Fwd Stbd	х	3.104	Stbd IMU RP	х	-0.455	Stbd IMU RP	Х	-12.701
	to Center of	у	0.000	to Center of	у	0.000	Ant to Stbd	У	-2.700	Ant to Stbd	у	-2.700	to Stbd SB	У	4.620	to Port SB	у	4.620
	IMU Plate	Z	0.1356	IMU Plate	z	0.1356	IMU RP	Z	12.920	IMU RP	z	12.920	RP	z	1.383	RP	z	1.381
	(from POSMV Guide		(in CARIS)	(from POSMV Guide		(in CARIS)	(from POS MV tab)		(in CARIS)	(from POS MV tab)		(in CARIS)	(from calcul	ations)	(in CARIS)	(from calc	ulations)	(in CARIS)
	Stbd IMU	x	-0.455	Stbd IMU	x	-12.701		x	-0.455		x	-12.701	Top Stbd	x	0.000	Top Stbd	x	0.000
	Plate to	у	4.620	Plate to Port	у	4.620	Stbd IMU to Stbd SB	у	4.620	Stbd IMU to Port SB	у	4.620	IMU to	У	0.000	IMU to	у	0.000
	Stbd SB	Z	1.247	SB	z	1.245		z	1.383		z	1.381	Waterline	z	2.431	Waterline	z	2.431
	(x/y from Impast 2013 dryd		(in CARIS)	(x/y from Impast 2013 dryd		(in CARIS)	(x/y from Impas 2013 dry		(in CARIS)	(x/y from Impas 2013 dry		(in CARIS)	(from water spreadsh		(in Hypack)	(from wa spreads		(in Hypack)
	Stbd II	/IU to Stb		Stbd II	MU to St		Fwd Stbd A	Ant to Por		Fwd Stbd A	Ant to Sta		Waterline	to Stbd		Waterlin	e to Stbo	l 7125 RP
		Х	-0.455		х	-12.701		Х	2.649		х	-9.597		х	-0.455		X	-12.701

у

Z

1.920

14.303

(in CARIS)

1.920

14.301

(in CARIS)

у

Z

4.620

3.835

(in Hypack)

4.620

3.861

(in Hypack)

Offsets: Klein 5000

Measurement	Port IMU to Tow	Point
Coord. Sys.		Caris
Х		7.161
у		-26.032
Z		-9.347
		(in CARIS)

U.S. Department of Commerce

National Oceanic & Atmospheric Administration National Ocean Service National Geodetic Survey Field Operations Branch

> HASSLER LAUNCH 2702 Component Spatial Relationship Survey Field Report

> > Kevin Jordan June 16, 2015



PURPOSE

The intention of this survey was to accurately position the POS/MV IMU, GPS Antennas, Sonar Equipment, bench marks, and reference marks located on the 2702 Launch.

PROJECT DETAILS

This survey was conducted on June 16, 2015 at the Kittery Point Yacht Yard in Eliot, ME. The launch was placed jack stands to stabilize the launch during the survey.

INSTRUMENTATION

The TOPCON GPT 3000 Series Theodolite was used to position all points on the launch.

A SECO 25 mm Mini Prism System configured to have a zero mm offset was used as target sighting and distance measurements.

SOFTWARE AND DATA COLLECTION

TDS Survey Pro Ver. 4.7.1

ForeSight DXM Ver. 3.2.2 was used for post processing.

PERSONNEL

Kevin Jordan NOAA/NOS/NGS/Field Operations Branch 757-441-3603

Steve Atkins NOAA/NOS/NGS/Field Operations Branch 757-441-3603

Temporary Control

A network of temporary control was established at KPYY consisting or two marks set on the ground. One mark was 10 meters behind the boat and the other was 13 meters off the starboard side.

OBSERVED POINTS

AFT BENCHMARK



PORT BENCHMARK



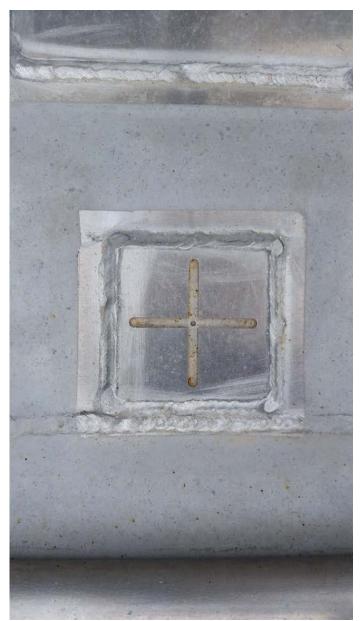
STARBOARD BENCHMARK





FWD BENCHMARK







NOTE: The four corners of the IMU were observed, but presented a challenge due to low overhead above the IMU and the rounded corners of the IMU. The best attempt was made using a plumb bob and prism.

Coordinates for these points are listed in the coordinate spreadsheet.

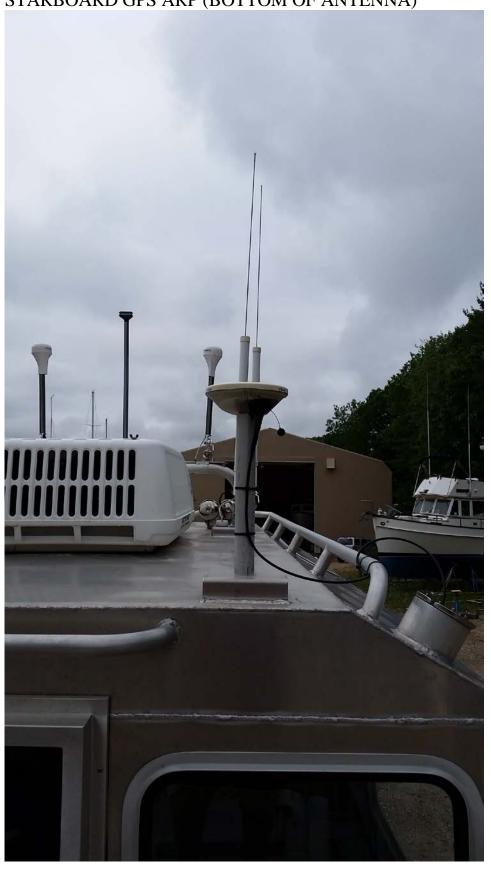
TRANSMITTER



RECEIVER



STARBOARD GPS ARP (BOTTOM OF ANTENNA)



PORT GPS ARP (BOTTOM OF ANTENNA)



R I (REFERENCE MARK ONE)





R III (REFERNCE MARK THREE) (NEAR IMU)



R IV (REFERENCE MARK FOUR)



PLUMB MARK OVER R IV



POST PROCESSING

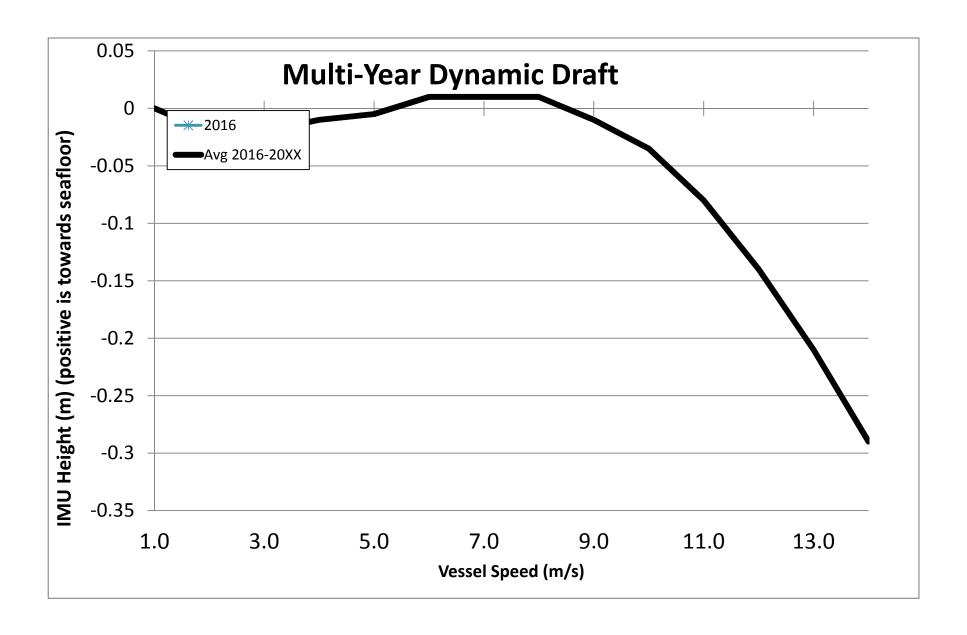
The collected points were referenced to Geodetic Coordinates and needed to be translated to reference the IMU as X=0, Y=0, Z=0. The azimuth from AFT BENCHMARK to FWD BENCHMARK needed to be oriented to 0° 00' 00". Post Processing was performed using ForeSight DXM to produce the following Coordinate Report. The X Axis is Positive toward the Bow. The Y Axis is positive toward the Starboard side. The Z Axis is positive downward.

DESCRIPTION	X (METERS)	Y (METERS)	Z (METERS)
IMU	0.000	0.000	0.000
BM AFT	-4.526	-0.005	-0.588
BM PORT	-1.146	-1.168	-0.759
BM STAR	-1.138	1.148	-0.765
PORT GPS ARP	-0.524	-0.522	-2.525
STAR GPS ARP	-2.033	0.560	-2.499
RI	-0.431	0.091	0.469
RII	-0.910	0.097	0.481
R III	0.191	-0.231	0.303
RIV	-1.268	-0.008	-2.040
PLUMB TAPE ON DECK	-1.260	-0.009	-0.112
IMU AFT STAR	-0.072	0.074	-0.002
IMU AFT PORT	-0.069	-0.076	-0.003
IMU FWD PORT	0.053	-0.084	-0.007
IMU FWD STAR	0.050	0.073	-0.007
BM FWD	1.674	-0.005	-0.988
TX	-0.633	0.231	0.403
RX	-0.833	0.237	0.407

2702 - Multi-Year Dynamic Draft Comparison

Speed (m/s)	2016-063	Average 2016- 20XX	Std Dev
0.0	0.00	0.00	0.00
0.5	-0.02	-0.02	0.00
1.0	-0.02	-0.02	0.00
1.5	-0.01	-0.01	0.00
2.0	-0.01	-0.01	0.00
2.5	0.01	0.01	0.00
3.0	0.01	0.01	0.00
3.5	0.01	0.01	0.00
4.0	-0.01	-0.01	0.00
4.5	-0.04	-0.04	0.00
5.0	-0.08	-0.08	0.00
5.5	-0.14	-0.14	0.00
6.0	-0.21	-0.21	0.00
6.5	-0.29	-0.29	0.00

^{***2011} and 2012 not used in multi-year average, prior to addition of buoyancy appendages***

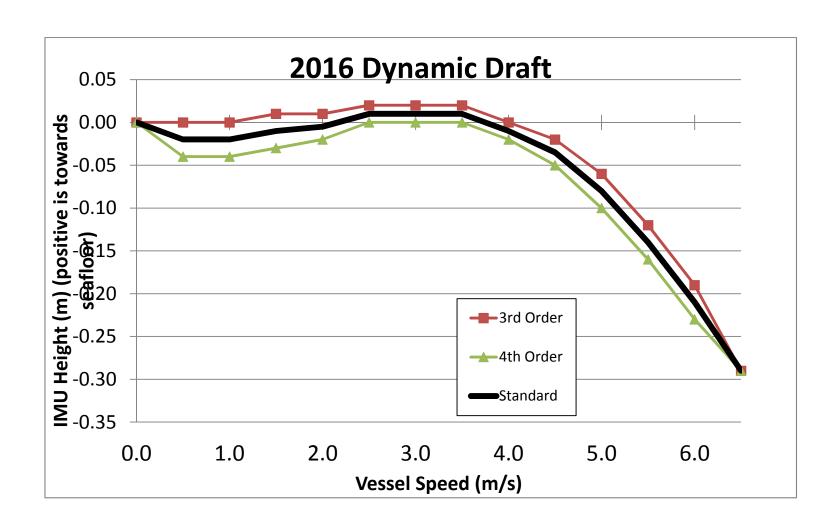


2702 - 2016 Elipsoid Referenced Dynamic Draft Results

Trim tabs? Jet bale?

Speed (m/s)	3rd Order	4th Order	Standard
0.0	0.00	0.00	0.00
0.5	0.00	-0.04	-0.02
1.0	0.00	-0.04	-0.02
1.5	0.01	-0.03	-0.01
2.0	0.01	-0.02	-0.01
2.5	0.02	0.00	0.01
3.0	0.02	0.00	0.01
3.5	0.02	0.00	0.01
4.0	0.00	-0.02	-0.01
4.5	-0.02	-0.05	-0.04
5.0	-0.06	-0.10	-0.08
5.5	-0.12	-0.16	-0.14
6.0	-0.19	-0.23	-0.21
6.5	-0.29	-0.29	-0.29

^{***}Standard is average of 3rd and 4th order values***



Waterline to IMU Offset

	NA RAFT OF 3.8	Personnel:	NA										
	TOON Draf						STRD DOM	ITOON Dr	aft Readings				
Fwd	TOON DIA	Fwd					Fwd	TOON DI	Fwd	,			
Outboard	3.85	Inboard	3.85				Inboard	3.85	Outboard	3.85			
Aft Outboard	3.85	Aft Inboard	3.85				Aft Inboard	3.85	Aft Outboard	3.85			
Port Ave	3.85]					Stbd Ave	3.85	5				
Center of IMU	x						Center of IMU	Х					
Plate to top of IMU	y z	-0.1356					Plate to top of IMU	y z	-0.1356				
I	x		Ī	x				x			x		
IMU Plate to Fwd Outboard 4.6 Draft Mark	у		IMU Plate to Fwd Inboard 4.6 Draft Mark	у			IMU plate to Fwd Inboard 4.6 Draft Mark	у		IMU plate to Fwd Outboard 4.6 Draft Mark	у		
Druit mark	Z	-3.313 (in CARIS)	mu k	Z	-3.308 (in CARIS)			Z	-3.426 (in CARIS)	Druit mark	Z	-3.428 (in CARIS)	
IMU Plate to Aft	x	()	IMU Plate to Aft	x			IMU plate to Aft	×	(5)	IMU plate to Aft Outboard 4.6	x	(5)	
Outboard 4.6 Draft Mark	y z	-3.306	Inboard 4.6 Draft Mark	y z	-3.305		Inboard 4.6 Draft Mark	y z	-3.344	Outboard 4.6 Draft Mark	y z	-3.358	
From 2013	Drydock	(in CARIS)			(in CARIS)	Ave -3.308	From 2013	Drydock	(in CARIS)			(in CARIS) Ave -3	380
1101112013	Diyuock					AVE -5.500	1101112013	Diyuock				AVC -5	
Fwd Outboard	x		Fwd Inboard Draft	Х		4.6	Fwd Inboard	x		Fwd Outboard	х		
Draft Mark to Waterline	y z	0.750	Mark to Waterline	y z	0.750		Draft Mark to Waterline	y z	0.750	Draft Mark to Waterline	y z	0.750	
		(in CARIS)	l I		(in CARIS)				(in CARIS)			(in CARIS)	
Aft Outboard Draft Mark to	х У		Aft Inboard Draft Mark to Waterline	x y			Aft Inboard Draft Mark to	X Y		Aft Outboard Draft Mark to	x y		
Waterline	z	0.750	Mark to Waterline	Z	0.750		Waterline	z	0.750	Waterline	z	0.750	
Calculated t	from draft m	(in CARIS) ark 4.6 to dra	ft readings		(in CARIS)	Ave 0.750	Calculated	from draft	(in CARIS) mark 4.6 to o	lraft reading	S	(in CARIS) Ave 0).750
IMU to Fwd	х		IMU to Fwd	Х			IMU to Fwd	Х		IMU to Fwd	Х		
Outboard Waterline	y z	-2.427	Inboard Waterline	y z	-2.422		Inboard Waterline	y z	-2.540	Outboard Waterline	y z	-2.542	
		(in CARIS)	!		(in CARIS)				(in CARIS)			(in CARIS)	
IMU to Aft Outboard	x y		IMU to Aft Inboard Waterline	x y			IMU to Aft Inboard	x y		IMU to Aft Outboard	x y		
Waterline	z	-2.420	waterine	Z	-2.419		Waterline	z	-2.458	Waterline	z	-2.472	
		(in CARIS)			(in CARIS)	Ave -2.694			(in CARIS)			(in CARIS) Ave -2	639
PORT Water	erline to Port	IMU				5 2.504	STBD Wat	erline to Stl	bd IMU			70 2	
Fwd Outboard	2.4274	Fwd Inboard	2.4224	-1			Fwd Inboard	2.5404	Fwd Outboard	2.5424	-1		
Aft	2.4204	Fwd	2.4194				Fwd	2.4584	Aft	2.4724			
Outboard		Inboard					Inboard		Outboard				
Port Ave	2.4224	J					Stbd Ave	2.5034	Ŋ				
Port W	aterline to I	Port IMU						Stbd W	aterline to S	tbd IMU			
Waterline	y							Waterline	y			PORT, STBD Ave	
to IMU (m)	Z	2.422						to IMU (m	ı) z	2.503		2.463	
	(In CARIS)						l		(In CARIS)				

Date: 6/14/2013 Personnel: Adler, Reed, Moehl Location: MOC-A Port ERLL/WRLL PORT PONTOON Draft Readings STBD PONTOON Draft Readings Fwd Fwd Port Fwd Stbd Fwd 3.66 3.65 3.75 3.59 Outboard Inboard Outboard Outboard Stbd Aft Port Aft Aft 3.92 Aft Inboard 3.91 3.85 3.78 Outboard Outboard Outboard 3.785 Port Ave Stbd Ave 3.743 Х Center of IMU Plate to top of IMU Center of IMU Plate to top of IMU у У -0.1675 z -0.1675 MU Plate to Fwd Outboard 4.6 Draft Mark MU Plate to Fwd nboard 4.6 Draft Mark MU plate to Fwd Outboard 4.6 Draft Mark IU plate to Fwd board 4.6 Draft Mark у у У у -3.313 -3.308 -3.313 -3.426 z z z z (in CARIS) (in CARIS) (in CARIS) (in CARIS) х х х х MU plate to Aft aboard 4.6 Draft Mark IMU Plate to Aft Inboard 4.6 Draft Mark IMU plate to Aft Outboard 4.6 Draft Mark MU Plate to Aft Outboard 4.6 M У У У у Draft Mark -3.306 -3.305 -3.306 -3.344 (in CARIS) (in CARIS) (in CARIS) (in CARIS) From 2013 Drydock Ave -3.308 From 2013 Drydock Ave -3.347 4.6 Х Fwd Inboard Draft Mark to Waterline У У у У 0.950 1.010 0.940 0.850 z z Z z (in CARIS) (in CARIS) (in CARIS) (in CARIS) Aft Outboard Draft Mark to Waterline t Inboard Draft Mark to Waterline Aft Outboard Draft Mark to Waterline у у У у 0.680 0.690 0.750 0.820 (in CARIS) (in CARIS) (in CARIS) (in CARIS) Calculated from draft mark 4.6 to draft readings Ave 0.815 Calculated from draft mark 4.6 to draft readings Ave 0.858 IMU to Fwd Inboard Waterline IMU to Fwd Outboard Waterline IMU to Fwd У У у -2.206 -2.191 -2.296 -2.249 z Z z Z (in CARIS) (in CARIS) (in CARIS) (in CARIS) IMU to Aft Outboard Waterline IMU to Aft Inboard Waterline MU to Aft Inboard у У у У -2.459 -2.448 -2.389 -2.357 Z Z Z (in CARIS) (in CARIS) (in CARIS) (in CARIS) Ave -2.661 Ave -2.490 PORT Waterline to Port IMU STBD Waterline to Stbd IMU Fwd Fwd Fwd Fwd 2.2055 2.1905 -1 2.2955 2.2485 -1 Outboard Inboard Inboard Outboard Fwd Fwd Aft Aft 2.4585 2.4475 2.3885 2.3565 Outboard Outboard Inboard Inboard Port Ave 2.3255 Stbd Ave 2.32225 Port Waterline to Port IMU Stbd Waterline to Stbd IMU Waterline Waterline to IMU (m) to IMU (m) 2.326 2.322 7 (In CARIS) (In CARIS)

•							
Δ	n	n	Δ	n	а	ix	ш
_	v	v	u		ч	1	

Echosounder Reports

Ferdinand R. Hassler Multibeam Echosounder Calibration

Ferdinand R. Hassler
Vessel

2/11/2016	042	Chesapeake E	Bay VA, Cape (Charles			
Date	Dn	Local Area					
Dorubo Wile	200						
Berube, Wils	Hydrographer(s)						
Calibrating i	iyurugrapner(s)						
Comments							
7125 200kH		port hull			winter 2015/2016	, EED/E	
MBES Syste	em	MBES System	n Location		Date of most rece	nt EED/Factory Chec	ck .
					Ī		
Sonar Seria	Number				Processing Unit S	erial Number	
oonar oona	rtarribor				1 recodering erint e	onar rambor	
TrueHeave f	ilename						
		•					
SV Cast #1	filename	UTC Time	Lat		Lon	Depth	Ext. Depth
		I	1		Ī	I	1
SV Cast #2	filename	UTC Time	Lat		Lon	Depth	Ext. Depth
	02-11_203956	OTO TIME	Lat		Lon	Берит	Ext. Doptii
	02 11_200000	view parallel t	o track one line	with induced	roll (outerheam) or	same lines bounded	slone (nadir)
NAV TIME	LATENCY		n, different spe		Ton (outorboarn) or		ciopo (riadir)
SV Cast #	XTF Line File		Heading	Speed (kts)	Remarks		
	2016_042070	5	140		Don't Use		
	0721		140		Don't Use		
	2006		320				
	2018		320	9.0			
PITCH		viou parallal t	o trook somo li	no (at nadir) [a	annocito direction o	omo cocodi	
SV Cast #	XTF Line File			Speed (kts)	pposite direction, s	ame speeuj	
OV Gast #	2016_042070		140		Don't Use		
	0712		320		Don't use		
	2006		320				
	2012		139				

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	2016_0420728	320	6.0	
	0736	140	6.0	
	2023	140	7.0	15 m off line, rerun
	2030	324	7.0	
	2037	136	7.0	rerun 2023

view across track, same line [opposite direction, same speed]

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	2016_0420746	050		USE PITCH LINES FOR ROLL
	0754	230		offline; aborted. 10m offset, USE PITCH LINES FOR RO
	0804	230		offline; aborted. 10m offset, USE PITCH LINES FOR RO
	0815			USE PITCH LINES FOR ROLL

Proces	Processing Log					
Date	Dn	Personnel				
	Data converted -	-> HDCS_Data in CARIS				
	TrueHeave applied					
	SVP applied					
	_					
	☐ Tide applied					
		Zone file				
		Lines merged				

	Compute correcto	ors in this order					
1. Precise Timing	2. Pitch bias	3. Heading bias	4. Roll bias				
Do not enter/apply correctors until all evaluations are complete and analyzed							

Data cleaned to remove gross fliers

PATCH TEST RESULTS/0 Evaluators Andvick Morgan Berube Miller	0.00 0.00 0.00 0.00 0.00	Pitch (deg) 0.36 0.44 0.45 0.40	Roll (deg) -0.26 -0.20 -0.20 -0.22	Yaw (deg) -0.62 -0.65 -0.60 -0.65				
Averages Standard Deviation FINAL VALUES Final Values based on	0.00 0.00 0.00 average	0.41 0.04 0.41	-0.22 0.03 -0.22	-0.63 0.02 -0.63				
MRU Ali	gn StdDev gyro 0.		K_2016 I deviation of Heading offset distandard deviations of pitcle					
NARRATIVE Used the pitch lines for roll because both roll lines that were in the project ran in the same direction (Morgan)								
✓ HVF Hydrograpi	hic Vessel File created or	updated with current offsets						

Ferdinand R. Hassler Multibeam Echosounder Calibration **Ferdinand Hassler** Vessel Chesapeake Bay VA, Cape Henry 2/11/2016 042 Date Local Area Berube, Wilson Calibrating Hydrographer(s) Comments winter 2015/2016 7125 Port 400kHz Port hull MBES System MBES System Location Date of most recent EED/Factory Check Processing Unit Serial Number Sonar Serial Number TrueHeave filename SV Cast #1 filename **UTC Time** Depth Ext. Depth Lon SV Cast #2 filename **UTC Time** Lat Lon Depth Ext. Depth view parallel to track, one line with induced roll (outerbeam) or same lines bounded slope (nadir) **NAV TIME LATENCY** [same direction, different speed] Speed (kts) Remarks SV Cast # XTF Line Filename Heading 2016_0420836 320 0850 140 9.0 offline; aborted 0859 320 9.0 **PITCH** view parallel to track, same line (at nadir) [opposite direction, same speed] SV Cast # XTF Line Filename Heading Speed (kts) Remarks 2016_0420824 140 6.0 0836 320 6.0

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	2016_0420906	140	7.0	not possible to go slower. Aborted line due to offline.
	0919	320	6.0	
	0928	140	7.0	
•				

view across track, same line [opposite direction, same speed]

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	2016_0420942	060	6.0	
	0950	240	6.0	

Proces	Processing Log					
Date	Dn	Personnel				
	Data converted -	-> HDCS_Data in CARIS				
	TrueHeave applied					
	SVP applied					
	_					
	☐ Tide applied					
		Zone file				
		Lines merged				

	Compute correcto	ors in this order					
1. Precise Timing	2. Pitch bias	3. Heading bias	4. Roll bias				
Do not enter/apply correctors until all evaluations are complete and analyzed							

Data cleaned to remove gross fliers

PATCH TEST RESULTS/0	1 - 1 1 1	D'Cala (La a)	D - H (1)	V(1)
Evaluators	Latency (sec) 0.00	Pitch (deg) 0.65	Roll (deg) -0.07	Yaw (deg) -0.67
Morgan	0.00	0.52	-0.07	-0.67
Andvick				
Berube	0.00	0.66	-0.10	0.05
Miller	0.00	0.60	-0.07	-0.80
Averages	0.00	0.61	-0.08	-0.41
Standard Deviation	0.00	0.06	0.01	0.39
FINAL VALUES	0.00	0.61	-0.08	-0.32
FINAL VALUES	0.00	0.61	-0.08	-0.32
Final Values based on	Pitch and Roll used a	verages. Yaw was a consens	sus after seeing high std dev	1
				-
.	EL COEN DODT DO	son7125_512bms_400kHz_9	S7K 2016.hvf	
MRU Ali MRU Align St	gn StdDev gyro 0	0.39 Value from standard	deviation of Heading offset distandard deviations of pitch	
MRU Ali MRU Align St NARRATIVE	gn StdDev gyro 0 dDev Roll/Pitch 0	Value from standard Value from averaged	deviation of Heading offset d standard deviations of pitcl	
MRU Ali	gn StdDev gyro 0 dDev Roll/Pitch 0	Value from standard Value from averaged	deviation of Heading offset d standard deviations of pitcl	
MRU Align St NARRATIVE Andvick, Berube, and Morgar	gn StdDev gyro 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Value from standard Value from averaged	deviation of Heading offset d standard deviations of pitcl	
MRU Align St NARRATIVE Andvick, Berube, and Morgar	gn StdDev gyro 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Value from standard Value from averaged or to come up with consensus	deviation of Heading offset d standard deviations of pitcl	

Multibeam Echosounder Calibration Vessel							
Date	Dn	Local Area					
Calibrating H	ydrographer(s)						
Comments							
MBES System	m	MBES Systen	n Location		Date of most rece	ent EED/Factory Checl	K
Sonar Serial	Number				Processing Unit S	Serial Number	
					3 -		
TrueHeave fi	lename						
SV Cast #1 fi	ilename	UTC Time	Lat		Lon	Depth	Ext. Depth
		I	1		I	1	·
SV Cast #2 fi	ilename	UTC Time	Lat		Lon	Depth	Ext. Depth
NAV TIME I SV Cast #	LATENCY XTF Line Filer	[same direction	o track, one line on, different spe Heading			or same lines bounded	slope (nadir)
	0531		320				
	0518		320	6.0			
				l			
PITCH SV Cast #	XTF Line File		o track, same li	ne (at nadir) [c	pposite direction,	same speed]	
SV Cast #	2016_042_051		140		approx 8m off line		
	0518	_	320			<u> </u>	
	0525		140		approx 10m off li	ne	
	0539		140		approx 8 m line		
	0556		140				
			1				
			1	1			
	1		1	1	 		

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	2016_0420548	320	6.0	
	0604	320	6.0	DO NOT USE - OFF LINE
	0611	140	6.0	

view across track, same line [opposite direction, same speed]

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	2016_0420643	050	6.0	
	0650	230	6.0	

Proces	sing Log	
Date	Dn	Personnel
	Data converted -	-> HDCS_Data in CARIS
	TrueHeave applied	
	SVP applied	
	_	
	☐ Tide applied	
		Zone file
		Lines merged

Compute correctors in this order					
1. Precise Timing	2. Pitch bias	3. Heading bias	4. Roll bias		
Do not enter/apply correctors until all evaluations are complete and analyzed.					

Data cleaned to remove gross fliers

PATCH TEST RESULTS/0	CORRECTORS			
Evaluators	Latency (sec)	Pitch (deg)	Roll (deg)	Yaw (deg)
Berube	0.00	0.10	0.10	0.55
Morgan	0.00	0.17	0.08	0.28
Andvick	0.00	0.10	0.08	0.61
Miller	0.00	0.15	0.08	0.50
Averages	0.00	0.13	0.09	0.49
Standard Deviation	0.00	0.04	0.01	0.14
FINAL VALUES	0.00	0.13	0.09	0.49
Final Values based on	This year's averages	S		
Resulting HVF File Name	FH_S250_STBD_R	eson7125_512bms_200kHz_5	67K_2016.hvf	
	· · · · · · · · · · · · · · · · · · ·		l deviation of Heading offset d standard deviations of pitc	
NARRATIVE Did not vary grossly from last	year's values			
HVF Hydrograpi	nic Vessel File created	or updated with current offsets		
, , ,		-		
Name:				Date:

Ferdinand R. Hassler Multibeam Echosounder Calibration **Ferdinand Hassler** Vessel Offshore Cape Charles, Chesapeake Bay, VA 2/11/2016 041 Berube, Wilson Calibrating Hydrographer(s) Comments Reson 7125, 400 kHz Stbd Winter 2015-2016 MBES System MBES System Location Date of most recent EED/Factory Check Processing Unit Serial Number Sonar Serial Number 2016_042_S250S.000 TrueHeave filename SV Cast #1 filename **UTC Time** Depth Ext. Depth Lon Lat SV Cast #2 filename **UTC Time** Lat Lon Depth Ext. Depth view parallel to track, one line with induced roll (outerbeam) or same lines bounded slope (nadir) **NAV TIME LATENCY** [same direction, different speed] Speed (kts) Remarks SV Cast # XTF Line Filename Heading 2016_0420308 0330 317 9.0 **PITCH** view parallel to track, same line (at nadir) [opposite direction, same speed]

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	2016_0420308	317	6.0	
	0319	137	6.0	

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	2016_0420338	137	6.0	not sufficient coverage over feature. Will rerun
	0345	317	6.0	not sufficient coverage over feature. Will rerun
	0444			aborted line
	0452	137	6.0	~8 m off line (closer to feature)
	0502	317	6.0	

view across track, same line [opposite direction, same speed]

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	20160420353	055	6.0	
	0403	245	6.0	

Proces	sing Log	
Date	Dn	Personnel
	Data converted -	-> HDCS_Data in CARIS
	TrueHeave applied	
	SVP applied	
	_	
	☐ Tide applied	
		Zone file
		Lines merged

Compute correctors in this order					
1. Precise Timing	2. Pitch bias	3. Heading bias	4. Roll bias		
Do not enter/apply correctors until all evaluations are complete and analyzed.					

Data cleaned to remove gross fliers

PATCH TEST RESULTS/C	CORRECTORS			
Evaluators	Latency (sec)	Pitch (deg)	Roll (deg)	Yaw (deg)
Berube	0.00	0.10	0.10	0.72
Morgan	0.00	0.08	0.11	0.43
Andvick	0.00	0.06	0.09	0.79
Miller	0.00	0.00	0.10	0.85
Averages	0.00	0.06	0.10	0.70
Standard Deviation	0.00	0.04	0.01	0.19
FINAL VALUES	0.00	0.04	0.10	0.88
I MAL VALUES	0.00	0.00	0.10	0.00
Final Values based on	Pitch and Roll use ave	erages. Yaw was consensus	of Andvick, Morgan and Ber	ube
Resulting HVF File Name	FH_S250_STBD_Res	on7125_512bms_400kHz_S	57K_2016.hvf	
	·		deviation of Heading offset	
MRU Align St	dDev Roll/Pitch 0.	03 Value from averaged	d standard deviations of pitch	and roll offset values
NARRATIVE Morgan's Yaw outlier prompte	ed review. After Andvick	, Berube and Morgan review	ed together, 0.88 was conse	nsus.
	hic Vessel File created or	updated with current offsets		
Name:				Date:

July 9, 2016

Reference Surfaces

Sonar	Frequency	Line#	Line Azimuth	Sonar
PORT	200 kHz	1911746	360 S-N	PORT
PORT	200 kHz	1911754	180 N-S	PORT
PORT	200 kHz	1911800	360 S-N	PORT
PORT	200 kHz	1911806	180 N-S	PORT
PORT	200 kHz	1911812	360 S-N	PORT
PORT	200 kHz	1911819	270 E-W	PORT
PORT	200 kHz	1911827	90 W-E	PORT
PORT	200 kHz	1911833	270 E-W	PORT
PORT	200 kHz	1911839	90 W-E	PORT
PORT	200 kHz	1911845	270 E-W	PORT
	_			
Sonar	Frequency	Line#	Line Azimuth	Sonar
Sonar STBD	Frequency 200 kHz	Line# 1912021		Sonar STBD
			180 N-S	
STBD	200 kHz	1912021	180 N-S 360 S-N	STBD
STBD STBD	200 kHz 200 kHz	1912021 1912028	180 N-S 360 S-N 180 N-S	STBD STBD
STBD STBD STBD	200 kHz 200 kHz 200 kHz	1912021 1912028 1912034	180 N-S 360 S-N 180 N-S 360 S-N	STBD STBD STBD
STBD STBD STBD STBD	200 kHz 200 kHz 200 kHz 200 kHz	1912021 1912028 1912034 1912041	180 N-S 360 S-N 180 N-S 360 S-N 180 N-S	STBD STBD STBD STBD
STBD STBD STBD STBD STBD	200 kHz 200 kHz 200 kHz 200 kHz 200 kHz	1912021 1912028 1912034 1912041 1912047	180 N-S 360 S-N 180 N-S 360 S-N 180 N-S 270 E-W	STBD STBD STBD STBD STBD
STBD STBD STBD STBD STBD STBD	200 kHz 200 kHz 200 kHz 200 kHz 200 kHz 200 kHz	1912021 1912028 1912034 1912041 1912047 1912054	180 N-S 360 S-N 180 N-S 360 S-N 180 N-S 270 E-W 90 W-E	STBD STBD STBD STBD STBD STBD
STBD STBD STBD STBD STBD STBD STBD STBD	200 kHz 200 kHz 200 kHz 200 kHz 200 kHz 200 kHz 200 kHz	1912021 1912028 1912034 1912041 1912047 1912054 1912102	180 N-S 360 S-N 180 N-S 360 S-N 180 N-S 270 E-W 90 W-E 270 E-W	STBD STBD STBD STBD STBD STBD STBD
STBD STBD STBD STBD STBD STBD STBD STBD	200 kHz 200 kHz 200 kHz 200 kHz 200 kHz 200 kHz 200 kHz 200 kHz	1912021 1912028 1912034 1912041 1912047 1912054 1912102	180 N-S 360 S-N 180 N-S 360 S-N 180 N-S 270 E-W 90 W-E 270 E-W 90 W-E	STBD STBD STBD STBD STBD STBD STBD STBD

Reference surfaces for all sonars (200/400 KHz port and starboard) completed at

Frequency	Line#	Line Azimuth
400 kHz	1911905	90 W-E
400 kHz	1911912	270 E-W
400 kHz	1911920	90 W-E
400 kHz	1911926	270 E-W
400 kHz	1911934	90 W-E
400 kHz	1911943	360 S-N
400 kHz	1911950	180 N-S
400 kHz	1911957	360 S-N
400 kHz	1912004	180 N-S
400 kHz	1912010	360 S-N

SV Casts Time (Local) Latitude

Frequency	Line#	Line Azimuth
400 kHz	1912132	90 W-E
400 kHz	1912139	270 E-W
400 kHz	1912147	90 W-E
400 kHz	1912154	270 E-W
400 kHz	1912200	90 W-E
400 kHz	1912207	0 S-N
400 kHz	1912213	180 N-S
400 kHz	1912219	0 S-N
400 kHz	1912225	180 N-S
400 kHz	1912232	0 S-N

Longitude

Ferdinar	nd R. Hass	ler					
Multibea	m Echoso	under Calibra	tion	Hassler			
				Vessel			
7/9/2016	191	Rhode Island	Sound				
Date	Dn	Local Area					
Morgan, Ma	rshall, Pye						
	Hydrographer((s)					
Comments							
Reson 7125	5/200kH z	Port			ı		
MBES Syste		MBES System	Location		Date of most rec	ent EED/Factory Checl	k
·		•				•	
Sonar Seria	l Number				Processing Unit	Serial Number	
					3		
TrueHeave	filename						
1140110410	monamo	_	_		_	_	_
0)/0 / ///		15:40:00 AM					
SV Cast #1	filename	UTC Time	Lat		Lon	Depth (m)	Ext. Depth
SV Cast #2	filename	UTC Time	Lat		Lon	Depth	Ext. Depth
		view perellel M	مداد معمان	ما المان	wall (ata wh a a wa)	ar ages lings barreded	_ (_ _
NAV TIME	LATENCY	[same direction			roli (outerbeam)	or same lines bounded	siope (nadir)
SV Cast #	S7K Line Fi		Heading	Speed (kts)			
	1911632		025		PORT 200kHz N		
	1911652		025	9.0	PORT 200kHz N	av/Timing	
PITCH		view parallel to	track, same I	ine (at nadir) [opposite direction	, same speed]	
SV Cast #	S7K Line Fi		Heading	Speed (kts)	Remarks		
	1911643		205		PORT 200kHz P		
	1911652		025	9.0	PORT 200kHz P	itch	
	+			 			
HEADING	YAW	view parallel to	track, offset l	ines (outerbea	ıms) [opposite dire	ection, same speed]	
SV Cast #	S7K Line Fi			Speed (kts)			

1911701	205	10.0	PORT 200kHz Yaw
1911715	205	10.0	PORT 200kHz Yaw/OK line, last one may be best
1911726	205	10.0	PORT 200kHz Yaw/OK line, last one may be best
1911739	205	10.0	PORT 200kHz Yaw

SV Cast #	S7K Line Filename	Heading	Speed (kts)	Remarks
	1911604	359	9.0	PORT 200kHz Roll
	1911615	179	9.0	PORT 200kHz Roll

Processing Log

7/9/2016	191			Morgan, Pye, Marshall		
Date	Dn	Personnel				
	✓ Data converted -	-> HDCS_Data in	CARIS			
√	TrueHeave applied					
	✓ SVP applied	2016_July_Pate	ch_Test_S250.svp			_
	✓ Tide applied	Predicted: 8452	660.tid			
		Zone file				
		Lines merged	✓			
	Data cleaned to rem	nove gross fliers	✓			
			Compute correct	tors in this order		
	1. Precise Timing		2. Pitch bias	3. Heading bias	4. Roll bias	
	Doı	not enter/apply c	orrectors until all e	valuations are complete and ana	alyzed.	_

Marshall Morgan Blass Andersen	0.00 0.00 0.00 0.00 0.10	Pitch (deg) 0.49 0.34 0.40 0.25	Roll (deg) -0.13 -0.15 -0.15 -0.14	Yaw (deg) -0.26 -0.15 -0.17 -0.28
Averages Standard Deviation FINAL VALUES Final Values based on	0.03 0.05	0.37 0.10	-0.14 0.01	-0.22 0.06
Resulting HVF File Name				
MRU Align Sto	gn StdDev gyro 0.0 dDev Roll/Pitch 0.0		deviation of Heading offset d standard deviations of pito	
MRU Align Sto				

	d R. Hass						
Multibea	m Echoso	under Calibr		Hassler Vessel			
				VESSEI			
7/9/2016	191	Rhode Island	d Sound				
Date	Dn	Local Area					
Morgan, Ma	rshall. Pve						
	Hydrographer(s)					
Comments							
		_			_		
Reson 7125		Port					
MBES Syste	em	MBES Syste	m Location		Date of most rece	ent EED/Factory Che	ck
					l		
Sonar Seria	Number				Processing Unit S	Serial Number	
TrueHeave	filename						
Tracricave	mename						
SV Cast #1	filename	UTC Time	Lat		Lon	Depth	Ext. Depth
		111.40	ı		I	ī	ı
SV Cast #2	filonomo	11:40 UTC Time	Lat		Lon	Depth	Ext. Depth
NAV TIME SV Cast #	LATENCY S7K Line Fi	[same directi	on, different spe			or same lines bounde	a slope (nadir)
	1911312		025		Do not use/ no s7		
	1911329		205		Do not use/ no s7		
	1911413		025		PORT 400kHz Na		
	1911437		025	9.0	PORT 400kHz Na	av timing	
					I		
PITCH	•	•		` -	opposite direction,	same speed]	
SV Cast #	S7K Line Fi	lename		Speed (kts)			
	1911426		205		PORT 400kHz Pi		
	1911437		025	9.0	PORT 400kHz Pi	tcn	
			+				
				,			
HEADING/						ction, same speed]	
SV Cast #	S7K Line Fi	iename	Heading	Speed (kts)	кетагкѕ		

1911447	205		PORT 400kHz Yaw
1911510	205	9.0	PORT 400kHz Yaw

SV Cast #	S7K Line Filename	Heading	Speed (kts)	Remarks
	1911521	359	9.0	PORT 400kHz Roll
	1911532	179	9.0	PORT 400kHz Roll

Processing Log

7/9/2016	191	Morgan, Pye, Marshall						
Date	Dn	Personnel						
✓ Data converted> HDCS_Data in CARIS								
√	TrueHeave applied							
SVP applied 2016_July_Patch_Test_S250.svp								
	✓ Tide applied	Predicted: 8452	660.tid					
		Zone file						
		Lines merged	✓					
	Data cleaned to rem	nove gross fliers	✓					
Compute correctors in this order								
	1. Precise Timing	•	2. Pitch bias	3. Heading bias	4. Roll bias			
Do not enter/apply correctors until all evaluations are complete and analyzed.								

PATCH TEST RESULTS/6 Evaluators	CORRECTORS Latency (sec)	Pitch (deg)	Roll (deg)	Yaw (deg)
Marshall	0.00	0.25	-0.15	-0.36
Pye	0.00	0.34	-0.15	-0.34
Morgan	0.00	0.58	-0.15	-0.26
Andersen	0.00	0.25	-0.13	-0.40
Blass	0.00	0.49	-0.14	-0.46
Averages Standard Deviation FINAL VALUES	0.00	0.38 0.15	-0.14 0.01	-0.36 0.07
Final Values based on				
Resulting HVF File Name				
MRU Ali	gn StdDev gyro 0.	07 Value from standard	d deviation of Heading offset	values
			d standard deviations of pito	
NARRATIVE				
	hic Vessel File created o	r updated with current offset	s	
Name:				Date:

Ferdinar	nd R. Hass	ler					
Multibea	m Echoso	under Calibr	ation	S250			
				Vessel			
7/9/2016	191	Rhode Island	Sound				
Date	Dn	Local Area					
Morgan, Ma	rshall Pve						
	Hydrographer((s)					
Comments							
					•		
7125/200kH MBES Syste		Starboard po MBES Syster			Data of most ro	cent EED/Factory Che	ok
MDES Syste	3111	MDES Syster	II Location		Date of most re	cent EED/Factory Che	CK
Sonar Seria	l Number				Processing Unit	t Serial Number	
TrueHeave	filename						
		11:15	I		I	Ī	I
SV Cast #1	filename	UTC Time	Lat		Lon	Depth	Ext. Depth
					•		•
SV Cast #2	filename	UTC Time	Lat		Lon	Depth	Ext. Depth
NAV TIME SV Cast #	LATENCY XTF Line Fi	[same directi	on, different spe Heading	eed] Speed (kts)	Remarks	or same lines bounde	d slope (nadir)
	1911200		025		STBD 200kHz N		
	1911224		025	9.0	STBD 200kHz I	nav timing	
	+						
						_	
PITCH SV Cast #	IVTE Lina Ei	•	to track, same I Heading	ine (at nadir) [Speed (kts)	opposite directio	n, same speed]	
SV Cast # XTF Line Filename 1911215		205		STBD 200kHz Pitch			
1911224		025		STBD 200kHz Pitch			
	+						
	<u> </u>						
HEADING	YAW	view parallel	to track, offset I	ines (outerbea	ıms) [opposite di	rection, same speed]	
SV Cast #	XTF Line Fi			Speed (kts)			

1911246	205	9.0	STBD 200kHz Yaw
1911259	205	9.0	STBD 200kHz Yaw

ROLL

view across track, same line [opposite direction, same speed]

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	1911131	359	9.0	STBD 200kHz Roll
	1911141	179	9.0	STBD 200kHz Roll

Processing Log

7/9/2016	191			Morgan, Pye, Marshall			
Date	Dn	Personnel					
	✓ Data converted -	-> HDCS_Data in	CARIS				
√	TrueHeave applied						
	✓ SVP applied	2016_July_Pato	h_Test_S250.svp				
	✓ Tide applied	Predicted: 8452	660.tid				
		Zone file					
		Lines merged	✓				
	Data cleaned to remove gross fliers						
			Compute correc	tors in this order			
	1. Precise Timing		2. Pitch bias	3. Heading bias	4. Roll bias		
	Doı	not enter/apply c	orrectors until all e	evaluations are complete and ar	nalyzed.		

PAICH IEST RESULTS/0 Evaluators	Latency (sec)	Pitch (deg)	Roll (deg)	Yaw (deg)
Pye	0.00	0.25	0.06	0.80
Morgan	0.00	0.33	0.06	0.63
Blass	0.00	0.33	0.06	0.79
Andersen	0.00	0.33	0.07	0.55
Averages Standard Deviation FINAL VALUES	0.00	0.31 0.04	0.06 0.01	0.69 0.12
Final Values based on				
Resulting HVF File Name				
MRU Alig	gn StdDev gyro	0.12 Value from standa	rd deviation of Heading offse	t values
MRU Align Sto	Dev Roll/Pitch	0.02 Value from averag	ed standard deviations of pite	ch and roll offset value
NARRATIVE				
☐ HVF Hydrograp	hic Vessel File created	or updated with current offse	ets	
Name:				Date:

Ferdinar	nd R. Hass	ler					
Multibea	m Echoso	under Calibra	ation	S250			
				Vessel			
7/9/2016	191	Rhode Island	Sound				
Date	Dn	Local Area					
Morgan, Ma	rehall Dvo						
	Hydrographer((s)					
		` ,					
Comments							
Comments							
7125 200kH		Starboard por					
MBES Syste	em	MBES Syster	n Location		Date of most rece	nt EED/Factory Che	ck
Sonar Seria	l Number				Processing Unit S	erial Number	
TrueHeave	filename						
		-	_		_	_	<u>-</u>
0)// 0 1 ///	C 1	8:25					<u> </u>
SV Cast #1	filename	UTC Time	Lat		Lon	Depth	Ext. Depth
		11:15	1				
SV Cast #2	filename	UTC Time	Lat		Lon	Depth	Ext. Depth
			ta tua ala ana lin		-l		d alama (madim)
NAV TIME	LATENCY		o track, one iin on, different spe		a roll (outerbeam) o	r same lines bounde	a siope (nadir)
SV Cast #	XTF Line F		Heading	Speed (kts)	Remarks		
	1910905		021	4kts		w timing line (record	ed on C:)
	1910915		021	Oleto	Logging test, disc		
	1910930		021	8kts	STBD 400khz pito	ch/timing combo	
			+				
PITCH		view parallel t	to track same I	ine (at nadir) l	opposite direction,	same speedl	
SV Cast #	XTF Line F	•	Heading	Speed (kts)		oao opoouj	
1910920			205	8kts	STBD 400khz Pitch line to SW		
	1910930		025	8kts	STBD 400khz pito	ch/timing combo	
HEADING	VΔW	view parallal	to track offect !	inge (autorba	ame) [annocito dire	ction, same speed]	
SV Cast #	XTF Line F			Speed (kts)		onon, same speedj	
				, , ,			

1910)942	205	9kts	STBD 400kHz yaw, 13 meters right of track line
1911	010	205	10kts	STBD 400kHz yaw, only partial feature, to be redone
1911	1023	205	10kts	STBD 400kHz yaw, call it good

ROLL view across track, same line [opposite direction, same speed]

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	1911044	359	9kts	STBD 400kHz roll
	1911055	179	10.0	STBD 400kHz roll

Processing Log

7/9/2016	191			Morgan, Pye, Marshall			
Date	Dn	Personnel					
	✓ Data converted -	-> HDCS_Data in	CARIS				
√	TrueHeave applied						
	✓ SVP applied	2016_July_Pate	ch_Test_S250.svp				
	✓ Tide applied	Predicted: 8452	660.tid				
		_					
		Lines merged	✓				
	Data cleaned to remove gross fliers						
			Compute correct	ors in this order			
	1. Precise Timing		2. Pitch bias	3. Heading bias	4. Roll bias		
	Do	not enter/apply c	orrectors until all ev	aluations are complete and ar	nalyzed.		

Evaluators	Latency (sec)		Pitch (deg)	Roll (deg)	Yaw (deg)
Pye	0.00		0.65	0.05	0.76
Blass	0.00		0.50	0.08	0.75
Andersen	0.00		0.70	0.08	0.60
Averages	0.00		0.62	0.07	0.70
Standard Deviation	0.00		0.10	0.02	0.09
FINAL VALUES					
Final Values based on					
Resulting HVF File Name					
MRU Alig	gn StdDev gyro	0.09	Value from standar	rd deviation of Heading offset	values
MRU Align Sto	dDev Roll/Pitch	0.06	Value from average	ed standard deviations of pitc	h and roll offset value
NARRATIVE					
☐ HVF Hydrograp	hic Vessel File crea	ted or upda	ated with current offse	ts	
Name:					Date:





NOAA Ship E.R. Hassler Survey Launch 2702 Report

R2Sonic visited the NOAA Ship E.R. Hassler the week of 16 Nov 2015. This is a brief report on that visit and recommendations to be considered.

The physical installation has the face of the projector even with the face of the receiver. With this orientation it is very important to put the vertical relationship, between the projector's acoustic center and the receiver's acoustic center in the control software. With the standard R2Sonic mounting frame, the vertical relationship between the two acoustic centers is 0.119m. To insure accurate sounding depths, when this vertical distance is changed, it is necessary to measure the new vertical offset and enter the new value in the Projector Z offset (Installation Settings). The measurement resulted in a new Projector Z offset of +0.054m; this was entered into Sonic Control's Installation Settings.

It was brought up, during initial conversations with the survey officer, that the Sonic sonars can work simultaneously with most single beam echosounders such as the navigation echosounder on board the launch. With the frequency agility of the sonar, it is easy to select a frequency that is off the operating frequency or off a harmonic of that frequency. With a 200kHz single beam echosounder, a sonar frequency of 330kHz works very well. On the water, this was tested and proved to be a satisfactory solution and allowed both the navigation echosounder and the multibeam sonar to be operated continuously without any cross talk or interference.

Initially there were issues with providing RTCM or CMR corrections to the Applanix POS MV using the default equipment installed on the survey launch. This did take up the entire first day of operations, but was solved by removing equipment from the Hassler and installing this on the launch and configuring it to output corrections to the POS MV. Once we had accurate positioning, with the POS MV, the GAMS calibration could be completed. We will not go into the GAMS calibration in this document as it is well known to the personnel of NOAA.

One of the prime tasks that R2Sonic wished to complete was an extensive multibeam calibration, better known as the Patch Test. To this end, an area was chosen that historically has been used for calibration and testing.



Figure 1: Calibration and test area





A thorough calibration calls for a large data set, for each computation, in order to derive a valid mean and standard deviation. Sea and wind conditions were such that there was some variability in the maneuvering of the vessel. The implication of the variability was that at times, where it was desirable for the sonar head to pass over the same feature, in both directions, the head passed over a slightly different area of the feature. When this occurs, the Yaw computation is very critical for the accuracy of the Pitch computation, even though the Pitch is computed prior to the Yaw solution. If the Yaw is greater than 1.0°, it is advisable to re-compute the Pitch offset using the determined Yaw offset; this was the case with the launch patch test data.

				Pitch - Yaw			
LIN	IES	ROLL	PITCH	adj.	YAW-	LINES	YAW
1715	1720	-24.90	N/A	0.60	1715	1723	1.30
1723	1725	-24.85	0.10	0.20	1720	1725	1.50
1732	1734	-24.80	-0.10	0.45	1723	1732	1.30
1737	1738	-24.75	N/A	0.45	1725	1734	1.30
1740	1742	-24.85	0.15	0.35	1732	1737	1.10
1802	1804	-24.85	0.20	0.40	1734	1738	0.90
1832	1833	-24.75	0.35	0.50	1832	1840	1.20
1835	1836	-24.75	0.45	0.55	1742	1833	1.20

	Ave.	σ
ROLL	-24.81	0.06
PITCH	0.19	0.19
YAW	1.23	0.18

Yaw ad	Ditch	0.45	0.07
iaw au	FILCII	0.43	0.07

As can be seen the final values are: Roll = -24.81°; Pitch = +0.45°; Yaw = +1.23°

Any thorough calibration should be truthed by having the vessel go about a feature in various directions and then comparing each run to see if the feature shifts in any direction. The following day we attempted to perform the truthing survey. Although the data were collected in different directions, over the features of the calibration area, the wind and seas had picked up considerably. This made vessel handling a serious issue, which we attempted to overcome by increase speed. Increasing speed induced squat; no vessel squat data is currently available. Although all cross sections, over the features, showed no horizontal shift, a slight vertical shift was observed. Without squat data or employing RTK heights, the slight vertical shift was attributed to the vessel squat. This is a valid assumption.





It is recommended that as soon as possible a squat determination be made for the launch or that RTK heights be employed to eliminate the effects of squat.

Further, it is recommended that a permanent solution for GPS corrections be found for the POS MV.

Further, it is recommended that a bar check or lead line be performed to verify the surveyed-in offsets on the launch. The adjustment of the Projector Z offset was critical to accurate depths, so is the physical verification of the surveyed-in offsets by either the bar check or lead line methods.

Further, it is recommended, due to the potential change in survey personnel that will be running the launch, that a check list be created that covers all the necessary, preliminary, checks prior to a multibeam survey.

R2Sonic verifies that the 2702 Survey Launch, as far as the Sonic 2022 multibeam is concerned, is survey ready.

Thank you,

Charles W Brennan

Co. W. Brenno

R2Sonic LLC

FH 2016 Sidescan Calibration Side Scan run on Dn068.

Contact is: R"6" Buoy Block Off Duck, NC

MBES Position of Contact

Lat	Loi	ng				
	36.2637083	-75.5936194				
SSS Contacts			Lat Diff (m)	Long Diff (m)	Distance (m)	
1	36.2637100	-75.5936370	0.188904001	-1.576896663	1.588171215	
2	36.2637150	-75.5936350	0.744504	-1.397703861	1.583623153	
3	36.2637210	-75.5936350	1.411224	-1.397703861	1.986234946	
4	36.2637100	-75.5936260	0.188904001	-0.591336249	0.620776353	
5	36.2637050	-75.5936020	-0.366696	1.558977382	1.60152316	
6	36.2637130	-75.5936250	0.522264001	-0.501739848	0.724225491	
7	36.2637120	-75.5935710	0.411144	4.336465822	4.355912673	
8	36.2636760	-75.5936040	-3.589176	1.37978458	3.845255498	
9	36.2636940	-75.5936250	-1.589016	-0.501739848	1.666347719	
10	36.2637250	-75.5936180	1.855704	0.125434961	1.859938511	
11	36.2637410	-75.5936120	3.633624001	0.66301337	3.693617482	
12	36.2636710	-75.5936290	-4.144775999	-0.860125454	4.233082078	
13	36.2637070	-75.5936580	-0.144456	-3.458421091	3.461436693	
N	13 Av	erage	-0.067526769	-0.170922366	2.401549613	-0.11922457
DOF: 2N-1	25 St[Dev	2.089422731	1.896534039		1.955707889

Criteria: 95% Confidence that any future measurement will not give a positional error greater than 10 meters.

Assuming x and y errors are governed by the same normal distribution, the square of the distance error is governed by Chi-squared statistics.

$$P\left[d^{2} > \frac{\sigma^{2}\chi_{n;\alpha}^{2}}{n}\right] = \alpha$$

Setting the distance error equal to 10 meters and using the Chi-squared value for one degree of freedom and alpha = 0.05, solve for the maximum value for the true value of the standard deviation of the x and y error.

Distance Error Limit (meters) 10 Max. x,y Std Deviation 5.1

The sample estimate of the standard deviation will also be Chi-squared distributed

At a 95% confidence interval the standard deviation range is:

	low	best est.	high	_
x,y StDev	1.5	2.0	2.7	
And the 95% confidence inteval of		the positioning er	ror is:	
Error	3.0	3.8	5.3	PASS

Note: FPM method of 1.96*RMS standard deviation

Error: 5.530718786 **PASS**

Positioning and Attitude System Reports

POSMV 320 INSTALLATION REPORT



Prepared for NOAA Ferdinand Hassler S250 SWATH May, 2011 By

> Bruce A. Francis Applanix Houston, TX









Company: **Oak Management**

Attention

Steve Laverty

of:

Email: steve.laverty@oakmanagement.com

From: Bruce A. Francis

Date: 18 May, 2011

POSMV Installation aboard Ref.:

Ferdinand Hassler-SWATH

Brundan Ax Exampoisation. 17461 Village Green Drive Houston TX 77040 USA

Tel: (713) 896-9900 Fax: (713) 896-9919 bfrancis@applanix.com http://www.applanix.com

During the period of May16th to May 18th, 2011 two POSMV systems were commissioned aboard NOAA vessel Ferdinand Hassler. The following is a summary of the events and final observations.

Chronology:

May 16th-

Travel from Houston TX to New Orleans LA. Overnight in Gulfport MS with the intention of meeting the ship in the morning to conduct dockside testing in the morning before the ship sets sail in the afternoon. Informed by Steve Laverty there has been a change in plan and the CO wants to depart the dock at 0900

tomorrow instead.

May 17th-

Arrive ship 0730. Brief review of POSMV installation with Briana Welton followed by cursory inspection. Both POSMV systems are up and running with no errors. Collected a set of dockside POSMV data from both systems for processing in POSPAC later today. Plan is to meet at the NOAA facility in Pascagoula at 0630

and transit out to ship in small boat.

May 18th-0630- Depart Pascagoula for Ferdinand Hassler. Upon arrival commenced

> system inspection and diagnostics. No faults found. Conducted two GAMS calibrations on both POSMV systems and completed system acceptance testing.

Calibration and testing results:

1. The GAMS calibration was completed on May 18th and checked against the calculations derived from the survey report. Further comparisons are required but it appears that the survey calculations differ somewhat from the GAMS measured values.

Notes:

As a result of post processing the data set collected during commissioning, it was discovered that the POSMV IMU's were actually reversed at the back of the POSMV PCS units. Because of the symmetry in the two systems, these errors were not immediately obvious during the trials; however the lever arm errors were apparent in the data set. After physically changing the IMU inputs the processed calibration data was now reasonable when compared to the measured survey results. A new GAMS calibration was performed by the NOAA personnel after the IMU cables were returned to the correct orientation and the information below is based upon the correct orientation.





Recommendations:

While the large separation between the GPS antennas across decks will improve heading accuracy, there is a possibility that flexure in the ship will cause poor GAMS performance as the baseline vectors may become unstable. We were unable to fully test this configuration in a calm sea but if this turns out to be the case after the ship experiences a modest increase in sea state, the solution might be to extend the separation between the antennas on the individual mounts and switch the antenna input to the POS from cross decks to using the pairs from each side to their corresponding POS unit. The minimum separation should be 1 meter whereas now the distance is only about 0.6m and slightly too short to expect normal GAMS performance.

Submitted By:

Bruce A. Francis Customer Support Engineer

Marine Products

713-896-9900

bfrancis@applanix.com





Vessel Name	Ferdinand R. Hassler
Year Built	2010
POSMV Location	Port Side
PCS Serial Number	3187
IMU Serial Number	
Top Hat	804 (Cable S/N 105)
Hardware Version	3.3-7
Firmware Version	5.03
POS IP Address	129.100.2.231
Subnet Mask	255.255.0.0
POS PC Address	129.100.2.234
Subnet Mask	255.255.255.0
Survey Software	Hypack 11.0.8.0
Multibeam System	Reson 7125



Port System Lever Arms: (Units are in Meters)

Point	X Axis	Y Axis	Z Axis	Notes
Reference point	0.0	0.0	0.0	PORT IMU
Ref to IMU	0.0	0.0	0.0	PORT IMU
Ref to Primary GPS	1.395	1.05	-13.084	Port Aft antenna
Ref to Secondary GPS	1.418	9.188	-13.080	Strb Aft antenna
Ref to AUX GPS	N/A	N/A	N/A	Not surveyed
Ref to Vessel	0.0	0.0	0.0	POS NMEA, message point
				of validity at target on IMU.
IMU frame w.r.t Ref	0.0	0.0	0.0	Rotation of IMU frame in
frame				comparison to ships frame.
Ref to Heave (COR)	0.0	0.0	0.0	Center of gravity (rotation)
				Information not available.
Ref to Sensor 1	0.0	0.0	0.0	Point of validity of HPR
				+Posn-Valid at IMU
Ref to Sensor 2	0.0	0.0	0.0	Point of validity-HPR +Posn-
				Valid at IMU

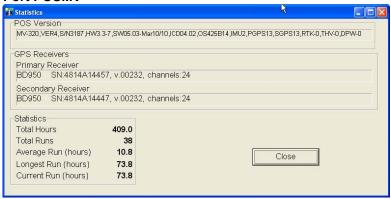




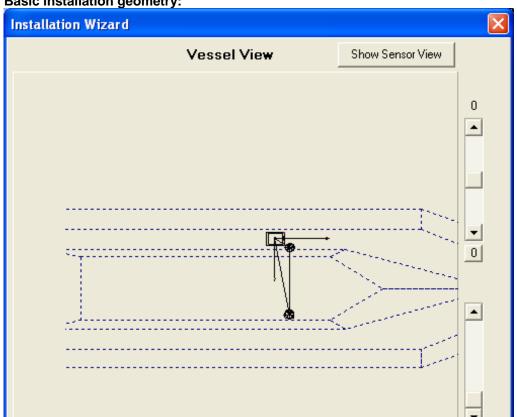
General System information:

Options included- RTK (RTK-0); True Heave (THV-0); (DPW-0) Password protection Disabled

Port POSMV



Basic installation geometry:







```
POSRT Data Extraction Utility [Jun 15 2011]
Copyright (c) 2008-2011 Applanix Corporation. All rights reserved.
Date: 07/25/11 Time: 15:12:36
First POS file
                  : E:\Clients config, IP, & test results\NOAA\NOAA
Swath\Final_Data_IMUcorrect\For Bruce Frances\2011_152_S250_Port_A_GAMS.000
Last POS file : E:\Clients config, IP, & test results\NOAA\NOAA
Swath\Final_Data_IMUcorrect\For Bruce Frances\2011_152_S250_Port_A_GAMS.000
Output path : C:\Documents and Settings\bfrancis\My Documents\POSPac
MMS\Unnamed(1)\Swath Port IMU\Extract
Output kernel : Swath Port IMU
Start time : 0.000
End time : 999999.000
VNAV output modulus : 1
    _____
307750.275 : The First Group 99: Versions & Statistics
   System Version:
    Product-Model: MV-320; Version: VER4; Serial Number: S/N3187;
    Hardware Version: HW3.3-7;
     Software Release Version-Date: SW05.03-Mar10/10;
    ICD release version: ICD04.02;
    Operating System Version: OS425B14;
     IMU Type: IMU2; Primary GPS Type: PGPS13; Secondary GPS Type: SGPS13;
     Option mnemonic-Expiry Time: DMI0;
    Option mnemonic-Expiry Time: GIMO;
    Option mnemonic-Expiry Time: RTK-0;
    Option mnemonic-Expiry Time: THV-0;
Option mnemonic-Expiry Time: DPW-0;
   Primary GPS Version: BD950 SN:4814A14457, v.00232, channels:24; Secondary GPS Version: BD950 SN:4814A14447, v.00232, channels:24;
   Total Hours
                    : 561.4; Number of Runs:
  Average Length of Run: 10.6; Longest Run: 126.2; Current Run: 12.1;
   ______
307750.275 : Diffcorr2 time1 gap: start 0.0, end 307750.2749
307750.280 : IMU type: IMU2 Data rate = 200 Hz
307750.280 : Extracting Group 4 : Time-tag data
307750.290 : SNV status changed to 0 (Full Nav)
307751.070 : Primary GNSS receiver type is GNSS13.
307751.090 : Secondary GNSS receiver type is GNSS13.
307755.275 : GenB(9): GAMS solution in use CLEARED.
307756.275 : GenB( 9): GAMS solution in use SET.
307758.275 : GenB( 9): GAMS solution in use CLEARED.
307759.275 : Message 50: Transition to NAVIGATE mode.
307759.275 : Message 37: Base 1 setup
   Input data type expected: RTCM 1 or 9
   Datum Type: NAD83
                    _____
 ______
307759.275 : Message 38: Base 2 setup
   Input data type expected: RTCM 1 or 9
   Datum Type: WGS84
307759.275 : Message 20: General parameters
   Time and distance tag types: 2 1
   Autostart selection:
                                        ENABLED
   Autostart selection: ENABLED

Reference-IMU lever arm: -0.008 -0.031 0.130

Reference-primary GPS lever arm: 1.395 1.050 -13.084
   Reference-auxiliary 1 GPS lever arm: 0.000 0.000 0.000
```





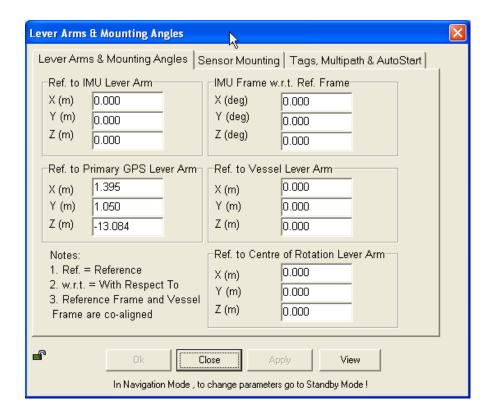
Reference-auxiliary 2 GPS lever arm: 0.000 0.000 0.000 0.000 0.000 0.000 Reference-IMU mounting angles: 0.000 0.000 0.000 Reference-vehicle mounting angles: Multipath environment: LOW ______ 307759.275 : Message 22: Aiding sensor install parameters 0.00 DMI scale factor: 0.00 0.00 Reference-DMI lever arm: 1.00 DVS scale factor correction: 0.00 0.00 Reference-DVS lever arm: 0.00 0.00 0.00 Reference-DVS attitude: 0.00 ______ 307759.275 : Message 24: User accuracy parameters 2.00 User position accuracy: 0.50 User velocity accuracy: 0.05 User attitude accuracy: 0.05 User heading accuracy: ______ 307759.275 : Message 106: Heave ratios Heave Bandwidth (sec): 12.000 Heave Damping Ratio: 0.707 307759.275 : Message 120: Heave and sensor 1&2 install parameters Reference->Sensor1 alignment angles (R,P,Y) in degrees: 0.00 0.00 0.00 Reference->Sensor2 alignment angles (R,P,Y) in degrees: 0.00 0.00 0.00 Reference->Sensorl lever arm in meters: 0.00 0.00 0.00 0.00 0.00 0.00 Reference->Sensor2 lever arm in meters: Reference->Center of Rotation in meters: 0.00 0.00 0.00 ______ 307759.275 : Message 121: Vessel Installation Parameters Reference-Vessel in meters: 0.00 0.00 0.00 307759.275 : Message 32: PCS IP address IP Address (Network part 1): 129 IP Address (Network part 2): 100 IP Address (Host part 1): 1 IP Address (Host part 2): 232 307759.275 : Message 56: General data Initial position: Initial distance: 0.00 Initial attitude: 0.000 0.000 0.000 _____ 307759.275 : Message 21: GAMS install parameters A-B antenna separation: 8.112 A-B baseline vector: -0.060 8.112 0.021 Heading error for calibration: 0.50 A-B azimuth correction: 0.000 Available subsystems : Primary GNSS : Secondary GNSS : Differential Corrections Vehicle to reference alignment angles: 0.000 0.000 0.000 Multipath setting : LOW Reference to IMU lever arm : -0.008 -0.031 0.130 Reference to IMU alignment angles : 0.000 0.000 0.000 Reference to primary GNSS lever arm : 1.395 1.050 -13.084 : 8.104 GAMS antenna separation GAMS baseline vector : 0.152 8.103 -0.004





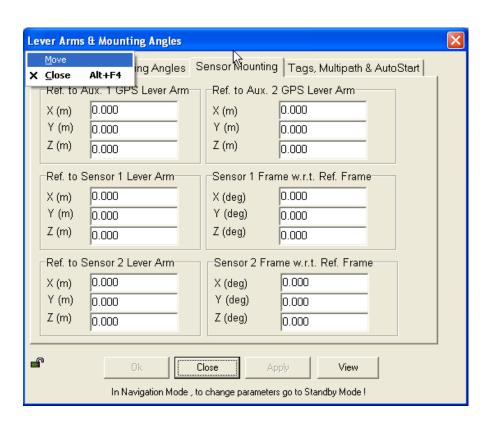
GAMS heading calibration threshold : 0.500 GAMS heading correction : 0.000





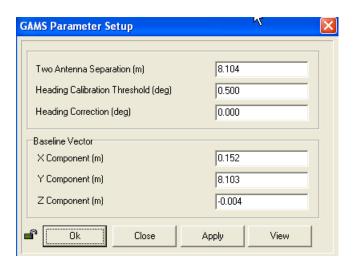






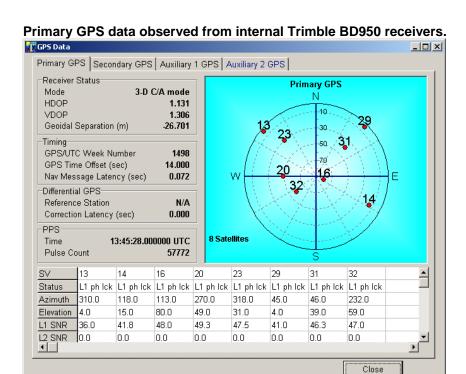
Observed GAMS values derived from the field calibration:

Port GAMS Cal #1

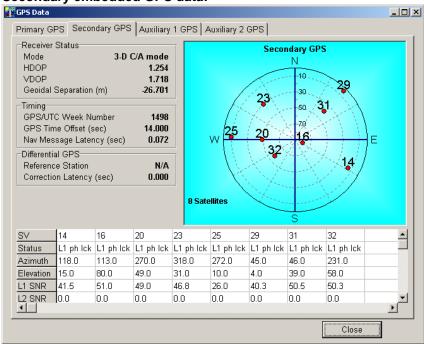








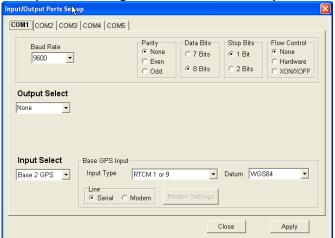
Secondary embedded GPS data:



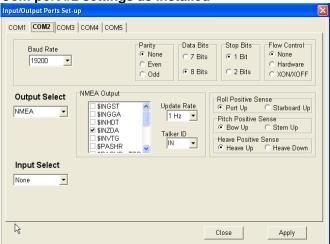




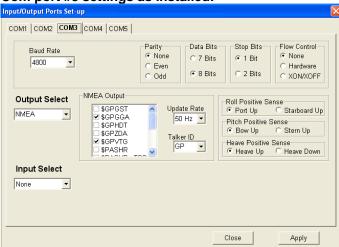
Com port #1 settings as installed: DGPS input from Trimble SPS Receiver.



Com port #2 settings as installed



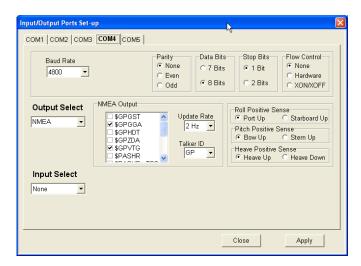
Com port #3 settings as installed:



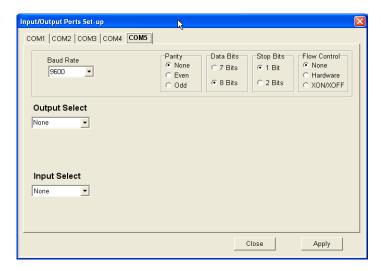




Com port #4 settings as installed:



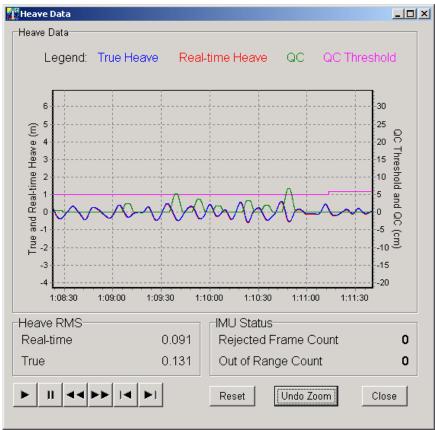
Com port #5 settings as installed



Heave data plot:

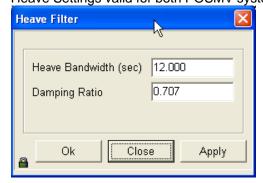






The heave plot above shows the relationship between the Real-time (RT) heave and the True (or delayed TH) heave measurements. The green line relates to quality control (QC) and represents the difference between the two values. When the delta between the RT and TH exceeds 5cm or 5% of total heave (pink line) then the radio light on the main controller screen will turn from green to red but does not affect the real-time heave data being collected. Quite often this occurs after the vessel makes a turn or an abrupt change in speed and is not necessarily cause for alarm. The heave filter has a 105 second buffer so the event which may have caused the impulse happened in the past. A red light merely calls the users attention to the difference and may also suggest that the filter settings need to be refined if the QC value is continually out of bounds.

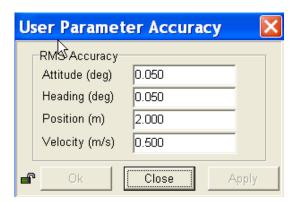
Note: The TrueHeave data filter is delayed about 3 minutes from the TH value. Also, Group 111 & 113 must be enabled in the Ethernet Real-time logging page. In addition, this filter should be adjusted as required for changes in the local swell conditions. Heave Settings valid for both POSMV systems.



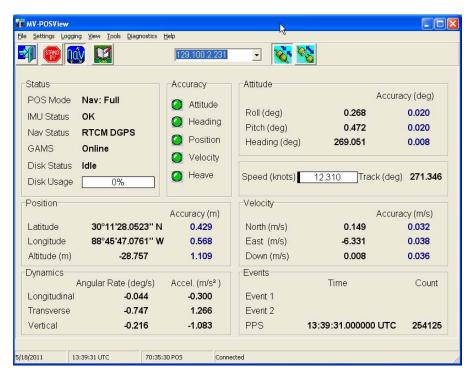




The main controller screens below shows normal POSMV operation. POS Mode is FULL indicating that all user accuracy settings have been satisfied. Note, when using RTK the position threshold should be set to a smaller value i.e. 0.100m or whatever is specified in the survey parameters. Exceeding any of the limits below will cause one of the radio lights to turn red and the POS mode will no longer report "Full Navigation" This however only affects the flag in the GGA or GGK message and not the performance.



Port POSMV Final Navigation







Port side antenna and IMU mounting:













Vessel Name	Ferdinand R. Hassler
Year Built	2010
POSMV Location	STRB Side
PCS Serial Number	3189
IMU Serial Number	
Top Hat	803 (Cable S/N 104)
Hardware Version	3.3-7
Firmware Version	5.03
POS IP Address	129.100.1.231
Subnet Mask	255.255.0.0
POS PC Address	129.100.1.234
Subnet Mask	255.255.255.0
Survey Software	Hypack 11.0.8.0
Multibeam System	Reson 7125



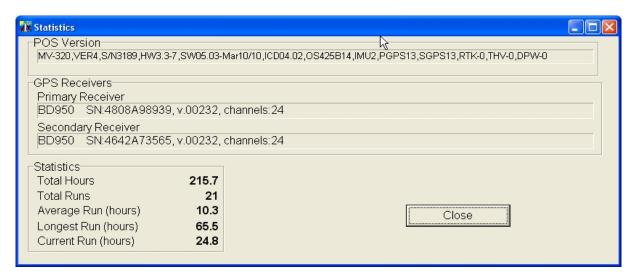
Port System Lever Arms: (Units are in Meters)

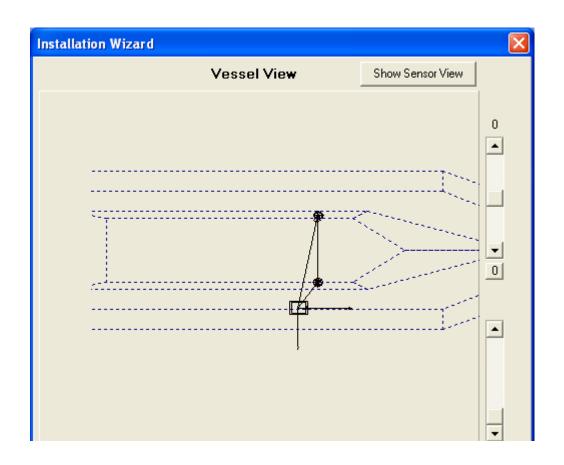
Point	X Axis	Y Axis	Z Axis	Notes
Reference point	0.0	0.0	0.0	STRB IMU
Ref to IMU	0.0	0.0	0.0	STRB IMU
Ref to Primary GPS	1.929	-11.199	-13.084	Port FWD antenna
Ref to Secondary GPS	1.953	-3.056	-13.083	Strb FWD antenna
Ref to AUX GPS	N/A	N/A	N/A	Not surveyed
Ref to Vessel	0.0	0.0	0.0	POS NMEA, message point
				of validity at target on IMU.
IMU frame w.r.t Ref	0.0	0.0	0.0	Rotation of IMU frame in
frame				comparison to ships frame.
Ref to Heave (COR)	0.0	0.0	0.0	Center of gravity (rotation)
				Information not available.
Ref to Sensor 1	0.0	0.0	0.0	Point of validity of HPR
				+Posn-Valid at IMU
Ref to Sensor 2	0.0	0.0	0.0	Point of validity-HPR +Posn-
				Valid at IMU





STRB POSMV









```
POSRT Data Extraction Utility [Jun 15 2011]
Copyright (c) 2008-2011 Applanix Corporation. All rights reserved.
Date: 07/25/11 Time: 15:12:36
                      : E:\Clients config, IP, & test results\Swath 250 Testing\Final
Report Files\Final_Data_IMUcorrect\For Bruce Frances\2011_152_S250_Stbd_GAMS.000
Last POS file : E:\Clients config, IP, & test results\Swath 250 Testing\Final
Report Files\Final_Data_IMUcorrect\For Bruce Frances\2011_152_S250_Stbd_GAMS.003
Output path : C:\Documents and Settings\bfrancis\My Documents\POSPac
MMS\Unnamed(2)\Mission 1\Extract
Output kernel : Mission 1
Start time : 0.000
End time : 999999.000
VNAV output modulus : 1
Opening file: E:\Clients config, IP, & test results\Swath 250 Testing\Final Report
Files\Final_Data_IMUcorrect\For Bruce Frances\2011_152_S250_Stbd_GAMS.000
307625.639: Output time 1 is in UTC time
307625.639 : Output time 2 is in POS time
307625.639 : Output distances are in POS distance
307625.639 : IMU type: IMU2 Data rate = 200 Hz
307625.639 : Extracting Group 4 : Time-tag data
307625.649 : SNV status changed to 0 (Full Nav)
307626.069 : Primary GPS receiver type is GPS13.
307626.094 : Secondary GPS receiver type is GPS13.
307626.144 : Extracting Group 10: The General Status & FDIR data.
307626.144 : GenA( 2): IIN quadrant resolved SET.
307626.144 : GenA( 3): IIN fine align active SET.
307626.144 : GenA( 4): IIN navigator initialized SET.
307626.144 : GenA( 5): IIN navigator alignment active SET.
307626.144 : GenA( 7): IIN full navigation solution SET. 307626.144 : GenA( 8): IIN initial position valid SET.
307626.144 : GenA(16): RAM config != NVM SET.
307626.144 : GenB( 0): IIN user attitude performance SET. 307626.144 : GenB( 1): IIN user heading performance SET. 307626.144 : GenB( 2): IIN user position performance SET.
307626.144 : GenB( 3): IIN user velocity performance SET.
307626.144 : GenB( 8): GAMS installation parameters valid SET. 307626.144 : GenB( 9): GAMS solution in use SET.
307626.144 : GenB(10): GAMS solution OK SET.
307626.144 : GenB(16): Primary GPS configuration file sent SET. 307626.144 : GenB(18): Primary GPS in CA mode SET. 307626.144 : GenB(23): Primary GPS observables in use SET.
307626.144 : GenB(24): GAMS secondary GPS observables in use SET.
307626.144 : GenC( 6): RTCM Type 1 or 9 in use SET. 307626.144 : GenC(13): IIN in RTCM DGPS aided mode SET.
307626.144 : FDIR1(13): Ephemeris missing SET.
     ______
307626.144 : The First Group 99: Versions & Statistics
   System Version:
      Product-Model: MV-320; Version: VER4; Serial Number: S/N3189;
      Hardware Version: HW3.3-7;
      Software Release Version-Date: SW05.03-Mar10/10;
      ICD release version: ICD04.02;
      Operating System Version: OS425B14;
      IMU Type: IMU2; Primary GPS Type: PGPS13; Secondary GPS Type: SGPS13;
     Option mnemonic-Expiry Time: DMIO;
      Option mnemonic-Expiry Time: GIMO;
     Option mnemonic-Expiry Time: RTK-0; Option mnemonic-Expiry Time: THV-0;
     Option mnemonic-Expiry Time: DPW-0;
   Primary GPS Version: BD950 SN:4808A98939, v.00232, channels:24; Secondary GPS Version: BD950 SN:4642A73565, v.00232, channels:24;
   Total Hours : 789.9; Number of Runs: 66
   Average Length of Run: 12.0; Longest Run: 84.0; Current Run: 12.2;
307626.144 : Diffcorr2 time1 gap: start 0.0, end 307626.1439
```





```
307633.139 : Message 50: Transition to NAVIGATE mode.
307633.139 : Message 37: Base 1 setup
  Input data type expected: RTCM 1 or 9
  Datum Type: NAD83
 ______
307633.139 : Message 38: Base 2 setup
  Input data type expected: RTCM 1 or 9
  Datum Type: WGS84
307633.139 : Message 20: General parameters
  Time and distance tag types:
                             2 1
  Autostart selection:
                                  ENABLED
                                -0.008 -0.031 0.130
  Reference-IMU lever arm:
  Reference-primary GPS lever arm: 1.929 -11.199 -13.076
  Reference-auxiliary 1 GPS lever arm: 0.000 0.000 0.000 Reference-IMU mounting angles: 0.000 0.000 0.000 0.000 Reference-vehicle mounting angles: 0.000 0.000 0.000 0.000
                                 LOW
  Multipath environment:
 ______
307633.139 : Message 24: User accuracy parameters
  User position accuracy: 2.00
User velocity accuracy: 0.50
  User velocity accuracy:
                          0.05
  User attitude accuracy:
  User heading accuracy:
                          0.05
 ______
______
307633.139 : Message 106: Heave ratios
  Heave Bandwidth (sec): 12.000
  Heave Damping Ratio: 0.707
______
307633.139 : Message 120: Heave and sensor 1&2 install parameters
  Reference-Sensor1 alignment angles (R,P,Y) in degrees: 0.000 0.000 0.000
  Reference-Sensor2 alignment angles (R,P,Y) in degrees: 0.000 0.000 0.000
                                                0.000 0.000 0.000
  Reference-Sensorl lever arm in meters:
                                               0.000 0.000 0.000
  Reference-Sensor2 lever arm in meters:
  Reference-Centre of Rotation in meters:
                                                0.000 0.000 0.000
307633.139 : Message 121: Vessel Installation Parameters
                                                0.00 0.00 0.00
  Reference-Vessel in meters:
  -----
307633.139 : Message 32: PCS IP address
  IP Address (Network part 1): 129
  IP Address (Network part 2): 100
  IP Address (Host part 1): 1
  IP Address (Host part 2): 231
  ______
307633.139 : Message 56: General data
  Initial status:
                 COARSE_LEVEL
                 30.339738973 -88.576114608 -17.526
  Initial position:
  Initial distance: 0.00
  Initial attitude: 0.000 0.000 0.000
   _____
307633.139 : Message 21: GAMS install parameters
  A-B antenna separation: 8.122

A-R haseline vector: 0.170 8.120 -0.003
  Heading error for calibration: 0.50
  A-B azimuth correction: 0.000
```

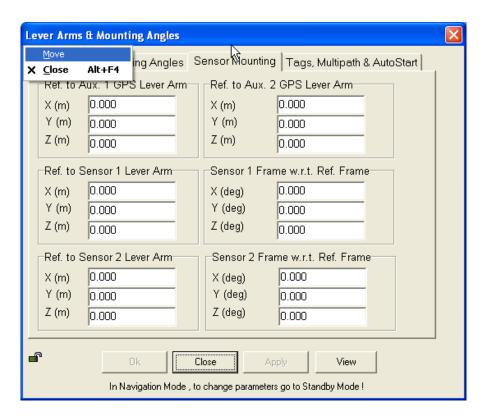




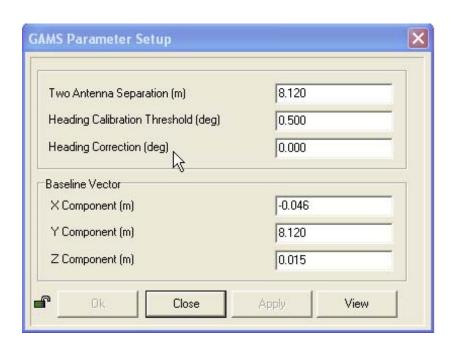
Lever Arms & Mounting Angles	
Lever Arms & Mounting Angles S	Sensor Mounting Tags, Multipath & AutoStart
Ref. to IMU Lever Arm X (m) 0 Y (m) 0 Z (m) 0	IMU Frame w.r.t. Ref. Frame X (deg) Y (deg) Z (deg)
Ref. to Primary GPS Lever Arm X (m) 1.929 Y (m) -11.199 Z (m) -13.076	J
Notes: 1. Ref. = Reference 2. w.r.t. = With Respect To 3. Reference Frame and Vessel Frame are co-aligned	Ref. to Centre of Rotation Lever Arm X (m) Y (m) D Z (m) O
- II: =	Close Apply View







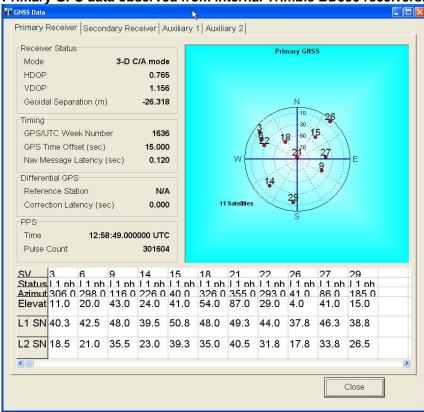
Observed GAMS values derived from the field calibration: STRB GAMS Cal #1



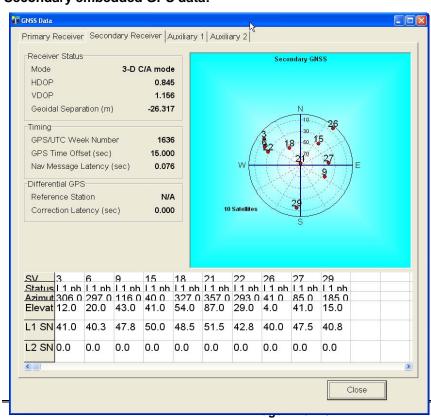




Primary GPS data observed from internal Trimble BD950 receivers.



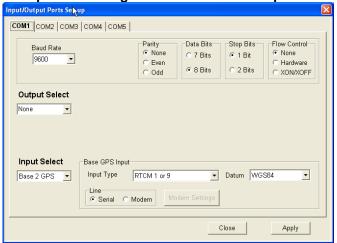
Secondary embedded GPS data:



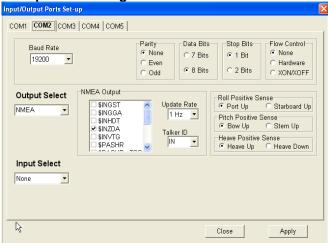




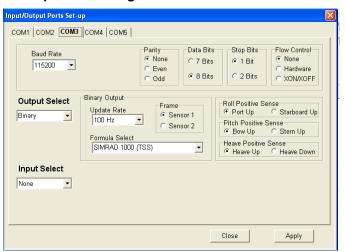
Com port #1 settings as installed: DGPS input from Trimble SPS Receiver.



Com port #2 settings as installed



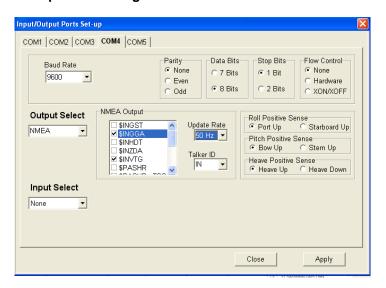
Com port #3 settings as installed:



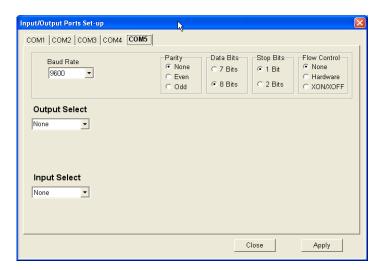




Com port #4 settings as installed:



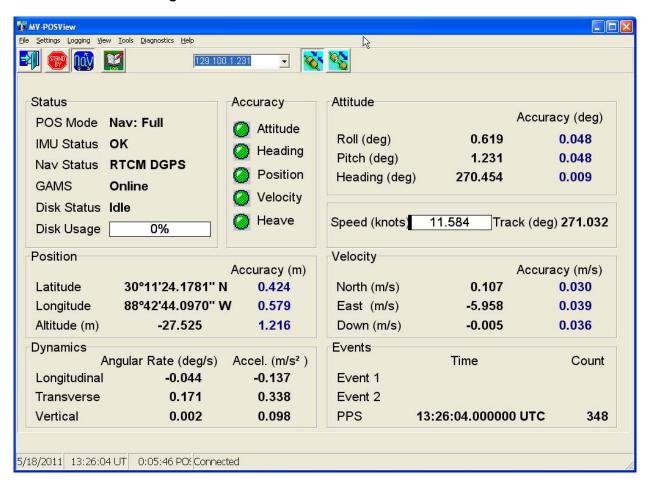
Com port #5 settings as installed







STRB POSMV Final Navigation







STRB side antenna and IMU mounting:



STRB IMU Mount







Certificate of Compliance

This document certifies that the system below meets the stated requirements.

Product	MV V5
Model	320
Sales Order #	SO 010674

Hardware Item	Part No	Serial No
POS	SAMVPCS02RM	5806
IMU TOP HAT	10004878	2423 423310

Requirement:

μPOS SA System Acceptance Test #PRO-WI-000094

Result:

Passed

Authorised signature:

Date:

Jul 26. 2013



Certificate of Compliance

This document certifies that the system below meets the stated requirements.

Product MV V5

Model 320

Sales Order # SO-010674

Hardware Item	Part No	Serial No
POS	SAMVPCS02RM	
IMU TOP HAT	10004878	2007
	10004078	2424_424204

Requirement:

μPOS SA System Acceptance Test #PRO-WI-000094

Result:

Passed

Authorised signature:

Date:

June 26. 2013

NOAA POS/MV Calibration Report

Fill out all fields! See previous years as an example.

Yellow areas require screen grabs!

Ship:	Ferdinand R. Hassler	Vessel:	2702
Snip:	refullatiu K. nassiei	vessei:	21

Date: 3/3/2016 Dn:

Personnel: Berube, Schoolcraft, Morgan

PCS Serial # IMU Serial #

IP Address: 129.100.1.231

POS controller Version (Use Menu Help > About)

POS Version (Use Menu View > Statistics)
GPS Receivers

Primary Receiver Serial #:

Secondary Receiver Serial #:

Calibration area

Location: York River

Approximate Position: Lat Lon

 37
 14
 22.5

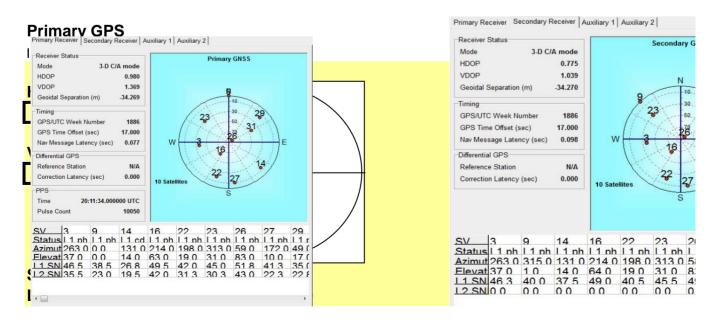
 76
 29
 58.9

DGPS Beacon Station: RTK AHB DGPS Receiver Serial#:

Frequency:

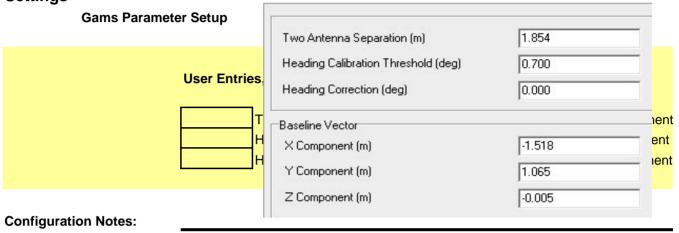
Satellite Constellation

(Use View> GPS Data)



PDOP 1.8 (Use View> GAMS Solution)

POS/MV Configuration Settings



POS/MV Calibration

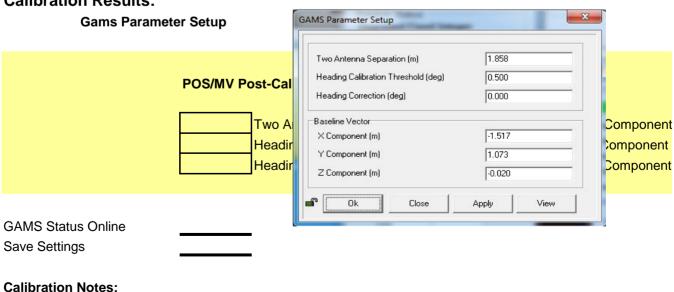
Calibration Procedure: (Refer to POS MV V4 Installation and Operation Guide, 4-25)

 Start time:
 2009

 End time:
 2011

Heading accuracy achieved for calibration: 0.230 before 0.028 after

Calibration Results:



(Use File > Store POS Settings on PC)

File Name:

General Notes:

The POS/MV uses a Right-Hand Orthogonal Reference System

The right-hand orthogonal system defines the following:

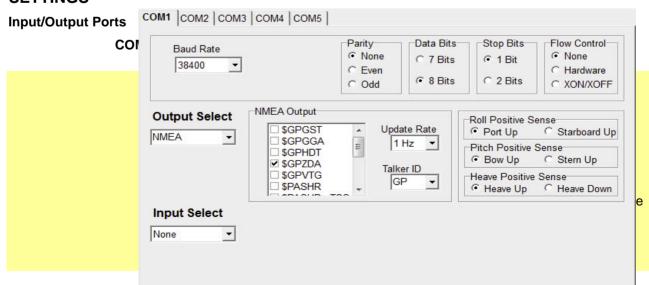
- The x-axis is in the fore-aft direction in the appropriate reference frame.
- The y-axis is perpendicular to the x-axis and points towards the right (starboard) side in the appropriate reference frame.
- The z-axis points downwards in the appropriate reference frame.

The POS/MV uses a Tate-Bryant Rotation Sequence

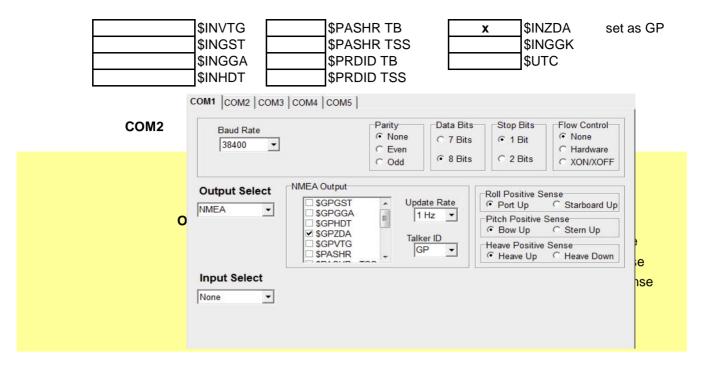
Apply the rotation in the following order to bring the two frames of reference into complete alignment:

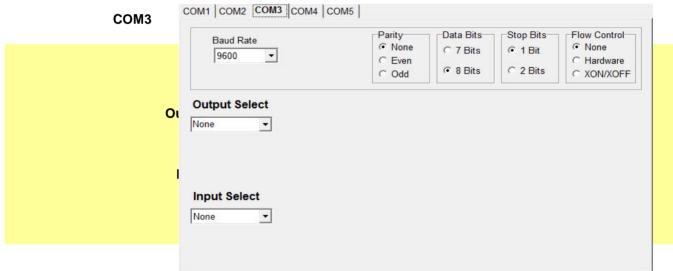
- a) Heading rotation apply a right-hand screw rotation θz about the z-axis to align one frame with the other.
- b) Pitch rotation apply a right-hand screw rotation θy about the once-rotated y-axis to align one frame with the other.
- c) Roll rotation apply a right-hand screw rotation θx about the twice-rotated x-axis to align one frame with the other.

SETTINGS

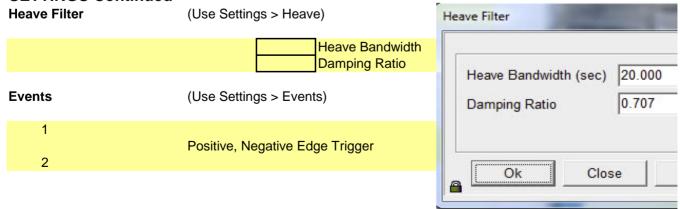


NMEA Output (selected strings shown here)



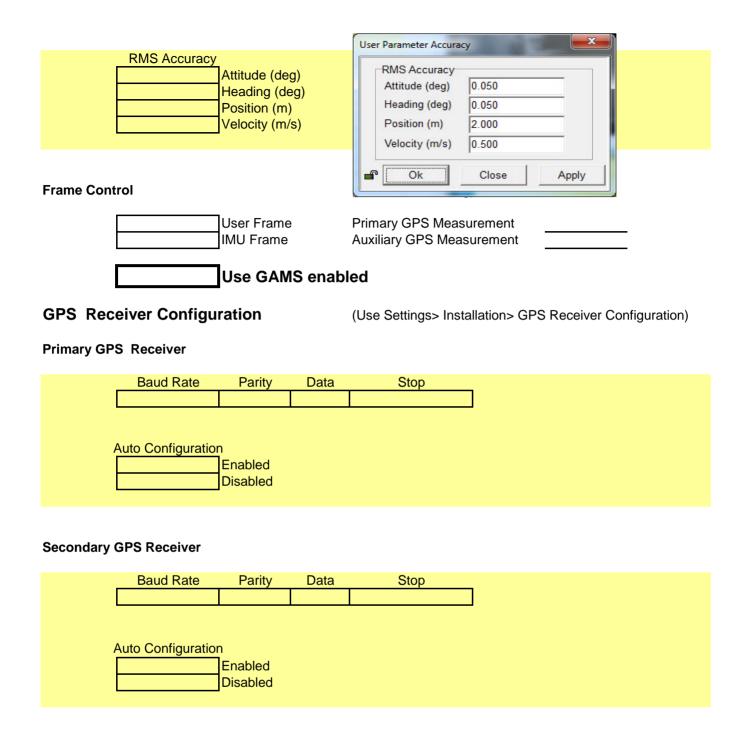






INSTALLATION (Use Settings > Installation)

Lever Arms and Mounting A Lever Arms & Mounting Angles					Arms and Offsets)
				and the same of th	r.t Reference Frame
Ref. to IMU Lever Arm		Frame w.r.t. Ref. Fra	ame		X (deg)
X (m) 0.000	X (de				Y (deg)
Y (m) 0.000	Y (de	0.000			Z (deg)
Z (m) 0.000	Z (de	g) 0.000			Duimanu Vanad Lavon Au
Ref. to Primary GPS Lever Arr	m ⊤Ref. t	to Vessel Lever Arm		erence to	Primary Vessel Lever Ar X (m)
X (m) -0.524	X (m)	0.000			Y (m)
Y (m) -0.522	Y (m		_		Z (m)
3 (1) (1)	Z (m)				
Z (m) -2.571		0.000		erence to	Centre of Rotation Leve
Notes:	Ref. t	o Centre of Rotation	Lever Arm	1	X (m)
1. Ref. = Reference	X (m)	0.000			Y (m)
2. w.r.t. = With Respect To	Y (m				Z (m)
Reference Frame and Vess	el (m)	1,000,000	_		
Frame are co-aligned		0.000			
Tags, Multipath and Auto St	Lev	ver Arms & Mounting Ang ime Tag 1 POS Time	les Sensor Mou	nting Tags, Multipath & A	Multipath and Auto Start)
	GPS C	GPS Time			
		UTC Time			
	T	ime Tag 2	1		
Time Tag 2	(4	POS Time			
	PU3	GPS Time			
	GPS	UTC Time			
	UTC L	User Time			
	000.	outoStart			
		○ Disabled • Enabled			
		riabled			
Sensor Mounting		(Use	e Settinas > I	nstallation > Senso	or Mounting)
J	Lever Ar	•		ing Tags, Multipath &	AutoStart
Reference to Aux. 1 GPS Le	V(Aux. 1 GPS Lever Arm		z. 2 GPS Lever Arm	'S Lever Arm
	X (m)	0.000	X (m)	0.000	
	Y (m)	0.000	Y (m)	0.000	
	Z (m)	0.000	Z (m)	0.000	
Reference to Sensor 1 Leve	Pof to	Sensor 1 Lever Arm	Connec 1 F	rame w.r.t. Ref. Frame	Reference Fram
Neierence to Sensor 1 Leve	1		and the same of th		Neierence i fair
	X (m) Y (m)	0.000	X (deg) Y (deg)	0.000	
	Z (m)	0.000	Z (deg)	0.000	
	_ ()	0.000		0.000	
Reference to Sensor 2 Leve	Ref. to	Sensor 2 Lever Arm	Sensor 2 F	rame w.r.t. Ref. Frame	Reference Fram
	X (m)	0.000	X (deg)	0.000	
	Y (m)	0.000	Y (deg)	0.000	
	Z (m)	0.000	Z (deg)	0.000	





,

(m) (m) (m)

(m) (m)

(m)



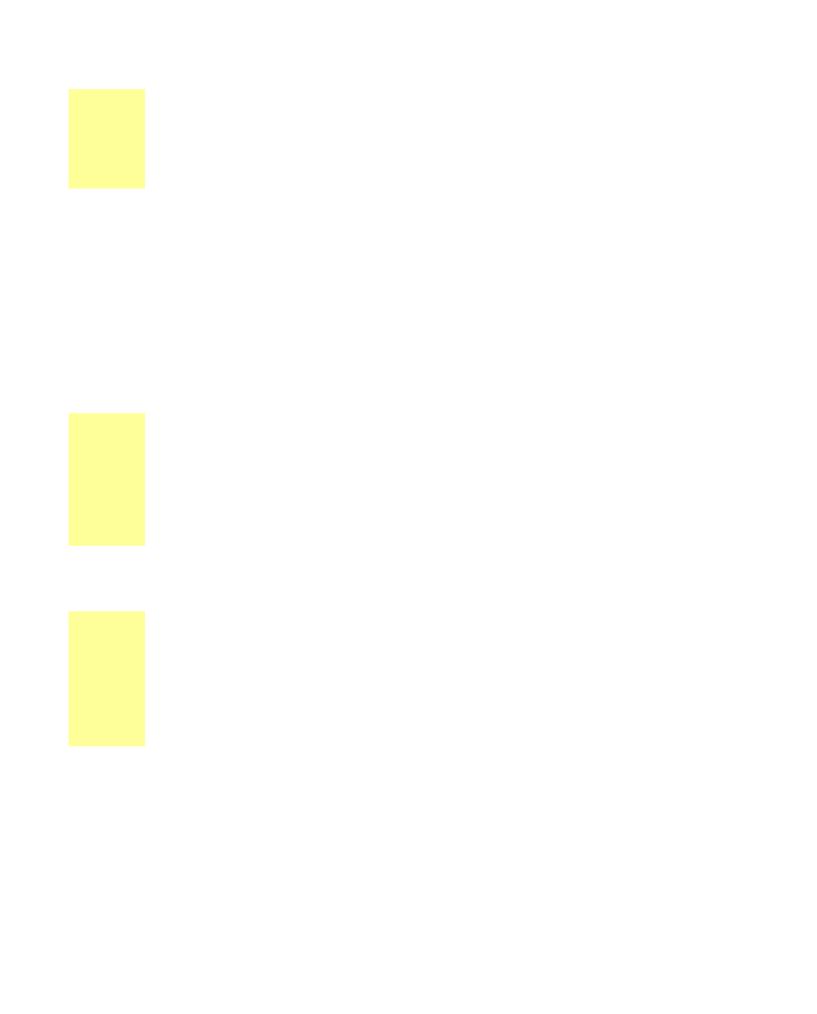


m

r Arm

ìе

ìе



NOAA POS/MV Calibration Report Fill out all fields! See previous years as an example. Yellow areas require screen grabs! Ferdinand R. Hassler **Ferdinand Hassler** Ship: Vessel: 2/11/2016 42 Date: Dn: Personnel: Berube. Wilson PCS Serial # IMU Serial # IP Address: 129.100.1.232 POS controller Version (Use Menu Help > About) 8.15 POS Version MV-320,VER5,5/N5807,HW1-03-11,SW08-23-Apr14/15,ICD07-24,OS6-4-1,IMU POS Version (Use Menu View > Statistics) GNSS Receivers Primary Receiver BD982 SN:5310K87740, v.00490, channels:224, OMNSN:1-**GPS Receivers** Primary Receiver Serial #: Secondary Receiver Statistics
Total Hours
Total Runs
861.8
Average Run (hours)107.7
Longest Run (hours) 539.2
Current Run (hours) 539.2 Secondary Receiver Serial #: Clo Calibration area Location: Chesapeake Bay, Cape Charles **Approximate Position:** Lat Latitude 37°14'38.9607" N 0.302 Lon Lonaitude 76°05'27.8236" W 0.506 **DGPS Beacon Station:** Driver, VA **DGPS Receiver Serial#:** 289 kHz Frequency: **Satellite Constellation** (Use View> GPS Data) **Primary GPS** Secondary GPS Primary Receiver | Secondary Receiver | Auxiliary 1 | Auxiliary 2 | Insert screen grabs Primary Receiver | Secondary Receiver | Auxiliary 1 | Auxiliary 2 ceiver Status 3-D DGPS mode Receiver Status OP 0.985 3-D DGPS mode OP 1.509 GPS8 GLONASS6 HDOP 0.985 oidal Separation (m) -32.720 1.502 **VDOP** Geoidal Separation (m) -32.720 1,1 30 PS/UTC Week Number 1883 2S Time Offset (sec) 17,000 GPS/LITC Week Number v Message Latency (sec) 0.209 GPS Time Offset (sec) 17.000 Nav Message Latency (sec) 0.195 ferential GPS ference Station Differential GPS rrection Latency (sec) 4.000 Reference Station Correction Latency (sec) PPS 2:26:19.000000 UTC Time BeiDou0 Pulse Count 1943086 L1 SNR > 30 LI JINN > **PDOP** 1.788 (Use View> GAMS Solution) **POS/MV Configuration** Settings **Gams Parameter Setup** Two Antenna Separation (m) 2.003 Heading Calibration Threshold (deg) 0.500 User Entries, Pre-Heading Correction (deg) 0.000 Baseline Vector

Two A

Headir

Headir

Configuration Notes:

X Component (m)

Y Component (m)

Z Component (m)

(m)

(m)

(m)

-2.003

0.016

-0.007

POS/MV Calibration

Calibration Procedure:	(Refer to POS MV V4 Installation and Operation Guide, 4-25)
Start time: aprox 0220	
End time: 236	
Heading accuracy achieved for calibration:	0.023

Calibration Results:

Gams Parameter Setup

(Use Settings > Installation > GAMS Intallation)

	Two Antenna Separation (m) Heading Calibration Threshold (deg) Heading Correction (deg)	0.500	Baseline Vector
	Baseline Vector X Component (m) Y Component (m)	-2.007 0.020	X Component (m) YComponent (m) Z Component (m)
GAMS Status Online Save Settings	Z Component (m) X X	-0.017	
Calibration Notes:			

Save POS Settings on PC

(Use File > Store POS Settings on PC)

File Name: 2012_042_Initial_GAMS

General Notes:

The POS/MV uses a Right-Hand Orthogonal Reference System

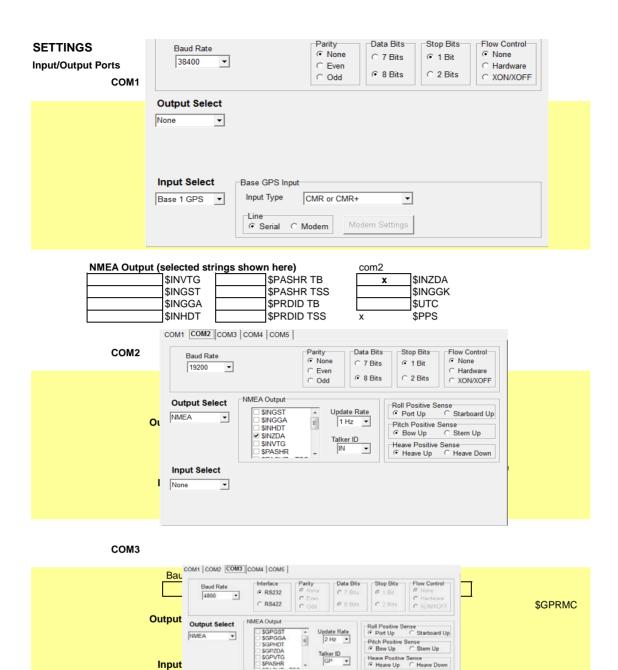
The right-hand orthogonal system defines the following:

- The x-axis is in the fore-aft direction in the appropriate reference frame.
- The y-axis is perpendicular to the x-axis and points towards the right (starboard) side in the appropriate reference frame.
- The z-axis points downwards in the appropriate reference frame.

The POS/MV uses a Tate-Bryant Rotation Sequence

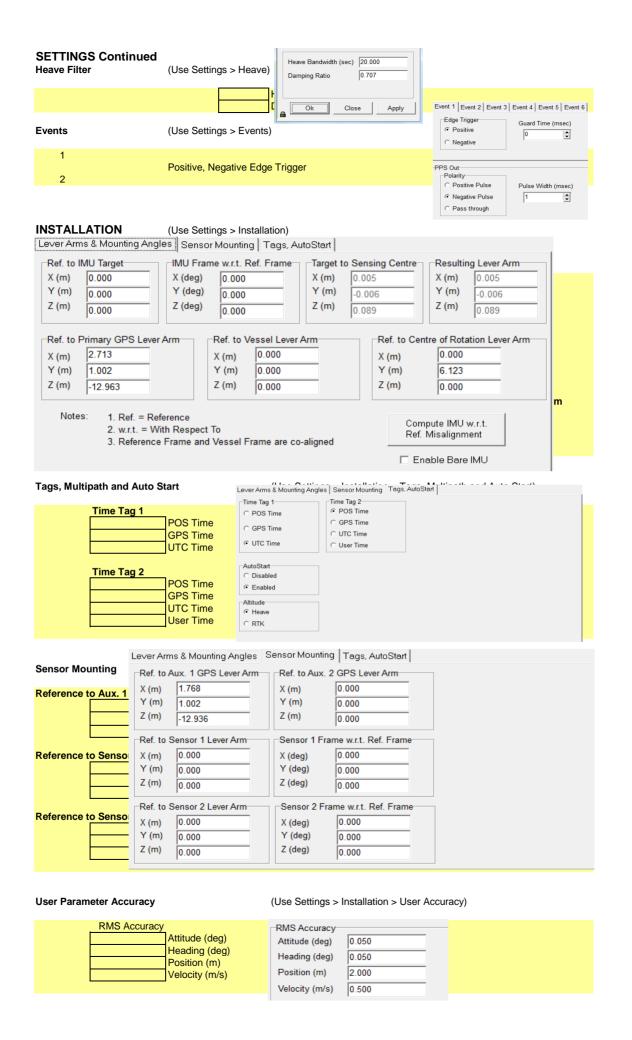
Apply the rotation in the following order to bring the two frames of reference into complete alignment:

- a) Heading rotation apply a right-hand screw rotation θz about the z-axis to align one frame with the other.
- b) Pitch rotation apply a right-hand screw rotation θy about the once-rotated y-axis to align one frame with the other.
- c) Roll rotation apply a right-hand screw rotation θx about the twice-rotated x-axis to align one frame with the other.

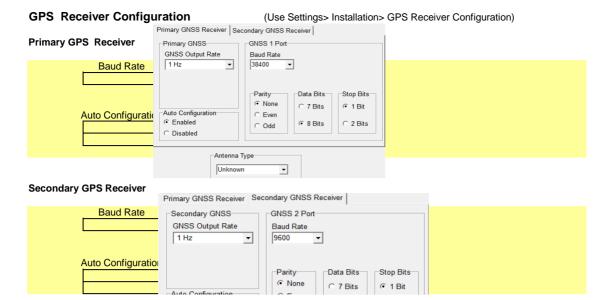


Input Select

Heave Filter



	Use GAMS enal	oled	
[User Frame IMU Frame	Primary GPS Measurement Auxiliary GPS Measurement	
Frame Cont	rol	(Use Tools > Config)	couldn't open menu



NOAA POS/MV Calibration Report

Fill out all fields! See previous years as an example. Yellow areas require screen grabs! Ferdinand R. Hassler **Ferdinand Hassler** Ship: Vessel: 2/11/2016 42 Date: Dn: Personnel: Berube. Wilson PCS Serial # IMU Serial # IP Address: 129.100.1.231 POS controller Version (Use Menu Help > About) 8.15 POS Version MV-320,VER5,S/N5807,HW1.03-11,SW08.23-Apr14/15,ICD07.24,OS6.4.1,IMU36,PGPS17,SGPS17,R POS Version (Use Menu View > Statistics) **GPS Receivers** Primary Receiver Serial #: Primary Receiver BD982 SN:5310K87740, v.00490, channels:224, OMNSN:1487740 Secondary Receiver Serial #: Secondary Receiver Calibration area Location: Chesapeake Bay, offshore Cape Charles Latitude 37°14'37.2694" N 0.396 **Approximate Position:** Longitude 76°05'27.1951" W 0.507 Lon **DGPS Beacon Station:** Driver, VA **DGPS Receiver Serial#:** 29 kHz Frequency: **Satellite Constellation** (Use View> GPS Data) **Primary GPS Secondary GPS** Insert screen grabs Note any differences from Primary GPS Receiver Receiver Status Receiver Status Mode 3-D DGPS mod 3-D DGP8 mode **HDOP** 0.985 **HDOP** 0.98 VDOP 1.510 **VDOP** 1.50 Geoidal Separation (m) Geoidal Separation (m) -32.72 VE-Timing GPS/UTC Week Number GPS Time Offset (sec) 1883 Timing-17.000 Nav Message Latency (sec) 0.208 GPS/UTC Week Number 188 Differential GPS GPS Time Offset (sec) 17.00 Reference Station 138 0.20 Nav Message Latency (sec) Correction Latency (sec) 7.000 PPS Differential GPS 2:25:46.000000 UTC Reference Station 13 Sa Pulse Count telites 1943821 Correction Latency (sec) 4.00 L1 JIVIN > LT SNR > **PDOP** 1.794 (Use View> GAMS Solution) **POS/MV Configuration** Settings GAMS Parameter Setup **Gams Parameter Setup** 2.006 Two Antenna Separation (m) 0.500 Heading Calibration Threshold (deg) User Entries, Pre-C Heading Correction (deg) 0.000 Baseline Vector Two Ant nponent (m) -2.006 X Component (m) Heading ponent (m) Y Component (m) -0.029 Heading nponent (m) Z Component (m) -0.024 **Configuration Notes:**

POS/MV Calibration

Calibration Procedure:

(Refer to POS MV V4 Installation and Operation Guide, 4-25)

Start time: Approx 0220
End time: 237

Heading accuracy achieved for calibration: 0.023

Calibration Results:

Gams Paramet	ter Setup	GAMS Parameter Setup		
	POS/MV Post-Cal	Heading Correction (deg)	0.500 0.000	
Two A	Baseline Vector X Component (m)	-2.002 -0.027 -0.031	component (m) component (m) component (m)	
GAMS Status Online Save Settings	X X			
Calibration Notes:				

Save POS Settings on PC

(Use File > Store POS Settings on PC)

File Name: 2016_042_Initial_GAMS

General Notes:

The POS/MV uses a Right-Hand Orthogonal Reference System

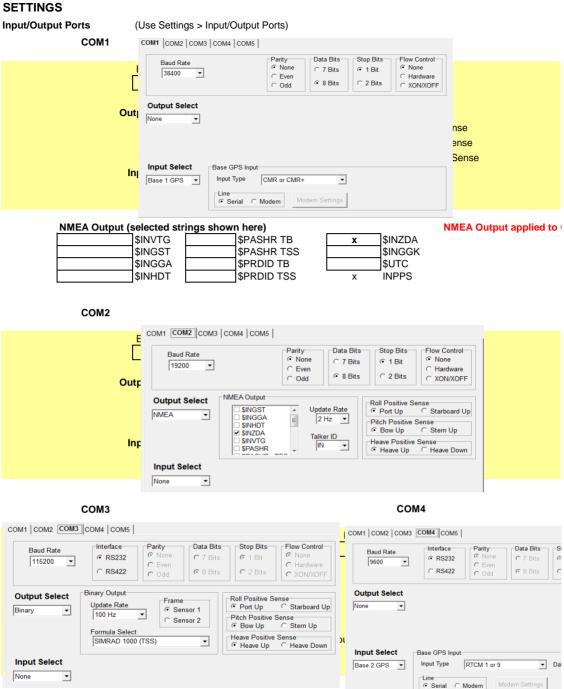
The right-hand orthogonal system defines the following:

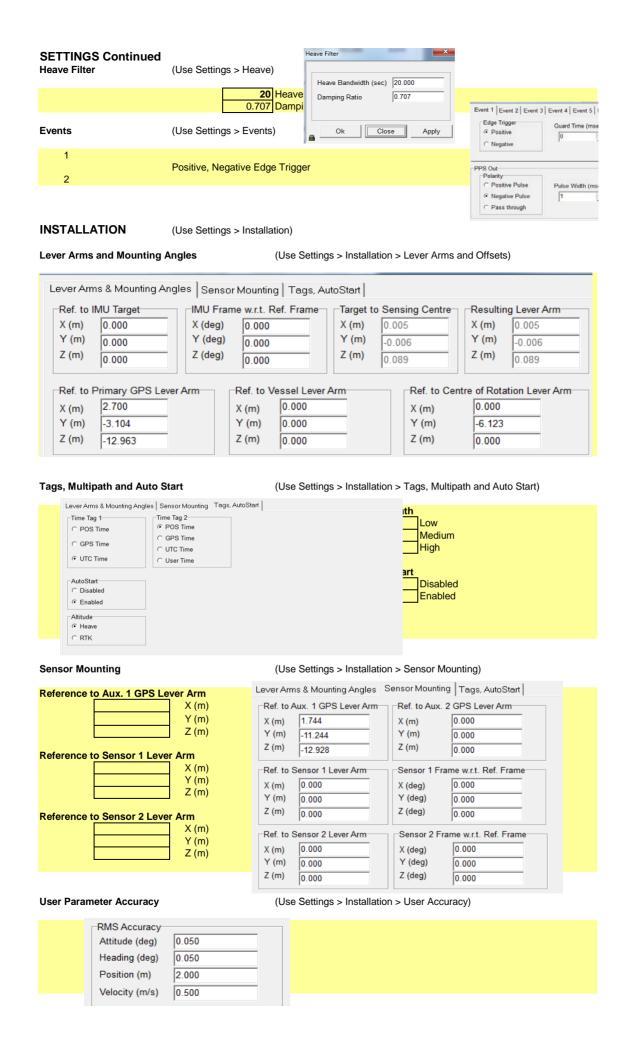
- The x-axis is in the fore-aft direction in the appropriate reference frame.
- The y-axis is perpendicular to the x-axis and points towards the right (starboard) side in the appropriate reference frame.
- The z-axis points downwards in the appropriate reference frame.

The POS/MV uses a Tate-Bryant Rotation Sequence

Apply the rotation in the following order to bring the two frames of reference into complete alignment:

- a) Heading rotation apply a right-hand screw rotation θz about the z-axis to align one frame with the other.
- b) Pitch rotation apply a right-hand screw rotation θy about the once-rotated y-axis to align one frame with the other.
- c) Roll rotation apply a right-hand screw rotation θx about the twice-rotated x-axis to align one frame with the other.

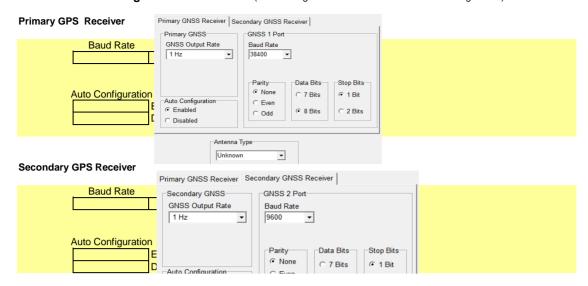




Frame Control		(Use Tools > Config)	Couldn't open menu
	lser Frame MU Frame	Primary GPS Measurement Auxiliary GPS Measurement	
u	Jse GAMS enabl	ed	

GPS Receiver Configuration

(Use Settings> Installation> GPS Receiver Configuration)



Sound Speed Sensor Reports



Certificate of Calibration

Customer:

NOAA - Marine Operations Center Atlantic

Asset Serial Number:

008609

Asset Product Type:

Micro CTD, Titanium, MVP, with Extended Temp & Cond Range

Calibration Type:

Conductivity

Calibration Range:

0 to 79 mS/cm

Calibration RMS Error: .0022

Calibration ID:

008609 006895 500349 140116 135141

Installed On:

Coefficient A: -9.800008E-3

Coefficient H: 6.757492E-14

Coefficient B: -3.740293E-7

Coefficient I:

0.000000E+0

Coefficient C: 5.527026E-9

0.000000E+0

Coefficient D: -2.108338E-11

Coefficient J:

Coefficient E: 3.141028E-5

Coefficient K: 0.000000E+0

Coefficient L: 0.000000E+0

Coefficient F: 1.198812E-9

Coefficient M: 0.000000E+0

Coefficient G: -1.771483E-11

Coefficient N: 0.000000E+0

Calibration Date (dd/mm/yyyy):

14/1/2016

Certified By:

Robert Haydock

President, AML Oceanographic

AML Oceanographic certifies that the asset described above has been calibrated or recalibrated with equipment referenced to traceable standards. Please note that Xchange[™] sensor-heads may be installed on assets other than the one listed above; this calibration certificate will still be valid when used on other such assets. If this instrument or sensor has been recalibrated, please be sure to update your records. Please also ensure that you update the instrument's coefficient values in any postprocessing software that you use, if necessary. Older generation instruments may require configuration files, which are available for download at our Customer Centre at www.AMLoceanographic.com/support



Certificate of Calibration

Customer: NOAA - Marine Operations Center Atlantic

Asset Serial Number: 008609

Asset Product Type: Micro CTD, Titanium, MVP, with Extended Temp & Cond Range

Calibration Type: Pressure
Calibration Range: 1000 dBar

Calibration RMS Error: .0516

Calibration ID: 008609 005155 999999 150116 082413

Installed On:

 Coefficient A:
 -1.233491E+2
 Coefficient H:
 0.000000E+0

 Coefficient B:
 0.000000E+0
 Coefficient J:
 0.000000E+0

 Coefficient D:
 0.000000E+0
 Coefficient K:
 0.000000E+0

 Coefficient E:
 1.898612E-2
 Coefficient L:
 0.000000E+0

 Coefficient F:
 0.000000E+0
 Coefficient M:
 -3.556292E-14

Coefficient G: 0.000000E+0 Coefficient N: 0.000000E+0

Calibration Date (dd/mm/yyyy): 15/1/2016

Certified By:

Robert Haydock

President, AML Oceanographic

AML Oceanographic certifies that the asset described above has been calibrated or recalibrated with equipment referenced to traceable standards. Please note that XchangeTM sensor-heads may be installed on assets other than the one listed above; this calibration certificate will still be valid when used on other such assets. If this instrument or sensor has been recalibrated, please be sure to update your records. Please also ensure that you update the instrument's coefficient values in any post-processing software that you use, if necessary. Older generation instruments may require configuration files, which are available for download at our Customer Centre at www.AMLoceanographic.com/support



Customer:

NOAA - Marine Operations Center Atlantic

Asset Serial Number:

008609

Asset Product Type:

Micro CTD, Titanium, MVP, with Extended Temp & Cond Range

Calibration Type:

Temperature

Calibration Range:

-2 to +45 Deg C

Calibration RMS Error: .001

Calibration ID:

008609 005155 400672 140116 135141

Installed On:

Coefficient A: -1.683849E+1

Coefficient H: 0.000000E+0

Coefficient B: 1.614658E-3

Coefficient I: 0.000000E+0

Coefficient C: -3.265849E-8

Coefficient J: 0.000000E+0

Coefficient D: 7.802240E-13

Coefficient K: 0.000000E+0 Coefficient L: 0.000000E+0

Coefficient E: -1.102127E-17 Coefficient F: 8.825508E-23

Coefficient M: 0.000000E+0

Coefficient G: -2.295774E-28

Coefficient N: 0.000000E+0

Calibration Date (dd/mm/yyyy):

14/1/2016

Certified By:

Robert Haydock

President, AML Oceanographic

AML Oceanographic certifies that the asset described above has been calibrated or recalibrated with equipment referenced to traceable standards. Please note that Xchange[™] sensor-heads may be installed on assets other than the one listed above; this calibration certificate will still be valid when used on other such assets. If this instrument or sensor has been recalibrated, please be sure to update your records. Please also ensure that you update the instrument's coefficient values in any postprocessing software that you use, if necessary. Older generation instruments may require configuration files, which are available for download at our Customer Centre at www.AMLoceanographic.com/support

AML Oceanographic

2071 Malaview Avenue, Sidney B.C. V8L 5X6 CANADA T: +1-250-656-0771 F: +1-250-655-3655 Email: service@AMLoceanographic.com



Certificate of Conformity

Customer:

Rolls-Royce Canada Limited, Naval Marine

AML Reference Number:

Sales Order #32499

Customer PO Number:

131074-13097

Asset Serial Number:

008615

Asset Product Type:

Micro CTD, Titanium, MVP, with Extended Temp & Cond Range

Housing Depth Rating:

1000 dbar / meters

Additional Description:

Certification Date (dd/mm/yyyy): 8/10/2013

Certified By:

Robert Haydock President

AML Oceanographic

AML Oceanographic certifies that the equipment described above has been tested in accordance with the product's technical specifications, brochures and / or relevant drawings. Housing depth rating refers to the maximum deployment depth of this instrument; on-board sensors may further restrict this range. AML Oceanographic certifies that calibrations on this instrument have been completed with equipment referenced to traceable standards.

Instrument configuration files and soft copy certificates are available at our on-line Customer Centre at www.AMLoceanographic.com/support



Customer:		
Asset Serial Number:		
Asset Product Type:		
Calibration Type:		
Calibration Range:		
Calibration RMS Error:		
Calibration ID:		
Installed On:		
Coefficient A:	Coefficient H:	
Coefficient B:	Coefficient I:	
Coefficient C:	Coefficient J:	
Coefficient D:	Coefficient K:	
Coefficient E:	Coefficient L:	
Coefficient F:	Coefficient M:	
Coefficient G:	Coefficient N:	
- W - W		
Calibration Date (dd/mm/yyyy):		
Certified By:		
	AM lakeatte drabbic	

Robert Haydock President, AML Oceanographic

AML Oceanographic certifies that the asset described above has been calibrated or recalibrated with equipment referenced to traceable standards. Please note that XchangeTM sensor-heads may be installed on assets other than the one listed above; this calibration certificate will still be valid when used on other such assets. If this instrument or sensor has been recalibrated, please be sure to update your records. Please also ensure that you update the instrument's coefficient values in any post-processing software that you use, if necessary. Older generation instruments may require configuration files, which are available for download at our Customer Centre at www.AMLoceanographic.com/support



Customer:		
Asset Serial Number:		
Asset Product Type:		
Calibration Type:		
Calibration Range:		
Calibration RMS Error:		
Calibration ID:		
Installed On:		
Coefficient A:	Coefficient H:	
Coefficient B:	Coefficient I:	
Coefficient C:	Coefficient J:	
Coefficient D:	Coefficient K:	
Coefficient E:	Coefficient L:	
Coefficient F:	Coefficient M:	
Coefficient G:	Coefficient N:	
- W - W		
Calibration Date (dd/mm/yyyy):		
Certified By:		
	AM lakeatte drabbic	

Robert Haydock President, AML Oceanographic

AML Oceanographic certifies that the asset described above has been calibrated or recalibrated with equipment referenced to traceable standards. Please note that XchangeTM sensor-heads may be installed on assets other than the one listed above; this calibration certificate will still be valid when used on other such assets. If this instrument or sensor has been recalibrated, please be sure to update your records. Please also ensure that you update the instrument's coefficient values in any post-processing software that you use, if necessary. Older generation instruments may require configuration files, which are available for download at our Customer Centre at www.AMLoceanographic.com/support



Customer:		
Asset Serial Number:		
Asset Product Type:		
Calibration Type:		
Calibration Range:		
Calibration RMS Error:		
Calibration ID:		
Installed On:		
Coefficient A:	Coefficient H:	
Coefficient B:	Coefficient I:	
Coefficient C:	Coefficient J:	
Coefficient D:	Coefficient K:	
Coefficient E:	Coefficient L:	
Coefficient F:	Coefficient M:	
Coefficient G:	Coefficient N:	
- W - W		
Calibration Date (dd/mm/yyyy):		
Certified By:		
	AM lakeatte drabbic	

Robert Haydock President, AML Oceanographic

AML Oceanographic certifies that the asset described above has been calibrated or recalibrated with equipment referenced to traceable standards. Please note that XchangeTM sensor-heads may be installed on assets other than the one listed above; this calibration certificate will still be valid when used on other such assets. If this instrument or sensor has been recalibrated, please be sure to update your records. Please also ensure that you update the instrument's coefficient values in any post-processing software that you use, if necessary. Older generation instruments may require configuration files, which are available for download at our Customer Centre at www.AMLoceanographic.com/support

SBE SEA-BIRD ELECTRONICS, INC. 13431 NE 20th St. Bellevue, Washington 98005 USA

Phone: (425) 643-9866 Fax: (425) 643-9954 www.seabird.com

Service					
Report	RMA Number 86435N				
Customer Information:					
Company Atlantic Marine Cent	Date 1/22/2016				
Contact Thanh Loi					
PO Number TBD					
Serial Number 19P32914-448	0				
Model Number SBE 19Plus					
Services Requested:					
Evaluate/Repair Instrumentation. Perform Routine Calibration Servi	ce.				
Problems Found:					
Services Performed:					
1. Performed initial diagnostic evalua	ation.				
2. Calibrated the pressure sensor.					
3. Performed "Post Cruise" calibration of the temperature & conductivity sensors.					
4. Performed complete system chec	c and full diagnostic evaluation.				
Special Notes:					
*					

Conductivity Calibration Report

Customer:	Atlantic Marine (Center				
Job Number:	86435N	[Date of Repo	rt:	1/12/20	016
Model Number	SBE 19Plus		Serial Numbe	er:	19P32914	l-4480
sensor drift. If the	calibration identifies a rk is completed. The 'd	ated 'as received', without of problem or indicates cell as received' calibration is	l cleaning is nece	essary, then o	a second cal	ibration is
conductivity. Users sensor condition du corrections for drift	must choose whether turing deployment. In	provided, listing the coefficithe 'as received' calibration SEASOFT enter the chose (consult the SEASOFT must data.	on or the previou en coefficients. T	s calibration The coefficie	better repr nt 'slope' all	esents the lows small
'AS RECEIVED (CALIBRATION'		✓ Perf	formed		Performed
Date: 1/12/2016		Drift sine	ce last cal:	-0.00	010	PSU/month*
Comments:						
'CALIBRATION	AFTER CLEANING	G & REPLATINIZINO	G' □ Perf	formed	✓ Not l	Performed
Date:		Drift sin	ce Last cal:			PSU/month*
Comments:						
*Measured at 3.0	S/m					

Cell cleaning and electrode replatinizing tend to 'reset' the conductivity sensor to its original condition. Lack of drift in post-cleaning-calibration indicates geometric stability of the cell and electrical stability of the sensor circuit.

13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4480 CALIBRATION DATE: 12-Jan-16

SBE 19plus CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

COEFFICIENTS:

i = -1.746279e-004j = 3.287798e-005

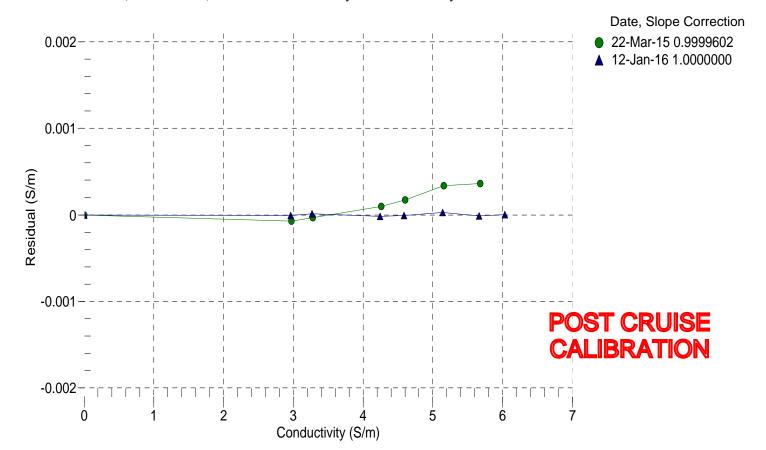
BATH TEMP	BATH SAL	BATH COND	INSTRUMENT	INSTRUMENT	RESIDUAL
(° C)	(PSU)	(S/m)	OUTPUT (Hz)	COND (S/m)	(S/m)
22.0000	0.0000	0.0000	2699.13	0.0000	0.00000
1.0000	34.6107	2.96006	5400.26	2.9601	-0.00001
4.5000	34.5927	3.26570	5604.88	3.2657	0.00001
15.0000	34.5549	4.24293	6213.17	4.2429	-0.00002
18.5000	34.5462	4.58639	6412.98	4.5864	-0.00001
24.0000	34.5361	5.14153	6723.08	5.1416	0.00003
29.0000	34.5320	5.66097	7000.42	5.6610	-0.00001
32.5000	34.5295	6.03161	7191.58	6.0316	0.00000

f = Instrument Output (Hz) / 1000.0

t = temperature (°C); p = pressure (decibars); $\delta = CTcor;$ $\epsilon = CPcor;$

Conductivity (S/m) = $(g + h * f^2 + i * f^3 + j * f^4)/10 (1 + \delta * t + \epsilon * p)$

Residual (Siemens/meter) = instrument conductivity - bath conductivity



13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4480 CALIBRATION DATE: 08-Jan-16

SBE 19plus PRESSURE CALIBRATION DATA 5076 psia S/N 3336

5000

COEFFICIENTS:

PA0 =	1.272218e+000	PTCA0	=	5.242189e+005
PA1 =	1.569654e-002	PTCA1	=	1.594674e+000
PA2 =	-6.715534e-010	PTCA2	=	8.265540e-002
PTEMPA0 =	-6.721580e+001	PTCB0	=	2.508287e+001
PTEMPA1 =	5.151440e+001	PTCB1	=	-2.500000e-005
PTEMPA2 =	-5.100431e-001	PTCB2	=	0.000000e+000

PRESSURE SPAN CALIBRATION

THERMAL CORRECTION

PRESSURE	INSTRUMENT	THERMISTOR	COMPUTED	RESIDUAL	TEMP	THERMISTOR	INSTRUMENT
(PSIA)	OUTPUT (counts)	OUTPUT (volts)	PRESSURE (PSIA)	(%FSR)	(°C)	OUTPUT (volts) OUTPUT (counts)
14.64	525160.0	1.8	14.77	0.00	32.50	1.97	525234.03
1114.89	595449.0	1.8	1114.68	-0.00	29.00	1.90	525210.10
2114.86	659716.0	1.8	2114.55	-0.01	24.00	1.80	525179.42
3114.68	724364.0	1.8	3114.76	0.00	18.50	1.69	525152.05
4114.84	789368.0	1.8	4114.81	-0.00	15.00	1.62	525137.68
5064.92	851458.0	1.8	5064.73	-0.00	4.50	1.41	525103.81
4114.83	789382.0	1.8	4115.02	0.00	1.00	1.34	525095.58
3114.71	724382.0	1.8	3115.04	0.01			
2114.84	659737.0	1.8	2114.88	0.00	TEMPER	RATURE (°C)	SPAN (mV)
1114.93	595458.0	1.8	1114.82	-0.00		-5.00	25.08
14.64	525158.0	1.8	14.73	0.00		35.00	25.08

y = thermistor output (counts)

-0.25

Ö

500

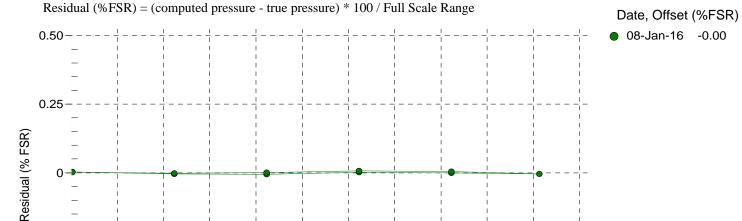
1000

 $t = PTEMPA0 + PTEMPA1 * y + PTEMPA2 * y^2$

 $x = instrument output - PTCA0 - PTCA1 * t - PTCA2 * t^2$

 $n = x * PTCB0 / (PTCB0 + PTCB1 * t + PTCB2 * t^{2})$

pressure (PSIA) = $PA0 + PA1 * n + PA2 * n^2$



-0.50 - דדדד לַדדדד לַדדדד לַדדדד לַדדדד לַדדדד לַדדדד לַדדדד לַדדדד לַדדדד לַ

2500

3000

Pressure (PSIA)

3500

4000

4500

2000

1500

13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4480 CALIBRATION DATE: 12-Jan-16

SBE 19plus TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

CALIBITATION DATE. 12-3aii-10

COEFFICIENTS:

a0 = 1.269875e-003 a1 = 2.564428e-004 a2 = 7.859616e-007 a3 = 1.180083e-007

BATH TEMP (° C)	INSTRUMENT OUTPUT (counts)	INST TEMP (° C)	RESIDUAL (° C)
1.0000	619138.288	1.0000	0.0000
4.5000	549768.712	4.4999	-0.0001
15.0000	377664.542	14.9999	-0.0001
18.5000	331462.322	18.5002	0.0002
24.0000	268748.983	23.9999	-0.0001
29.0000	221011.237	28.9999	-0.0001
32.5000	192174.712	32.5001	0.0001

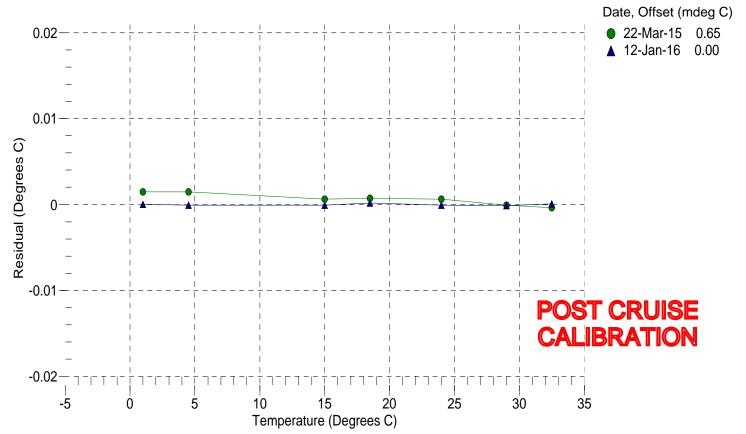
n = Instrument Output (counts)

MV = (n - 524288) / 1.6e + 007

R = (MV * 2.900e + 009 + 1.024e + 008) / (2.048e + 004 - MV * 2.0e + 005)

Temperature ITS-90 (°C) = $1/{a0 + a1[ln(R)] + a2[ln^2(R)] + a3[ln^3(R)]} - 273.15$

Residual (°C) = instrument temperature - bath temperature



Atlantic Marine Center

Temperature Calibration Report

Customer:	Atlantic Marine C	Center					
Job Number:	86435N	Date of Rep	ort:	1/12/2016			
Model Number	SBE 19Plus	Serial Numl	ber:	19P32914-4480			
Temperature sensors are normally calibrated 'as received', without adjustments, allowing a determination sensor drift. If the calibration identifies a problem, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or non-functional, or by customer request. An 'as received' calibration certificate is provided, listing coefficients to convert sensor frequency to temperature. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients. The coefficient 'offset' allows a small correction for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair apply only to subsequent data.							
'AS RECEIVED O	CALIBRATION'	✓ Pe	rformed	☐ Not Performed			
Date: 1/12/2016		Drift since last cal:	-0.000	Degrees Celsius/year			
Comments:							
'CALIBRATION	AFTER REPAIR'	□ Pe	erformed	✓ Not Performed			
Date:]	Drift since Last cal:		Degrees Celsius/year			
Comments:							



Phone: (425) 643-9866 Fax: (425) 643-9954 www.seabird.com

Service	_		- Li			
	Report	RMA	Number 8	6435N		
Customer Info	ormation:					
Company	Atlantic Marine Center			Date	1/22/2016	
Contact	Thanh Loi					
PO Number	TBD					
Serial Number	19P36399-4642					
Model Number	SBE 19Plus					
Services Requested:						
Evaluate/Repair Instrumentation. Perform Routine Calibration Service.						
Problems Fou	ınd:					
1. The switch m	The switch magnet was found to have corrosion damage.					
Services Perf	ormed:					
1. Performed in	itial diagnostic evaluatio	1.				
2. Installed NE	W switch magnet assem	bly.				
3. Calibrated the pressure sensor.						
4. Performed "Post Cruise" calibration of the temperature & conductivity sensors.						
5. Performed complete system check and full diagnostic evaluation.						
Special Notes	:					

Page 5 of 7

Atlantic Marine Center

Conductivity Calibration Report

customer:	rtianio manno t	961161				
Job Number:	86435N] [Date of Repo	rt:	1/12/20	16
Model Number	SBE 19Plus		erial Numb	er:	19P36399	4642
sensor drift. If the	calibration identifies a rk is completed. The '	ated 'as received', without c problem or indicates cell as received' calibration is n	cleaning is nec	essary, then o	a second cali	bration is
conductivity. Users sensor condition du corrections for drift	must choose whether the right of the string deployment. In	provided, listing the coeffict the 'as received' calibration SEASOFT enter the chosen (consult the SEASOFT ma nt data.	n or the previou n coefficients. T	s calibration The coefficie	n better repre nt 'slope' allo	ws small
'AS RECEIVED O	CALIBRATION'		✓ Perf	formed	□ Not P	erformed
Date: 1/12/2016		Drift since	e last cal:	-0.00	020 F	SU/month*
Comments:						
'CALIRRATION	AFTER CI FANIN	G & REPLATINIZING	' Dore	formed	✓ Not P	erformed
				ormed		
Date:		Drift sinc	e Last cal:		F	SU/month*
Comments:						
*Moasurod at 3 0	S/m					

*Measured at 3.0 S/m

Cell cleaning and electrode replatinizing tend to 'reset' the conductivity sensor to its original condition. Lack of drift in post-cleaning-calibration indicates geometric stability of the cell and electrical stability of the sensor circuit.

13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4642 CALIBRATION DATE: 12-Jan-16 SBE 19plus CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

COEFFICIENTS:

i = 7.221811e-005j = 1.200735e-005

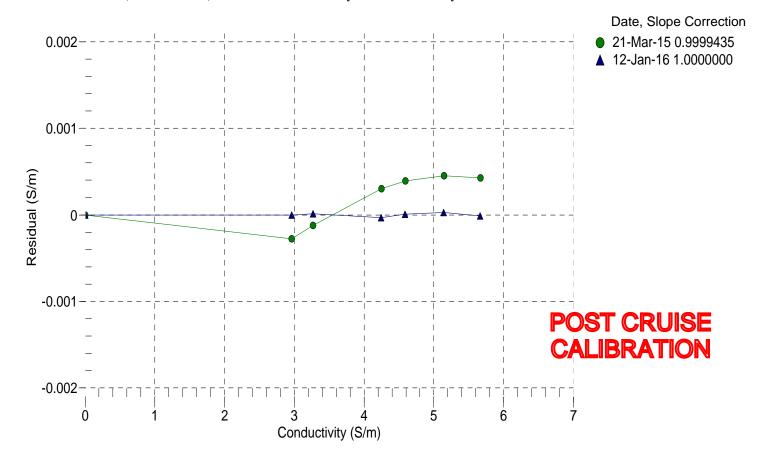
BATH TEMP (° C)	BATH SAL (PSU)	BATH COND (S/m)	INSTRUMENT OUTPUT (Hz)	INSTRUMENT COND (S/m)	RESIDUAL (S/m)
` ,	` ,	` ,	` ,	, ,	,
22.0000	0.0000	0.00000	2840.16	0.0000	0.00000
1.0000	34.6107	2.96006	5591.29	2.9601	-0.00000
4.5000	34.5927	3.26570	5800.82	3.2657	0.00001
15.0000	34.5549	4.24293	6424.28	4.2429	-0.00003
18.5000	34.5462	4.58639	6629.27	4.5864	0.00001
24.0000	34.5361	5.14153	6947.54	5.1416	0.00003
29.0000	34.5320	5.66097	7232.35	5.6610	-0.00001
32.5000	34.5295	6.03161	7428.56	6.0312	-0.00038

f = Instrument Output (Hz) / 1000.0

t = temperature (°C); p = pressure (decibars); $\delta = CTcor;$ $\epsilon = CPcor;$

Conductivity (S/m) = $(g + h * f^2 + i * f^3 + j * f^4)/10 (1 + \delta * t + \epsilon * p)$

Residual (Siemens/meter) = instrument conductivity - bath conductivity



13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4642 CALIBRATION DATE: 08-Jan-16

SBE 19plus PRESSURE CALIBRATION DATA 508 psia S/N 5632

COEFFICIENTS:

PA0 =	6.581024e-001	PTCA0	=	5.322959e+005
PA1 =	1.547891e-003	PTCA1	=	2.256678e+001
PA2 =	7.193046e-012	PTCA2	=	-1.620840e-001
PTEMPA0 =	-7.514541e+001	PTCB0	=	2.569025e+001
PTEMPA1 =	4.830836e+001	PTCB1	=	-3.500000e-004
PTEMPA2 =	-2.203947e-001	PTCB2	=	0.000000e+000

PRESSURE SPAN CALIBRATION

THERMAL CORRECTION

PRESSURE	INSTRUMENT	THERMISTOR	COMPUTED	RESIDUAL	TEMP	THERMISTOR	INSTRUMENT
(PSIA)	OUTPUT (counts)	OUTPUT (volts)	PRESSURE (PSIA)	(%FSR)	(°C)	OUTPUT (volts) OUTPUT (counts)
14.64	541747.0	2.0	14.64	0.00	32.50	2.25	542116.64
104.91	600028.0	2.0	104.90	-0.00	29.00	2.18	542074.78
204.91	664558.0	2.0	204.91	-0.00	24.00	2.07	542005.74
304.92	729042.0	2.0	304.91	-0.00	18.50	1.96	541916.37
404.92	793494.0	2.0	404.91	-0.00	15.00	1.88	541857.41
504.93	857910.0	2.0	504.92	-0.00	4.50	1.66	541653.43
404.92	793514.0	2.0	404.94	0.00	1.00	1.59	541578.71
304.93	729060.0	2.0	304.93	0.00			
204.92	664574.0	2.0	204.93	0.00	TEMPER	RATURE (°C)	SPAN (mV)
104.92	600048.0	2.0	104.93	0.00		-5.00	25.69
14.64	541755.0	2.0	14.64	-0.00		35.00	25.68

y = thermistor output (counts)

 $t = PTEMPA0 + PTEMPA1 * y + PTEMPA2 * y^2$

 $x = instrument output - PTCA0 - PTCA1 * t - PTCA2 * t^2$

 $n = x * PTCB0 / (PTCB0 + PTCB1 * t + PTCB2 * t^{2})$

pressure (PSIA) = $PA0 + PA1 * n + PA2 * n^2$ Residual (%FSR) = (computed pressure - true pressure) * 100 / Full Scale Range Date, Offset (%FSR) 08-Jan-160.00 0.50 -0.25 Residual (% FSR) -0.25-0.50 - \top \top \top \top Ö 200 50 100 150 250 300 350 400 450 500 550

Pressure (PSIA)

13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4642 CALIBRATION DATE: 12-Jan-16 SBE 19plus TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

COEFFICIENTS:

a0 = 1.184792e-003 a1 = 2.769344e-004 a2 = -1.221819e-006 a3 = 2.009333e-007

BATH TEMP (° C)	INSTRUMENT OUTPUT (counts)	INST TEMP (° C)	RESIDUAL (° C)
1.0000	625326.780	1.0000	0.0000
4.5000	556563.966	4.4999	-0.0001
15.0000	385279.492	15.0000	0.0000
18.5000	339089.847	18.5001	0.0001
24.0000	276210.542	23.9999	-0.0001
29.0000	228181.881	29.0000	0.0000
32.5000	199092.915	32.5000	0.0000

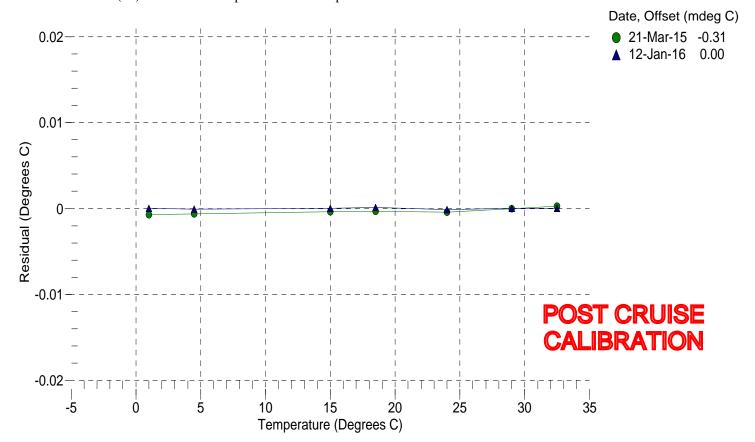
n = Instrument Output (counts)

MV = (n - 524288) / 1.6e + 007

R = (MV * 2.900e+009 + 1.024e+008) / (2.048e+004 - MV * 2.0e+005)

Temperature ITS-90 (°C) = $1/{a0 + a1[ln(R)] + a2[ln^2(R)] + a3[ln^3(R)]} - 273.15$

Residual ($^{\circ}$ C) = instrument temperature - bath temperature



Customer:

Atlantic Marine Center

Phone: (425) 643-9866 Fax: (425) 643-9954 www.seabird.com

Temperature Calibration Report

Job Number:	86435N	Date o	f Report:	:	1/12/2016
Model Number	SBE 19Plus	Serial	Number:		19P36399-4642
the calibration iden	tifies a problem, then	nted 'as received', without adjustm a second calibration is performed is damaged or non-functional, or	after work	is complei	v v
must choose whethe during deployment.	er the 'as received' call In SEASOFT enter t	provided, listing coefficients to con ibration or the previous calibration he chosen coefficients. The coeff ASOFT manual). Calibration coefficients	n better rep icient 'offse	oresents the et' allows o	ne sensor condition on small correction for over a repair apply only to
'AC DECEIVED ('AT IDD ATION'	ū	/ Danfar		Not Domformed
'AS RECEIVED C		[Perfor		Not Performed
		Drift since last		med -0.00038	
Date: 1/12/2016		Drift since last	cal:	-0.00038	Degrees Celsius/year Not Performed
Date: 1/12/2016 Comments:			cal:	-0.00038	Degrees Celsius/year



Phone: (425) 643-9866 Fax: (425) 643-9954 www.seabird.com

Service	_					
	Report		RMA Number	8643	5N	
Customer Info	ormation:					
Company	Atlantic Marine Cente	r			Date	1/22/2016
Contact	Thanh Loi					
PO Number	TBD					
Serial Number	er 19P65591-6918	3				
Model Number	er SBE 19Plus					
Services Req						
Evaluate/Rep Perform Rou	oair Instrumentation. tine Calibration Servic	е.				
Problems Fou						
1. No comms u	pon arrival. The U21 (component was f	ound to be bad.			
Services Perf	ormed:					
Performed in	iitial diagnostic evaluat	tion.				
2. Performed in	ternal inspection and	O-ring replaceme	ent.			
3. Performed hy	ydrostatic pressure tes	st.				
4. Calibrated th	e pressure sensor.					
5. Performed "F	Post Cruise" calibration	of the temperati	ure & conductivity se	nsors.		
6. Performed co	omplete system check	and full diagnost	ic evaluation.			
Special Notes	3:					

Conductivity Calibration Report

Customer:	Atlantic Marine (Center			
Job Number:	86435N	Date of 1	Report:	1/18	3/2016
Model Number	SBE 19Plus	Serial N	umber:	19P655	591-6918
sensor drift. If the	calibration identifies a rk is completed. The 'd	ted 'as received', without cleaning of problem or indicates cell cleaning as received' calibration is not perfor	is necessary	, then a second	calibration is
conductivity. Users sensor condition du corrections for drift	must choose whether t cring deployment. In S	provided, listing the coefficients used the 'as received' calibration or the p SEASOFT enter the chosen coefficien (consult the SEASOFT manual). Cont data.	revious cali ents. The co	ibration better ro oefficient 'slope'	epresents the allows small
'AS RECEIVED C	CALIBRATION'	✓	Perform	ed 🗆 No	ot Performed
Date: 1/16/2016		Drift since last ca	ıl:	-0.00040	PSU/month
Comments:					
'CALIBRATION	AFTER CLEANING	G & REPLATINIZING'	Perform	ed ☑ No	ot Performed
Date:		Drift since Last c	al:		PSU/month
Comments:					

*Measured at 3.0 S/m

Cell cleaning and electrode replatinizing tend to 'reset' the conductivity sensor to its original condition. Lack of drift in post-cleaning-calibration indicates geometric stability of the cell and electrical stability of the sensor circuit.

13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 6918 CALIBRATION DATE: 16-Jan-16 SBE 19plus V2 CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

COEFFICIENTS:

j = 5.253847e-005

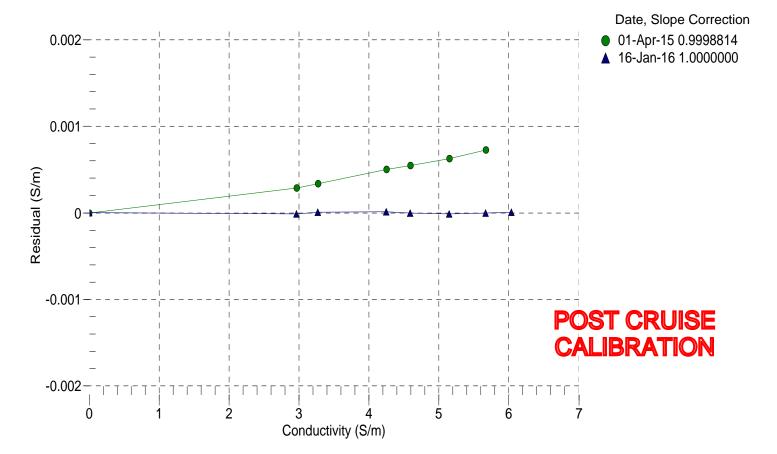
BATH TEMP	BATH SAL	BATH COND	INSTRUMENT	INSTRUMENT	RESIDUAL
(° C)	(PSU)	(S/m)	OUTPUT (Hz)	COND (S/m)	(S/m)
22.0000	0.0000	0.0000	2523.01	0.0000	0.00000
1.0000	34.6520	2.96326	5048.12	2.9632	-0.00001
4.4999	34.6323	3.26906	5239.42	3.2691	0.00001
15.0000	34.5899	4.24677	5808.17	4.2468	0.00001
18.5000	34.5812	4.59053	5995.06	4.5905	-0.00000
24.0000	34.5717	5.14625	6285.15	5.1462	-0.00001
29.0000	34.5669	5.66605	6544.54	5.6660	-0.00000
32.5000	34.5646	6.03704	6723.36	6.0371	0.00001

f = Instrument Output (Hz) / 1000.0

 $t = temperature \ (^{\circ}C); \quad p = pressure \ (decibars); \quad \delta = CTcor; \quad \epsilon = CPcor;$

Conductivity (S/m) = $(g + h * f^2 + i * f^3 + j * f^4)/10 (1 + \delta * t + \epsilon * p)$

 $Residual \ (Siemens/meter) = instrument \ conductivity \ - \ bath \ conductivity$



13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 6918 CALIBRATION DATE: 13-Jan-16

SBE 19plus V2 PRESSURE CALIBRATION DATA 508 psia S/N 3313900

COEFFICIENTS:

PA0 =	7.710222e-002	PTCA0	=	5.245112e+005
PA1 =	1.547684e-003	PTCA1	=	4.210420e+000
PA2 =	7.017601e-012	PTCA2	=	-1.040188e-001
PTEMPA0 =	-5.538239e+001	PTCB0	=	2.490900e+001
PTEMPA1 =	5.427974e+001	PTCB1	=	-1.400000e-003
PTEMPA2 =	-2.598829e-001	PTCB2	=	0.000000e+000

PRESSURE SPAN CALIBRATION

THERMAL CORRECTION

PRESSURE	INSTRUMENT	THERMISTOR	COMPUTED	RESIDUAL	TEMP	THERMISTO	R INSTRUMENT
(PSIA)	OUTPUT (counts)	OUTPUT (volts)	PRESSURE (PSIA)) (%FSR)	(°C)	OUTPUT (volt	s) OUTPUT (counts)
14.50	533864.0	1.4	14.51	0.00	32.50	1.63	534094.54
104.77	592086.0	1.4	104.76	-0.00	29.00	1.57	534103.05
204.78	656554.0	1.4	204.75	-0.01	24.00	1.47	534110.55
304.78	720997.0	1.4	304.76	-0.00	18.50	1.37	534110.58
404.78	785406.0	1.4	404.78	-0.00	15.00	1.30	534106.91
504.79	849770.0	1.4	504.78	-0.00	4.50	1.11	534084.83
404.79	785427.0	1.4	404.81	0.00	1.00	1.04	534072.70
304.79	721032.0	1.4	304.81	0.00			
204.79	656582.0	1.4	204.79	0.00	TEMPER	RATURE (°C)	SPAN (mV)
104.79	592120.0	1.4	104.81	0.00		-5.00	24.92
14.51	533867.0	1.4	14.51	0.00		35.00	24.86

y = thermistor output (counts)

50

100

150

250

300

Pressure (PSIA)

350

400

450

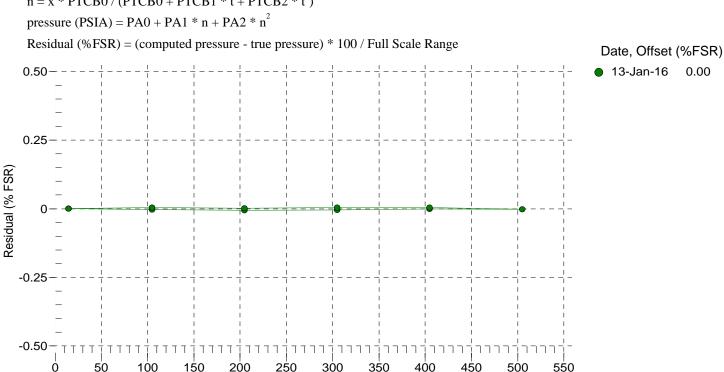
500

550

 $t = PTEMPA0 + PTEMPA1 * y + PTEMPA2 * y^2$

 $x = instrument output - PTCA0 - PTCA1 * t - PTCA2 * t^2$

 $n = x * PTCB0 / (PTCB0 + PTCB1 * t + PTCB2 * t^{2})$



13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 6918 CALIBRATION DATE: 16-Jan-16 SBE 19plus V2 TEMPERATURE CALIBRATION DATA

ITS-90 TEMPERATURE SCALE

COEFFICIENTS:

a0 = 1.290840e-003 a1 = 2.693568e-004 a2 = -9.878554e-007 a3 = 1.738923e-007

BATH TEMP	INSTRUMENT	INST TEMP	RESIDUAL
(° C)	OUTPUT (counts)	(° C)	(° C)
1.0000	563963.644	0.9999	-0.0001
4.4999	497041.780	4.5000	0.0001
15.0000	333872.034	14.9999	-0.0001
18.5000	290815.186	18.4999	-0.0001
24.0000	232913.610	24.0000	0.0000
29.0000	189289.966	29.0001	0.0001
32.5000	163143.678	32.4999	-0.0001

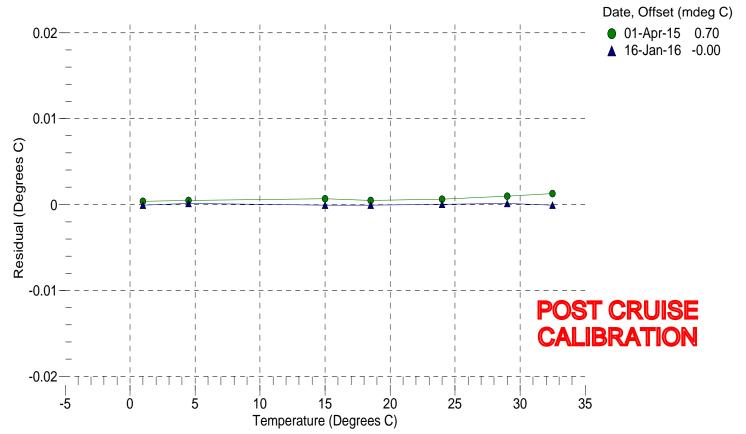
n = Instrument Output (counts)

MV = (n - 524288) / 1.6e + 007

R = (MV * 2.900e + 0.09 + 1.024e + 0.08) / (2.048e + 0.04 - MV * 2.0e + 0.05)

Temperature ITS-90 (°C) = $1/{a0 + a1[ln(R)] + a2[ln^2(R)] + a3[ln^3(R)]} - 273.15$

Residual (°C) = instrument temperature - bath temperature



Comments:

Temperature Calibration Report

Customer:	Atlantic Marine C	zenter		
Job Number:	86435N	Date of Ro	eport:	1/18/2016
Model Number	SBE 19Plus	Serial Nu	mber:	19P65591-6918
If the calibration id calibration is not po An 'as received' cal must choose wheth during deployment.	lentifies a problem, the erformed if the sensor libration certificate is p er the 'as received' cali In SEASOFT enter to ations (consult the SE	nted 'as received', without adjustments on a second calibration is performed aj is damaged or non-functional, or by corovided, listing coefficients to convert fibration or the previous calibration be the chosen coefficients. The coefficient ASOFT manual). Calibration coefficients	fter work is com ustomer reques sensor frequen etter represents nt 'offset' allows	the contraction of the contracti
Date: 1/16/2016		Drift since last cal:	-0.0008	B Degrees Celsius/year
Comments:				
'CALIBRATION	AFTER REPAIR'	□ 1	Performed	✓ Not Performed
Date:		Drift since Last cal	l :	Degrees Celsius/year

Conductivity Calibration Report

Customer:	Atlantic Marine (Center	
Job Number:	83595	Date of Rep	oort: 4/2/2015
Model Number	SBE 45	Serial Num	ber: 4553332-0276
sensor drift. If the	calibration identifies a ork is completed. The 'c	ted 'as received', without cleaning or ad problem or indicates cell cleaning is no as received' calibration is not performed	ecessary, then a second calibration is
conductivity. Users sensor condition di corrections for drif	must choose whether turing deployment. In	provided, listing the coefficients used to o the 'as received' calibration or the previous SEASOFT enter the chosen coefficients. (consult the SEASOFT manual). Calibrated at a.	ous calibration better represents the The coefficient 'slope' allows small
'AS RECEIVED	CALIBRATION'	✓ Pe	erformed
Date: 3/25/2015	5	Drift since last cal:	-0.00660 PSU/mon t
Comments:			
'CALIBRATION	AFTER CLEANING	G & REPLATINIZING' ✓ Pe	erformed
Date: 4/2/2015		Drift since 19 Mar 14	4 +0.00160 PSU/mon t
Comments:			
*Measured at 3 () S/m		

Cell cleaning and electrode replatinizing tend to 'reset' the conductivity sensor to its original condition. Lack of drift in post-cleaning-calibration indicates geometric stability of the cell and electrical stability of the sensor circuit.

13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 0276 CALIBRATION DATE: 02-Apr-15

SBE 45 CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

COEFFICIENTS:

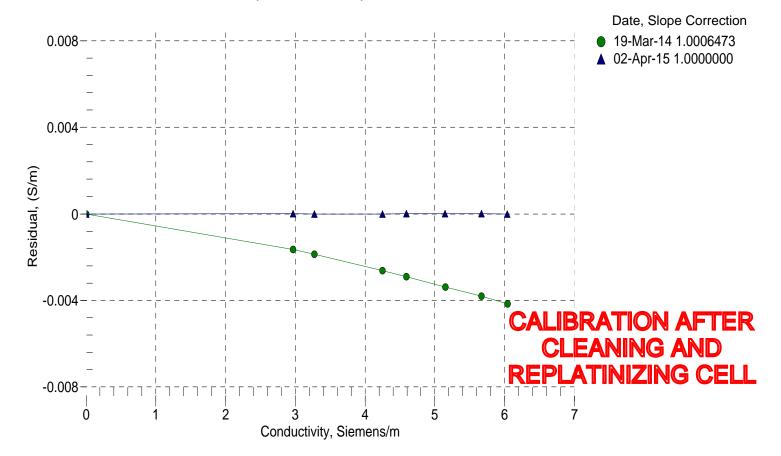
BATH TEMP (ITS-90)	BATH SAL (PSU)	BATH COND (Siemens/m)	INST FREQ (Hz)	INST COND (Siemens/m)	RESIDUAL (Siemens/m)
22.0000	0.0000	0.0000	2527.81	0.00000	0.00000
1.0000	34.6697	2.96463	5027.82	2.96463	0.00001
4.5000	34.6499	3.27057	5217.49	3.27056	-0.00000
15.0000	34.6072	4.24867	5781.55	4.24866	-0.00001
18.4999	34.5981	4.59253	5966.93	4.59253	0.00000
24.0000	34.5881	5.14842	6254.71	5.14843	0.00001
29.0000	34.5829	5.66838	6512.06	5.66838	0.00000
32 5000	34 5803	6 03947	6689 49	6 03947	-0 00000

f = INST FREQ * sqrt(1.0 + WBOTC * t) / 1000.0

Conductiv ity = $(g + h * f^2 + i * f^3 + j * f^4) / (1 + \delta * t + \epsilon * p)$ Siemens / meter

 $t = temperatur e[^{\circ}C)$; p = pressure[decibars]; $\delta = CTcor$; $\epsilon = CPcor$;

Residual = instrument conductivity - bath conductivity



13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 0276 CALIBRATION DATE: 25-Mar-15

SBE 45 CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

COEFFICIENTS:

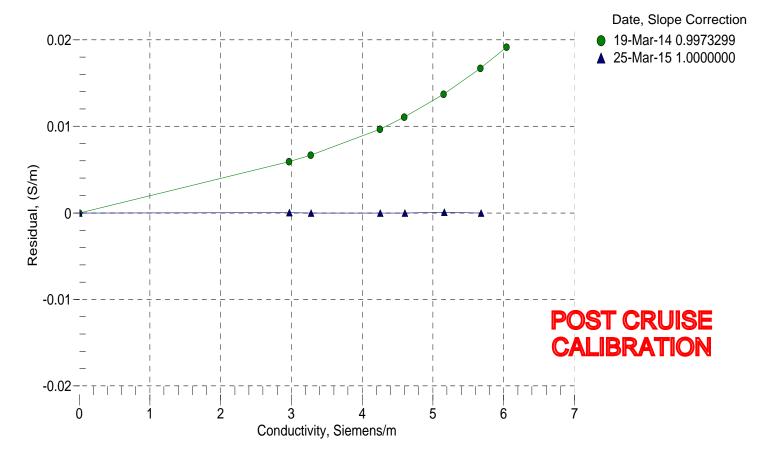
BATH TEMP	BATH SAL	BATH COND	INST FREQ	INST COND	RESIDUAL
(ITS-90)	(PSU)	(Siemens/m)	(Hz)	(Siemens/m)	(Siemens/m)
22.0000	0.0000	0.0000	2528.66	0.00000	0.00000
1.0000	34.7572	2.97139	5027.34	2.97144	0.00005
4.5000	34.7372	3.27800	5216.82	3.27795	-0.00004
15.0000	34.6945	4.25825	5780.06	4.25821	-0.00004
18.5000	34.6851	4.60284	5965.01	4.60284	-0.00000
23.9999	34.6747	5.15988	6251.92	5.15996	0.00008
29.0000	34.6686	5.68084	6508.16	5.68080	-0.00004
32.5000	34.6643	6.05248	6684.37	6.05184	-0.00064

f = INST FREQ * sqrt(1.0 + WBOTC * t) / 1000.0

Conductivity = $(g + h * f^2 + i * f^3 + j * f^4) / (1 + \delta * t + \epsilon * p)$ Siemens / meter

 $t = temperatur e[^{\circ}C)$; p = pressure[decibars]; $\delta = CTcor$; $\epsilon = CPcor$;

Residual = instrument conductivity - bath conductivity



13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 0276 CALIBRATION DATE: 02-Apr-15

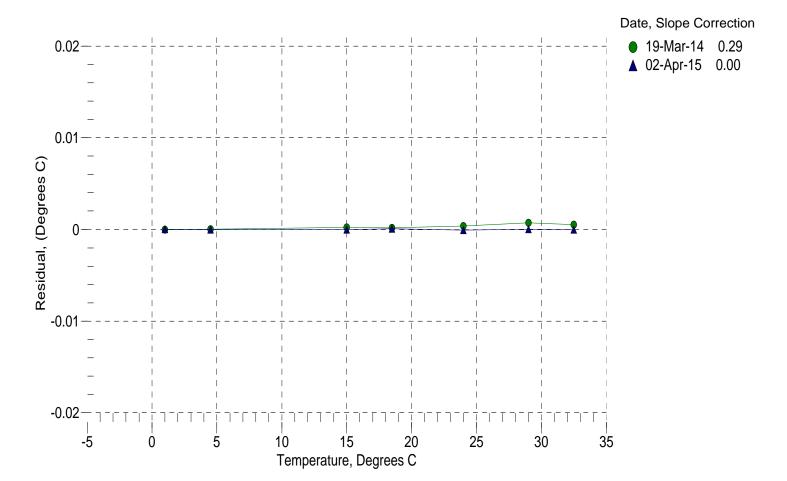
SBE 45 TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

COEFFICIENTS:

a0 = 5.804378e-005 a1 = 2.697794e-004 a2 = -2.132790e-006 a3 = 1.422788e-007

BATH TEMP (ITS-90)	INSTRUMENT OUTPUT	INST TEMP (ITS-90)	RESIDUAL (ITS-90)
1.0000	695531.4	1.0000	0.0000
4.5000	593246.7	4.5000	-0.0000
15.0000	375471.7	15.0000	-0.0000
18.4999	324402.1	18.5000	0.0001
24.0000	259368.8	23.9999	-0.0001
29.0000	212934.6	29.0000	0.0000
32.5000	186093.8	32.5000	-0.0000

Temperature ITS-90 = $1/{a0 + a1[ln(n)] + a2[ln^2(n)] + a3[ln^3(n)]} - 273.15$ (°C) Residual = instrument temperature - bath temperature n = instrument output



13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

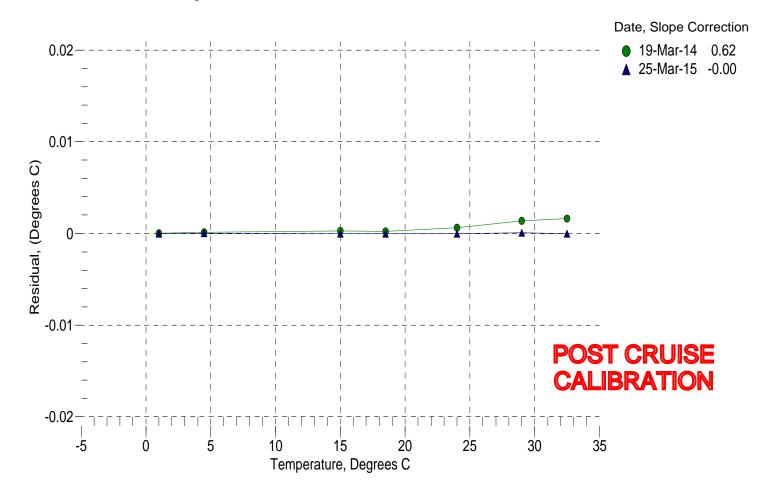
SENSOR SERIAL NUMBER: 0276 CALIBRATION DATE: 25-Mar-15 SBE 45 TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

COEFFICIENTS:

a0 = 1.670173e-005 a1 = 2.793181e-004 a2 = -2.866220e-006 a3 = 1.610718e-007

BATH TEMP (ITS-90)	INSTRUMENT OUTPUT	INST TEMP (ITS-90)	RESIDUAL (ITS-90)
1.0000	695533.7	1.0000	-0.0000
4.5000	593248.4	4.5000	0.0000
15.0000	375472.6	15.0000	-0.0000
18.5000	324403.0	18.5000	-0.0000
23.9999	259371.7	23.9999	-0.0000
29.0000	212939.7	29.0001	0.0001
32.5000	186101.7	32.5000	-0.0000

Temperature ITS-90 = $1/\{a0 + a1[ln(n)] + a2[ln^2(n)] + a3[ln^3(n)]\}$ - 273.15 (°C) Residual = instrument temperature - bath temperature n = instrument output



Customer:

Atlantic Marine Center

Phone: (425) 643-9866 Fax: (425) 643-9954 www.seabird.com

Temperature Calibration Report

Job Number:	83595	Date of R	eport:	4/2/2015	
Model Number	SBE 45	Serial Nu	mber:	4553332-02	76
the calibration ident	ifies a problem, then	ated 'as received', without adjustment a second calibration is performed aft is damaged or non-functional, or by	er work is co	ompleted. The 'as rec	0 0
must choose whether during deployment.	r the 'as received' cali In SEASOFT enter to tions (consult the SE.	provided, listing coefficients to conver ibration or the previous calibration b he chosen coefficients. The coefficie ASOFT manual). Calibration coeffic	etter represo nt 'offset' a ients obtain	ents the sensor condit illows a small correcti ned after a repair appi	tion ion for
'AS DECEIVED C	AT IRRATION!		Darfarma	d Not Dor	formed
	ALIBRATION'		Performe		rformed
'AS RECEIVED C. Date: 3/25/2015	ALIBRATION'	Drift since last cal			rformed Celsius/year
	ALIBRATION'				
Date: 3/25/2015		Drift since last cal		Degrees C	Celsius/year
Date: 3/25/2015 Comments:		Drift since last cal	e: -0.0	Degrees C	Celsius/year

Conductivity Calibration Report

Customer:	Atlantic Marine C	Center				
Job Number:	83595		Date of Repor	rt:	4/2/201	5
Model Number	SBE 45		Serial Numbe	er:	4553332-0)277
sensor drift. If the	calibration identifies a rk is completed. The 'd	ted 'as received', without problem or indicates ce as received' calibration is	ll cleaning is nece	ssary, then d	a second calib	ration is
conductivity. Users sensor condition du corrections for drift	must choose whether t cring deployment. In S	rovided, listing the coeff the 'as received' calibrat SEASOFT enter the chos (consult the SEASOFT n nt data.	on or the previous en coefficients. T	s calibration The coefficien	better repre nt 'slope' allo	ws small
'AS RECEIVED C	CALIBRATION'		✓ Perf	ormed	□ Not P	erformed
Date: 3/25/2015		Drift sin	ce last cal:	-0.00	340 P	SU/month*
Comments:						
'CALIBRATION	AFTER CLEANING	G & REPLATINIZIN	G' ✓ Perf	ormed	□ Not P	erformed
Date: 4/2/2015		Drift sir	ce 08 Mar 14	+0.00	0010 P	SU/month*
Comments:						
*Measured at 3.0	S/m					

Cell cleaning and electrode replatinizing tend to 'reset' the conductivity sensor to its original condition. Lack of drift in post-cleaning-calibration indicates geometric stability of the cell and electrical stability of the sensor circuit.

13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 0277 CALIBRATION DATE: 02-Apr-15

SBE 45 CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

COEFFICIENTS:

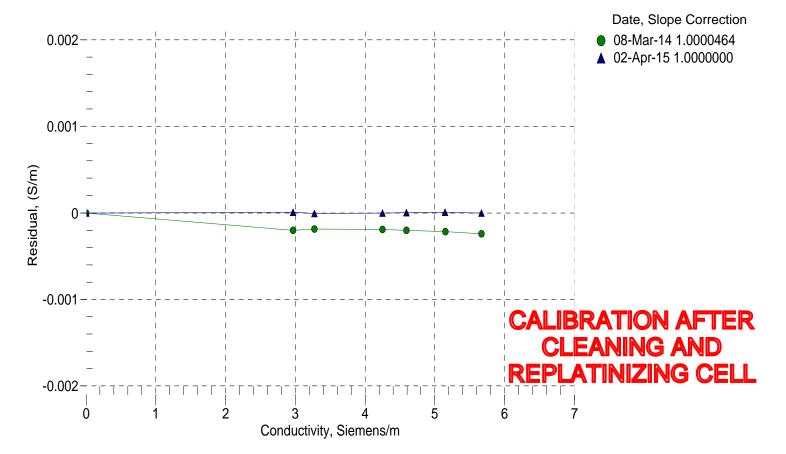
BATH TEMP	BATH SAL	BATH COND	INST FREQ	INST COND	RESIDUAL
(ITS-90)	(PSU)	(Siemens/m)	(Hz)	(Siemens/m)	(Siemens/m)
22.0000	0.0000	0.0000	2527.75	0.00000	0.00000
1.0000	34.6697	2.96463	5074.20	2.96463	0.00001
4.5000	34.6499	3.27057	5266.78	3.27056	-0.00001
15.0000	34.6072	4.24867	5839.29	4.24866	-0.00000
18.4999	34.5981	4.59253	6027.38	4.59253	0.00000
24.0000	34.5881	5.14842	6319.31	5.14843	0.00001
29.0000	34.5829	5.66838	6580.32	5.66837	-0.00000
32.5000	34.5803	6.03947	6760.30	6.03957	0.00010

f = INST FREQ * sqrt(1.0 + WBOTC * t) / 1000.0

Conductiv ity = $(g + h * f^2 + i * f^3 + j * f^4) / (1 + \delta * t + \epsilon * p)$ Siemens / meter

 $t = temperatur e[^{\circ}C)$; p = pressure[decibars]; $\delta = CTcor$; $\epsilon = CPcor$;

Residual = instrument conductivity - bath conductivity



13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 0277 CALIBRATION DATE: 25-Mar-15

SBE 45 CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

COEFFICIENTS:

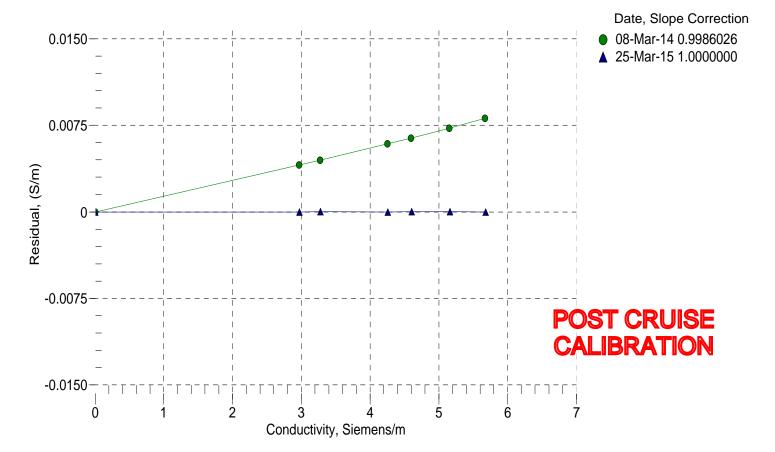
BATH TEMP (ITS-90)	BATH SAL (PSU)	BATH COND (Siemens/m)	INST FREQ (Hz)	INST COND (Siemens/m)	RESIDUAL (Siemens/m)
22.0000	0.0000	0.00000	2528.08	0.00000	0.00000
1.0000	34.7572	2.97139	5075.81	2.97139	-0.00001
4.5000	34.7372	3.27800	5268.50	3.27801	0.00001
15.0000	34.6945	4.25825	5841.23	4.25823	-0.00002
18.5000	34.6851	4.60284	6029.38	4.60285	0.00001
23.9999	34.6747	5.15988	6321.35	5.15988	0.00001
29.0000	34.6686	5.68084	6582.35	5.68084	-0.00000
32.5000	34.6643	6.05248	6762.20	6.05253	0.00006

f = INST FREQ * sqrt(1.0 + WBOTC * t) / 1000.0

Conductiv ity = $(g + h * f^2 + i * f^3 + j * f^4) / (1 + \delta * t + \epsilon * p)$ Siemens / meter

 $t = temperatur e[^{\circ}C)$; p = pressure[decibars]; $\delta = CTcor$; $\epsilon = CPcor$;

Residual = instrument conductivity - bath conductivity



13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 0277 CALIBRATION DATE: 02-Apr-15

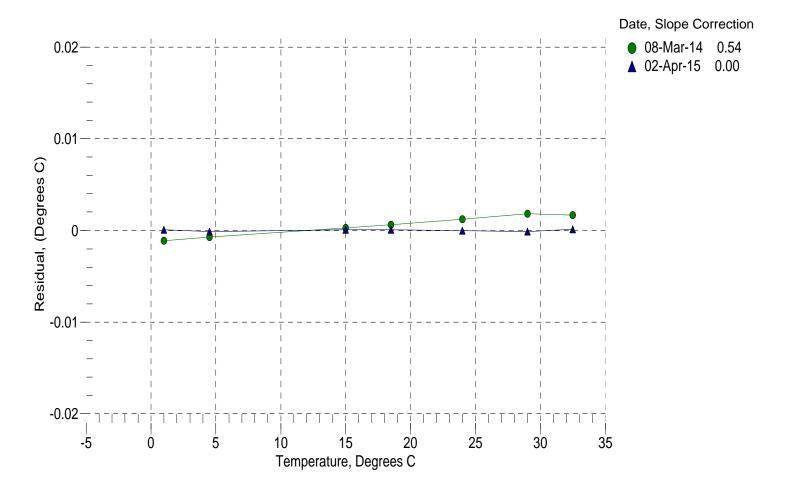
SBE 45 TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

COEFFICIENTS:

a0 = 8.931750e-005 a1 = 2.676627e-004 a2 = -1.972607e-006 a3 = 1.393936e-007

BATH TEMP (ITS-90)	INSTRUMENT OUTPUT	INST TEMP (ITS-90)	RESIDUAL (ITS-90)
1.0000	638596.3	1.0001	0.0001
4.5000	544690.2	4.4999	-0.0001
15.0000	344735.8	15.0001	0.0001
18.4999	297846.3	18.5000	0.0001
24.0000	238133.4	24.0000	-0.0000
29.0000	195499.7	28.9999	-0.0001
32.5000	170852.3	32.5001	0.0001

Temperature ITS-90 = $1/\{a0 + a1[ln(n)] + a2[ln^2(n)] + a3[ln^3(n)]\}$ - 273.15 (°C) Residual = instrument temperature - bath temperature n = instrument output



13431 NE 20th Street, Bellevue, WA 98005-2010 USA

Phone: (+1) 425-643-9866 Fax (+1) 425-643-9954 Email: seabird@seabird.com

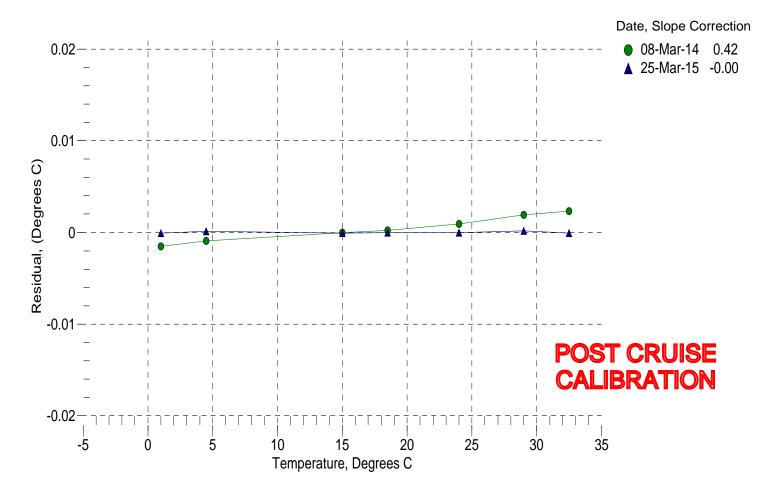
SENSOR SERIAL NUMBER: 0277 CALIBRATION DATE: 25-Mar-15 SBE 45 TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

COEFFICIENTS:

a0 = 1.717778e-005 a1 = 2.845634e-004 a2 = -3.291842e-006 a3 = 1.737056e-007

BATH TEMP (ITS-90)	INSTRUMENT OUTPUT	INST TEMP (ITS-90)	RESIDUAL (ITS-90)
1.0000	638588.2	0.9999	-0.0001
4.5000	544679.5	4.5001	0.0001
15.0000	344732.9	14.9999	-0.0001
18.5000	297841.7	18.5000	-0.0000
23.9999	238131.4	23.9999	-0.0000
29.0000	195498.1	29.0002	0.0002
32.5000	170857.9	32.4999	-0.0001

Temperature ITS-90 = $1/{a0 + a1[ln(n)] + a2[ln^2(n)] + a3[ln^3(n)]} - 273.15$ (°C) Residual = instrument temperature - bath temperature n = instrument output



Temperature Calibration Report

Customer:	Atlantic Marine (Center			
Job Number:	83595		Date of Repo	ort:	4/2/2015
Model Number	SBE 45		Serial Numb	er:	4553332-0277
the calibration iden calibration is not po	tifies a problem, then erformed if the sensor	a second calibration is p is damaged or non-func	erformed after we tional, or by custo	ork is comple omer request.	
must choose wheth during deployment.	er the 'as received' cali In SEASOFT enter t ations (consult the SE	ibration or the previous he chosen coefficients.	calibration better The coefficient 'c ration coefficient	r represents to offset' allows	
Date: 3/25/2015		Drift si	nce last cal:	-0.00040	Degrees Celsius/year
Comments:			_		<u> </u>
'FINAL CALIBRA' Date: 4/2/2015	ATION'	Drift si	☑ Per	-0.0005	Not Performed Degrees Celsius/year
Comments:	_				



Worldwide rental of Marine Electronic Equipment www.seatronics-group.com

Calibration Certificate Number:	SH16797
Campiation Certificate Number.	31110131

This document certifies that the instrument detailed below has been calibrated according to Valeport Limited's Standard Procedures, using equipment with calibrations traceable to UKAS or National Standards.

Instrument Type:	miniSVS - SV only
Instrument Serial Number:	48002
Calibrated By:	B. Scott
Date:	21-Jan-16
Signed:	DOA
QA Check:	5-

Full details of the results from the calibration procedure applied to each fitted sensor are available in separate documents. This summary certificate should be kept with the instrument.

an ACTEON company

Calibrated in a Valeport approved facility
Seatronics Inc.
1319 W. Sam Houson Pkwy N.
Suite 150
Houston, TX 77043
Tel:(713) 464-3311 Fax:(713) 464-6111

Instrument type			mini	miniSVS - SV only		Calibra	Calibration History:	Certificate	ate		Date
Serial number Path Length, mm Baud rate set ex factory				48002 100 19200				SH16797	76		21-Jan-16
System Components	Par	As Rec	As Received Serial Ra	Range / Firmware	Modification Serial Sarial Range	Range / Firmware	Modification Serial Iss Number	on Range / Firmware	Part	Modification Serial Iss Number	tion Range / Firmware
Main Board	0920202	E 1016	101609	0650713B5 0650714C			DOM:				
SV Sensor		101	101659								
Bootloader Fitted	YES										
	Name			B. Scott Name	lame	Name			Name		
	Signed		V.		Signed	Signed			Signed		
				0/10							

nstrument Serial Number	48002
Fransducer Type, mm	100
Fransducer Ser No	101659
CB Part No	0650505E
CB Ser No	101609
Processor Firmware Version	0650713B5
PGA Firmware Version	0650714C
Sertificate Number	SH16797

Calibr	Calibration Equipment used	ent used
Instrument	Type	Serial No
Temp Bridge	MicroK 400	08-PO51 ITL271940/1
PRT	Isotech 909L	909∐141

Stage 1: First order fit

Temp	SoS from Bilaniuk & Wong	Measured ToF	Coefficients	Calc SoS from coefficients	Error (Calc - True)	Acceptable Error	Pass/Fail
060。	s/m	nsec*100		s/m	s/m	m/s	
2.3407	1413.867	14480437	3.844800E+05	1413.867	0.000	±0.001	Pass
14.3011	1463.474	14002626	5.017611E+06	1463.474	0.000	±0.001	Pass

Stage 2: Enter calibration string

#022;5017611;384480

Stage 3: Check point

Тетр	Actual SoS	Measured SoS	Error SoS Reading- Actual	Acceptable Error	Pass/Fail
060.	s/m	s/m	m/s	m/s	
2.3393	1413.860	1413.859	-0.001	±0.005	Pass



SVP Test and Calibration certificate

Valid for surface use*

SVP Type:	SVP70
SVP Serial No.	2011276

Date of issue: 24-03-2015

Temperature Calibration:

Hart 1504 s/n A6B554 & Thermistor s/n 3014 4.6 ℃

Point 1: Point 2:

16.6 ℃

Point 3:

25.6 ℃

RMS Speed of Sound Errors

Temperature Validation:

0.0032 m/s

Calibration & Final Function Test: Sign: Jind Peterser

QA Signature:

* Surface use: 0 to 20m water depth.



TELEDYNE RESON TELEDYNE-RESON A/S, Fabriksvangen 13, DK-3550 Slangerup Everywhereyoulook Fax: +45 4738 0066, Phone: +45 4738 0022