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# OPR-O168-FA-07 Data Acquisition & Processing Report Endicott Arm , AK



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# INTRODUCTION

This hydrographic project was completed as specified by Hydrographic Survey Letter Instructions OPR-O168-FA-07, signed September 25, 2007. This Data Acquisition and Processing Report includes project level information common to sheet A (H11759) and sheet B (H11760).

All sheets have the general locality of Endicott Arm and are located in the state of Alaska.

Survey specific details will be listed in Descriptive Reports as needed. Unless otherwise noted, the acquisition and processing procedures used and deliverables produced are in accordance with the *Standing Instructions for Hydrographic Surveys, April 3, 2006, the NOAA Hydrographic Survey Specifications and Deliverables Manual (HSSDM) April 2007, and the Field Procedures Manual (FPM), March 2007.* Hydrographic Surveys Technical Directives (HTD) 2004-1, and 2007-3 through 2007-9 were followed during the course of this project.

# A EQUIPMENT

Detailed descriptions of the equipment and systems, including hardware and software, used for bathymetric data acquisition, horizontal and vertical control operations, shoreline acquisition, and processing are listed below.

### 1.0 Hardware

The hardware listed in this section was used during project OPR-O168-FA-07.

#### 1.1 Hardware Systems Inventory

Detailed hardware information, including installation dates and serial numbers, is included in Appendix I of this report. Manufacturer's product specifications are included in Appendix II.

#### 1.2 Echo Sounding Equipment

#### 1.2.1 Reson 8111ER Multibeam Echosounder (MBES)

FAIRWEATHER is equipped with a RESON SeaBat 8111 MBES with the Extended Range (ER) and snippet options. The 8111ER is a 100 kHz multibeam system with swath coverage of 150°. The swath is made up of 101 discrete beams with an along-track and across-track beamwidth of 1.5°. The typical operational depth range of the 8111ER on the FAIRWEATHER is 20 to 600 meters. No calibration information was provided by the manufacturer for the system.

The 8111ER is hull-mounted within a reinforced projection that extends 27 inches below the keel. It is located 39.5" starboard of the centerline at approximately frame 29. It has a specified depth range of 3 to 1200 meters.



Figure 1: RESON SeaBat 8111ER MBES

# NOAA Ship FAIRWEATHER



Figure 2: RESON SeaBat 8111ER MBES on FAIRWEATHER



Figure 3: RESON SeaBat 8160



Figure 4: RESON SeaBat 8160 on FAIRWEATHER

# 1.2.2 RESON 8160 Multibeam Echosounder (MBES)

FAIRWEATHER is equipped with a RESON SeaBat 8160 MBES with the snippet option. The 8160 is a 50 kHz multibeam system with a swath coverage of greater than 4x water depth. Each swath is made up of 126 discrete beams with an along-track and across-track beamwidth of 1.5°. It has a specified depth range of 10 to 3000 meters. No calibration information was provided by the manufacture for the system.

The 8160 is hull-mounted within a reinforced projection that extends 13.6 inches below the keel. It is located 54 inches port of the centerline at approximately frame 29.

# 1.2.3 RESON 8101ER Multibeam Echosounder (MBES)

Survey Launches 1010 and 1018 are each equipped with a RESON SeaBat 8101 MBES with the Extended Range and snippet option. The 8101ER is a 240 kHz multibeam system with swath coverage of 150°. The swath is made up of 101 discrete beams with an along-track and across-track beamwidth of  $1.5^{\circ}$ . It has a specified depth range of up to 500 meters. The typical operational depth range of the 8101 on launches 1010 and 1018 in 2006 was 3 to 120 meters. Under optimal conditions with a hard bottom, high power and high gain, the depth range of the 8101 ER was observed to be as deep as 350 m producing a swath of  $\pm 45^{\circ}$  from nadir. No calibration information was provided by the manufacturer for the system.

Each system is attached to a launch using a swing mount which is starboard of the keel and approximately centered fore and aft (see Figures 5 & 6).



Figure 5: Launch 1010 with 8101 extended



Figure 6: Launch 1010 with 8101 retracted

# **1.3** Manual Sounding Equipment – Lead Lines

Vessels 1010, 1018, 1706, and 2302 are each equipped with a lead line. Lead lines are mainly used for depth measurements near shore and for echosounder depth comparison.

Lead lines were created, measured and calibrated according to Section 1.5.3 of the FPM with the exception that the lines were calibrated to the meter instead of decimeter. Calibration was performed during March and April 2007. Calibration reports for the lead lines are included in Appendix V.

# 1.4 Positioning, Heading, and Attitude Equipment

#### 1.4.1 TSS Positioning and Orientation System for Marine Vehicles (POS/MV)

FAIRWEATHER and her launches are each equipped with a TSS POS/MV 320 V4, configured with TrueHeave<sup>™</sup> and Precise Timing. The POS/MV calculates position, heading, attitude, and vertical displacement (heave) of a vessel. It consists of a rack mounted version 2.12 POS Computer System (PCS), a strap down IMU-200 Inertial Measurement Unit (IMU), and two GPS antennas corresponding to GPS receivers in the PCS. The port side antenna is designated as the primary receiver, and the starboard side antenna is the secondary receiver. Differential correctors are supplied to the POS MV by a CSI wireless MBX-3S Automatic Differential GPS receiver. On May 6, 2007 (DN 126) FAIRWEATHER changed the POS MV firmware to version 3.41 and the controller software to version 3.4.0.0.

For all multibeam systems aboard FAIRWEATHER and her launches, timing between the sonar swath, position, heading and attitude information was synchronized by utilizing the TSS POS/MV 320 v.4's. A timing string was sent from the POS/MV to the RESON topside unit and to the ISIS computer recording the incoming data. Vessel wiring diagrams are included in Appendix III.

POS/MV controller software was used to monitor position accuracy and quality during data acquisition. This ensured that positioning accuracy requirements were met, as outlined in the *HSSDM*. The POS/MV controller software provides clear visual indications whenever accuracy thresholds are exceeded.

During acquisition, several IMU failures were noted. There were no actual IMU failures; instead, problems with the POS/MV PCS unit were detected. Due to the suspected hardware problem on the POS/MV PCS unit in launch 1018, it was swapped with the ship's POS/MV PCS on the evening of September 22, 2007. POS/MV PCS serial number 2411 was removed from the ship and installed on Launch 1018, while POS/MV PCS serial number 2560

was removed from Launch 1018 and installed on the ship. On October 29, 2007, two replacement POS/MV PCS's were obtained. The ship's original PCS was replaced, 2411. Launch 1010 received unit 2254 to replace unit 2564. Launch 1018 received unit 2438 to replace unit 2560. The POS/MV PCS serial number 2560 was later confirmed to be malfunctioning and was repaired by Applanix.

#### 1.4.2 POS/MV GAMS Calibration

GAMS (GPS Azimuth Measurement Sub-system) calibrations were performed on each of the three POS/MV units. The GAMS calibration procedure was conducted in accordance with instructions in chapter 4 of the *POSMV V4 Installation and Operation Guide*, 2005. Results are included in the individual vessel reports and spreadsheets, with calibration details located in Appendix III-5.



Figure 7: POS/MV antennas on 1018

Figure 8: POS/MV antennas on 1010

# 1.4.3 CCSI Wireless MBX-3S DGPS Receiver

FAIRWEATHER is equipped with commercial grade CSI Wireless MBX-3S DGPS Receivers that are used in conjunction with TSS POS/MV to provide vessel positioning during data acquisition. The DGPS receivers are configured in manual mode to allow reception of only one U.S. Coast Guard (USCG) differential GPS beacon station. Beacons used for a given survey will be reported in individual descriptive reports. Vessel wiring diagrams are in Appendix III.

Differential GPS (DGPS) was the sole method of positioning. Differential corrections from the U.S. Coast Guard beacons at Annette Island (323 kHz), Gustavus (288 kHz) and Level Island (295 kHz) were used.

#### 1.4.4 Trimble Backpack

FAIRWEATHER uses two GPS Pathfinder® Pro XRS receivers in conjunction with a field computer to acquire detached and generic positions during shoreline verification in the field. Data can also be collected with a handheld TSCe data collector. FAIRWEATHER's field computers consist of three Panasonic CF-18 Tuffbooks and one CF-29 Tuffbook. The receivers have integrated beacon/satellite differential antennas which allow access to digital real-time sub-meter accuracy solutions. Data quality assurance testing was conducted by FAIRWEATHER personnel in April 2007. The Trimble backpack GPS unit testing was combined with the Ashtech testing and the results are located in the Positioning Equipment Confidence Check file in Appendix V.



Figure 9: Trimble Backpack Unit

#### 1.4.5 Impulse LR Hand-held Laser

The Impulse Laser Rangefinder and TruPulse 200 Laser Rangefinder are used in conjunction with the Trimble Backpack GPS unit to acquire distances and heights during shoreline verification. These data are entered directly into the TerraSync shoreline acquisition software and annotated on the detached position forms. The Impulse LR and TruPulse 200 Laser Rangefinder do not function properly in low light or in choppy seas when a feature is not distinguishable from surroundings.



Figure 10: IMPULSE LR laser



Figure 11: TruPulse 200 Laser Rangefinder

Data quality assurance testing was conducted on the Impulse LR on February 27, 2006 by FAIRWEATHER personnel. Comparison testing among the Laser Rangefinder, the TruPulse 200 Laser Rangefinder and the Trimble Backpack units was performed on March 3, 2006. Vertical and horizontal readings were taken with the laser level and compared to measurements taken with a fifteen meter steel tape and a graduated metric staff. Three marks were placed on the staff with SOLAS reflective tape in order to get a good fix. The laser level was set up on a bipod at 10, 20, 50 and 100 meter intervals from the staff. Three horizontal and three vertical readings were taken at each interval. The results of the testing are located in Appendix V.

The laser levels were tested less extensively in 2007 but their accuracy was verified by using them to obtain an offset to BM NO 37 at the USCG ISC Ketchikan facility in the horizontal positioning equipment check of the Trimble backpack units and the Ashtech Z-Xtreme receiver.

#### 1.5 Sound Velocity Equipment

#### 1.5.1 SBE 19plus SEACAT Profiler

FAIRWEATHER is equipped with three SBE 19*plus* SEACAT sound velocity profilers used to acquire conductivity, temperature, and depth (CTD) data in the water column to determine the speed of sound through water. Two of the SBE 19*plus* profilers have pressure sensors rated to 1000 meters. The third has a pressure sensor rated to 3,500 meters.

The SBE 19*plus* SEACAT sound velocity profilers were calibrated by the manufacturer and current calibration files were returned with the units. Calibration files for 2007 are located in Appendix V.

Periodic quality assurance checks include comparison casts between CTD instruments. Data quality assurance (DQA) checks include comparison casts between two instruments as per section 1.5.2.2 of the *FPM* for each survey. Results of the comparison casts are located in the *SV\_Maintenance and Testing\_2007.xls* file in Appendix VI.

#### **1.5.2** SBE 45 Micro Thermosalinograph (TSG)

FAIRWEATHER is equipped with one SBE 45 MicroTSG. The SBE 45 uses continuously pumped sea water to measure conductivity and temperature near the ship's hull mounted transducers. The intake is located 9 feet below the DWL (13 ft) between frames 11 and 12.

The conductivity and temperature information is converted to sound velocity and output to the RESON 8160's and 8111's processing units. The 8160 requires sound velocity information for beam forming and pitch stabilization while the 8111 only requires it for pitch stabilization. The 8160 cannot be used to acquire data without real time sound velocity information. The calibration report is included in Appendix V.

#### 1.5.3 Moving Vessel Profiler 200

A Brooke Ocean Technology, Ltd. (BOT) Moving Vessel Profiler 200 (MVP200) is mounted in the aft starboard corner of the fantail (see Figure 12). The MVP200 system is a self contained sound velocity profiling system capable of sampling water column profiles to 200m depth from a vessel moving up to 12 knots. The system is configured with a Single Sensor Free Fall Fish (SSFFF) outfitted with an Applied Microsystems Ltd. Sound Velocity and Pressure Smart Sensor. Deeper profiles can be obtained by reducing the vessel speed. When the vessel is holding station, the system is capable of recording casts over 600m in depth.

The MVP system consists of a winch, cable, fish (the towed unit with the sound velocity sensor), support assembly, and controlling hardware and software. During ship acquisition, the fish is deployed using the on-deck controller and towed with enough cable out to keep the fish 3-5 m below the water surface. A "messenger" (a short cable-thickening sleeve) is set to allow the system to keep the appropriate amount of cable out and is reset as needed when the ship acquisition speed is altered.

During SVP acquisition, the controlling computer application, BOT MVP version 2.26 is used to control the MVP system and to acquire SVP data. MVP allows for three acquisition modes: 1) automatic continuous multiple cast freefall casting while at speed, 2) single cast freefall casting while at speed, and 3) single cast winch speed casting while stationary. The user limits the depth to which the fish will fall by setting 1) the depth-off-bottom and 2) the maximum depth. Either single, individually initiated casts can be performed at the discretion of the Hydrographer or the auto deploy function can be enabled and set with varying intervals (every 2 minutes, for example) for deployment.

Periodic quality assurance checks include comparison casts between the MVP and one of the SBE 19*plus* SEACATs. Data quality assurance (DQA) checks include comparison casts among the instruments as per section 1.5.2.2 of the *FPM* for each survey. A record of the DQA tests performed aboard the ship is kept and is included in Appendix VI.



Figure 12: FAIRWEATHER's MVP200 sound velocity system

# 1.6 Vertical Control Equipment

#### 1.6.1 Water Level Gauges

Three Sutron 8210 tide gauges are provided to FAIRWEATHER by the Center for Operational Oceanographic Products and Services (CO-OPS). These gauges are equipped with Paros Scientific Sensors (SDI-12) for pressure measurements. The tide gauges are checked annually by CO-OPS Field Operations Division personnel to ensure that their accuracy standards are being met.

CO-OPS does not provide calibration or quality assurance documentation to the FAIRWEATHER. FAIRWEATHER personnel are responsible for installation and removal of the water level gauges. CO-OPS is responsible for delivering final approved vertical correctors to the field unit or processing branch for application to the hydrographic data set. As FAIRWEATHER received new gauges, data quality assurance checks were conducted to ensure full functionality prior to deployment.

#### 1.6.2 Leveling Equipment

FAIRWEATHER is equipped with four universal automatic levels (two Zeiss NI2 333 and two Leica NA2 100) and graduated metric staffs to assist in leveling tide gauges.

A Kukkamaki procedure is performed prior to leveling in order to verify the collimation error. Procedures were followed as described in the *User's Guide for the Installation of Bench Marks and Leveling Requirements for Water Level Stations,* October 1987. Kukkamaki results for 2007 are located in the Tides folder in Appendix V.

#### 1.7 Horizontal Control Equipment

FAIRWEATHER is equipped with one Ashtech Z-Xtreme dual-frequency GPS receiver used for the positioning of tidal benchmarks, aids to navigation and portable DGPS reference stations (Fly-Away). The Ashtech Z-Xtreme 12 channel, L1/L2 receiver is connected to 4 Ashtech Geodetic GPS antennas.

The antennas can be equipped with an optional ground plane and mounted on fixed height Seco GPS tripods.

Data quality assurance testing of the Horizontal Control equipment was performed on 14 March 2007 (DN073) by FAIRWEATHER personnel. The Ashtech Z-Xtreme GPS receiver (SN ZE1200339016) was set up over

Benchmark No. 37 in Ketchikan, AK using a Seco fixed height tripod. Data was collected for 2 hours 30 minutes and submitted to OPUS which returned an ultra rapid solution position the same day. The OPUS position was less than a centimeter off the published NGS Control Point for BM No. 37. The OPUS solution and a map of the results of the test (Positioning Equipment Confidence Check) are located in Appendix V. Accuracy standards have been met according to NOAA Technical Memorandum NOS NGS-58.

Horizontal control equipment serial numbers and installation dates are located in the hardware section of Appendix I, System Tracking.

#### 2.0 Software

#### 2.1 Software Systems Inventory

An extensive software inventory with documentation, of the software systems used by the NOAA ship FAIRWEATHER, is maintained as a *Survey Software* spreadsheet and included in Appendix I. This spreadsheet includes specifics such as software applications, versions, and hot fixes, in addition to dates loaded on specific computers within the survey department.

#### 2.2 Data Acquisition Software

#### 2.2.1 Isis Sonar/ BathyPro/ DelphMap/ DelphNav

The FAIRWEATHER uses the Triton Imaging Inc. software packages Isis Sonar and Sonar Suite to acquire multibeam echo sounder and backscatter data on all of its multibeam platforms. Sonar Suite has two software packages, DelphNav and DelphMap, which work together along with Isis Sonar to produce real time data planning, acquisition, and execution.

Triton Imaging BathyPro is an add-on package for Isis Sonar which processes XTF data real-time to produce DTMs supported by DelphMap. Triton Imaging DelphNav is an add-on package to DelphMap used for line planning and vessel navigation. Triton Imaging DelphMap is a stand-alone GIS program which combines georeferenced bathymetric digital terrain models and reference files such as raster charts and vector shoreline files to display real-time bathymetric bottom coverage.

#### 2.2.2 TerraSync/ Pathfinder Office

For GPS positioning and shoreline verification FAIRWEATHER uses two Trimble Navigation Limited software programs: TerraSync 2.41 and GPS Pathfinder 3.1.

GPS Pathfinder is run on a Microsoft Windows operating system and is used to manage and process Trimble GPS data, transfer files to and from GPS receivers and handheld data collectors, and export processed data.

Trimble TerraSync 2.41 supports a data dictionaries built with S57 objects and attributes and georeferenced TIFF images. The georeferenced TIFF images are used for reference and navigation purposes as well as for immediate S-57 attribution of positions in the field. TerraSync is installed and configured for data collection on all of the Tuffbook field computers, the TuffTab, and the TSCe handheld computer.

GPS precision masks in TerraSync using the following parameters:

- Horizontal Dilution of Precision (HDOP)  $\leq 2.5$
- Signal-to-Noise Ratio (SNR)  $\geq$  4
- Elevation Mask  $\geq \sim 8^{\circ} 15^{\circ}$  (varies by location)

Differential GPS correction is applied in real-time, using the unit's integrated beacon as the first choice corrector, and specifying "wait for real-time" as the secondary option. Positions are filtered so that only those with a

minimum of 4 satellites (3D position), and HDOP  $\leq$  2.5, and Positional Dilution of Precision (PDOP)  $\leq$  6 will be recorded.

### 2.3 Data Processing Software

#### 2.3.1 NOAA Hydrographic Systems and Technology Programs (HSTP) Software

Sound velocity data is processed with Velocwin, in-house software produced and maintained by NOAA's Hydrographic Systems and Technology Programs (HSTP) division. Velocwin creates and archives water column profiles, performs quality assurance, and processes pressure based depth data. Velocwin creates a standard file format across NOAA's hydrographic fleet for sound velocity profiles applied to shallow water multibeam and single beam data.

Pydro, another NOAA program produced and maintained by HSTP, is used to process features such as detached positions (DP), generic positions (GP), and Automated Wreck and Obstruction Information System (AWOIS) contacts. PYDRO also converts and attributes features according to S-57 standards for insertion into CARIS Notebook.

#### 2.3.2 CARIS

CARIS HIPS<sup>™</sup> (Hydrographic Information Processing System) is used to process all shallow water multibeam data including data conversion, filtering, sound velocity, tide correcting, merging and cleaning. CARIS HIPS also calculates the Total Propagated Error (TPE) used to produce Bathymetry Associated with Statistical Error (BASE) surfaces which assist the Hydrographer in data cleaning and analysis.

CARIS Notebook<sup>™</sup> is used to compile and display source shoreline, shoreline updates and S-57 features imported from Pydro. The .hob files created in Notebook are the current shoreline deliverables.

#### 2.3.3 Fledermaus<sup>TM</sup>

Fledermaus <sup>TM</sup>, an Interactive Visualization Systems 3D<sup>TM</sup> (IVS 3D) program, is used for data visualizations and creation of data quality control products, public relations material and reference surface comparisons. As an additional data quality assurance check, Fledermaus <sup>TM</sup> may be used to examine the CARIS surfaces prior to submission.

#### **2.3.4** МарІпfо<sup>тм</sup>

MapInfo<sup>TM</sup> is used to review tables and workspaces associated with assigned projects received from Hydrographic Survey Division (HSD). MapInfo may also be used to produce scaled plots produced for public relation purposes. HydroMI, an HSTP produced MapBasic program, is used through MapInfo to convert tide and tidal zoning files into a format that is useable in CARIS HIPS, and obtain latitude/longitude coordinates for pre-survey planning.

#### 3.0 Vessels

#### 3.1 Vessel Inventory

The NOAA Ship FAIRWEATHER (S220) and her survey launches 1010 and 1018 are equipped to acquire multibeam echosounder (MBES) and sound velocity profile (SVP) data. Launch 1018 is also the primary vessel for dive operations. The AMBAR (2302) and Monarch (1706) are used during shoreline verification, bottom samples, and horizontal and vertical control operations. All vessels except the ship were used in support of tide gauge operations. See Appendix I for the complete vessel inventory.

### 3.2 Noise Analysis

The FAIRWEATHER sonar system RESON 8111ER underwent noise analysis testing on October 11, 2004. The results are used during acquisition to enhance data quality and are included in Appendix III-S220-7. Standard operating procedures utilizing the RESON 8111ER aboard the FAIRWEATHER have survey speeds set to minimize noise based on the noise analysis.

#### 4.0 Data Acquisition

#### 4.1 Horizontal Control

A complete description of horizontal control for the project can be found in the *OPR-O168-FA-07 Horizontal and Vertical Control Report (HVCR)*, submitted under separate cover.

The horizontal datum for this project is the North American Datum of 1983 (NAD83).

Multibeam and shoreline data were differentially corrected in real time using correctors provided by Coast Guard beacons at Gustavus (288 kHz) or Level Island (295 kHz). If loss of the differential beacon resulted in any data being recorded with C/A GPS positions it will be noted in the descriptive report for the survey.

Specific DGPS quality control checks were not performed during this project. Based on correspondence between personnel from the Hydrographic Systems and Technology Program and FAIRWEATHER, system checks were deemed unnecessary. Refer to correspondence included in Appendix VII.

#### 4.2 Multibeam Echosounder Acquisition and Monitoring Procedures

Methods of acquisition took into consideration system performance limitations, the bottom topography, water depth, and the ability of the vessel to safely navigate the area.

All multibeam data were acquired in Triton Elic's extended transfer format (XTF) and monitored in real-time using the 2-D and 3-D data display windows and the on-screen displays for the RESON SeaBat 8101ER and 8111ER. Adjustable parameters that were used to control the RESON from the ISIS software include range scale, power, gain, and pulse width. Vessel speed was also adjusted as needed to eliminate noise from the data. These parameters were adjusted as necessary to ensure best data quality. Additionally, vessel speed was adjusted as necessary to ensure the required along-track coverage for object detection in accordance with the *HSSDM*. Survey personnel follow standard operating procedures documented aboard the FAIRWEATHER while setting and utilizing the RESON systems and Isis for acquisition of data.

Mainscheme multibeam sounding lines using the RESON SeaBat 8111ER were generally run parallel to the contours at a line spacing approximately three to four times the water depth. For discrete item developments, line spacing was reduced to 2 times water depth to ensure least-depth determination by multibeam near-nadir beams. Triton Elic's DelphMap Real Time Bathy was used in lieu of planned line files. The Real Time Bathy displayed the acquired multibeam swath during acquisition and was monitored to ensure overlap and full bottom coverage. If coverage was not adequate, additional lines were run while still in the area.

### 4.3 Shoreline Verification

FAIRWEATHER personnel conducted field shoreline verification at times near predicted low water, in accordance with the Standing Project Instructions, the FPM (March 2007), and HTD 2007-7. Standard operating procedures on the use of Trimble TerraSync and GPS Pathfinder for shoreline verification were followed by survey personnel.

CARIS Notebook 3.0 was used to review the project level composite source (.000) file supplied by HSD and described in HTD 2007-7. The composite source file for OPR-O168-FA-07 contained features from a sole

source: Geographic Cell (GC), or Digital Data (DD), shoreline compiled by the Remote Sensing Division (RSD). The file was opened in Notebook and copied to a .hob file using the same name. The project level composite source .hob file was edited by the survey manager to include only features within the survey limits and renamed according to survey number, HXXXXX\_Composite\_Source.hob. A copy was made of the unedited survey level composite source .hob file and named HXXXXX\_Original\_Composite\_Source.hob. All modifications to source shoreline features addressed during field verification were made in the HXXXXX\_Composite\_Source.hob, with the original composite source .hob file remaining unedited. These HOB files are submitted as shoreline deliverables.

No AWOIS were assigned to this project.

Shoreline verification was not conducted on this project due to lack of appropriate low water conditions.

No Detached positions (DPs) and generic positions (GPs) were acquired and no DP forms or boat sheets were utilized.

#### 4.4 Shoreline Data Processing

Features imported into Pydro were given short descriptive comments listed under the Remarks tab in Pydro. Features were flagged as Primary, unless there were multiple DPs or GPs taken on the same feature. In that case, the most important DP was marked Primary and any associated DPs/GPs were flagged Secondary. All features were S57 attributed.

Significant features that deserved special attention or additional discussion, were flagged Report in Pydro and included in the Pydro feature report. Along with the hydrographer notes and investigation methods provided in the Remarks tab, the Hydrographer included recommendations to the cartographer in the Recommendations tab when warranted. All features were flagged according to section 4.4.4 of the FPM. All features flagged as "report" in Pydro were included in the Shoreline Feature Report.

Photos labeled and associated with a DP/GP number were included in the Pydro PSS session and stored in a folder with the PSS file.

HDCS\_DATA lines associated with DPs were tide corrected in CARIS HIPS. GPs do not have heights associated with them and required no additional processing.

All primary and accepted DPs and GPs were exported from Pydro as an .xml to CARIS Notebook 3.0. Two separate stand alone .hob files were created from the Pydro .xml files. The files are named H#####\_Updates.hob and H###### Disprovals.hob.

An original composite source file (H#####\_Original\_Composite\_Source.hob) was saved prior to being edited and will be submitted with the survey. No edits were applied to the H#####\_Composite\_Source.hob.

The SORIND and SORDAT S57 attribute fields for new features or modified source features were updated to reflect the information for their associated survey number and date. All unmodified source features retain their original SORIND and SORDAT values.

The CARIS Notebook files along with CARIS HIPS BASE surface(s) were viewed to compare soundings and features simultaneously. Standard operating procedures, for processing shoreline features in Pydro and CARIS Notebook, were followed by survey personnel as documented.

Final Shoreline Deliverables include the Pydro PSS, the Pydro Shoreline Feature Report, and up to four Notebook HOB files:

HXXXXX\_Original\_Composite\_Source (without edits) HXXXXX\_Composite\_Source (with edits) HXXXXX\_Updates (Pydro Data Import, if applicable)

### HXXXXX\_Disprovals (Pydro Data Import, if applicable)

# 5.0 Bottom Sample Acquisition

Bottom samples were conducted according to section 7.1 of the *HSSDM*. Bottom samples (GPs) were acquired with TerraSync 2.41. Data were imported into GPS Pathfinder 3.1 and were reviewed for quality. The line features were exported to a Microsoft Access Database file (.mdb) and NALL buffer lines were exported to ESRI shape files (.shp).

Bottom samples results are found in the Pydro PSS and the Notebook HOB deliverable layer, HXXXXX\_Updates.

# **B** QUALITY CONTROL

The FAIRWEATHER has numerous standard operating procedures (SOPs) that are followed by personnel throughout the survey to ensure consistent high quality data and products.

# **1.0** Uncertainty Modeling

Error values for the multibeam and positioning systems on FAIRWEATHER and her survey launches were compiled from manufacturer specification sheets for each sensor (Heave, Pitch, Roll, Position, and Heading) and from values set forth in Chapter 4 Appendix of the FPM.

Estimates for the error in measuring vessel offsets, multibeam system biases (timing, pitch, roll and yaw) and dynamic draft are the standard deviations of the set of values reached for each of these corrections resulting from several people processing the data.

In the specific case of MRU Alignment error; values were set after an email exchange between Rainier, Fairweather, HSTP and CO-OPS (see TPE\_MRU Alignment.txt email messages in Appendix VII). The error value for MRU alignment deviated from that set in Chapter 4 Appendix of the FPM due to the directive's value for MRU alignment error being set too high (possibly due to a misinterpretation of what the alignment error represented). This error should represent the standard deviation of measurement of the error derived from multiple people processing the patch test. Based on this, the MRU alignment errors were significantly lower than the 1 degree value set in Chapter 4 Appendix of the FPM.

An estimate of the total error due to tides was not included in the Letter Instructions for the project, but a value of 0.09 meters (two sigma - 95% confidence level) was given by CO-OPS in the above noted email exchange. Using this value as a reference, tidal errors were set at 0.01 m for the gauge and 0.1 meters for zoning. The 0.01 meter estimate for the gauge is a conservative estimate that can be recalculated based on the sigma values in the final approved water levels. The 0.1 meter estimate for zoning is also a conservative one sigma value based on the total two sigma tide error of 0.09 meters.

The final uncertainty values for FAIRWEATHER and her launches, tides, and sound velocity, along with information on how the values were derived, are shown in the FA\_TPE\_Values.xls spreadsheet located in Appendix IV. Uncertainty values relating to vessels and survey systems were entered into the HIPS Vessel File (HVF) for each platform. Uncertainty values for tide and sound velocity were entered during the CARIS Compute TPE process.

#### 2.0 Data Processing

#### 2.1 Multibeam Echosounder Data Processing

Bathymetry processing followed section 4.2 of the FPM unless otherwise noted.

Raw XTF multibeam data were converted to Caris HDCS format using FAIRWEATHER documented settings. True heave, sound velocity and water level data were then applied to all lines and the lines merged. Once lines were merged Total Propagated Error (TPE) was computed.

Vessel heading, attitude, and navigation data were reviewed in HIPS navigation editor and attitude editor. Where necessary, fliers or gaps in heading, attitude, or navigation data were manually rejected or interpolated for small periods of time.

BASE surfaces were created using the Combined Uncertainty and Bathymetric Estimator (CUBE) algorithm and parameters contained in the Cubeparams.xml file. This file contains settings for "Deep" or "Shallow" surveys. As stated in HTD 2007-2, the "Deep" setting corresponds to NOAA "Complete" multibeam coverage and "Shallow" to NOAA "Object Detection" coverage. As the Letter Instructions for project OPR-O168-FA-07 require "complete" multibeam coverage, all BASE surfaces were created using the "Deep" configuration of CUBE parameters.

Multibeam data were reviewed and edited in HIPS swath editor and in subset mode as necessary. The BASE surface was used for directed data editing in subset editor, to demonstrate coverage, and to check for errors resulting from tide, sound velocity, attitude and timing.

Table 1 lists the general resolution and depth ranges used by FAIRWEATHER. These values will be adjusted by sheet managers for individual surveys based on bathymetry and conditions in the survey area. A detailed listing of the actual resolutions and depth ranges used during the processing of each survey, along with the corresponding fieldsheet(s), will be provided in the descriptive report of each survey.

FAIRWEATHER									
Depth F	Ranges	Resolutions							
Lo (m)	Hi (m)	Overlap (m)	Res. (m)						
0	40		2						
30	70	10	5						
50	120	20	10						
100	200	20	20						
180	350+	20	35						

**Table 1: Resolutions and Depth Ranges** 

In areas of navigational significance where the BASE surface did not depict the desired depth for the given area, a designated sounding was selected. Designated soundings were selected as outlined in chapter 5 of the *HSSDM*.

# **3.0 DATA REVIEW**

Specific procedures were used on FAIRWEATHER to ensure quality control of data throughout acquisition, processing, and submission. These procedures are documented and followed by the Hydrographer. A detailed in Quality Control Check is preformed by the survey manager. A detailed Review is conducted by qualified survey personnel (FOO, CST, SST, or PS) other than the survey manager as an outside review of the survey data and deliverables. The Data and Analog Submission checklists are used to ensure that all data and deliverables are complete and included upon submission. Documentation of these tasks are completed for every survey but only the final processing log, *HXXXXX\_Data\_Log*, is submitted with the individual survey data.

# **C** Corrections to Echo Soundings

### 1.0 Vessel HVFs

CARIS HIPS Vessel Files (HVF) were created by FAIRWEATHER personnel and used to define a vessel's offsets and equipment uncertainty. The HVF is used for converting and processing data collected by each survey platform. For each survey platform, an *HVF Report*, listing specific HVF entries, was produced in the CARIS Vessel Editor and is included in Appendix III. The HVFs used for the current project are included with the digital separates submitted with the individual survey data.

### 2.0 Vessel Offsets

Sensor offsets were measured with respect to each vessel's reference point. The reference point for FAIRWEATHER and survey launches 1010 and 1018 is the IMU. Specific offset values were input into the POS/MV and the CARIS HIPS Vessel File (HVF).

A ship survey was completed for the FAIRWEATHER by Westlake Consultants, Inc on September 23, 2003 and a POS/MV component spatial relationship survey of the FAIRWEATHER was conducted by NGS in February, 2007. The results of both of these surveys were used to determine the offsets for ship. The reports from each survey are located in documents in Appendix III-S220-2, and the final values for FAIRWEATHER's offsets and explanations of how they were calculated are located in the S220\_Offsets & Measurements spreadsheet in the same folder.

Permanent control points were established on launches 1010 and 1018 in July of 2004. Sensor offsets were measured by Fairweather personnel according to documented procedures. Total stations were utilized for positioning the permanent control points. The total station specifications are located in Appendix II-7, the calibration certificates for the *Nikon DTM 310* and the *Sokkia SET 5F* are included in Appendix V. A steel tape was used to verify and update specific vessel offsets in April 2007. The final offsets for survey launches 1010 and 1018 were derived from a combination of values from the original full survey and the values updated in the verification surveys. The measurements, derivations, descriptions of methodology used, diagrams, and coordinate system references are included in the respective vessel's *Offsets & Measurements* spreadsheet in Appendix III.



Figure 7: Permanent Control Point "Benchmark C" on launch 1018

# **3.0** Static and Dynamic Draft

Static draft (*Waterline Height* in the HVF) for launch 1010 and 1018 was calculated based on steel tape measurements of the distance from benchmarks on the port and starboard quarter of the vessel to the waterline. Although static draft tubes have been installed in launch 1010 and 1018 the tubes have not yet been calibrated, nor have procedures for the determination of loading been developed.

The bow and stern draft marks were used to perform a linear interpolation of the static draft at the FAIRWEATHER'S IMU. The static draft was measured multiple times with the vessel under different loading conditions: with and without launches on board and with different amounts of fuel. The final value for the static draft was an average of the most likely loading conditions during survey operations.

The values and calculations for static draft are listed in each vessel's Offsets Measurement spreadsheet (Waterline to RP) located in Appendix III.

Dynamic Draft Settlement and Squat (DDSSM) tests were conducted for FAIRWEATHER and survey launches 1010 and 1018 in April 2007. The final DDSSM values are the average of results obtained from multiple individuals processing the DDSSM data. Detailed processing spreadsheets of DDSSM results for each vessel are located in the respective vessel's folder in Appendix III.

### 4.0 Patch Tests

Patch tests were conducted for the multibeam acquisition systems on FAIRWEATHER and survey launches 1010 and 1018 in April 2007. The results of the patch tests, along with the acquisition and processing logs, are included in the individual MBES Calibration Tables in Appendix III-3.

It was discovered during processing of the 2007 patch tests that the new POS/MV's for launches 1010 and 1018 were set to output GPS time instead of UTC time. This introduced a fourteen second error (the precise difference between GPS and UTC time) into the navigation time. To avoid time spent rerunning the patch tests, the tests were processed using a time correction value of fourteen seconds, which effectively canceled out the time error. An entry in the HIPS vessel files for launches 1010 and 1018 dated 2007-001 show the fourteen second correction in the "Time Correction(s)" column. The POS/MV units were subsequently changed to output UTC time and a second entry in the HIPS vessel files, removing the fourteen second navigation latency value, was entered on 2007-102. All data collected for the project took place after the POS/MV's were corrected to output UTC time.

Additional testing for adjustments were required throughout the field season on both Launch 1010 and 1018 due to the instability of the roll arm mount. Launch 1010 was retested on Dn252 prior to this project due to mount tightening. Launch 1018 was tested and had roll values updated on Dn236 prior to this project.

#### 5.0 Attitude

All attitude corrections were generated by the POS/MV using data from the IMU-200 Inertial Measurement Unit (IMU). IMU values for uncertainty of heave, pitch and roll are included in the manufacturer specification in Appendix II and are included in the FA\_TPE\_Values\_2007.xls spreadsheet located in Appendix IV. IMU failures noted during this project were actually attributed to faulty POS/MV PCS units as documented in section 1.4.1above. IMU correctors applied to the data were not affected and no additional patch testing was required.

### 5.1 True Heave

FAIRWEATHER and her launches are equipped with the POS/MV TrueHeave<sup>™</sup> (TH) option. True Heave<sup>™</sup> is a 'delayed' heave corrector as opposed to 'real time' heave corrector and is fully described in Section 6 of the *POS/MV Version 4 Installation and Operation Manual*. Daily TH files were logged through the Ethernet Logging function in the POS/MV controller software. To ensure proper calculation of TH, files were logged for at least three minutes past the end of each day's survey operations.

In cases where TrueHeave<sup>™</sup> could not be applied, real time heave correctors were used. Real time heave data were recorded in Triton Elic's Isis software, stored in the .xtf format and applied as the heave corrector for multibeam data. Data that does not have TrueHeave<sup>™</sup> applied will be listed in the individual Descriptive Report for the survey.

# 6.0 Sound Velocity

Seacat SBE 19*plus* sound velocity profilers were used to collect sound velocity data for survey launches 1010 and 1018's Reson 8101 multibeam systems. The Brooke Ocean Technology Moving Vessel Profiler (MVP) was used to collect sound velocity data to correct data collected with FAIRWEATHER's Reson 8111 and 8160 multibeam systems.

Daily sound velocity profiles from the SBE 19*plus* were processed with Velocwin and concatenated into a single .svp file for the sheet. Individual .svp files and the concatenated file for the survey will be submitted with each survey.

Sound velocity profiles acquired using the Brooke Ocean Technology Moving Vessel Profiler 200 (MVP) are stored in files labeled .001, .001c, .001d, and .001e (collectively called BOT files) where the number increments by one with each subsequent cast. The .00#c file for each cast was opened with Velocwin and converted into CARIS .svp file format. The individual .svp profiles were concatenated into a single .svp file for the sheet. Individual sound velocity profile files taken by the MVP will not be submitted due to the large number of casts acquired; however, the daily concatenated files are submitted.

The concatenated sound velocity files were applied to multibeam data in CARIS HIPS during data processing. CARIS HIPS uses one of four different algorithms to automatically apply a sound velocity profile stored in the concatenated sound velocity file. They are: "previous in time," "nearest in time," "nearest in distance" and "nearest in distance within time." In general, "previous in time" was the method used for applying sound velocity information in HIPS, but the other methods may have been used in certain situations. The method of applying sound velocity is included in the processing logs that are submitted with each survey.

# 7.0 Water Level

The vertical datum for this project is Mean Lower-Low Water (MLLW). Predicted water level correctors from the primary tide stations at Juneau, Alaska (945-2210) were downloaded from the CO-OPS website and used for water level corrections during the course of the project.

The files for the relevant days were collated into a tide station master file which was converted to CARIS .tid file format in MapInfo using HydroMI. Water level data in the .tid files were applied to data using the zone definition file (O168FA2007CORP.zdf) supplied by CO-OPS. Upon receiving final approved water level data, all data were reduced to MLLW using the final approved water levels (smooth tides) as noted in the Descriptive Report included with the survey data.

A complete description of vertical control for the project can be found in the *OPR-O168-FA-07 Horizontal and Vertical Control Report (HVCR)*, submitted under separate cover.

# **Appendix I**

# **System Tracking**

# FA Hydrographic Vessel Inventory

**FA Hardware Inventory** 

**FA Computer Inventory** 

# **FA Personnel Inventory**

# FA Survey Software

- Software Systems
- ISIS Sonar
- Triton Suite
- TerraSync
- CARIS Licenses
- CARIS HIPS & SIPS
- CARIS Utilities
- CARIS GIS
- CARIS NOTEBOOK
- PYDRO
- Pathfinder
- Velocwin
- Fledermaus
- MapInfo
- Ashtech
- Acrobat Pro
- Other

#### Hydrographic Vessel Inventory

Field Unit: FAIRWEATER

Effective Date: June 1, 2006

Updated Through: April 30, 2007

SURVEY VESSELS											
Vessel Name	el Name FAIRWEATHER La		Launch 1018	Skiff	FRB	Ambar 700					
Vessel Image											
Hull Number	S 220	1010	1018	1706	2301	2302					
Call Letters	WTEB										
Manufacturer	Aerojet-General Shipyards Jacksonville, FL	Jensen	Jensen	MonArk	Zodiak of North America	Marine Silverships, Inc					
Year of Construction	1967	1967 1973 1973			2004	1998					
Type of Construction	Welded steel hull - ice strengthened	Aluminum hull	Aluminum Hull	Aluminum Hull	RHIB	RHIB					
Length Overall	70.4 m (231 ft)	8.8 m (28ft 10in)	8.8 m (28ft 10in)	5.2 m (17 ft)	6.7 m (22 ft)	7.0 m (23 ft)					
Beam	12.8 m (42 ft)	3.3 m (10ft 8in)	3.3 m (10ft 8in)	2.3 m (7ft 2in)	2.6 m (8ft 6in)	2.9 m (9ft 4in)					
Draft	4.7 m (15ft 6in)	1.2 m (4 ft)	1.2 m (4 ft)	0.4 m (1ft 3in)	0.6 m (22 in)	0.4 m (17 in)					
Date of Effective Full Vessel Static Offset Survey	Origninal Survey 9/2003 POS/MV Offsets Surveyed 2/2007	2004	2004								
Organization which Conducted the Effective Full Offset Survey	Original Survey - Westlake Consultants POS/MV Survey - NGS	NOAA Personnel (Wexler, Sampadian, Froelich)	NOAA Personnel (Wexler, Sampadian, Froelich)								
Date of Last Partial Survey or Offset Verification & Methods Used	April - 2007?	April-2007 Steel Tape	April-2007 Steel Tape								
Date of Last Static Draft Determination & Method Used	April-2007 Draft Marks on Hull	April-2007 Draft Marks on Hull	April-2007 Draft Marks on Hull								
Date of Last Settlement and Squat Measurements & Method Used	April-2007 Echosounder Method	April-2007 Echosounder Method	April-2007 Echosounder Method								

RED - info needs to be verified

ORANGE - info needs to be found

GREY - info not available

	Hydrographic Hardware Inventory										
	Field Unit:	FAIRWI	EATHER								
	Effective Date:	2/10/	2007								
	Updated Through:	11/30	/2007								
SONAR & SOUNDING E	QUIPMENT										
Equipment Type	Manufacturer	Model	Serial Number	Firmware and/or Software Version	Version Install Date	Location	Date of last Calibration	Date of last Service	Additional Information		
Processor	Reson	81-P (8111)	35652	N/A	May-04	\$220	N/A		Bar Code : CD0001065312		
Processor	Reson	81-P (8160)	35385	N/A	May-04	S220	N/A		Bar Code : CD0001065313		
Transducer	Reson	8111ER	unknown	Dry: 8111-E209-6114 Wet: 8111-E101-AFAA	Apr-04	S220	4/20/2006				
Transducer	Reson	8160	unknown	Dry: 8160-2.09-7C6D Wet: 8160-1.00-E9E1	Apr-04	\$220	incomplete				
Processor	Reson	81-P	34497	N/A	Jul-04	1010	N/A		Bar Code : CD0001065351		
Transducer	Reson	8101 ER	2701011	Dry: 8101-2.09-E34D Wet: 8101-1.08-C215	Jul-04	1010	4/10/2006		removed 10/6/04 for repair; removed 10/1/05 for welding		
Processor	Reson	81-P	35737	N/A	Jul-04	1018	N/A		Bar Code : CD0001065349		
Transducer	Reson	8101 ER	3102026	Dry: 8101-2.09-E34D Wet: 8101-1.08-C215	Jul-04	1018	incomplete				
Lead Line	CST-FA	Traditional	10_01_05	N/A	N/A	any	3/14/2007				
Lead Line	CST-FA	Traditional	10_02_05	N/A	N/A	any	3/11/2005				
Lead Line	CST-FA	Traditional	20_01_05	N/A	N/A	any	3/20/2007				
Lead Line	CST-FA	Traditional	20_02_05	N/A	N/A	Ambar	4/10/2007				
Lead Line	CST-FA	Traditional	20_03_05	N/A	N/A	any	4/6/2007				
Lead Line	CST-FA	Traditional	30_01_05	N/A	N/A	any	4/9/2007				
Lead Line	CST-FA	V-100/Non-Traditional	pending	N/A	N/A	any	incomplete		in work		
Lead Line	CST-FA	V-100/Non-Traditional	pending	N/A	N/A	any	incomplete		in work		
Divers Least Depth Gauge	PTC	MODIII	68322	N/A	N/A	\$220	unknown	unknown	*acquired 5/22/06; stopped working 9/1/06		
*Klein 3000									*03/21 /07-not yet on the FA		
Odom Echotrac CVM	Odom Hydrographic	ETCVM-A	26034	ET-CVM COM Ver 3.29 DSPDual Ver 3.28		any			ChartView Dongle (100.001.001.098)		

POSITIONING & ATTITUDE EQUIPMENT										
Equipment Type	Manufacturer	Model	Serial Number	Firmware and/or Software Version	Version Install Date	Location	GAMS Calibration	Date of last Service	Additional Information	
POS/MV PCS	Applanix	320 V.4	2411	HW2.9-7, SW03.22	Jun-06	S220	3/29/2007		Auth. No. 811025-00534537	
POS/MV IMU	Applanix	LN200	292	N/A	Apr-04	S220			Bar Code : CD0001696450	
POS/MV Port Ant.	Applanix	OEM2 3151R	SGN 98490013	HW1	Apr-04	S220				
POS/MV Stbd Ant.	Applanix	OEM2 3151R	CGN 9620009	HW1	Apr-04	S220				
DGPS Receiver	CSI Wireless	MBX-3S	0426- 16627- 0001	N/A	Jul-04	\$220				
DGPS Ant.	CSI Wireless	MGL3		N/A	Apr-04	\$220				
POS/MV PCS	Applanix	320 V.4	2564	HW 1.9.7, SW 03.26	Jul-06	1010	3/30/2007			
POS/MV IMU	Applanix	LN200	294	N/A	Jul-04	1010			Bar Code : CD0001696449	
POS/MV Port Ant.	Applanix	OEM2 3151R	S/N 60162863	HW1	Mar-07	1010				
POS/MV Stbd Ant.	Applanix	OEM2 3151R	S/N 60145247	HW1	Mar-07	1010				
DGPS Receiver	CSI Wireless	MBX-3S	0331-12579-0008	N/A	Jul-04	1010				
DGPS Ant.	CSI Wireless	MGL3	0331-12579-0009	N/A	Jul-04	1010				
POS/MV PCS	Applanix	320 V.4	2560	HW 1.9.7, SW 03.26	Jul-06	1018	3/30/2007			
POS/MV IMU	Applanix	LN200	37	N/A	Feb-07	1018			Bar Code : CD0000832907	
POS/MV Port Ant.	Trimble	39105-00 DC 4618	60145158	N/A	Feb-07	1018				
POS/MV Stbd Ant.	Trimbe	39105-00 DC 4604	60130644	N/A	Feb-07	1018				
DGPS Receiver	CSI Wireless	MBX-3S	0328-12362-0001	N/A	Jul-04	1018				
DGPS Ant.	CSI Wireless	MGL3	0328-12352-0002	N/A	Jul-04	1018				
Trimble Backpack 1	Trimble	Pathfinder Pro XRS	0224078543	N/A	N/A	\$220				
Trimble Backpack 1: Antenna	Trimble	33580-50	0220341062	N/A	N/A	\$220				
Trimble Backpack 2	Trimble	Pathfinder Pro XRS	0224090101	N/A	N/A	\$220				
Trimble Backpack 2: Antenna	Trimble	33580-50	0220321059	N/A	N/A	\$220				
Handheld data collector	Trimble	TSCe	37318	N/A	N/A	S220				
Laser	Laser Tech Inc.	Impulse Laser Rangefinder	i09290	N/A	N/A	\$220				
Laser	Laser Tech Inc.	TruPulse 200 Laser Rangefinder	001481	N/A	N/A	S220				
Laser	Laser Tech Inc.	TruPulse 200 Laser Rangefinder	000676	N/A	N/A	S220				
Antenna cable	Trimble					S220			P/N22628	
Camcorder Batteries	Trimble					\$220			P/N17466	
NMEA/RTCM cable	Trimble					\$220			P/N30232-00	
data/power cable	Trimble					\$220			P/N30231-00	
dual battery cable	Trimble					\$220			P/N24333	
GPS Pathfinder field deviced cable	Trimble					S220			P/N45052	

SOUND SPEED MEASU	SOUND SPEED MEASUREMENT EQUIPMENT											
Equipment Type	Manufacturer	Model	Serial Number	Firmware and/or Software Version	Version Install Date	Location	Date of last Calibration	Date of last Service	Additional Information			
Moving Vessel Profiler winch	Brooke Ocean Technology Inc.	MVP-200-5	10328			S220			Calibration by ACME Velocimeters, not manufacturer. Brooke Ocean too backed up.			
Moving Vessel Profiler fish	Brooke Ocean Technology Inc.	MVP-FFF-SS-32-1	Spare			\$220			Spare Fish			
Moving Vessel Profiler fish	Brooke Ocean Technology Inc.	MVP-FFF-SS-32-1	10329			\$220						
Moving Vessel Profiler sensor	Brooke Ocean Technology Inc.	Smart SV +P	5229			\$220			Spare Sensor			
Moving Vessel Profiler sensor	Brooke Ocean Technology Inc.	AML SV +P	4986			\$220			*26 June - lost one fish and sensor; 1-166			
Penetrometer	Brooke Ocean Technology Inc.	FFCPT-35-2	10416			\$220						
Penetrometer sensor	Brooke Ocean Technology Inc.	AML SV +P	191-3			S220						
SEACAT Profiler	Sea-Bird	SBE 19plus	19P36026-4585	1.4D		\$220	Nov-06	N/A	CON files: 4585.con			
SEACAT Profiler	Sea-Bird	SBE 19plus	19P36026-4617	1.4D		1010 or 1018	Nov-06	N/A	CON files: 4617.con; connector pin broke 25 Sept.			
SEACAT Profiler	Sea-Bird	SBE 19plus	19P36026-4616	1.4D		1010 or 1018	Nov-06	N/A	CON files: 4616.con			
Micro Thermosalinograph	Sea-Bird	SBE 45 (TSG)	4536628-0117	N/A	N/A	\$220	Nov-06	N/A	P/N 4536628			
TIDES & LEVELING EQ	UIPMENT	•	•	•	•	•	•	•				
Equipment Type	Manufacturer	Model	Serial Number	Firmware and/or Software Version	Version Install Date	Location	Date of last Calibration	Date of last Service	Additional Information			
Level	Carl Zeiss	N12 333	100056	N/A	N/A	S220	Mar-07					
Level	Carl Zeiss	N12 333	103567	N/A	N/A	\$220	Mar-07					
Level	Leica	NA2 100	5332739	N/A	N/A	\$220						
Level	Lecia	NA2 100	5332747	N/A	N/A	\$220						

HORIZONTAL AND VER	HORIZONTAL AND VERTICAL CONTROL EQUIPMENT											
Equipment Type	Manufacturer	Model	Serial Number	Firmware and/or Software Version	Version Install Date	Location	Date of last Calibration	Date of last Service	Additional Information			
Receiver	Ashtech	Z-Xtreme	ZE1200339016	ZE00	Apr-04	\$220	Mar-07	obtained April 2004				
GPS Antenna	Ashtech	Geodetic 4	8365	N/A	N/A	\$220	Mar-07	obtained April 2004				
Position Data Link High Powered Base Unit	Pacific Crest	PDL 4135	0424 0171	2.40	Apr-04	S220	Mar-07	obtained April 2004				
Position Data Link Rover	Pacific Crest	PDL 4100	04240154	2.4	Apr-04	\$220	Mar-07	obtained April 2004				
Position Data Link Rover	Pacific Crest	PDL 4100	03473047	2.32	Apr-04	\$220	Mar-07	obtained April 2004				
Position Data Link Rover	Pacific Crest	PDL 4100	04240155	2.4	Apr-04	\$220	Mar-07	obtained April 2004				
Marine Deep Cycle Battery	Magnatron					\$220		purchased July 2004	7 as of May 2006			
Solar Panel	Uni-Solar	FLX-32	USF-32-14639	N/A	N/A	\$220						
Solar Panel	Uni-Solar	FLX-32	USF-32-14634	N/A	N/A	\$220						
Solar Panel	Uni-Solar	FLX-32	USF-32-14633	N/A	N/A	\$220						
Solar Panel	Uni-Solar	FLX-32	USF-32-14529	N/A	N/A	\$220						
Solar Panel	Uni-Solar	FLX-32	USF-32-14631	N/A	N/A	\$220						
Solar Panel	Uni-Solar	FLX-32	USF-32-14625	N/A	N/A	\$220						
Solar Panel	Uni-Solar	FLX-32	USF-32-14645	N/A	N/A	S220						
Solutions Dongles	Ashtech	600586 (A)	KEB2083	N/A	N/A	\$220						
Solutions Dongles	Ashtech	600586 (A)	KEB2077	N/A	N/A	S220						
GPS Receiver	Trimble	DSM-232	22511661	3.5	Feb-07	\$220						
GPS Receiver	Trimble	DSM-232RS	225111655	3.5	Feb-07	\$220			DGPS Reference Station			
DGPS Ant.	Trimble	33580-00	220395038	N/A	N/A	\$220						
GPS Antenna	Trimble	Geodetic Reference Station Antenna	30325441	N/A	N/A	\$220						
OTHER EQUIPMENT					-	-	-	-				
Equipment Type	Manufacturer	Model	Serial Number	Firmware and/or Software Version	Version Install Date	Location	Date of last Calibration	Date of last Service	Additional Information			

FAIRWEATHER Computers													
Machine Name		or and the second second	Operation	a Staten Date Put	ased Date of L	ast Rebuild	ocessor speed	longinal)	RAN Mart	h 2000 utes	Video PAM Ser	ie <sup>189</sup> p <sup>s</sup>	Contraction
FA_Proc_1	Plot Room	DELL PWS 650	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.8 GHz	1 GB	3 GB	2	128 MB	J5PSH31	CD0001354993	
FA_Proc_2	Plot Room	DELL PWS 360	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.8 GHz	1 GB	2 GB	2	128 MB	6WYB451	CD0001741478	
FA_Proc_3	Plot Room	DELL PWS 360	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.8 GHz	1 GB	3 GB	2	128 MB	GBBG451	CD0001741480	
FA_Proc_4	Plot Room	DELL PWS 360	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.8 GHz	1 GB	3 GB	2	128 MB	CBBG454	CD0001741481	
FA_Proc_5	Plot Room	DELL PWS 450	2000 SP4	~ March 2004	~ September 2005	2. GHz	unknown	2 GB	2	64 MB	344RH31	CD0001354979	FA_Process_5 added & configured 10/11/05
FA_Proc_6	Plot Room	DELL PWS 450	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.8 GHz	1 GB	2 GB	2	128 MB	356JG31	CD0001354468	
FA_Proc_7*	Plot Room	DELL PWS 360	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.8 GHz	1 GB	3 GB	2	128 MB	7WYB451	CD0001741477	*Formerly known as S220_NAV FA_Process_7 added & configured 5/6/05
FA_Proc_8	Plot Room	DELL PWS 360	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.8 GHz	1 GB	3 GB	2	128 MB	DBBG451	CD0001741482	
FA_Proc_9	Plot Room	DELL PWS 450	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.8 GHz	1 GB	3 GB	2	128 MB	846JG31	CD0001354463	
FA_Proc_10	DP-2	DELL PWS 450	2000 SP4	~ March 2004	~ September 2005	2.4 GHz	1 GB	2 GB	2	64 MB	644RH31	CD0001354984	FA_Process_10 added & configured 8/28/05
FA_CST	Field Office	DELL PWS 360	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.8 GHz	1 GB	2 GB	2	128 MB	FBBG451	CD0001741479	
FA_FOO	Field Office	DELL PWS 450	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.8 GHz	1 GB	3 GB	2	128 MB	646JG31	CD0001354465	
FA_O-LAB*	O-LAB	DELL PWS 450	2000 SP4	~ March 2004	~ September 2005	2.4 GHz	unknown	3 GB	2	64 MB	144RH31	CD0001354980	*formerly FA_Process_8b
FA_Mobile1	Laptop	DELL Inspiron 1100	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.4 GHz	2.5 GB	2.5 GB	1	64 MB	HGHWM41	CD0001272964	
FA_Mobile2	Laptop	DELL Inspiron 1101	XP Pro 2002 SP2	~ March 2004	~ September 2005	2.4 GHz	2.5 GB	2.5 GB	1	64 MB	GGHWM41	CD0001272965	
Toughbook 1	Laptop	Panasonic CF-18	XP Pro 2002 SP2	~ March 2004	~ July 2006	1.1 GHz	2.5 GB	N/A	1	64 MB	4HKSA59499	CD0001269860	*rebuilt after crash July 2006
Toughbook 2	Laptop	Panasonic CF-18	XP Pro 2002 SP2	~ March 2004	~ September 2005	1.1 GHz	2.5 GB	N/A	1	64 MB	4HKSA59560	CD0001269858	
Toughbook 3	Laptop	Panasonic CF-29	XP Pro 2002 SP2	March 2006	N/A	1.6 GHz	2.5 GB	N/A	1	128 MB	6AKSB06863	CD0001698251	
Toughtab 1	Laptop	Panasonic CF-18	XP Pro 2002 SP2	~ March 2004	~ September 2005	1.1 GHz	2.5 GB	N/A	1	64 MB	4GKSA55049	CD0001269589	
1010_ACQ	Launch 1010	DELL PWS 670	XP Pro 2002 SP3	~ March 2004	~ September 2005	2.8 GHz	2 GB	2 GB	3	64 MB	4JD0S61	CD0001696433	
1018_ACQ	Launch 1018	DELL PWS 670	XP Pro 2002 SP4	~ March 2004	~ September 2005	2.8 GHz	2 GB	2 GB	3	64 MB	71NKT61	CD0001696419	
S220_ACQ	Plot Room	Supermicro Xeon	XP Pro 2002 SP2	~ March 2004	N/A	2.8 GHz	896 MB	896 MB	3	128 MB	N/A	CD0001269853	
FA_MVP200	Plot Room	MVP-C1-2001	2000 SP4	~ March 2004	~ September 2005	2.4 GHz	230 MB	230 MB	1	64 MB	SN: 10330	CD0001269854	

External Hard Drives	/ `	and the second sec	PAM <sup>C</sup>	5 <sup>5</sup> 8 <sup>5</sup>	ode comments	
	Plot Room	Maxtor One Touch II	300 GB	S/N L618M19H	CD0001698248	
	Plot Room	Maxtor One Touch II	300 GB	S/N B60Y1QJH	CD0001474757	
	Plot Room	Maxtor One Touch II	300 GB	S/N L617HX5H	CD0001698245	
FA-SUBMISSION-UNIT4	Plot Room	Maxtor One Touch II	300 GB	S/N L60DP6TG	CD0001698250	
FA-SUBMISSION-UNIT1	Plot Room	WD1200B006-RNN	300 GB	S/N: WCAEK1371526	CD0001696434	
Western Digital 2	Plot Room	WD1200B008-RNN	120 GB	S/N: WCAES1181707	CD0001696417	
Western Digital 3	Plot Room	WD1200B008-RNN	120 GB	S/N: WCAES1182576	CD0001269837	
Western Digital 1	Plot Room	WD1200B011-RNN	120 GB	S/N: WCAES1181609	CD0001269824	
1010 Hard Drive	Plot Room	2.5" ION DRIVE GHD225U40		none	CD0001269826	
1018 Hard Drive	Plot Room	2.5" ION DRIVE GHD225U40		none	CD0001696418	
Net Disk	Plot Room	Ximeta Inc. ND Series Model: ND 10	80 GB	S/N: N4061100095	CD0001478894	

#### Hydrographic Personnel Roster

#### Field Unit: FAIRWEATHER S-220 Effective Date: 2/1/2007 Updated Through: 10/31/2007

OFFICERS				
Name and Grade	Current Position	Years of Hydro Experience (calculated)	Hydro Experience Since	Notes
CDR Andrew L. Beaver	Commanding Officer	15 year(s) + 9 month(s)	January-87	Arrived June-06
LCDR Edward J. Van Den Ameele	Executive Officer	14 year(s) + 4 month(s)	June-93	Departed August-07
LCDR Richard Fletcher	Executive Officer	13 year(s) + 6 month(s)	April-94	Arrived August-07
LT Jennifer Dowling	Field Operations Officer	6 year(s) + 11 month(s)	November-00	Arrived February -06
LTjg Michael Gonsalves	Junior Officer	2 year(s) + 11 month(s)	November-04	Nav Officer; Departed July-07
LTjg Jonathan French	Junior Officer	2 year(s) + 11 month(s)	November-04	ECO Officer; Departed April-07
LTjg Guinevere Lewis	Junior Officer	2 year(s) + 4 month(s)	June-05	Tides Officer; Promoted to LTjg April-07
LTjg Allison Martin	Junior Officer	2 year(s) + 4 month(s)	June-05	DC Officer, Nav Officer; Promoted to LTjg April-07
ENS Matthew Glazewski	Junior Officer	1 year(s) + 11 month(s)	November-05	
ENS Llian Breen	Junior Officer	0 year(s) + 10 month(s)	December-06	
ENS Nick Morgan	Junior Officer	0 year(s) + 10 month(s)	December-06	ECO Officer
ENS Mark Andrews	Junior Officer	0 year(s) + 3 month(s)	July-07	
ENS Patrick Redmond	Junior Officer	0 year(s) + 3 month(s)	July-07	
SURVEY DEPARTMENT				
Name and Rate	Current Position	Years of Hydro Experience	Hydro Experience Since	Notes
Lynnette Morgan	Chief Survey Technician	7 year(s) + 9 month(s)	January-00	departed August-06; return date tba
Grant Froelich	Chief Survey Technician	5 year(s) + 2 month(s)	August-02	
Stephanie Mills	Survey Technician	1 year(s) + 7 month(s)	March-06	Promoted to SST Sept 07
Dan Jacobs	Assistant Survey Technician	1 year(s) + 1 month(s)	September-06	Promoted to ST Sept 07
Brenna Campbell	Assistant Survey Technician	1 year(s) + 1 month(s)	September-06	Promoted to ST Sept 07
Adam Argento	Assistant Survey Technician	0 year(s) + 7 month(s)	March-07	
Andrew Evans	Assistant Survey Technician	0 year(s) + 4 month(s)	June-07	
DECK DEPARTMENT (involved in s	urvey work)			

Name and Rate	Current Position	Years of Hydro Experience	Deck Experience Since	Notes
Garry Guice	Chief Boatswain	N/A	April-82	
Eric Heiner	Third Mate	N/A	April-93	Promoted to Third Mate August -07
Ron Walker	BGL	N/A	June-84	
Kerri Curtin	AB	N/A	February-02	departed July 07
Emily Evans	DU	N/A	January-06	
Mills Dunlap	GVA	N/A	June-06	
Carter Terry	AB	N/A	February-07	
Chris Marcum	GVA	N/A	August-07	arrived Aug 07
Alex Davis	AB	N/A	January-07	

<b>ROTATING HYDROGRAPHERS &amp; V</b>	ISITORS (involved in survey wo	rk)											
Name and Rate	Current Position	Years of Hydro Experience	Hydro Experience Since	Notes & Dates Embarked									
Sarah Wolfskehl	ERT			P183, P909 Arr Apr-7, Dep Jun-27									
Sarah Wolfskehl     ERT     P183, P909 Arr Apr-7, Dep Jun-27       Matt Foss     Physical Scientist     P183, P909 Arr Apr-21, Dep Jun-27													
Toshi Wozumi	Physical Scientist			P183, P909, P903, P132 Arr Jul-7, Dep Sept-04									
Katie Reser	Physical Scientist			P183, P909, P903, P132 Arr Aug-06, Dep Sep -28									
Matt Foss	Physical Scientist			P903, P132 Arr Sep-5, Dep Oct-02									
Dave Sinson	Physical Scientist			P903, P132 Arr Sep-17, Dep Nov-03									

NOTES:

	FAIRWEATHER Sur	vey Software Systems	
Acquisition	Processing	Miscellaneous	Tracking
ISIS Sonar v7.0.2	CARIS HIPS & SIPS v6.0	Adobe Acrobat Professional	Microsoft Office
Triton Suite	CARIS HIPS & SIPS v6.1	Macromedia Dreamweaver 7.0.1	Corel Word Perfect Office 2002
POS MV Controller 3.3.2.2 (1010 and 1018)	CARIS Utilities	Snag It 7.1	McAffee
MV POS View 3.3.1 (S220)	CARIS GIS v4.4a	Paint Shop Pro v8	Computer Defragmentation
Brooke Ocean Technology MVP 2.26	CARIS Notebook v3.0	Global Mapper 7	
TerraSync 2.41	PYDRO v7.3	SevenCs - SeeMyDEnc	
	Pathfinder 3.1		
	Velocwin 8.8		
	Fledermaus 6.21		
	MapInfo 8.0		
	MapInfo 8.5		
	Ashtech Solutions v2.6		

ISIS Son	ar																						
Version	FA	PIOCES	Proce	Process Process	Process A	2TOCES	A H	PHOU PHOU	Proc	8 255 P10 A	0. 855 910 7	297 C	5/4 5/4	00	AN CO	the w	obile'	ought,	000	poot 2 1	in ACO IS	UN <sup>8</sup> ACO	n <sup>o co</sup> Doments
v.6.5.0				d.u																d.u	d.u	d.u	
v6.5.1				d.u																d.u	d.u	d.u	
v6.6.0				d.u																d.u	d.u	d.u	
v6.7.0				10/1/04																10/1/04	10/1/04	9/20/04	ISIS removed 2/14/05
v6.7.193.0																							
v6.8				N/A																2/10/05	2/28/05	2/14/05	FA_Process_4 No longer back-up computer
v6.9				N/A	10/7/05*															9/10/05	9/10/05	8/5/05	FA_Process_5 needs to be uninstalled, was backup acq
v7.0				N/A																		1/11/06	
v7.0.2																				4/27/06	4/27/06	4/27/06	
v7.0.410																				3/22/06	3/21/06	3/22/06	Uninstalled due to nav problems
v7.0.414	4/20/06																			4/24/06	4/24/06	4/21/06	FA_Process_1 setup for Dual 8111/8160 acquistion Uninstalled due to datagram frequency issue
ISIS Dongle	TEI 03-1527																			TEI 03-1525	TEI 03-1527	TEI 03-1526	

d.u.=date unknown; exact intall date not documented

Triton Suite:	: Dep	olhMa	ap, D	)elph	Nav, Ba	thyP	ro, R	T Ba	thy, a	81XX	< Ser	ver,	Miss	ion N	/lonite	or							
Version	EP.	PIOCE	255 PT00	255 P100	PTOCESS	ANDCESS F	A Proce	255 00 P100	1 55 P100 P100	255 P100 P100	PTOC	10 3/5 4		O'IA O'IA	a len	A Mot	ile' not	oughor o	oughor ~	ough ab 101	o ACO 101	.a.A.C.Q. 5.22	Comments
v2.12																				2/10/05	2/28/05	2/14/05	
v2.13					10/7/05															9/10/05	9/10/05	8/5/05	
v3.1.410																				3/22/06	3/21/06	3/22/06	
v3.1.2																				4/27/06	4/27/06	4/27/06	
DelphMap Dongle																				-1525	-1527	-1526	
DelphNav Dongle																				ТЕІ 03	ТЕІ 03	ТЕІ 03	
SevenC's S57 Dongle																				U10930	U10933		

TerraSync																							
Version	/4	P10	2000 00 00 00 00 00 00 00 00 00 00 00 00	A H	A A	2 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2			6/1 5830 010	PHO PHO PHO	PIO PIO		9 5) 60 41 61	D-LAB	ab) rate for the second	Nobile	A MODILE?	nbook Tough	BOOK 2 TOUS	ahtab	1010 1	1018 P	CO CO S <sup>2</sup> Comments
v2.40	NA	NA	NA	d.u			NA	NA	d.u.			NA			d.u		7/18/06		d.u				
v2.41	NA	NA	NA				NA	NA				NA	3/21/06		10/6/2004		7/18/2006	10/13/2004	10/5/2004				also installed on TCSe
Product													498	8295-0	00110								
Serials													ι	inkno	wn								
Software												498	295-001 <sup>-</sup>	10-04	309-7073A4	IA7							
Install Serials												4982	295-0011	0-050	68-EBD4E/	A8B							

d.u.=date unknown; exact intall date not documented

CARIS Licenses	;						
Caris License #	On	GIS	HIPS	Notebook	Expires	Туре	Comments
CW9604403	roving	1	1			Purple USB	replaces CW9604041
CW9604042	roving			1	12/31/07	Purple USB	
CW9604366	FADC3	7	7	5	10/31/07	Red USB	new key inst. 10/31/05

CARIS HIPS 8	SIPS 6.0																					
Version	EA Pro	ess the pro	CESS 2 FAPIC	cess? EA Pro	eess A FAPIO	COSS 5 FAPIC	cess o FA Pro	cess 1 FA Pro	cass of the pro	cess? cA Pro	66855 10 FA	C <sup>ST</sup> FA	F00 EN	LAB BB	Mobile	FAMO	alled hor	oughbo	over a	1010 4	0 0	Comments
v6.0 full	04/23/06	04/23/06	10/04/05	10/04/05	03/08/06	04/23/06	04/23/06	10/03/05	04/23/06	04/26/06	08/05/06	8/24/2006	í `	1/17/2006	i Í	Í	ŕ	ŕ	í	Ĺ	<u>    í</u>	
v6.0 HF1			10/04/05	10/04/05	03/08/06																	
v6.0 HF2			10/04/05	10/04/05	03/08/06																	
v6.0 SP1	4/23/2006	4/23/2006	12/14/05	4/23/2006	03/08/06	4/23/2006	4/23/2006	4/23/2006	4/23/2006	4/26/06	08/05/06	8/24/2006		01/17/06								
SP1 HF1			12/14/05		03/08/06									01/17/06		$\downarrow$	<u> </u>		⊢			
SP1 HF2			12/14/05		03/08/06								-	01/17/06			<u> </u>		┝──┥			
SP1 HF3 SP1 HF4			12/14/05	-	03/08/06		ł							01/17/06		+	+		r			
SP1 HF5			01/11/06		03/08/06								1	01/17/06		+	+					
SP1 HF6			01/11/06		03/08/06									01/17/06			1		-			
SP1 HF7			01/17/06		03/08/06									01/17/06					-			
SP1 HF8			03/08/06		03/08/06																	
SP1 HF9			03/08/06		03/08/06											$\vdash$	<u> </u>		⊢ →			
SP1 HF10			03/08/06		03/08/06								-				<u> </u>		┝──┥			
SP1 HF12			03/08/06		03/08/06										_	+	<u> </u>		<del>ا ا</del>			
SP1 HF13			03/08/06		03/08/06								1			+	+					
SP1 HF14			03/08/06		03/08/06		1							1		1	1					
SP1 HF 15			04/12/06		04/12/06														-			
SP1 HF16			04/12/06		04/12/06																	
SP1 HF17			04/12/06		04/12/06										_	$\downarrow$	<u> </u>		⊢			
SP2	4/23/2006	4/23/2006	04/16/06	4/23/2006	4/23/2006	4/23/2006	4/23/2006	4/23/2006	4/23/2006	4/26/06	08/05/06	8/24/2006	-	4/16/2006	5		<u> </u>		┝──┥			
SP2 HF2	4/23/2006 5/7/2006	4/23/2006 5/7/2006	5/7/2006	5/7/2006	5/7/2006	5/7/2006	5/7/2006	5/7/2006	5/7/2006	5/7/2006	08/05/06	8/24/2006	-	4/23/2006 5/22/2006	) i	+		$ \rightarrow $	r			
SP2 HF3	5/7/2006	5/7/2006	5/7/2006	5/7/2006	5/7/2006	5/7/2006	5/7/2006	5/7/2006	5/7/2006	5/7/2006	08/05/06	8/24/2006		5/22/2006	;	+	+	$\vdash$				
SP2 HF4	7/8/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006		08/05/06	8/24/2006		5/22/2006	5		1					
SP2 HF5	7/8/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006		08/05/06	8/24/2006		5/22/2006	5							
SP2 HF6	7/8/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006		08/05/06	8/24/2006		5/22/2006	;							
SP2 HF7	7/8/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006		08/05/06	8/24/2006		5/22/2006	5	—	<u> </u>		⊢			
SP2 HF8	7/8/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006		08/05/06	8/24/2006				+	+		<u> </u>			
SP2 HF10	7/8/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006		08/05/06	8/24/2000				+	+	$\vdash$				
SP2 HF11	7/8/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006		08/05/06	8/24/2006				1	1					
SP2 HF12	7/8/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006	7/6/2006		08/05/06	8/24/2006				1						
SP2 HF13	7/14/2006	7/14/2006	7/14/2006	7/19/2006	7/14/2006	7/14/2006	8/23/2006	8/12/2006	7/14/2006		08/05/06	8/24/2006										
SP2 HF14	7/14/2006	7/14/2006	7/14/2006	7/19/2006	7/14/2006	7/14/2006	8/23/2006	8/12/2006	7/14/2006		08/05/06	8/24/2006				$\downarrow$	<u> </u>		⊢			
SP2 HF15	8/23/2006	8/23/2006	8/23/2006	8/23/2006	8/23/2006	8/23/2006	8/23/2006	8/23/2006	8/23/2006		08/24/06	8/24/2006	-				<u> </u>		┝──┥			
SP2 HF10	9/18/2006	9/18/2006	9/18/2006	9/18/2006	9/18/2006	9/18/2006	date unknown	9/18/2006	9/18/2006		09/18/06	09/16/06			_	+	<u> </u>		<del>ا ا</del>			
SP2 HF18	9/18/2006	9/18/2006	9/18/2006	9/18/2006	9/18/2006	9/18/2006	date unknown	9/18/2006	9/18/2006		09/18/06	09/18/06	1			+	+					
SP2 HF19	10/2/2006	10/2/2006	10/2/2006	10/2/3006	10/3/2006	10/3/2006	10/3/2006	10/3/2006	10/3/2006		10/2/2006	10/03/06					1		-			
	removed	removed	removed	removed	removed	removed	removed	removed	removed	removed	removed	removed										
CARIS HIPS	5 & SIPS 6	.1																				
Vesion	FA Pro	ess fr pro	Deess 2 FA Pro	cess ? FA Pro	pross A FA Pro	10555 FA Pro	cess 6 FA Pro	LESS 1 FA Pro	tess of the pro-	CESS? FAPIO	6655 10 FA	CST FA	FOO FA	JILAB (BB) FA	Mobile	FANO	ile2	oughbo	ought?	an an ar	018 A	Comments
v6.1 full	02/25/07	02/25/07	02/13/07	02/25/07	02/25/07	02/25/07	02/25/07	02/25/07	02/25/07	03/06/07	04/03/07	08/11/07	04/02/07									
v6.1 HF1	03/06/07	03/06/07	03/04/07	03/06/07	03/07/07	04/09/07	03/07/07	03/05/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07	<u> </u>	1	$\vdash$	$\vdash$	ĻЦ	⊢₋₋ӏ		[	
v6.1 HF2	03/06/07	03/06/07	03/06/07	03/06/07	03/07/07	04/09/07	03/07/07	03/05/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07			<u> </u>	<u> </u>		⊢ →			
VO.1 HF3	03/06/07	03/06/07	03/06/07	03/06/07	03/07/07	04/09/07	03/07/07	03/05/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07			—	—	$\vdash$	┍━━┥			
v6.1 HF5	03/06/07	03/06/07	03/06/07	03/06/07	03/07/07	04/09/07	03/07/07	03/05/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07	<del> </del>	+	+	┼──	$\vdash$	┌──┤			
v6.1 HF6	03/06/07	03/06/07	03/06/07	03/06/07	03/07/07	04/09/07	03/07/07	03/05/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07		+	+	+	┝──┦	-+			
v6.1 HF7	03/06/07	03/06/07	03/06/07	03/06/07	03/07/07	04/09/07	03/07/07	03/07/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07		1	1	1					
v6.1 HF8	04/02/07	04/02/07	04/03/07	04/02/07	04/02/07	04/09/07	04/02/07	04/02/07	04/02/07	04/02/07	04/03/07	08/11/07	04/02/07			1						
v6.1 HF9	04/02/07	04/02/07	04/03/07	04/02/07	04/02/07	04/09/07	04/02/07	04/02/07	04/02/07	04/02/07	04/03/07	08/11/07	04/02/07									
v6.1 HF10	04/22/07	04/22/07	04/22/07	05/06/07	04/22/07	04/22/07	05/06/07	04/22/07	04/22/07	05/22/07	04/22/07	08/11/07	07/10/07			$\vdash$	$\vdash$	$\square$	⊢−−			
v6.1 HF11	05/06/07	05/06/07	05/06/07	05/06/07	05/06/07	05/06/07	05/06/07	05/06/07	05/06/07	05/23/07	05/06/07	08/11/07	07/10/07	I	1	<u> </u>	<u> </u>		<u> </u>			

v6.1 HF12	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/29/07	05/28/07	05/24/07	05/28/07	08/11/07	07/10/07					
v6.1 HF13	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/29/07	05/28/07	05/25/07	05/28/07	08/11/07	07/10/07					
v6.1 HF14	07/08/07	07/07/07	07/11/07	07/11/07	07/08/07	07/08/07	07/08/07	07/11/07	07/11/07	07/09/07	07/08/07	08/11/07	07/10/07					
v6.1 HF15	07/08/07	07/07/07	07/11/07	07/11/07	07/08/07	07/08/07	07/08/07	07/11/07	07/11/07	07/09/07	07/08/07	08/11/07	07/10/07					
v6.1 SP1	07/19/07	07/19/07	07/20/07	07/20/07	08/02/07	08/02/07		08/02/07	08/02/07	07/29/07	07/19/07	08/11/07	07/20/07					
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-	41	41	48	48	48	48	4	4	48	14	/ `	/ `	14	1 44	/ 47	~~~/	10%	^%/ `)	7 7	7 5	Comments
v6.1 full	02/25/07	02/25/07	02/13/07	02/25/07	02/25/07	02/25/07	02/25/07	02/25/07	02/25/07	03/06/07	04/03/07	08/11/07	04/02/07		ſ	Í	Í	ÍÍ	Í	Í	
v6.1 HF1	03/06/07	03/06/07	03/04/07	03/06/07	03/07/07	04/09/07	03/07/07	03/05/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07								
v6.1 HF2	03/06/07	03/06/07	03/06/07	03/06/07	03/07/07	04/09/07	03/07/07	03/05/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07								
v6.1 HF3	03/06/07	03/06/07	03/06/07	03/06/07	03/07/07	04/09/07	03/07/07	03/05/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07								
v6.1 HF4	03/06/07	03/06/07	03/06/07	03/06/07	03/07/07	04/09/07	03/07/07	03/05/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07								
V6.1 HF5	03/06/07	03/06/07	03/06/07	03/06/07	03/07/07	04/09/07	03/07/07	03/05/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07				_	_			
V6.1 HF6	03/06/07	03/06/07	03/06/07	03/06/07	03/07/07	04/09/07	03/07/07	03/05/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07			_	_				
V0.1 HF7	03/06/07	03/06/07	03/06/07	03/06/07	03/07/07	04/09/07	03/07/07	03/07/07	03/07/07	03/06/07	04/03/07	08/11/07	04/02/07			_	_				
V6.1 HF9	04/02/07	04/02/07	04/03/07	04/02/07	04/02/07	04/09/07	04/02/07	04/02/07	04/02/07	04/02/07	04/03/07	08/11/07	04/02/07							-	
v6.1 HF10	04/22/07	04/22/07	04/22/07	05/06/07	04/22/07	04/22/07	05/06/07	04/22/07	04/22/07	05/22/07	04/22/07	08/11/07	07/10/07			-					
v6.1 HF11	05/06/07	05/06/07	05/06/07	05/06/07	05/06/07	05/06/07	05/06/07	05/06/07	05/06/07	05/23/07	05/06/07	08/11/07	07/10/07								
v6.1 HF12	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/29/07	05/28/07	05/24/07	05/28/07	08/11/07	07/10/07								
v6.1 HF13	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/28/07	05/29/07	05/28/07	05/25/07	05/28/07	08/11/07	07/10/07								
v6.1 HF14	07/08/07	07/07/07	07/11/07	07/11/07	07/08/07	07/08/07	07/08/07	07/11/07	07/11/07	07/09/07	07/08/07	08/11/07	07/10/07								
v6.1 HF15	07/08/07	07/07/07	07/11/07	07/11/07	07/08/07	07/08/07	07/08/07	07/11/07	07/11/07	07/09/07	07/08/07	08/11/07	07/10/07								
v6.1 SP1	03/06/08	07/19/07	07/20/07	07/20/07	08/02/07	08/02/07	d.u.	08/02/07	08/02/07	07/29/07	07/19/07	08/11/07	07/20/07					$\bot$ $\Box$			
SP1 HF1	03/06/08	09/28/07	09/28/07	09/28/07	09/28/07	09/26/07	09/26/07	09/26/07	09/28/07	09/28/07	09/28/07	09/28/07	09/28/07								
SP1 HF2	03/06/08	09/28/07	09/28/07	09/28/07	09/28/07	09/26/07	09/26/07	09/26/07	09/28/07	09/28/07	09/28/07	09/28/07	09/28/07					+			
SP1 HF3	03/06/08	09/28/07	09/28/07	09/28/07	09/28/07	09/26/07	09/26/07	09/26/07	09/28/07	09/28/07	09/28/07	09/28/07	09/28/07								
571 HF4	03/06/08	09/28/07	09/28/07	09/28/07	09/28/07	09/26/07	09/26/07	09/26/07	09/28/07	09/28/07	12/02/07	09/28/07	03/11/02			_	_	+		_	low processing moching
SPI HE6	03/06/08	11/14/07	11/20/07	11/20/07	11/21/07	12/03/07	12/03/07	12/03/07	12/03/07	d.u.	12/03/07	du.	03/11/08					+		r	aew processing machines:
SP1 HF0	03/06/08	01/14/07	01/22/08	01/22/08	01/22/08	01/22/08	02/11/08	01/22/08	01/22/08	02/13/08	01/22/08	01/22/08	03/11/08			_	-		-	- 1	1, F2, F3, F4, F3, F7 (F10
SP1 HF8	03/06/08	01/14/08	01/22/08	01/22/08	01/22/08	01/22/08	02/11/08	01/22/08	01/22/08	02/13/08	01/22/08	01/22/08	03/11/08			_	-		-	-	
SP1 HF9	03/06/08	01/16/08	01/22/08	01/22/08	01/22/08	01/22/08	02/11/08	01/22/08	01/22/08	02/13/08	01/22/08	01/22/08	03/11/08			-					
SP1 HF10	03/06/08	03/05/08	02/12/08	02/11/08	03/05/08	03/06/08	02/11/08	03/05/08	03/06/08	02/13/08	03/06/08	03/06/08	03/11/08								
SP1 HF11	03/06/08	03/05/08	03/06/08	03/05/08	03/05/08	03/06/08	03/11/08	03/05/08	03/06/08	03/05/08	03/06/08	03/06/08	03/11/08								
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Utility	FAPT	ocess , FA Pro	seess ? FA Pr	ocess ?	ocess A P	ocess fr pr	peess o FA Pr	ocess 1 FA Pri	ocess of FA Pri	ocess ?	peess to the	EST ER	00 FN 01	ABIBDI	Divelation of the second	Aobile'	obilez	outho	0042730 0191780	0 1010	CO ACO 5-20 ACO 5-20 Comments	
LUv2.1.0	05/05/04	08/02/04	05/05/04	08/02/04	10/11/05	09/11/04	05/06/05	08/02/04	08/02/04	08/28/05	08/04/04	08/13/04	10/12/05									
CPCR v2.0	06/14/04	08/02/04	08/02/04	08/02/04	10/11/05	09/11/04	05/06/05	08/02/04	08/02/04	08/28/05	08/04/04	08/11/04	10/12/05									
EasyENCv3.0	11/05/04	10/07/04	10/07/04	10/08/04	10/11/05	09/23/04	05/06/05	10/08/04	09/23/04	08/28/05	10/07/04	10/07/04	10/12/05									
ConvUtilityv2.0.0.2	2/9/2005	2/14/2005	2/9/2005	2/9/2005	10/11/05	2/10/2005	05/06/05	2/9/2005	2/9/2005	08/28/05	2/14/2005	2/15/2005	10/12/05									
CARIS GI	s																					
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Service Pack & HotFix	FAPT	ocess   FA Pro	peess ? FA Pr	ocess 3 FAPT	ocess A P	ocess 5 FAPT	ocess o FA Pri	beess 1 FAPT	beess of the private states of the private s	ocess ?	peess 10 FA	-5 <sup>51</sup> +A	FOO FA O'	ABIBDI	ivelab FAM	obile' Not	oller oughpr	ougho	ow?	1010 AC	0 10 <sup>18</sup> 4	9 c9 20 C0 Comments
v4.4a	05/05/04	08/02/04	05/05/04	08/02/04	<del>10/11/05</del>	09/11/04	05/06/05	08/02/04	08/02/04	08/28/05	08/04/04	08/13/04	10/12/05									
SP4	05/05/04	08/02/04	05/05/04	08/02/04		09/11/04	05/06/05	08/02/04	08/02/04		08/04/04	08/13/04										<u> </u>
SP4+HF1	06/14/04	08/02/04	05/05/04	08/02/04		09/11/04	05/06/05	08/02/04	08/02/04		08/04/04	08/13/04										
SP4+HF2	06/14/04	08/02/04	05/05/04	08/02/04		09/11/04	05/06/05	08/02/04	08/02/04		08/04/04	08/13/04										<u> </u>
SP4+HF3	06/14/04	08/02/04	05/05/04	08/02/04		09/11/04	05/06/05	08/02/04	08/02/04		08/04/04	08/13/04										
SP4+HF4	06/17/04	08/02/04	05/05/04	08/02/04		09/11/04	05/06/05	08/02/04	08/02/04		08/04/04	08/13/04										<u> </u>
SP4+HF5	06/17/04	08/02/04	08/03/04	08/02/04		09/11/04	05/06/05	08/02/04	08/02/04		08/04/04	08/13/04										<u> </u>
SP4+HF6	08/03/04	08/02/04	08/03/04	08/02/04		09/11/04	05/06/05	08/02/04	08/02/04		08/04/04	08/13/04										
SP4+HF7	08/03/04	08/02/04	08/03/04	08/02/04		09/11/04	05/06/05	08/02/04	08/02/04		08/04/04	08/13/04										<u> </u>
SP4+HF8	08/03/04	08/02/04	08/03/04	08/02/04		09/11/04	05/06/05	08/02/04	08/02/04		08/04/04	08/13/04										
SP4+HF9	08/26/04	08/26/04	08/26/04	08/26/04		09/11/04	05/06/05	08/26/04	08/26/04		08/26/04	08/26/04										<u> </u>
SP4+HF10	08/31/04	08/31/04	08/31/04	08/31/04		09/11/04	05/06/05	08/31/04	09/01/04		08/31/04	09/01/04										ļ
SP4+HF11	11/05/04	11/05/04	11/04/04	11/06/04		11/06/04	05/06/05	11/06/04	11/06/04		11/06/04	11/06/04										<u> </u>
SP4+HF12	11/05/04	11/05/04	11/04/04	11/06/04		11/06/04	05/06/05	11/06/04	11/06/04		11/06/04	11/06/04										ļ
SP4+HF13	11/05/04	11/05/04	11/04/04	11/06/04		11/06/04	05/06/05	11/06/04	11/06/04		11/06/04	11/06/04										
SP4+HF14	11/05/04	11/05/04	11/04/04	11/06/04		11/06/04	05/06/05	11/06/04	11/06/04		11/06/04	11/06/04										<u> </u>
SP4+HF15	11/05/04	11/05/04	11/04/04	11/06/04		11/06/04	05/06/05	11/06/04	11/06/04		11/06/04	11/06/04										ļ
SP4+HF16	01/10/05	01/10/05	01/13/05	01/12/05		01/12/05	05/06/05	01/04/05	01/06/05		01/14/05	01/12/05										<u> </u>
SP4+HF17	01/10/05	01/10/05	01/13/05	01/12/05		01/12/05	05/06/05	01/04/05	01/06/05		01/14/05	01/12/05										<u> </u>
SP4+HF18	01/10/05	01/10/05	01/13/05	01/12/05		01/12/05	05/06/05	01/04/05	01/06/05		01/14/05	01/12/05										ļ
SP4+HF19	01/10/05	01/10/05	01/13/05	01/12/05		01/12/05	05/06/05	01/04/05	01/06/05		01/14/05	01/12/05										ļ
SP4+HF20	01/10/05	01/10/05	01/13/05	01/12/05		01/12/05	05/06/05	01/04/05	01/06/05		01/14/05	01/12/05										
SP4+HF21	01/10/05	01/10/05	01/13/05	01/12/05		01/12/05	05/06/05	01/04/05	01/06/05		01/14/05	01/12/05										<u> </u>
SP4+HF22	2/9/2005	2/14/2005	02/09/05	02/09/05		2/9/2005	05/06/05	02/09/05	02/09/05		02/01/05	02/15/05										
SP4+HF23	2/9/2005	2/14/2005	02/09/05	02/09/05		2/9/2005	05/06/05	02/09/05	02/09/05		02/01/05	02/15/05										
SP4+HF24	2/9/2005	2/14/2005	02/09/05	02/09/05		2/9/2005	05/06/05	02/09/05	02/09/05		02/01/05	02/15/05										<u> </u>
SP4+HF25	2/9/2005	2/14/2005	02/09/05	02/09/05		2/9/2005	05/06/05	02/09/05	02/09/05		2/14/2005	02/15/05										
SP4+HF26	2/9/2005	2/14/2005	02/09/05	02/09/05		2/9/2005	05/06/05	02/09/05	02/09/05		2/14/2005	02/15/05										<u> </u>
SP4+HF27	2/9/2005	2/14/2005	02/09/05	02/09/05		2/9/2005	05/06/05	02/09/05	02/09/05		2/14/2005	02/15/05										
SP4+HF28	2/9/2005	2/14/2005	02/09/05	02/09/05		2/9/2005	05/06/05	02/09/05	02/09/05		2/14/2005	02/15/05										
SP4+HF29	2/9/2005	2/14/2005	02/09/05	02/09/05		2/9/2005	05/06/05	02/10/05	02/09/05		2/14/2005	02/15/05										·
SP4+HF30	03/16/05	05/18/05	03/16/05	03/16/05		03/23/05	05/06/05	03/16/05	03/16/05		03/29/05	03/29/05										<u> </u>
SP4+HF31	05/24/05	05/18/05	04/25/05	04/25/05		05/24/05	05/06/05	05/23/05	05/23/05		05/24/05	05/24/05										
SP4+HF32	05/24/05	05/18/05	04/25/05	04/25/05		05/24/05	05/06/05	05/23/05	05/23/05		05/24/05	05/24/05				_	1					ļ
SP4+HF33	05/24/05	05/18/05	05/06/05	05/24/05		05/24/05	05/06/05	05/23/05	05/23/05		05/24/05	05/24/05						<u> </u>				ļ
SP5					10/11/05				08/02/05	08/28/05			10/12/05					<u> </u>				ļ
SP5+HF1					10/11/05				08/02/05	08/28/05			10/12/05			_	1					J
SP5+HF2					+0/11/05				08/02/05	08/28/05			10/12/05			_	1					J
SP5+HF3	l		L	L	<del>10/11/05 - 10/11/05</del>	L		1	08/02/05	08/28/05		1	10/12/05				<u> </u>					·

CARIS Noteb	ook																					
Service Pack & HotFix	EN Pro	cess the pro	ocess 2 FA Pri	FA Pro	cess A FA Pr	Coss 5 FAPT	Cess o FA Pro	cess 1 FA Pr	Cess of FA Pri	Cess 9 FA Pro	10 FA	1.551 FA	400 FA OI	AB(BD) FA	abile1 FA	Mobile2	ughbook'	ibook 2	ughtab	ano Acc	018 AC	+ KQ 2 <sup>20</sup> Comments
v2.1	05/14/04	08/06/04	08/09/04	08/06/04		09/11/04	05/06/05	08/02/04	08/06/04		08/06/04	08/13/04			01/23/05							
SP1	06/23/04	08/06/04	08/09/04	08/06/04		09/11/04	05/06/05	08/02/04	08/06/04		08/06/04	08/13/04			01/23/05							
SP1+HF1	08/06/04	08/06/04	08/09/04	08/06/04		09/11/04	05/06/05	08/06/04	08/06/04		08/06/04	08/13/04			01/23/05							
v2.2BETA	2/9/2005	02/14/05	2/9/2005	2/14/2005		01/31/05	05/06/05	2/9/2005	2/9/2005		02/01/05	02/15/05			01/23/05							
v2.2BETA2	03/25/05										03/25/05											
v2.2	07/11/05	07/12/05	07/12/05	07/12/05	03/23/06	07/11/05	07/12/05	07/12/05	07/12/05	08/28/05	07/11/05	08/24/06	10/12/05	01/17/06								
v2.2+HF1	09/02/05	09/02/05	09/02/05	09/02/05	03/23/06	09/02/05	09/02/05	09/02/05	09/02/05	08/28/05	08/01/05	don't need	10/12/05									
SP1	01/18/06	04/23/06	01/18/06	04/23/06	03/23/06	04/23/06	04/23/06	04/23/06	04/23/06	01/18/06	d.u.	08/24/06	05/11/06	01/17/06								
SP1+HF1	01/18/06	04/23/06	01/18/06	04/23/06	03/23/06	04/23/06	04/23/06	04/23/06	04/23/06	01/18/06	d.u.	08/24/06	05/11/06	01/17/06								
SP1+HF2	04/23/06	04/23/06	04/12/06	04/23/06	04/23/06	04/23/06	04/23/06	08/23/06	04/23/06	d.u.	d.u.	08/24/06	05/11/06									
SP1+HF3	04/23/06	04/23/06	04/12/06	04/23/06	04/23/06	04/23/06	04/23/06	04/23/06	04/23/06	04/26/06	d.u.	08/24/06	05/11/06									
SP1+HF4	08/23/06	06/06/06	08/23/06	06/18/06	06/18/06	08/23/06	08/23/06	08/23/06	08/23/06		08/24/06	08/24/06	08/24/06									
SP1+HF5	08/23/06	06/06/06	08/23/06	06/18/06	06/18/06	08/23/06	08/23/06	08/23/06	08/23/06		08/24/06	08/24/06	08/24/06									
SP1+HF6	08/23/06	08/23/06	08/23/06	08/23/06	08/23/06	08/23/06	08/23/06	08/23/06	08/23/06		08/24/06	08/24/06	08/24/06									
v3.0	04/02/07	04/02/07	03/15/07	04/02/07	04/02/07	04/09/07	04/02/07	04/02/07	04/02/07	04/02/07	04/03/07	d.u.	04/02/07				3/15/2007					
v3.0+HF1	04/02/07	04/02/07	04/02/07	04/02/07	04/02/07	04/09/07	04/02/07	04/02/07	04/02/07	04/02/07	04/03/07	08/11/07	04/02/07									

PYDRO																						
Version	FA Pro	cess , FA Pro	Geess 2 FA Pro	cess? FA Pri	cess A FA Pr	FA PT	Deess FA Pri	ocess 1 FA Pro	cess P FA Pro	scess Property for the pro-	peess 10 FA	est re	100 FA OI	ABIBBI	Mobi	A Nobil	e2	ov hood	t 2 not	ol ACC	2 AC	2 A <sup>R</sup> Comments
v6.2.9HF1,2,3 S57 Cat	05/11/06	05/11/06		05/11/06		05/03/06		05/03/06	05/03/06		05/11/06	05/11/06	05/11/06									
v6.4.9	05/23/06	05/22/06	05/21/06	06/18/06	05/22/06	05/22/06	05/22/06	05/22/06	09/13/06	09/13/06	09/13/06	09/13/06	05/22/06									
v6.4.9HF1&2	05/31/06	05/26/06	06/16/06	06/18/06	05/31/06		05/26/06	05/26/06	09/13/06	09/13/06	09/13/06	09/13/06	05/31/06									
v6.4.9HF3&4	06/07/06	07/14/06	06/16/06	06/18/06	1/0/1900	07/14/06	6/8/2006	6/8/2006	09/13/06	09/13/06	09/13/06	09/13/06	6/8/2006									
v6.4.9HF6	06/08/06	07/14/06	06/16/06	06/18/06	6/8/2006	07/14/06	6/8/2006	6/8/2006	09/13/06	09/13/06	09/13/06	09/13/06	6/8/2006									
v6.4.9HF6pp	09/13/06	09/13/06	09/12/06	09/13/06	09/13/06	09/13/06	09/13/06	09/13/06	09/13/06	09/13/06	09/13/06	09/13/06	09/18/06									
v7.1.0 (r1940)	01/30/07	01/30/07	01/30/07	01/30/07	01/30/07	d.u.	01/30/07	01/30/07	01/30/07	01/30/07	01/30/07	n/a	01/30/07									
v7.2.0 (r1982)	03/04/07	03/04/07	03/04/07	02/27/07	03/07/07	03/14/07	03/07/07	03/07/07	03/07/07	03/05/07	03/07/07	08/11/07	03/05/07									
v7.2.0 (r1984)	03/04/07	03/04/07	03/04/07	02/27/07	03/07/07	03/14/07	03/07/07	03/07/07	03/07/07	03/05/07	03/07/07	08/11/07	03/05/07									patch update
v7.2.2 (r1991)	03/07/07	03/07/07	03/07/07	03/07/07	03/07/07	03/14/07	03/07/07	03/07/07	03/07/07	04/02/07	03/07/07	08/11/07	d.u.									
v7.3 (r2002)	04/02/07	04/02/07	04/16/07	03/20/07	04/02/07	04/09/07	04/02/07	04/02/07	04/02/07	04/02/07	04/03/07	08/11/07	d.u.									
v7.3 (r2014)	04/02/07	04/02/07	04/16/07	04/02/07	04/02/07	04/09/07	04/02/07	04/02/07	04/02/07	04/02/07	04/04/07	08/11/07	d.u.									
v7.3 (r2014_TCfix)	d.u.	04/16/07	04/16/07	04/16/07	d.u.	05/06/07	d.u.	04/16/07	d.u.	d.u.	d.u.	08/11/07	d.u.									
v7.3 (r2110)	07/07/07	07/07/07	d.u.		d.u.	d.u.		d.u.	d.u.	07/09/07	d.u.	08/11/07	07/10/07									
v7.3 (r2114)		07/12/07	d.u.	07/12/07	d.u.	d.u.		d.u.	d.u.	d.u.	d.u.	08/11/07	d.u.									
v7.3 (r2119)		d.u.	d.u.	07/20/07	08/02/07	08/02/07		d.u.	08/02/07	07/29/07	07/19/07	08/11/07	07/20/07									
v7.3 (r2143)				08/23/07		08/30/07																
			d.u.=date un	known; exac	t install date	not docum	ented															
2007-2008	4				<u> </u>		- 0				- 40	<u> </u>		<u>г г</u>								
Licenses	d3b9bf48d2ada4a1d	19165d5744542751	19165d574432e27al	0a2e1a24b44aa2e7;	d3b9bf48ded331c78	d3b9bf48d2aac21f1	0a2e1a24b42d3c996	19165d574b44d10ei	d3b9bf48d317fc41e6	d3b9bf48d20a9b8aa	19165d57469c003f2	d3b9bf48d8d1c38f34	d3b9bf48dec82f7b90									
License expires	Jan-08	Jan-08	Jan-08	Jan-08	Jan-08																	
License File updated?	Yes	Yes	Yes		Yes																	
MAC Address	00-0B-DB-5A-62-2f	00-11-11-0F-84-44	00-11-11-06-9D-42	00-01-02-69-5A-45	00-0b-db-c5-f7-ec	00-0B-DB-56-68-2E	00-01-02-69-56-43	00-11-11-06-A1-B5	00-0B-DB-56-68-30	00-0B-DB-5A-D1-2	00-11-11-06-A4-68	00-0B-DB-56-68-8(	00-0b-db-c5-f5-ed									

PYDRO																						
Version	FA Pre	cess   FA Pt	ocess 2 FA Pro	ocess <sup>3</sup> FA Pt	Deess A FAPT	ocess FAP	ocess FAP	ocess <sup>1</sup> FA Pro	ocess of FA Pt	ocess? FA Pri	peess 10 FA	CST FA	FOO FAO	LABIBI	ANOF	inel Not	ule?	oughbe	over 1		018 4	2 2 <sup>20</sup> Comments
v7.1.0 (r1940)	01/30/07	01/30/07	01/30/07	01/30/07	01/30/07	d.u.	01/30/07	01/30/07	01/30/07	01/30/07	01/30/07	n/a	01/30/07									
v7.2.0 (r1982)	03/04/07	03/04/07	03/04/07	02/27/07	03/07/07	03/14/07	03/07/07	03/07/07	03/07/07	03/05/07	03/07/07	08/11/07	03/05/07									
v7.2.0 (r1984)	03/04/07	03/04/07	03/04/07	02/27/07	03/07/07	03/14/07	03/07/07	03/07/07	03/07/07	03/05/07	03/07/07	08/11/07	03/05/07									patch update
v7.2.2 (r1991)	03/07/07	03/07/07	03/07/07	03/07/07	03/07/07	03/14/07	03/07/07	03/07/07	03/07/07	04/02/07	03/07/07	08/11/07	d.u.									
v7.3 (r2002)	04/02/07	04/02/07	04/16/07	03/20/07	04/02/07	04/09/07	04/02/07	04/02/07	04/02/07	04/02/07	04/03/07	08/11/07	d.u.									
v7.3 (r2014)	04/02/07	04/02/07	04/16/07	04/02/07	04/02/07	04/09/07	04/02/07	04/02/07	04/02/07	04/02/07	04/04/07	08/11/07	d.u.									
v7.3 (r2014_TCfix)	d.u.	04/16/07	04/16/07	04/16/07	d.u.	05/06/07	d.u.	04/16/07	d.u.	d.u.	d.u.	08/11/07	d.u.									
v7.3 (r2110)	07/07/07	07/07/07	d.u.	d.u.	d.u.	d.u.	d.u.	d.u.	d.u.	07/09/07	d.u.	08/11/07	07/10/07									
v7.3 (r2114)	d.u.	07/12/07	d.u.	07/12/07	d.u.	d.u.	d.u.	d.u.	d.u.	d.u.	d.u.	08/11/07	d.u.									
v7.3 (r2119)	d.u.	d.u.	d.u.	07/20/07	08/02/07	08/02/07	d.u.	d.u.	08/02/07	07/29/07	07/19/07	08/11/07	07/20/07									
v7.3 (r2143)	d.u.	d.u.	d.u.	08/23/07	d.u.	08/30/07	d.u.	d.u.	09/28/07	09/28/07	d.u.	d.u.	d.u.									
v7.3 (r2180)	d.u.	d.u.	d.u.	11/02/07	d.u.		d.u.		11/02/07	03/11/08												
v7.3 (r2196)	11/20/07	11/14/07	11/20/07	11/20/07	11/20/07		11/20/07		11/02/07	03/11/08												
v7.3 (r2239)	12/03/07	12/03/07	12/03/07	12/04/07	12/03/07	12/03/07	12/03/07	12/03/07	12/03/07	03/11/08	12/03/07	12/03/07										
v7.3 (r2252)	03/11/08	03/11/08	03/11/08	02/28/08	02/26/08	03/11/08	03/11/08	03/11/08	03/11/08	03/11/08	03/11/08	03/11/08										
			d.u.=date ur	hknown; exa	ct install dat	e not docur	nented															
2008-2009		σ	13	Φ	8	~	0	8		5	-	8	8	1								
Licenses	a96fb9b9d4b4f3ff01	a96fb9b9d4afb102e	a96fb9b9d68db203	a96fb9b9dfeb032eb	a96fb9b9d4895c41t	d217461ea2aac21f	a96fb9b9d0af0fa60	1873e42d0b44d10e	d217461ea317fc41e	1873e42d04c1ba4e	1873e42d069c003f2	1873e42d0432e27a	d217461eaec82f7b9									
License expires	Jan-09	Jan-09	Mar-09	Jan-09	Jan-08	Jan-09	Jan-08	Jan-08	Jan-08	Mar-09	Mar-09	Mar-09	Jan-08									
License File updated?	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes										
MAC Address	00-1A-A0-BE-41-4A	00-1A-A0-BE-27-4B	00-1A-A0-BE-5C-69	00-1A-A0-BE-25-FF	00-1A-A0-BE-59-49	00-0B-DB-56-68-2B	00-1A-A0-BE-6C-0B	00-11-11-06-A1-B5	00-0B-DB-56-68-30	0011-11-29-91-4D	00-11-11-06-A4-68	00-11-11-06-9D-42	00-0b-db-c5-f5-ed									
0007 0000																						
2007-2008	2	ee	355	ec.	9	~	94	302	90	ia d	25	4	0							-		
Licenses	a81232e414b4f3ff0	a81232e414afb102¢	a81232e4168db203	a81232e41feb032et	a81232e414895c41	d3b9bf48d2aac21f1	0a2e1a24b42d3c99	19165d574b44d10e	d3b9bf48d317fc41e	d3b9bf48d20a9b8a	19165d57469c003f	d3b9bf48d8d1c38f3	d3b9bf48dec82f7b9									
License expires	Jan-08	Jan-08	Jan-08	Jan-08	Jan-08	Jan-08	Jan-08	Jan-08	Jan-08	Jan-08	Jan-08	Jan-08	Jan-08									
License File updated?	n/a	yes	n/a	n/a	n/a	yes	Yes	Yes	Yes	Yes	Yes	0	Yes									
MAC Address		00-1a-a0-be-27-4b	00-1A-A0-BE-5C-6	00-1A-A0-BE-25-FI	00-1A-A0-BE-5C-6	00-0B-DB-56-68-2		00-11-11-06-A1-B5	00-0B-DB-56-68-30	00-0B-DB-5A-D1-2	00-11-11-06-A4-68	00-0B-DB-56-68-8	00-0b-db-c5-f5-ed									
														1	1		1					

2006-2007	4		2	g	0		4	N		~								
Licenses	dc5c387302ada4a1d	16b8d68174542751d	16b8d6817432e27ab	05d0934ed44aa2e73	dc5c38730ed331c78	dc5c387302aac21f17	05d0934ed42d3c99d	16b8d6817b44d10e0	dc5c38730317fc41e6	dc5c3873020a9b8aa	16b8d681769c003f25	dc5c387308d1c38f34	dc5c38730ec82f7b90					
License expires	Jan-07	Jan-07	Jan-07	Jan-07	Jan-07	Jan-07	Jan-07	Jan-07	Jan-07	Jan-07	Jan-07	Jan-07	Jan-07					
License File updated?	Yes	Yes	Yes	Yes	Yes	Yes		Yes	Yes	Yes		0	Yes					
MAC Address	00-0B-DB-5A-62-2	00-11-11-0F-84-44	00-11-11-06-9D-42	00-01-02-69-5A-45	00-0b-db-c5-f7-ec	00-0B-DB-56-68-2h	00-01-02-69-56-43	00-11-11-06-A1-B5	00-0B-DB-56-68-30	00-0B-DB-5A-D1-2	00-11-11-06-A4-68	00-0B-DB-56-68-80	00-0b-db-c5-f5-ed					

<b>Pathfind</b>	er																					
Version	FA Pre	Sce55	A 4	Pro Pro				6 / 1 5 9 0 7 0	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	PLO PLO PLO			LAB	obl Divelab	obile1	FA Mobile?	DOOK TOUGH	Jook2 Tough	Tab	1010	1918	CO CO BAND Comments
v3.0	3/22/2005	NA	NA	d.u.		NA	NA	d.u.	NA		NA	3/21/06		d.u		7/18/2006	10/13/2004	10/4/2004				
v3.02		NA	NA			NA	NA		NA		NA			3/10/2006		7/18/2006	3/10/2006	3/10/2006				
Product												01174	16-00	300								
Serials												unl	know	n								
Software											<b>024</b> <sup>-</sup>	156-00300·	-0506	8-0E94DA58								
Install											0117	746-00300-	0430	9-3BAD03D2								

Veloc	win																					
Version	FA Pro	Ce55 /	Proc	Proc	255 P100	555 P100	25 2100 2100	Proc Proc	Process Pro	5055°	Proces	20 39 4	th too	ABIBB	A Dive	ANODI	Nobile Nobile	ughpo	ot )	oughtab 1 1010	ACQ 1018	ACO
v8.5.2													07/31/04									
v8.6.0													n/a									
v8.7.2													2/9/2005							2/11/2005	2/28/2005	
v8.7.3																						
v8.7.5	4/5/2005																					
v8.7.6	5/6/2005																					
v8.7.7	10/6/2005																					
v8.8	3/30/2006																					
v8.81	5/26/2006								5/26/2006				5/26/2006							5/26/2006	5/26/2006	
v8.83	4/11/2007												3/29/2007									

0
A A A A A A A A A A A A A A A A A A A
Comments
doesn't apply directly to us
For mvp .bot file processing
received new CON files Dec 2004
Seaterm Win 32 V 1.30, Seabird 5.27a

FLEDERMAUS																							
Version	FAPT	OCESS I FAP	rocess 2 FAP	ocess ?	OCESS A	IOCESS F. P.	ocess of the pr	ocess 1 FA Pt	OCESS <sup>9</sup> FAPT	ocess ? FA P	ocess V	EN CO	4N-0	6 01 4 P 01	AB Dive	A MOD	Net Mobile	ile2	ovighbo	oughtab	ono Acc	018 A	Comments
v6.1.0			07/28/04					07/28/04															
V6.1.1			08/03/04					08/03/04		08/13/04													
v6.1.2c			10/05/04					10/07/04		10/07/04													
v6.1.3			01/10/05					01/04/05		01/12/05													2 roving keys
v6.1.3i			03/07/05							03/29/05													What does this do? We don't know.
v6.1.4a			04/18/05																				
v6.1.4d	8/15/2005	08/13/05	08/13/05	08/15/05		08/13/05	08/13/05	08/13/05	08/13/05														1 local key on Proc 3 and 1 Network key on FADC1
v6.1.5			d.u.		10/11/05					10/12/05													
v6.2.0.a			03/06/06																				
v6.2.1			03/17/06																				
Lfledermaus FLEXid			9-65012FE																				9-6153BBA5 on FADC1 (network key)
License			B18BA0DE2D3F																				21DE819F1F03 on FADC1 (network key)

<b>MapInfo</b>																							
Version	FAS	tocess I	HOCESS ?	HOLESS ?	Cess A	Process P	tocess 6	HOLESS 1	ocess B	OCESS O	Process f	Les Le	400 FA	DILAB F	A Divel	ab Nobile	Mobile	athook Tour	ahoot 2	ntab 1	ACO	0 A 6 50	20 20 Comments
v7.5 (4)	06/15/04		07/30/04			10/07/04					08/04/04	09/01/04										F	Removed from FA_Process_1
v7.8			05/06/05				05/18/05				05/24/05	05/24/05										ι	Jpgrade
v8.0		10/12/05	10/05/05	3/6/2006		10/11/05	10/06/05	10/4/2005	3/10/2006		10/20/05	10/05/05	10/12/2005									3	new licenses and 4 upgrades
v8.5		10/09/06	10/10/06	10/19/2006																		7	copies to upgrade all 7 licenses
v9.0			ē									08/16/07								_			
MapBasic Licenses		N	2MBUWE U08500122					N															
MapInfo Licenses		MIUWEU08000387	MIUWEU08000387/	MIUWEU08000387		MIUWEU08000387		MIUWEU08000387/	MIUWEU08000387/			MIUWEU08000387											
Mapinfo Licenses v8.5		MIUWEU0850038722	MIUWEU0850038720	MIUWEU0850038723		MIUWEU0850038724		MIUWEU0850038726	MIUWEU0850038725			MIUWEU0850038721											



Adobe	Acrobat Profe	ssional 7.0																			
Version	FA Process	A Process 2	HOLESS ?	ocess A Pri	FA Pro	POCESS PART	FAPT	ocess of FAP	ocess?	SCESS 10 FP		FU FU	LAB (B)	A Dive	A NOO	A NODI	et poot	10042	ab 1 0	018 1918	CO CO 2017 2017 2017 Comments
v 7.0	3/30/06 3/30	et         et<																			
Mfg						54016	883IE (3 u	narades to	Pro 7)												
Item						04010	00012 (0 0	pgrades to	1101)												
Mfg						541	3725IE (10	Pro 7 licen	ses)												
Item						5410	57 201E (10	i io i liceli	500)												
Install Serial						1118-	1411-9394	-8097-7071	-5317												13 licenses

Macro	ned	ia D	rean	nweaver N	NX 2	2004	ļ																
Version	/4	PIO	255 210 210 210	2 2 2 2 1 2 1 0 2 1 0 2 5 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	50855 F	A Pro	2553 210 210	Pro Pro	2853 2910 2910	PTO		A Ci	velab	obile's	bile?	000¥	1042	1010	1010	ACO 1 5:201	Cor Cor	nment	<b>S</b>
v7.0.1				12/1/2005																			
Activation Code				3121258115691410000																			
Product Serial				DWD700-09955-92300-85366																			

#### **Equipment Specifications**

#### 1\_RESON

- 8101 Product Specs
- 8111 Product Specs
- 8160 Product Specs

#### 2\_POS/MV

POSMV v320

#### 3\_DGPS

MBX-3S

#### 4\_Shoreline

- Trimble Specs
- Trimble Accuracy
- Trimble TSCe
- Impulse 200LR Specs
- TruPulse 200LR Specs

#### 5\_SV

- MVP
- SBE 45
- Specs-19p-4585 (titanium)
- Specs-19p-4616 and -4617

#### 6\_Control

- Leica NA2 level
- Zeiss NI2 level
- PDL Flyaway Specs
- ZXtreme Ashtech GPS

#### 7\_Total Stations

- Nikon DTM 310 Specs
- Sokkia set5f Specs



# SeaBat 8101 PRODUCT SPECIFICATION 240kHz MULTIBEAM ECHO SOUNDER



- ! 240 kHz Frequency
- Up to 500m Range Capability
- Portable Configuration
- Meets USACE Class 1 Standards
- ! Meets IHO Standards

The SeaBat 8101 Multibeam Echo Sounder measures discrete depths, enabling complex underwater features to be mapped with precision. Dense coverage is achieved utilizing up to 3,000 soundings per second for a swath that can be over 500 meters wide, even as the survey vessel travels at speeds of over 18 knots.

With high accuracy and a measurement rate up to 30 profiles per second, the SeaBat 8101 enables surveys to be completed faster and in greater detail than previously realized. The SeaBat is an integral part of the new, integrated bathymetry surveying systems.

The SeaBat transducer is available pressurized for depths from 100 to over 3,000 meters. Small and lightweight, it can be can be mounted on small un vehicles (ROV, AUV or towed) and taken to where accurate measure required.

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SeaBat 8101 Built-In Test Environment ("BITE") Screen

#### SYSTEM SPECIFICATIONS

<b>Operating Frequency:</b>	240kHz
Range Scales:	5, 10, 15, 20, 25, 35, 50, 75, 100, 125,
	150, 175, 200, 250, 300, 350, 400, 450,
	500m.
Range Resolution:	1.25 cm
Number of Beams:	101
Horizontal Beamwidth:	1.5°
Horizontal Coverage:	150°
Vertical Beamwidth:	1.5°
Update Rate:	Range-variable up to
	30 times per second

#### SONAR HEAD SPECIFICATIONS

Power Requirement:	24VDC, 2 Amps max.	
-	(Power available from	
	surface processor.)	
Uplink:	Digital, 76.8 Mbaud	
Down Link Control:	RS-232 or RS-422, 19,200 baud	
Operating Depth:	100 meters	
	(300m, 1500m, 3000m & 6000m avbl.)	
Dimensions:	266x320mm W/Diam	
	(does not include projector)	
Temperature:	Operating: -5° to +40°C	
	Storage: -30° to +55°C	
Weight (aluminum):	Dry: 26.8 kg (59 lbs)	
	Wet: 4.8 kg (10.6 lbs)	
Weight (titanium): D	0ry: 40 kg (88 lbs)	
	Wet: 18 kg (39.6 lbs)	

#### **DISPLAY SPECIFICATIONS**

Screen Size:14 inch DiagonalInput:SVGA (800x600, 72 Hz)Display:High Resolution ColorPower Consumption:62 W

#### **PROCESSOR SPECIFICATIONS**

Power Requirements:	115/230VAC, 50/60Hz,
	100W max.
Data Output:	Selectable, 300-155.2 Kbaud
	or Ethernet 10 base T
	or 10 base 2
Video Output:	SVGA (800x600, 72 Hz)
	or NTSC or PAL video.
Graphics Colors:	256 colors (8-bit)
Display Mode:	Sector Format
Display Arc:	150°
Input Device:	3-Button Trackball
Dimensions:	19" rack, 4U high
	(266x483x434mm HWD)
Temperature:	Operating: 0° to +40°C
	Storage: -30° to +55°C
Weight:	20 kg (44 lbs)



SeaBat 8101 Head with Optional Fairings

Option 033:	Side Scan Upgrade
Option 034:	Mounting Plate Assembly
Option 035:	Fairings (pictured above)
Option 036:	Spares Kit
Option 037:	Titanium Housing
Option 038:	210° Swath
Option 040:	Extended-Range Projector
Option 049:	Increase Transducer Depth
	Rating



# SeaBat 8111 **PRODUCT SPECIFICATION MULTIBEAM ECHOSOUNDER**



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a

- Phase and amplitude bottom detection
- 100 kHz frequency
- 150° swath coverage
- **Real-time quality** control
- Sidescan upgradeable
- Modular and portable
- Pitch stabilization

The SeaBat 8111 is a modular multibeam echosounder system operating at 100 kHz. When installed on a vessel, it produces high-density, high-accuracy soundings on the seafloor over a 150° swath. Major system components include a transducer array, a transceiver unit, and a processor unit.

The SeaBat 8111 transducer array is comprised of a cylindrical receive array and a linear transmitter array, mounted together on a support cradle that provides mounting points to the vessel. Lightweight and portable, the array can be installed temporarily over the side of a vessel of opportunity-a first for a system in this frequency range.

The SeaBat 8111 transceiver features plug-in cards for easy maintenance and is controlled from the sonar processor.

The Seabat 8111 processor is compatible with other SeaBat sonar heads, can be updated in minutes to accommodate future requirements, and features a user-friendly point-and-click interface.



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# SeaBat 8111 SYSTEM SPECIFICATIONS

# SYSTEM PERFORMANCE

Frequency:	100 kHz
Range Resolution:	3.7 cm
Swath Coverage:	150°
Range:	3m to 1200m (with Option 040)
Number of Beams:	101
Along-Track Beamwidth:	1.5° 3.0° 4.5° 6.0°*
Across-Track Beamwidth:	1.5°
Stabilization:	Pitch stabilization within +/-15°
Projector Beam Control:	External motion sensor required
Accuracy:	IHO Compliant
<b>Operational Speed:</b>	Up to 20 knots
Max. Update Rate:	35 Hz
Transducer Pressure Rating:	100m

# **MECHANICAL INTERFACE**

Dimensions (in mm): Transducer Array:	
Hydrophone:	636 x 118 (Dia./Length)
Projector:	113 x 650 (Dia./Length)
Processor:	177 x 483 x 417
Transceiver:	267 x 483 x 489
Weight:	
Transducer Array:	72 kg (dry) / 59 kg (wet) with cables
Processor:	20 kg
Transceiver:	13.6 kg
Cable Length:	15m





### INTERFACE

\*operator selectable

System Supply:	90 to 260VAC, 50/60 Hz, 200W max.
Video Display:	SVGA, 800 x 600, 72 Hz
System Control:	Trackball or from Ethernet
Data Output:	10 MB Ethernet or serial RS232C
Data Uplink:	High-speed digital coax with fiber-optic option
Temperature:	Operating: 0° to +40° C

#### Storage: -30° to +55° C

### **RELATED PRODUCTS**

- Option 040 Extended range capabilities
- Option 033 Sidescan upgrade
- Option 051 24DC power supply for SeaBat 81-P Processor





Transducer Array

# SEAFLOOR COVERAGE

#### (with Extended Range option)

Bottom Depth (meters)	Swath Width (meters)
5 to 150	Up to 1110 (7.4 x water depth)
300	960 (3.2 x water depth)
450	810 (1.8 x water depth)
600	600 (1.0 x water depth)
750	450 (0.6 x water depth)
900	360 (0.4 x water depth)



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# SeaBat 8160 PRODUCT SPECIFICATION MULTIBEAM ECHOSOUNDER SYSTEM



- Swath coverage greater than 4x water depth
- Operational depth: 10m to 3000m
- 50 kHz frequency
- 126 beams
- Hull-mount or portable
- Meets IHO accuracy
- Sidescan upgradable

The SeaBat 8160 is a new addition to the 8100 series of multibeam echosounders. Operating at 50 kHz, the system ensonifies the whole swath in a single ping, generating 126 simultaneous high-resolution receive beams.

The SeaBat 8160 transducer array is comprised of a linear receive and transmit array mounted together on a support base. The T-shaped array geometry provides the basis for a compact, high-resolution sonar which is easily installed for portable or hull mounts—a first for a high-resolution system in this frequency range.

The system features a pitch-stabilized transmitter and an active rollcompensated receiver.

The SeaBat 8160 processor is compatible with other SeaBat sonar heads. It can be updated in minutes to accommodate future requirements, and features a user-friendly point-and-click interface.



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# SeaBat 8160 SYSTEM SPECIFICATIONS

### SYSTEM PERFORMANCE

Frequency:	50 kHz
Depth Resolution:	2.4 cm / 9.6 cm
Swath Coverage:	Greater than 4x water depth
Max Operational Depth:	3000 m
Number of Beams:	126
Along-Track Beamwidth:	1.5°
Across-Track Beamwidth:	1.5°
Pitch Stabilization:	±10°
Accuracy:	IHO Special Order
<b>Operational Speed:</b>	Up to 20 knots
Max. Update Rate:	15

#### Transducer Depth Rating:



### INTERFACE

System Supply:	115V/230V 50/60 Hz, 350W
Video Display:	SVGA, 800 x 600, 72 Hz
System Control:	Trackball or from Ethernet
Data Output:	10 MB Ethernet or serial RS232C
Data Uplink:	High-speed digital coax with fiber-optic option
Temperature:	Operating: 0° to +40° C Storage: -30° to +55° C

# MECHANICAL INTERFACE

#### Dimensions (HWD in mm):

Transducer Array:	1474.5 x 1100 x 90.5
Processor:	177 x 483 x 417
Transceiver:	265 x 483 x 492

#### Weight:

Transducer Array: Processor: Transceiver: 50 kg (dry) / 30 kg (wet) 20 kg 13.6 kg





Processor

Version: B34-PDF-011009 Due to our policy of continuous product improvement, RESON reserves the right change specifications without notice.

# **POS** MV<sup>™</sup> 320

#### Performance

	RTK	DGPS
Position (m)	0.02 - 0.10	0.5 - 4.0
Velocity (m/s)	0.03	0.03
Roll and Pitch	0.01û	0.02û
True Heading	4m baseline: 0.01, 2	2m baseline: 0.02û
Heave	5% of heave amplitude or 5cm	

#### **Physical Specifications**

Size	IMU	204 x 204 x 168mm
	PCS	441 x 111 x 346mm, 2.5U 19" rack mount
	Antenna	178 Ø x 77mm (2x)
	Choke Ring	360 Ø x 61mm (2x)
Weight	IMU	3.5 Kg
	PCS	7 Kg
Power		110/220 VAC, 60/50 Hz, 60W
Operating Temperature	IMU & Antennas	-40ûto +600C
	PCS	0ûto +60ứC
Humidity	IMU & Antennas	0 to 100%
	PCS	5 to 95% RH non-condensing
Cables	IMU	8m standard
	Antennas	15m standard (2x)

#### Interfaces

Ethernet Interface	Function	Operate POS MV <sup>TM</sup> & record data
(10base-T)	Data	Position, attitude, heading, velocity, track and speed, acceleration, status and performance, raw data. All data has time and distance tags
	UDP Ports	Display port - low rate (1Hz) data
		Data port - high rate (1-200Hz) data
	IP Ports	Control port - used by POSTM controller
RS232 Interface (DB9	NMEA Port	GGA, HDT, VTG, GST, ZDA, PASHR, PRDID (1-50Hz), GGK
males)	High rate attitude data port	Roll, pitch, true heading and heave in all multibeam proprietary formats (1-200 Hz)
	Auxillary GPS input	GGA, GST, GSA, GSV from Auxilliary DGPS, P-code or RTK reciever
Options	Internal RTK GPS receiver; analog interface (roll, pitch & heave); field support kit	

All performance figures are RMS, unless otherwise noted. Specifications subject to change without notice.



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# **POS** MV<sup>™</sup> marine vessels

# DATASHEET

# **The New POS MV - Providing the Marine Industry with robust, reliable, and repeatable position and orientation solutions**

The new POS MVV4 - a tightly-coupled system utilizing advanced Inertially-Aided Real-Time Kinematic (IARTK) technology designed to increase your operational capability and reduce downtime.

**Tightly integrated inertial navigation** – Continuous positioning data can be generated while surveying in areas where GPS reception is compromised by multipath effect and signal loss, such as close to offshore structures, or in ports, harbors, near-shore coastal waters and rivers. Raw GPS data from as few as one satellite can now be processed directly within the POS MV reducing position drift and RTK re-acquisition time.

#### The V4 Advantage

#### The Major Benefits

- Faster, more robust heading aiding from GPS Azimuth Measurement Subsystem (GAMS) when compared to V3
- Proprietary Inertially Aided RTK providing almost instantaneous reacquisition of RTK following a GPS outage
- Superior low elevation tracking performance using lighter, smaller Trimble Zephyr ™ geodetic antenna technology
- Faster initial system calibration
- Maintains heading accuracy longer when in a high multipath environment
- Increased component reliability
- Automatic identification and error estimation for lever arm distances and angles

#### **The Latest Technology**

# V4 uses the latest Trimble BD950 receivers with the following attributes:

- Extremely fast response time
- Latency of less than 20 milliseconds (at 20 times per second)
- Very low noise L1 and L2 carrier phase measurements
- Uses the Maxwell 4 Custom Survey GPS chip for enhanced tracking capability

#### Straightforward Installation and Operation

 All components mounted and installed using a straightforward, one-time-only, systematic procedure.

#### Faster, More Reliable Networking Potential

 An improved Ethernet raw data logging capability for streamlined data acquisition of all motion variables with microsecond-accurate time stamping

#### Upgradeability\*

 Convenient upgrade program for PCS and antennas, to allow for maximum interoperability when moving from L1 only to a full L1/L2 RTK unit

#### The Most Accurate Position and Orientation Solution

POS MVV4 maintains positioning accuracy under the most demanding conditions regardless of vessel dynamics. With its high data update rate, the system delivers a full six degree-of-freedom position and orientation solution to provide the following:

- Position (latitude, longitude and elevation)
- Velocity (north, east and vertical)
- Attitude (roll, pitch and true heading)
- Heave (real-time, delayed)
- Acceleration Vectors
- Angular Rate Vectors

\* For detailed upgrade information please call your Applanix Marine office



#### SYSTEM COMPONENTS

**POS Computer System (PCS)** – A rugged, compact computer system contains the core POS processor and IMU interface electronics, plus two GPS receivers and an optional removable PC-card disk drive. The PCS provides system timing, position and velocity aiding, together with GPS raw observables for use with GAMS.

**POS Inertial Measurement Unit** – The system's primary sensor allows for the continuous output of position and orientation data.

**Primary GPS Receiver Antenna** – A dual frequency antenna for use with GAMS.

Secondary GPS Receiver Antenna - A dual frequency antenna for use with GAMS.



# **POS** MV<sup>™</sup> marine vessels

# **SPECIFICATIONS**

#### Accuracy

POS MV 320 Mai	n Specifications (with Differential Corrections)
Roll, Pitch accuracy:	0.02° (I sigma with GPS or DGPS)
	0.01° (1 sigma with RTK)
Heave Accuracy:	5 cm or 5% (whichever is greater) for periods of 20 seconds or less
Heading Accuracy:	0.02° (I sigma) with 2 m antenna baseline, 0.01 (I sigma) with 4 m baseline
Position Accuracy:	0.5 - 2 m (1 sigma) depending on quality of differential corrections
	0.02 - 0.10 m (RTK) with input from auxiliary RTK or optional internal RTK receiver
Velocity Accuracy:	0.03 m/s horizontal

#### POS MV 320 during GPS Outages

Roll, Pitch accuracy:	0.02° (1 sigma)	
Heave accuracy:	5 cm or 5% (whichever is greater) for wave periods of 18s or less	
Heading accuracy:	Drift less than 1° per hour (negligible for outages < 60s)	
Position accuracy degradation:	2.5 m (I sigma) for 30 s outages <6 m (I sigma) for 60 s outages	

#### POS MV 220 Main Specifications (with Differential Corrections)

Roll, Pitch accuracy:	0.05° (I sigma with GPS or DGPS)	
	<0.05° (I sigma with RTK)	
Heave Accuracy:	5 cm or 5% (whichever is greater) for periods of 20 seconds or less	
Heading Accuracy:	0.1° (1 sigma) with 2 m antenna baseline, 0.05° (1 sigma) with 4 m baseline	
Position Accuracy:	0.5 - 4 m (1 sigma) depending on quality of differentia corrections	
	0.02 – 0.10 m (RTK) with input from auxiliary RTK or optional internal RTK receiver	
Velocity Accuracy:	0.05 m/s horizontal DPGS, .03 m/s horizontal RTK	

#### POS MV 220 during GPS Outages

Roll, Pitch accuracy:	0.05° (1 sigma)
Heave accuracy:	5 cm or 5% (whichever is greater) for wave periods of 18s or less
Heading accuracy:	Drift less than 3° per hour (negligible for outages < 60s)
Position accuracy degradation:	2.5 m (1 sigma) for 30 s outages <6 m (1 sigma) for 60 s outages

#### **Physical Characteristics**

Size		
IMU:	204 mm X 204 mm X 168 mm	7.95 in X 7.95 in X 6.55 in
PCS:	432 mm X 89 mm X 356 mm	17.00 in X3.50 in X 14.05 in
	2.0U 19 in rack mount	
GPS Antenna (x2):	187 mm X 53 mm	7.4 in X 2.1 in
Weight		
IMU:	3.5 kg	7.7 lb (international)
Processor:	5 kg	II.0 lb (international)
GPS Antenna:	<0.5 kg	<1.1 lb (international)
Power		
Processor	110/2301/26 50/60 6	auto switching 80 W/s

Processor:	I 10/230 Vac, 50/60 Hz, auto-switching 80 Watt
IMU:	Power provided by PCS
GPS Antennas:	Power provided by PCS

#### Environmental

#### Temperature Range (Operating)

IMU:	-40 °C to +60 °C	-40 °F to +140 °F
Processor:	0 °C to +55 °C	+32 °F to +131 °F
GPS Antenna:	-40 °C to +70 °C	-40 °F to +158 °F

#### Temperature Range (storage)

IMU:	-40 °C to +60 °C	-40 °F to +140 °F
Processor:	-25 °C to +85 °C	-13 °F to +185 °F
GPS Antenna:	-50 °C to +70 °C	-58 °F to +158 °F

10 - 80% RH, Ingress Protection of 65 10 - 80% RH, non-condensing

#### Humidity

IMU: Processor: GPS Antenna:

#### Shock & Vibration (IMU)

Operating:	90 g, 6 ms terminal saw tooth
Non-Operating:	220 g, 5 ms half-sine

0 - 100% RH

### **Applanix Marine Offices**

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csi wireless.

#### • Dual-channel Coast Guard beacon receiver

- Supplements GPS systems with free differential corrections, enhancing accuracy
- Fast signal acquisition
- Wide input voltage range for a variety of power sources

# MBX-3S

# The most popular commercial-grade Coast Guard Beacon Receiver

- Low power consumption extends battery life
- Automatic tuning mode for hands-free operation
- Integrated signal splitter outputs GPS signal from combined GPS /differential antennas
- Front-panel interface for easy configuration and status monitoring





#### The most popular commercial-grade DGPS Beacon Receiver



MBX-3S

Channels: Channel Spacing: Frequency Range: MSK Bit Rates: Cold Start Time: Warm Start Time: Demodulation: Sensitivity: Dynamic Range: Frequency Offset: Adjacent Channel Rejection: Correction Output Protocol: Input Status Protocol: 2 independent channels 500 Hz 283.5 to 325.0 Hz 50, 100, 200 bps <1 min <2 seconds Minimum shift keying 2.5  $\mu$ V/m for 6 dB SNR 100 dB ±8 Hz (27 ppm) 61 dB f<sub>o</sub> ± 400 Hz RTCM SC-104 NMEA 0183

#### **Communications**

Interface: Baud Rates: RS-232C or RS-422 2400, 4800, 9600

class A digital device

#### **Environmental Specifications**

Operating Temperature:	-30°C to +70°C
Storage Temperature:	-40°C to +80°C
Humidity:	95% non-condensing
EMC:	EN 60945
	EN 50081-1
	EN 50082-1
	FCC: Part 15, sub-part J,

#### **Power Specifications**

Input Voltage Range:9 to 40 VDCNominal Power:2.5 WNominal Current:210 mAAntenna Voltage Output:10 VDC (5 VDC optional)Antenna Input Impedance:50 Ω

#### **Mechanical Specifications**

Dimensions:

Weight: Display: Keypad: Power Connector: Data Connector: Antenna Connector: Optional GPS Output Port: 150 mm L x 125 mm W x 51 mm H (5.9" L x 4.9" W x 2.0" H) 0.64 kg (1.4 lb) 2-line x 16-character LCD 3-key switch membrane 2-pin circular locking DB9-S BNC-S TNC-S

#### **Operating Modes** MBX-3 Mode (Default):

MBX-E Mode:

RTCM SC-104 correction and NMEA status message output (Default Mode) RTCM SC-104 correction and NMEA status message output and GPS NMEA message input for position and satellite status display

#### NMEA 0183 I/O

- Receiver Automatic and Manual tune command
- Frequency and data rate query
- Receiver performance and operating status queries
- Automatic search almanac queries (proprietary)
- Baud rate selection command
- Receiver tune command
- Force cold start command (proprietary)
- Software upgrade command (proprietary)
- Configuration up-load command (proprietary)

#### Accessories

Antenna: Power Cables: Antenna Cables: Data Cables: CSI Beacon Command Center: Various Various Various Various

MS Windows 95<sup>®</sup> beacon control software

#### Pin-out

Pin 2

Pin 3

Pin 5

RS, 232C (DB9 PIN#)

TXD,RTCM SC-104/Status Output RXD, configuration input Signal return

#### RS-422 (DB9 PIN#)

Pin I	TXD +, RTCM SC-104 /
Pin 2	Status Output TXD -, RTCM SC-104 /
D: 4	Status Output
Pin 4 Pin 5	Signal return
Pin 7	RXD +, configuration input

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Warranty: Each CSI Wireless product is covered by a limited one-year warranty on parts and labor.





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Printed in Canada.

# **GPS Pathfinder Pro XRS**

# High-performance GPS with a world of real-time options

The versatile GPS Pathfinder<sup>®</sup> Pro XRS receiver is the thoroughbred of GPS receivers. Offering a full range of accurate real-time correction sources, great performance in all GPS conditions, and rugged design for the toughest environments, the Pro XRS is an essential tool for collecting and maintaining GPS data.

#### Built to meet your demands

With the Pro XRS, you don't have to worry whether your GPS receiver can stand up to harsh conditions. All its components are sealed in a robust casing. Waterproof, dustproof, and shock-resistant, the Pro XRS can work anywhere you can.

Just as tough is the custom-designed ergonomic backpack. But it's light and comfortable, so you can wear it all day.

#### You're spoiled for real-time choice

If you're navigating in the field, or finding your way back to a previously recorded feature, you've got all the real-time options covered. Corrections from a radiobeacon, a satellite differential service such as OmniSTAR, or a satellite-based augmentation system (SBAS) like WAAS<sup>1</sup> or EGNOS<sup>2</sup> are not just built in, they're seamlessly integrated into the receiver. Want the freedom to connect to an external correction source like a virtual reference station (VRS)? You've got it. This array of real-time sources makes the Pro XRS the most adaptable real-time GPS receiver around.

#### High quality, accurate data for your GIS

With the Pro XRS, you can be sure that the data you collect meets your high standards. Offering submeter accuracy in real time, and centimeterlevel postprocessed accuracy, it's the obvious choice for collecting the high quality GPS data



you need in your GIS. And it has advanced design features, like EVEREST<sup>™</sup> multipath rejection technology, to ensure you get only the best positions.

#### Get the results you want

The GPS Pathfinder Pro XRS's advanced design gives you complete control over GPS quality. You can focus on productivity, to keep working even in adverse GPS conditions. Or you can configure the receiver to deliver only the most precise positions. It's up to you.

#### Flexible data collection options

Pick the field device and software that fits your workflow. The Pro XRS is ready to use with a variety of field computers, including Trimble's own range of handheld computers: the GIS TSCe<sup>™</sup> field device, the Trimble<sup>®</sup> Recon<sup>™</sup> handheld, and the GeoExplorer<sup>®</sup> series.

Choosing software? Try the TerraSync<sup>™</sup> software, for a complete solution from the field to the office and back. Choose off-the-shelf GPS field software. Or use the GPS Pathfinder Tools SDK to build your own application that's totally customized to your needs.

# Key Features

- Real-time submeter accuracy
- Integrated satellite, beacon, and WAAS/EGNOS differential receiver
- EVEREST multipath rejection
- Rugged design
- Ergonomic, comfortable backpack system
- Choice of field device and field software

#### All you need

You need equipment that's as adaptable and hard-working as you are. So when you're choosing GPS equipment, don't compromise. Get a GPS Pathfinder Pro XRS receiver and have it all.



# What Can the GPS Pathfinder Systems Receivers Do?

The GPS Pathfinder Systems receivers, with Trimble controlling software, make an ideal system for all GIS data collection and maintenance projects. The system allows you to collect precise data for utility, urban, and natural resource databases. As the demand for accurate and up-to-date position and attribute information increases, the system allows you to update existing GIS data, ensuring that decisions made with the GIS are based upon the most accurate, current, and reliable data available.

The foundation of the GPS Pathfinder Systems receivers is precise GPS positioning technology. The GPS receivers feature 12 parallel channels for continuous satellite tracking. Using differential GPS, the GPS Pathfinder Systems receivers deliver differentially corrected C/A code positions to submeter accuracy on a second-by-second basis under the most challenging operating conditions.

# Integrated Satellite Based Augmentation System (SBAS) receiver

Satellite Based Augmentation System (SBAS) support is integrated into the GPS Pathfinder Pro XR, Pro XRS, and Power receiver. It allows you free access to real-time solutions transmitted from geostationary SBAS satellites, such as the Wide Area Augmentation System (WAAS) in the United States and the European Geostationary Navigation Overlay Service (EGNOS) in Europe.

#### Integrated beacon receiver

The MSK beacon receiver is included in the GPS Pathfinder Pro XR and Pro XRS receivers. It allows you free access to real-time solutions transmitted from DGPS radiobeacons operating in the MF (medium frequency) band from 283.5 kHz to 325 kHz. The integrated MSK beacon receiver is an advanced dual-channel radiobeacon receiver. It tracks broadcasts from DGPS radiobeacons conforming to the IALA Standard. The beacon receiver uses its *all-digital signal processing* techniques to track and demodulate signals from DGPS radiobeacons.

For an up-to-date list of beacon stations, visit the following Web page:

• www.trimble.com/findbeacon.asp

#### Integrated satellite differential receiver

The integrated satellite differential capability of the GPS Pathfinder Pro XRS and Power receivers decodes and uses satellite differential corrections to provide submeter position accuracy. To receive and decode these satellite signals, you must subscribe to a satellite differential correction service. The GPS Pathfinder Pro XRS and Power receivers support the OmniSTAR satellite differential correction services. For information on obtaining a subscription, subscription rates, and satellite coverage maps, visit www.omnistar.com

Once you have a subscription, you activate the service through an on-the-air signal or an encrypted activation message entered into the controlling software.

Satellite differential signals provide valid corrections over a large area. Integrated virtual reference/base station (VRS/VBS) technology permits the satellite corrections to be uniformly accurate over the entire satellite coverage area, without the degradation in accuracy associated with increasing distance from fixed reference stations.

Satellite differential signals are line-of-sight and can be blocked by mountains, buildings, or tree canopy. Wet canopy, from a heavy rain, reduces the signals even more. The same environmental factors that affect the GPS signal, such as radar and microwave transmitters, can interfere with the satellite signal. Power lines usually have no effect.

#### External differential correction receiver

The GPS Pathfinder Systems receivers can also receive differential corrections from any external differential correction receiver that communicates in the standard RTCM SC-104 data format.

### Standard GPS Pathfinder Pro XR and Pro XRS Features

The GPS Pathfinder Pro XR and Pro XRS receivers offer the following:

- 12-channel DGPS receiver with EVEREST<sup>™</sup> multipath rejection technology, L1 C/A code tracking with carrier-phase smoothing, and instantaneous full-wavelength carrier-phase measurements.
- Submeter accuracy Typically horizontal accuracy less than 50 cm RMS with GPS Pathfinder Office software postprocessing. This requires data to be collected with a minimum of 4 satellites, maximum PDOP of 6, minimum SNR of 4, minimum elevation of 15 degrees, and reasonable multipath conditions.
- Integrated WAAS/EGNOS differential corrections
- 1 Hz position and velocity update rate.
- Velocity computations incorporate carrier-phase data.
- Time to First Fix typically less than 30 seconds.
- Two RS-232 serial ports.
- NMEA-0183 output to external NMEA devices (supported messages are ALM, GGA, GLL, GSA, GSV, VTG, and ZDA).
- RTCM-SC 104 input from an external differential correction receiver.
- TSIP protocol to/from the field device.
- Fully automatic and manual beacon operating modes, fast acquisition of differential beacon signals.

- Immunity to MSK jamming signals, advanced techniques for combating atmospheric noise in the beacon receiver.
- Integrated GPS/MSK beacon antenna.
- User-upgradeable receiver firmware.
- Receiver manual.
- CE Mark compliance.

#### Additional GPS Pathfinder Pro XRS receiver features

The GPS Pathfinder Pro XRS GPS/MSK/beacon/satellite differential receiver offers the items previously listed, and also:

- Integrated L-band satellite differential correction receiver
- Combined L1 GPS/beacon/satellite differential antenna

#### Combined L1 GPS/beacon/satellite differential antenna

The GPS Pathfinder Pro XRS receiver integrated L1 GPS/beacon/satellite differential antenna (P/N 33580-50) features two antenna components:

L1 GPS/satellite differential antenna

This active antenna is designed to filter out unwanted signals and amplify the L1 GPS and satellite differential signals for transmission over the antenna cable to the receiver.

MSK H-field loop beacon antenna

This antenna features a pre-amplifier for filtering out signal interference such as AM radio broadcasts and noise from switching power supplies. After filtering, the pre-amplifier amplifies the MF signal for transmission over the same antenna cable to the beacon receiver.

The coaxial antenna cable also carries DC power to the pre-amplifier of both the L1 GPS/satellite differential and beacon antennas over the center conductor of the cable.

The antenna assembly integrates the L1 GPS/satellite differential antenna and a beacon antenna into a single antenna assembly, as shown in Figure 2.2. The antenna assembly is completely weatherproof and is designed to withstand harsh environmental conditions.



Figure 2.2 Combined L1 GPS/beacon/satellite differential antenna (for the GPS Pathfinder Pro XRS receiver)

### Introduction

This appendix lists specifications for GPS Pathfinder Systems receivers and antennas, and pinouts for cables that are supplied with the receivers.

### Specifications

Table B.1 lists specifications for the GPS Pathfinder Pro XR and Pro XRS receiver.

Parameter	Specification			
General	12 channel, L1/CA code tracking with carrier phase filtered measurements and multibit digitizer			
Update Rate	1 Hz			
Time to First Fix	< 30 seconds, typical			
Size	11.1 cm $\times$ 5.1 cm $\times$ 19.5 cm (4.4" $\times$ 2.0" $\times$ 7.7")			
Weight	0.76 kg (1.68 lb)			
Power	XR 6 W (maximum)			
	XRS 7 W (maximum)			
	both 10 to 32 VDC			
Temperature	-20 °C to 65 °C (-4 °F to 149 °F) operating			
	–30 °C to 85 °C (–22 °F to 185 °F) storage			
Humidity	100% non-condensing			
Casing	Dustproof, splashproof, shock-resistant, sealed to 5psi			

# Table B.1 GPS Pathfinder Pro XR and Pro XRS receiver specifications

#### Table B.3 lists specifications for the GPS Pathfinder Pro XRS antenna.

# Table B.3 Combined L1 GPS/beacon/satellite differential antenna specifications

Parameter	Specification
General	Right-hand, circular polarized; omnidirectional; hemispherical coverage
Size	15.5 cm diameter $\times$ 14 cm high (6.1" $\times$ 5.5")
Weight	0.55 kg (1.2 lb)
Temperature	-20 °C to 65 °C (-4 °F to 149 °F) operating
	-40 °C to 85 °C (-40 °F to 185 °F) storage
Humidity	100% fully sealed
Casing	Dustproof, waterproof, shock resistant

# **Pinouts**

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Table B.5 lists the pinouts for the GPS Pathfinder Pro XR and Pro XRS receiver's data/power cable.

Table	B.5	Data/power	cable	pinout	(P/N	30231-00)	)
		· · · · · · · · · · · · · · · · · · ·			•		

To GPS Pathfinder Pro XR and Pro XRS receiver			Field Device		Input Power			
Conn P1			7 Cond Cbl #1	Co	onn P2 E9-F	2 Conn Cbl #2	Co TA	onn P3 \3-M
Event In	1	in						
TXD out	2		Orange	2	RXD			
RXD	3	in	Red	3	TXD		_	
Chg Ctrl	4	in	Black	4	DTR			
Sig Gnd in/out	5		Shield	5	Sig Gnd	-		
DSR out	6		Yellow	6	DSR	_		
Pwr On	7	in	Brown	7	RTS	_		
CTS out	8		Green	8	CTS	_		ł
Charge out	9		Blue	9	RI	_		i
V+ In	10	in				White	1	V+ In
V– In	11	in	-	_		Black	2	V- Out
PPS —	12		_	-		_		

Table B.7 lists the pinouts for the GPS Pathfinder Pro XR and Pro XRS receiver's NMEA/RTCM cable.

To GPS Pathfinder Pro XR and Pro XRS receiver		NMEA/RTCM output connectors					
Conn P1			9 Cond Cbl #1	Conn P2 DE9-M	7 Conn Cbl #1	Conn P3 DE9-F	
Event In	1	in					
TX- (232)	2	out	_		Orange	2 TXD	
RX- (232)	3	in	Red	2 RXD			
Chg Ctrl	4	in		_	Shield		
Sig Gnd	5	in/out	Shield	5 Sig Gnd	_	5 Sig Gnd	
TX+ (422)	6	out					
Pwr On	7	in				_	
RX+ (422)	8	out					
Charge	9	out	Yellow	9 Pwr			
V+ In	10	in					
V– In	11	in			_	<u> </u>	
PPS	12				Brown	4 DTR	

#### Table B.7 NMEA/RTCM cable pinout (P/N30232-00)

# Introduction

The GPS Pathfinder Systems receivers calculate very accurate GPS positions on a second-by-second basis. After postprocessed differential correction, the horizontal accuracy of each position for the GPS Pathfinder Pro XR and Pro XRS receivers is better than 50 cm (RMS) + 1 part per million (ppm) times the distance between the base and the rover. For the GPS Pathfinder Power receiver, the horizontal accuracy is submeter (RMS) + 1 ppm. Using real-time corrections, each position can be as accurate as submeter with the GPS Pathfinder Systems, but is subject to a number of operational conditions.

*Note – RMS means that approximately 63% of the positions are within the specified value.* 

# **Differential GPS Positioning Techniques**

Differential GPS (DGPS) requires two or more receivers. One receiver, called the reference station, is located at a known point to determine the GPS measurement errors and compute corrections to these errors. An unlimited number of mobile GPS Pathfinder Systems receivers, commonly called *rovers*, collect GPS data at unknown locations within the vicinity of the reference station. Errors common at both the reference and rover receivers are corrected with DGPS either in real time or during postprocessing.

*Note –* For more information about GPS and DGPS, review the All About GPS tutorial on the Trimble website at www.trimble.com.

The GPS Pathfinder Systems receivers, in combination with Trimble controlling software and the GPS Pathfinder Office software, provide three ways of obtaining submeter positions:

- Real-time DGPS
- Postprocessed DGPS
- Postprocessed real-time DGPS
The accuracy figures given in the sections below are obtained under the following conditions:

- Number of satellites used:  $\geq 4$
- PDOP:  $\leq 6$
- Signal-to-noise ratio:  $\geq 4$
- Satellite elevation mask:  $\geq 15^{\circ}$
- Reference station receiver is a Trimble GPS Pathfinder Pro XL, Pro XR, Pro XRS, 4700, 4800, 5700, 5800, 4600 LS<sup>™</sup>, Series 4000 GPS receiver, DSM<sup>™</sup>, Reference Station, or equivalent.
- Synchronized measurements are logged at the reference station.
- The logging interval for the roving receiver is the same as, or a multiple of, the logging interval at the reference station.
- The reference station uses the correct antenna.

#### Real-Time DGPS

When using real-time DGPS, the reference station broadcasts the correction values to the rovers within coverage range, through a transmitter such as a radiobeacon (beacon DGPS) or a satellite (satellite DGPS). The rover applies the corrections to its position in real time.

The positions calculated by the GPS Pathfinder Systems receivers using real-time DGPS are of submeter accuracy + 1 ppm. If you use a provider of real-time DGPS that uses VRS/VBS techniques, there is no degradation associated with distance from the reference station, and the accuracy always stays at the submeter level (RMS).

GPS Pathfinder Systems also supports corrections from satellite-based augmentation systems (SBAS) such as WAAS and EGNOS.

For information on postprocessing GPS data collected with real-time DGPS, see Postprocessed real-time DGPS, page 20.

#### Postprocessed DGPS

When real-time DGPS is not available, or is available only part of the time, you have to postprocess the autonomous GPS data in your rover file to obtain the stated accuracy. When using postprocessed DGPS, the reference station stores the correction values in base data files on a computer.

Many reference station owners provide their base data to the community through the Internet or other means of communication. Often this means that you do not have to set up your own reference station for postprocessed DGPS, but can use an existing one. For a list of available reference stations, visit the Trimble website www.trimble.com/trs/findtrs.asp.

#### Postprocessed real-time DGPS

Postprocessed DGPS positions are generally more accurate than DGPS positions obtained in real time. If you collect SuperCorrect records as well as GPS positions using Trimble TerraSync or GPScorrect<sup>™</sup> software, or applications developed using the GPS Pathfinder Tools SDK, you can use the SuperCorrect option in the GPS Pathfinder Office software to process the data if the accuracy of the real-time DGPS positions is not sufficient, provided that you have access to suitable reference station base files.

The accuracy using postprocessed real-time DGPS is the same as for postprocessed DGPS (see the previous section).

#### Factors Affecting Postprocessed DGPS Accuracy

The accuracy that you obtain after data collection depends on several factors, including:

- Number of visible satellites
- Multipath
- Distance between reference station and rover receivers

- Position Dilution of Precision (PDOP)
- Signal-to-noise ratio (SNR)
- Satellite elevations
- Occupation time at a point
- Receiver type at reference station
- Accuracy of the reference station position
- Synchronized measurements are logged at the reference station.
- The logging interval for the roving receiver is the same as, or a multiple of, the logging interval at the reference station.
- The reference station uses the correct antenna.

#### Number of visible satellites

Generally, you need a minimum of four satellites to get a good position. If you have five or more satellites, accuracy increases by a small amount. You can obtain positions from only three satellites by supplying a height value manually. However, Trimble recommends that you do not use this method, as an inaccurate height can significantly reduce horizontal accuracy.

*Note – The TerraSync software always uses a minimum of four satellites. You cannot configure this setting.* 

When the number of visible satellites drops below the required number, the controlling software stops logging positions and displays the message Too few satellites.

#### Multipath

GPS signals are sometimes reflected off nearby objects, particularly metallic objects, creating false or erroneous results. This phenomenon is known as *multipath*. Severe multipath may cause position errors of many meters, while mild multipath may cause small, undetectable errors. For optimal accuracy, collect data in an environment that is free

of large reflective surfaces, such as buildings and trees. EVEREST multipath reduction technology in the receiver helps reduce the effects of multipath.

#### Distance between reference station and rover

When you postprocess GPS Pathfinder Pro XR and Pro XRS data using the GPS Pathfinder Office software Differential Correction utility, the horizontal accuracy of the positions received is 50 cm (RMS) at a 1 km base line (distance from reference station). For the GPS Power receiver, the horizontal accuracy of the positions received is submeter (RMS) at a 1 km base line.

Accuracy degrades by 1 ppm as the distance between the reference station and the rover increases. This means that 1 mm of degradation occurs for every kilometer between the reference station and the rover. For example, you must collect data within 500 km (310 miles) of your reference station to obtain submeter accuracy for the GPS Pathfinder Pro XR and Pro XRS receiver.

#### PDOP

PDOP (Position Dilution of Precision) is a unitless measure of the current satellite geometry. It indicates when the most accurate results are provided. When satellites are spread around the sky, the PDOP value is low, and the computed position is more accurate. When the satellites are grouped closely together, the PDOP value is high, and the computed position is less accurate. The lower the PDOP value, the more accurate the GPS positions.

You can configure the PDOP mask so that if the PDOP exceeds the mask value, the controlling software stops logging positions. A PDOP mask of 6 is required for submeter accuracy.

#### SNR

SNR (signal-to-noise ratio) is a measure of the satellite signal strength relative to the background noise. A strong signal with low noise provides better accuracy. You can raise the SNR mask so that weak signals with an SNR below the mask are excluded from the position computation. In areas of dense canopy, the SNR mask can be lowered so that you can collect GPS positions, although you may not achieve submeter accuracy. For best results, the recommended setting for the SNR mask is 4.

#### **Elevation mask**

When a satellite is low on the horizon, the GPS signals must travel further through the atmosphere, delaying reception by the receiver. To minimize noisy data, adjust the elevation mask. Satellites below the mask are excluded from the position computation. For best results, the recommended setting is  $15^{\circ}$ .

#### **Occupation period**

The GPS Pathfinder Systems receivers achieve the specified horizontal accuracy with a one-second occupation time.

**Note** – To achieve higher levels of accuracy using a GPS Pathfinder Systems receiver, collect carrier-phase data and postprocess using the GPS Pathfinder Office software.

#### **Receiver type**

The following Trimble receiver models use Maxwell<sup>™</sup> technology and, when used as the reference station, yield submeter accuracy with GPS Pathfinder Systems receivers:

- GPS Pathfinder Pro XRS
- GPS Pathfinder Pro XR
- GPS Pathfinder Pro XL

- 5800 GPS receiver
- 5700 GPS receiver
- 4800 GPS receiver
- 4700 GPS receiver
- 4600 LS Surveyor
- 4000 series receiver
- DSM Reference Station



**Warning** – If the GPS receiver at the reference station has fewer than 12 channels, you may be unable to differentially correct some of your data. If the reference station is not capable of logging data from all of the satellites the rover is using, the data collected by the rover cannot be differentially corrected using postprocessing.

#### Accuracy of the reference station position

Any inaccuracy in the reference station position is reflected in your rover position accuracy. For information on the accuracy of your local DGPS reference station coordinates, contact the provider of that service, and check the Integrity Index in the GPS Pathfinder Office version 3.00 Differential Correction utility when selecting a new base station provider.

The Integrity Index provides you with an indication as to the quality of available base data in comparison to other available sources. Poor base data can result from a number of factors, such as an incorrect reference position, bad environmental location, or a large distance between the base and rover receivers. Base data downloaded from each station is analyzed to formulate the quality indicator values and three key measures are taken into account:

- Bias (the measure of distance between an averaged GPS position and a specified reference position)
- Precision (the measure of the spread of actual GPS positions)
- The distance between the base and rover receivers

Use the Integrity Index to avoid selecting base data that may provide an inferior differential correction result. The quality indicator has a range of 0 to 100, where 0 represents low quality base data and 100 represents high quality base data. For more information, refer to the GPS Pathfinder Office 3.00 Differential Correction Help.

#### Synchronized measurements

To obtain optimal accuracy from differential correction, the reference station must record reference data (or output differential corrections) from synchronized measurements. Synchronized measurements occur when the reference station receiver and rover receivers simultaneously make measurements to all the satellites they are tracking.

When you use one of the receivers listed in Receiver type, page 23, as a reference station receiver, the data is always synchronized. When measurements are not synchronized, there is no equivalent reference station position measured at exactly the same time as the rover position. A simultaneous reference station position must be interpolated, which reduces accuracy.

#### Logging intervals

Ideally, the logging interval at the reference station should be the same as the logging interval at the rover. For example, if the reference station is using a 5-second logging interval, the rover logging interval should be 5 seconds. The rover logging interval can also be a direct integer multiple of the interval at the reference station. For example, if the reference station is logging every 5 seconds, the rover can log every 10 seconds.

If the rover logging interval is not synchronized with the reference station, the accuracy of the GPS positions logged by the rover may not be submeter. This is because the reference station measurements must be interpolated to correct the roving receiver's measurements. For more information, see Synchronized measurements, page 25. If the synchronized measurement logging interval at the reference is 1 second, you can use any logging interval at the rover. However, this generates a large file at the reference station. If the computer or data collector at the reference station runs out of space, you cannot differentially correct any rover data collected after the base file ends.

When disk space is at a premium, the best option is a 5-second logging interval for synchronized measurement data at the reference station and a 5-second logging interval for positions at the rover. This is frequent enough to be practical at the rover and uses the default reference station logging interval, which results in base files that are not too large.

Table 3.1 gives examples of various reference station and rover intervals and their effect on accuracy. They are valid for both postprocessed and real-time corrections.

Reference station interval (seconds)	Rover interval (seconds)	Base data interpolated?	Notes
1	1	No	Recommended for best accuracy.
5	5	No	Recommended if reference station disk space is at a premium.
1	3, or 5, or 6, etc.	No	The rover interval is a direct integer multiple of the reference station interval.
5	10	No	The rover interval is a direct integer multiple of the reference station interval.
5	1	Yes	Base data is interpolated at seconds 1, 2, 3, and 4. A slight degradation of accuracy occurs with interpolation. One in five of the rover positions is not interpolated.

#### Table 3.1 Logging Interval Accuracy

### Factors Affecting Real-Time DGPS Accuracy

Real-time DGPS offers similar accuracies to postprocessed GPS. However, in addition to the factors discussed in Factors Affecting Postprocessed DGPS Accuracy, page 20, there are other factors that affect the accuracy of real-time DGPS positions. These factors include:

- Update rate of the corrections
- Corrections based on a different datum

#### Update rate of the corrections

The frequency, or rate, at which the RTCM differential correction messages are output from the reference station affects the accuracy of the GPS positions recorded by the roving receiver. The latency of the corrections (that is, the time it takes for up-to-date information to get from the reference station to the rover) also affects the rover position accuracy.

#### **Datum of corrections**

Errors can occur if the reference stations use a datum other than WGS-84 as the basis for the DGPS corrections. The error introduced by using a reference station that transmits coordinates using a different datum is generally quite small. However, in some places the margin of error can be 5-10 meters. To avoid this type of error, set Trimble controlling software to collect SuperCorrect data. You can then postprocess the real-time DGPS positions if required.

## **Reference Materials**

Reference

Hardware Specifications

If you have a problem and cannot find the information you need in the product documentation, *contact your local Distributor*. Alternatively, go to the Trimble Support page at www.trimble.com/support.html, and then do one of the following:

- Browse the available online support resources.
- Request technical assistance from Trimble Support, click the submit an inquiry link, fill in the form, and then click **Send**.

Trimble: www.trimble.com/support.html Survey Controller: www.trimble.com/tsce.html Survey Pro: www.tdsway.com GIS TSCe: www.trimble.com/gistsce.html ActiveSync<sup>TM</sup>: www.microsoft.com/windowsmobile/ resources/downloads/pocketpc/default.mspx

#### Windows CE: www.microsoft.com/windows/embedded/ce.net

### **Hardware Specifications**

Feature	TSCe
Processor	Intel StrongARM SA-1110, 206 MHz
Memory	64 MB low-power SDRAM
Storage	512 MB non-volatile flash disk
Screen	1/4 VGA transflective color LCD
Touch Screen	Passive - 87% transmissivity
Keyboard	57 key tactile action
9-Pin serial port	RS232 COM1
26-Pin MultiPort	RS232 COM2, Ethernet 10BaseT, USB client, power in/out and audio in/out
Infrared	IrDA Type1 COM3
Audio	Integrated speaker and microphone
Batteries	NiMH rechargeable pack, 3800 mAH, 18.5 W-h, 4.8 V
AC Adaptor	Line voltage: 100 - 240 V AC 47-63 Hz

# IMPULSE 200 LR LASER

Our Impulse lasers are specifically designed for optimal performance under whatever conditions you might encounter in the field. They are lightweight, extremely rugged, completely waterproof and versatile. Use them as a handheld unit or mount them on a tripod for added stability.

#### Hardware Specifications:

Typical Target	IMPULSE	200 LR	
Accuracy & Range	(Imperial)	(Metric)	
Accuracy (Typical)	0.1 - 0.2 ft	3 - 5 cm	
Accuracy (Max)	0.5 ft	15 cm	
Overhead cable / Stake	330 ft	100 m	
Phone pole / Stockpile	655 ft	200 m	
Tree / Tower	985 ft	300 m	
Rock Face / Building	1640 ft	500 m	
Max Distance	1885 ft	575 m	
Range Resolution	.01 ft	0.01 m	
Inclination Limits	+/- 90 deg	+/- 90 deg	
Inclination Accuracy	+/- 0.1 deg	+/- 0.1 deg	
Weight	2.2 lbs.	1 kg	
Size	6 x 2.5 x 5 in.	15.2 x 6.4 x 12.7 cm	
Power Supply	(2) AA batteries (20 hours of use)		
Environment	Waterproof to IP 67 a	nd NEMA 6	
Temperature	- 22 to + 140 F	-30 to + 60 C	

(Max distances are approximate)

#### **Key Features:**

- Custom backlit LCD display
- Audible and visual indicators
- RS232 serial output for electronic data storage
- Selective range gating for positive target acquisition
- Built-in tilt sensor
- Filter system to discriminate reflective targets
- Cumulative distance capability
- Determines the distance between two in-line objects
- Integrates with GPS



### Package Includes:

- Impulse laser
- Red-dot scope
- Hand strap
- Tripod / monopod mounting bracket
- (2) AA batteries
- Operator's manual
- Padded carrying case

#### **Optional Accessories:**

- 1.5 to 4 X zoom scope
- Yoke and staff
- Remote trigger data cable

Impulse Laser w/ 1.5 to 4 X Zoom Scope and Mounting Bracket





For 3-D data collection, integrate the Impulse with a MapStar System.







7070 S. Tucson Way, Centennial, CO 80112 USA\* All specifications are subjectToll Free: 1 (800) 280-6113 | Local: 1 (303) 649-1000to change without notice.Web Page: www.lasertech.comE-mail: info@lasertech.com(Rev. 11/15/03)

Dimensions	5" x 2" x 3.5" (12cm x 5cm x 9cm)
Weight	8 ounces (220 g)
Data Communication	Serial, via wired RS232 (standard)
Power	3.0 volts DC nominal
Battery Type	(2) AA or (1) CRV3
Battery Duration	AA: Approximately 7,500 measurements CRV3: Approximately 15,000 measurements
Eye Safety	FDA Class 1 (CFR 21)
Environmental	Impact, Water & Dust Resistant. NEMA 3, IP 64
Temperature	$-4^{\circ}F$ to $+140^{\circ}F$ ( $-20^{\circ}C$ to $+60^{\circ}C$ )
Optics	7X Magnification (Field-of-view; 330 ft @ 1000 yards)
Display	In-scope LCD
Units	Feet, Yards, Meters, and Degrees
Monopod/tripod mount	<sup>1</sup> / <sub>4</sub> " - 20 female thread
Measurement Range	
Distance	0 to 3280 ft (1000 m) typical, 6560 ft (2000m) max to reflective target
Inclination	± 90 degrees
Accuracy	
Distance	$\pm 1$ ft ( $\pm 30$ cm) to high quality targets, $\pm 1$ yd ( $\pm 1$ m) to low quality targets
Inclination	±0.25 degrees
Measurement Modes	Horizontal Distance, Vertical Distance, Slope Distance and Inclination, and 3-point flexible height routine with auto sequencing
Target Modes	Standard, Closest, Farthest, Continuous, and Filter (requires reflector and foliage filter)



### MVP200 OPERATION AND MAINTENANCE MANUAL



BROOKE OCEAN TECHNOLOGY LIMITED 50 Thomhill Drive Dartmouth, Nova Scotia Canada B3B 1S1

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[OM-0449-04-010]

December 15, 2004

#### 1 SYSTEM DESCRIPTION

The MVP200 system is a self-contained profiling system capable of sampling water column profiles to 200m depth from a vessel moving at up to 12 knots, and deeper depths at slower speeds. The system provides vertical profiles of oceanographic data such as Sound Velocity, CTD, particle counts, etc. for various operations including the calibration of multi-beam sounder systems for hydrographic operations. The MVP200 is completely autonomous and can be controlled by computer without the requirement for personnel on deck. The system consists of a single or multi-sensor free-fall fish (fish), an integrated winch and hydraulic power unit, towing boom and a remotely located user interface controller. The MVP200 system is shown in Figure 1. The system block diagram is shown in Figure 2.



Figure 1: MVP200



Figure 2: System Block Diagram

Upon actuation, the system deploys the fish from a towed position by setting the winch in 'freewheel' mode and releasing the brake. This allows the fish to free-fall almost straight down through the water at its terminal velocity of approximately 3 m/s. Once the (pre-set) depth limit is reached, the brake is applied to stop the cable pay-out. When the winch drum has stopped, the motor is engaged to haul in the cable until the fish is towed at the surface. Subsequent deployments occur from this position, either actuated by the operator or timed automatically with the automatic deployment setting.

The system operates in the automatic mode described above or in manual mode operated from controls at the winch. Manual mode is used as a convenient method to launch and recover the fish, but is not intended for moving vessel profiling.

#### 1.1 FREE-FALL FISH

The free-fall fish can be either a single sensor or a multi sensor fish. The fish houses the main instrument, either a CTD or SV&P sensor. The instrument is normally configured for RS-485 serial communications.

The multi-sensor fish can support auxiliary sensors in addition to the main CTD/SV&P instrument. If auxiliary sensors are used, a DTM/Mux is required in the fish. The DTM/Mux is a data telemetry module with additional digitization and multiplexing circuitry. This allows data from various analog and digital sensors to be added to the main instrument's serial output stream, which is transmitted to the surface.

#### 1.1.1 Single-Sensor Free-Fall Fish

The Single Sensor Free-Fall Fish (SSFFF) (see Figure 3) is machined from brass with a stainless steel towing bridle. The sensor guard at the tail of the fish is made from stainless steel. The shape of the fish allows minimal resistance while providing stability during free-fall and retrieval. The fish can be fitted with an Applied Microsystems Ltd. (AML) Sound Velocity and Pressure (SV&P) Smart Sensor or an AML CTD Micro Sensor. (A small plastic support is built into the sensor guard for use with the sound velocity sensor). An Impulse underwater connector allows the fish to be removed easily from the electromechanical cable.

The AML CTD Micro Sensor measures conductivity, temperature and pressure. The AML SV&P Smart Sensor measures sound velocity and pressure. The information is sent through the Electro-Mechanical cable to the main control box, through the deck cable to the Instrument Interface box where it then connects to the MVP Controller. If the sensor is a CTD, software in MVP Controller then computes sound velocity and salinity from the measured parameters using the UNESCO equations of state.



Figure 3: Single Sensor Free-Fall Fish

#### **3 SPECIFICATIONS**

#### 3.1 OPERATING DEPTH

- 600 m @ 0 knots\*
- 350 m @ 5 knots
- 200 m @ 12 knots

#### \* Ensure sensor(s) are rated for this depth before operations

#### 3.2 WINCH AND HYDRAULIC POWER UNIT

- Drum dimensions: 324 mm (12.7") barrel diameter 99 mm (3.9") wide 711 mm (28.0") flange OD
- Line Pull: Bare Drum 410 kg (900 lbs.)
- Capacity: 660 m (2132 ft) of 6.0 mm (0.24") cable
- Cable: Jacketed Electro-Mechanical, 4 conductor, 1089 kg (2400 lbs.) maximum break strength
- Hydraulic Winch Motor: Valmet Black Bruin # 403 040 2120
- Rotator Motor: White # 700540C8540ALAAA
- Slip Ring: Focal Technologies Model 180 ESR
- Hydraulic Pump: Rexroth #AA10VG18EP21/10R-NSC66-F004S
- Reservoir: 40 litre Stainless Steel Reservoir
- Maximum operating pressure: 3000 psi (207 Bar)
- Electric motor: 15 hp TEFC 230/460VAC 60 Hz, 208/416VAC 50 Hz, 3-phase
- Suction line filter: LHA Element #SPE-15-BTA-10
- Footprint: 1.22m x 0.71m (48" x 28") excluding boom
- Height: 3.18m (125")
- Approximate Weight: 680 kg (1500 lbs.)

#### 3.3 FREE-FALL FISH

#### 3.3.1 Single Sensor Free-Fall Fish

- Weight: 32 kg (72 lbs.) with sensor, in air
- Body Length: 673 mm (26.5") excluding bridle
- Body Diameter: 114 mm (4.5")
- Sensors: AML Sound Velocity and Pressure (SV&P) "Smart Sensor", or
  - AML SVP&T Micro Sensor
    - AML CTD Micro Sensor

#### 3.3.2 Multi-Sensor Free-Fall Fish

- Weight: 88.5 kg (195 lbs.) with sensor, in air
- Body Length: 1041 mm (41") excluding bridle
- Body Section: 147 mm x 279 mm (5.8" x 11.0")

Sensors:

- AML Sound Velocity and pressure (SV&P) "Smart Sensor"
  - AML CTD Micro Sensor
  - AML Dissolved Oxygen (DO) Sensor
  - Wet Labs fluorometers (Wet star, FLF300, and ECO)
  - Satlantic OCR-500 series digital optical sensors
  - Brooke Ocean Technology Ltd. Laser Optical Plankton Counter (LOPC)

#### 3.4 MVP CONTROLLER

#### Minimum requirements (refer to system factory configuration for details)

- Windows 2000 Professional Operating system:
- Processor: Pentium 600 or higher
- Ram: 128 Mb
- Hard Disk: 5 GB Hard drive
- Video: 1024x768 SVGA with 64 thousand colors
- Pointing Device: Microsoft Wheel Mouse
- Serial ports: 4 serial (RS232) ports
- Drive: CD-ROM drive and a 1.44 Mb Floppy drive
- Monitor: 15" Video Monitor
- Keyboard: PS/2 Keyboard
- Hardware: Network Card

#### 3.5 POWER REQUIREMENTS

#### Winch Power Ratings:

- Vessel circuit breaker value 90A at 230v and 45A at 460v, maximum setting
- Voltage: 3-phase, 4-wire
  - 230/460V ±10%, 34/17A at 60 Hz or
  - 208/416V ±10%, 42/21A at 50 Hz

(Note that system supply voltage must be selected at time of order. It is not a field configurable item)

- 50A main disconnect, circuit breaker
- 15 HP Motor, dual frequency rating with 110V anti-condensation heater
- Motor contactor with thermal overload.
- Includes internal 110V auxiliary distribution: 7A/120V/840W

#### MVP Controller (Lab Computer) Power Ratings:

- Voltage: 1-phase, 100-230 VAC
- Current: 5-8A
- Frequency: 50 or 60 Hz

The SBE 45 MicroTSG Thermosalinograph is an externally powered, high-accuracy instrument, designed for shipboard determination of sea surface (pumped-water) conductivity and temperature. Salinity and sound velocity can also be computed. The MicroTSG is constructed of plastic and titanium to ensure long life with minimum maintenance.

#### **OPERATION OVERVIEW**

Communication with the MicroTSG is over an internal, 3-wire, RS-232C link, providing real-time data transmission. Commands can be sent to the MicroTSG to provide status display, data acquisition setup, data display and capture, and diagnostic tests. User-selectable operating modes include:

- Polled sampling On command, the MicroTSG takes one sample and sends the data to the computer.
- Autonomous sampling At pre-programmed intervals, the MicroTSG samples and sends the data to the computer. The MicroTSG does not enter quiescent (sleep) state between samples.
- Serial Line Sync A pulse on the serial line causes the MicroTSG to wake up, sample, and enter quiescent state automatically.



Calibration coefficients stored in EEPROM allow the MicroTSG to transmit data in engineering units.

#### SENSORS

The MicroTSG retains the temperature and conductivity sensors used in the SBE 21 Thermosalinograph, but has improved acquisition electronics that increase accuracy and resolution, and lower power consumption. The MicroTSG's aged and pressure-protected thermistor has a long history of exceptional accuracy and stability (typical drift is less than 0.002 °C per year). Electrical isolation of the conductivity electronics eliminates any possibility of ground-loop noise.

The MicroTSG's internal-field conductivity cell is unaffected by external fouling, and uses expendable anti-foulant devices.

#### OPTIONAL PN90402 - SBE 45 POWER, NAVIGATION, and REMOTE TEMPERATURE INTERFACE BOX

An optional AC- or DC-powered Interface Box:

- Provides isolated DC power and an optically isolated RS-232 data interface.
- Contains a NMEA 0183 port for appending navigation information from a NMEA navigation device to the data stream.
- Contains an RS-232 port for appending the output of an optional remote temperature sensor (SBE 38), allowing for measurement of sea surface temperature with minimal thermal contamination from the ship's hull.
- Outputs the data stream (MicroTSG, NMEA navigation device, and SBE 38 data) to the computer over an RS-232 interface.

#### SOFTWARE

The MicroTSG is supplied with a powerful Win 95/98/NT/2000/XP software package, SEASOFT<sup>©</sup>-Win32. SEASOFT's modular programs include:

- SEATERM terminal program for instrument setup and data display. .
- SEASAVE real-time data acquisition and display
- SBE Data Processing filtering, aligning, averaging, and plotting of data and derived variables.



## MicroTSG (Thermosalinograph)

### **SBE 45**



\* For specifications for optional SBE 38 remote temperature sensor, see SBE 38 datasheet.

#### System Schematic: SBE 45 with Optional PN 90402 Interface Box and Remote Temperature Sensor





Sea-Bird Electronics, Inc. 1808 136th Place NE, Bellevue, Washington 98005 USA Website: http://www.seabird.com E-mail: seabird@seabird.com Telephone: (425) 643-9866 Fax: (425) 643-9954

## SBE 19plus SEACAT PROFILER

Conductivity, Temperature, and Pressure Recorder with RS-232 Interface



## Serial Number: 19P36026-4585

Sea-Bird Electronics, Inc. 1808 136<sup>th</sup> Place NE Bellevue, Washington 98005 USA Tel: 425/643-9866 Fax:425/643-9954

#### LIMITED LIABILITY STATEMENT

Extreme care should be exercised when using or servicing this equipment. It should be used or serviced only by personnel with knowledge of and training in the use and maintenance of oceanographic electronic equipment.

SEA-BIRD ELECTRONICS, INC. disclaims all product liability risks arising from the use or servicing of this system. SEA-BIRD ELECTRONICS, INC. has no way of controlling the use of this equipment or of choosing the personnel to operate it, and therefore cannot take steps to comply with laws pertaining to product liability, including laws which impose a duty to warn the user of any dangers involved in operating this equipment. Therefore, acceptance of this system by the customer shall be conclusively deemed to include a covenant by the customer to defend, indemnify, and hold SEA-BIRD ELECTRONICS, INC. harmless from all product liability claims arising from the use of servicing of this system.

## WARNING !!

Do not submerge this instrument (S/N 19P36026-4585) beyond the depth rating of the lowest rated component listed below!

Main Housing (Titanium)

7000 meters

Pressure Sensor (3500 dBar) Druck

Pump (SBE 5M)

**3500 meters** 10500 meters

3

## SYSTEM CONFIGURATION

14 June 2004

Model SBE 19plus Instrument Type Firmware Version Communications Memory Housing 0 Conductivity Raw Frequency Pressure Sensor Number of Voltages Sampled: S/N 19P36026-4585 SBE 19plus SeaCaT Profiler 1.4D 9600 baud, 8 data bits, no parity, one stop bit 8192K 7000 meter (3AL-4V Titanium) 2630.97 Hz Strain Gauge: 3500 dBar, S/N 5433

Serial RS-232C Sensor

Data Format: Count Frequency Count None

0

Temperature Conductivity Pressure, Strain gauge

Pump (SBE 5M)

050647

Voltage Delay Setting (standard)

(standard) 0 seconds

#### **IMPORTANT SOFTWARE & HARDWARE CONFIGURATION INFORMATION**

Sea-Bird supplies two versions of our software package for communication, real-time data acquisition, and data analysis and display:

• SEASOFT-Win32 - Windows software for PC running Win 95/98/NT/2000/XP

• SEASOFT-DOS - DOS software for IBM-PC/AT/386/486 or compatible computer with a hard drive Detailed information on the use of the **Windows** software follows:

#### SEASOFT-Win32

SEASOFT-Win32 software was supplied on a CD-ROM with your CTD. This software package is designed to run on a PC running Win 95/98/NT/2000/XP. The CD-ROM also contains software manuals that describe the appropriate applications for the various programs, the procedure for installing the software, and instructions on using the programs. There are three primary programs used with the CTD for setup, data collection and retrieval, data display, and data processing:

- SEATERM terminal program for setup of the CTD and uploading of data from the CTD memory (Note: If using the CTD with the 90208 Auto Fire Module or SBE 17*plus* V2 SEARAM, use SeatermAF instead of SEATERM)
- SEASAVE real-time data acquisition program
- SBE Data Processing data processing program

Instructions for using the software are found in their Help files.

To communicate with the CTD to set it up or to upload data from the CTD memory to the computer hard drive, **SEATERM** must have information about the CTD hardware configuration (communication parameters, internal firmware, etc.) and about the computer. To communicate with the CTD, double click on Seaterm.exe: 1. In the Configure menu, select the CTD. The Configuration Options dialog box appears.

- A. On the COM Settings tab, select the firmware version (if applicable), baud rate, data bits, and parity to match the CTD's configuration sheet. If necessary, change the com port to match the computer you are using.
  - B. On the Upload Settings tab, enter upload type (all as a single file, etc.) as desired.
    For the SBE 17 and 25 only: enter the serial number for the SBE 3 (temperature) and SBE 4 (conductivity) modular sensors, exactly as they appear in the configuration (.con) file.
- C. On the Header Information tab, change the settings as desired.
- Click OK when done. SEATERM saves the settings in a SEATERM.ini file.
- 2. On the Toolbar, click Connect to communicate with the CTD.
- 3. To set up the CTD prior to deployment: On the Toolbar, click Status. SEATERM sends the Status command and displays the response. Verify that the CTD setup matches your desired deployment. If not, send commands to modify the setup.
- 4. To upload data from the CTD: On the Toolbar, click Upload to upload data from the CTD memory to the computer.

Sea-Bird CTDs store and/or transmit data from their primary and auxiliary sensors in the form of binary or hexadecimal number equivalents of the sensors' frequency or voltage outputs. This is referred to as the *raw* data. The calculations required to convert from *raw* data to *engineering* units of the measured parameters (temperature, conductivity, pressure, dissolved oxygen, pH, etc.) are performed using the software, either in real time, or after the data has been stored in a file. SEASAVE creates the file in real time. As noted above, SEATERM uploads the recorded data and creates the file on the computer hard drive.

To successfully store data to a file on the computer and subsequently convert it to engineering units, the software must know the CTD type, CTD configuration, and calibration coefficients for the sensors installed on the CTD. This information is unique to each CTD, and is contained in a *configuration* file. The configuration file, which has a .con extension, was written onto a floppy disk and the CD-ROM shipped with the CTD. The .con file for a given CTD is named with the last four digits of the serial number for that CTD (e.g., 1234.con). The configuration file is created or modified (e.g., changing coefficients after recalibration, or adding another sensor) by using the Configure menu in **SEASAVE** or

**SBE Data Processing**. The configuration file is used by SEASAVE to convert raw data to engineering units when it acquires, stores, and displays real-time data. The configuration file is also used by some modules in SBE Data Processing (Data Conversion and Derive) that convert raw data to engineering units during data processing.

The instrument type and instrument configuration settings of the .con file and the required setup for the SEATERM.ini file for the CTD *as delivered* are documented below. The calibration coefficients for the CTD's sensors are contained in the calibration coefficient section of the CTD manual.

#### NOTE:

SEATERM will not upload data correctly without a properly configured SEATERM.ini file. SEASAVE and SBE Data Processing will not interpret the data correctly without the correct .con file.

#### **SEASOFT CONFIGURATION:**

The correct instrument type for your instrument is SBE 19plus SEACAT Profiler. The correct settings for the configuration of your instrument as delivered are documented below:

Configuration for the	SBE 19 Seacat plus CTD	×
ASCII file opened: Nor	ne	
Pressure sensor type	Strain Gauge	]
External voltage chann	nels 0 💌	
Mode	Profile	
Sample interval secon	ds 10	
Scans to average	1	
🗖 Surface PAR volta	ge added	
NMEA position dat	a added	
Channel	Sensor	New
1. Count	Temperature	
2. Frequency	Conductivity	
3. Count	Pressure, Strain Gauge	Save
		Save As
	-	Select
		Modify
Report Help	Exit	Cancel

# **SPECIFICATIONS**

1

3

SBE 19plus Specifications	
SBE 5M Pump	

## **SEACAT** Profiler

# SBE 19plus

The SBE 19*plus* is the next generation *Personal CTD*, bringing numerous improvements in accuracy, resolution (in fresh as well as salt water), reliability, and ease-of-use to the wide range of research, monitoring, and engineering applications pioneered by its legendary SEACAT predecessor. The 19*plus* samples faster (4 Hz vs 2), is more accurate (0.005 vs 0.01 in T, 0.0005 vs 0.001 in C, and 0.1% vs 0.25% — with *seven* times the resolution — in D), and has more memory (8 Mbyte vs 1). There is more power for auxiliary sensors (500 ma vs 50), and they are acquired at higher resolution (14 bit vs 12). Cabling is simpler and more reliable because there are four differential auxiliary inputs on two separate connectors, and a dedicated connector for the pump. All exposed metal parts are titanium, instead of aluminum, for long life and minimum maintenance.

The 19*plus* can be operated without a computer from even the smallest boat, with data recorded in non-volatile FLASH memory and processed later on your PC. Simultaneous with recording, real-time data can be transmitted over single-core, armored cable directly to your PC's serial port (maximum transmission distance dependent on number of auxiliary sensors, baud rate, and cable properties). The 19*plus'* faster sampling and pump-controlled TC-ducted flow configuration significantly reduces salinity spiking caused by ship heave, and allows slower descent rates for improved resolution of water column features. Auxiliary sensors for dissolved oxygen, pH, turbidity, fluorescense, PAR, and ORP can be added, and for moored deployments the 19*plus* can be set to *time-series* mode using software commands. External power and two-way real-time communication over 10,000 meters of cable can be provided with the SBE 36 CTD Deck Unit and Power and Data Interface Module (PDIM).

The 19*plus* uses the same temperature and conductivity sensors proven in 5000 SEACAT and MicroCAT instruments, and a superior new micro-machined silicon strain gauge pressure sensor developed by Druck, Inc. Improvements in design, materials, and signal acquisition techniques yield a low-cost instrument with superior performance that is also easy to use. Calibration coefficients, obtained in our computer-controlled high-accuracy calibration baths, are stored in EEPROM memory. They permit data output in ASCII engineering units (degrees C, Siemens/m, decibars, Salinity [PSU], sound velocity [m/sec], etc.). The 19*plus* can be factory-configured to emulate the .hex output format and 2 Hz data rate of old SEACATs for compatibility with existing software or instrument fleets.

Accuracy, convenience, portability, software, and support; compelling reasons why the 19plus is today's best low-cost CTD.

#### **CONFIGURATION AND OPTIONS**

A standard SBE 19plus is supplied with:

- · Plastic housing for depths to 600 meters
- Strain-gauge pressure sensor
- 8 Mbyte FLASH RAM memory
- 9 D-size alkaline batteries
- Impulse glass-reinforced epoxy bulkhead connectors: 4-pin I/O, 2-pin pump, and two 6-pin (two differential auxiliary A/D inputs each)
- SBE 5M miniature pump and T-C Duct

Options include:

- Titanium housing for depths to 7000 meters
- Sensors for oxygen, pH, fluorescence, light (PAR), light transmission, and turbidity
- SBE 5T pump in place of SBE 5M for use with dissolved oxygen and/or other pumped sensors
- Stainless steel cage
- MCBH Micro connectors
- · Ni-Cad batteries and charger

#### SOFTWARE

SEASOFT<sup>®</sup>-Win32, our complete Windows 95/98/NT/2000/XP software package, is included at no extra charge. Its modular programs include:

- SEATERM<sup>®</sup> communication and data retrieval
- SEASAVE<sup>®</sup> real-time data acquisition and display
- SBE Data Processing<sup>®</sup> filtering, aligning, averaging, and plotting of CTD and auxiliary sensor data and derived variables



#### Sea-Bird Electronics, Inc.

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1808 136th Place NE, Bellevue, Washington 98005 USA Website: http://www.seabird.com

Email: seabird@seabird.com Telephone: (425) 643-9866 Fax: (425) 643-9954 The SBE 5M pump module consists of a centrifugal pump head and a long-life, DC ball bearing motor contained in a compact, titanium, pressure housing usable to 10,500 meters deep. The pump impeller and electric drive motor are coupled magnetically through the housing, providing high reliability by eliminating moving seals. Motor speed and pumping rate remain constant over the entire input voltage range. The motor drive electronics is intrinsically protected against accidental reversed polarity.

#### APPLICATIONS

The SBE 5M is standard on the SBE 19 and 19*plus* SEACAT Profiler CTD. It is optional on the SBE 16, 16*plus*, and 16*plus*-IM SEACAT C-T Recorder. The pump flushes water through the conductivity cell at a constant rate, independent of the CTD's motion, improving dynamic performance. For applications requiring pumping through additional sensors (for example, a dissolved oxygen sensor), use the SBE 5T pump instead.

Specify:

- Option 5M-1 for profiling (continuous duty) applications such as the SBE 19*plus*.
- Option 5M-2 for moored (pulsed duty) applications such as the SBE 16*plus* or 16*plus*-IM.

Contact Sea-Bird for use in other applications.

#### SPECIFICATIONS

Option 5M-1 (continuous duty): Input voltage range 9 - 18 VDC

Flow Rate 25 ml/s supply current 95 ma

Note: Supply current is independent of operating voltage.

#### Option 5M-2 (pulsed duty): Input voltage range 6 - 18 VDC

Pulse Duration	Flow Volume	Electrical Charge
0.5 seconds	15 ml	0.148 amp-seconds
1.0 seconds	21 ml	0.283 amp-seconds
1.5 seconds	31 ml	0.418 amp-seconds
2.0 seconds	40 ml	0.553 amp-seconds

#### Weight

In Air:	0.42 k
In Water:	0.28 k

).42 kg (0.91 lbs) ).28 kg (0.60 lbs)





SBE 5M



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#### FAX: (425) 643-9954

Tel: (425) 643-9866 Email: seabird@seabird.com

#### SBE 5M MINI SUBMERSIBLE PUMP CONFIGURATION SHEET

Serial Number:	0647
Job Number:	36026
Customer:	NOAA/PMC
Delivery Date:	6/14/2004

Single Connector Housing with Titanium screws

Pressure Case: 10,500 meters (titanium)

Maxon Motor Type:

P/N 90337, Motor PN 20130 (Low power 6 VDC, 2000 RPM MAX)	]
P/N 90335, Motor PN 20130 (Low power 9 VDC, 2000 RPM MAX)	•

Vin 15V voltage across C2:	8.015	VDC	Current	7.73	mΑ
Vin 9V voltage across C2:	8.014	VDC	Current	7.4	mA
Vin 6V voltage across C2:	5.888	VDC	Current	7.61	mA

Pump submerged test, no load, Vin 12VDC Average current draw in water: 121 mA

## SBE 19plus SEACAT PROFILER

Conductivity, Temperature, and Pressure Recorder with RS-232 Interface



## Serial Number: 19P36026-4616 and -4617

Sea-Bird Electronics, Inc. 1808 136<sup>th</sup> Place NE Bellevue, Washington 98005 USA Tel: 425/643-9866 Fax:425/643-9954

## WARNING !!

## Do not submerge this instrument (S/N 19P36026-4616) beyond the depth rating of the lowest rated component listed below!

600 meters

Pressure Sensor (1000 dBar) Druck

Pump (SBE 5M)

1000 meters

10500 meters

## WARNING !!

## Do not submerge this instrument (S/N 19P36026-4617) beyond the depth rating of the lowest rated component listed below!

Main Housing (Plastic)	<i>l</i> lain I	Housina	(Plastic)	
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#### 600 meters

Pressure Sensor (1000 dBar) Druck

Pump (SBE 5M)

1000 meters

10500 meters

## SYSTEM CONFIGURATION

14 June 2004

Model SBE 19plus Instrument Type Firmware Version Communications Memory Housing 0 Conductivity Raw Frequency Pressure Sensor S/N 19P36026-4616 SBE 19plus SeaCaT Profiler 1.4D 9600 baud, 8 data bits, no parity, one stop bit 8192K 600 meter (Celcon plastic) 2686.52 Hz Strain Gauge: 1000 dBar, S/N 5512

Number of Voltages Sampled:

Serial RS-232C Sensor

Data Format: Count Frequency Count 0

None

Temperature Conductivity Pressure, Strain gauge

Pump (SBE 5M)

050651

Voltage Delay Setting (standard)

(standard) 0 seconds

## SYSTEM CONFIGURATION

14 June 2004

Model SBE 19plus Instrument Type Firmware Version Communications Memory Housing 0 Conductivity Raw Frequency Pressure Sensor S/N 19P36026-4617 SBE 19plus SeaCaT Profiler 1.4D 9600 baud, 8 data bits, no parity, one stop bit 8192K 600 meter (Celcon plastic) 2801.47 Hz Strain Gauge: 1000 dBar, S/N 5513

Number of Voltages Sampled:

Serial RS-232C Sensor

Data Format: Count Frequency Count 0

None

Temperature Conductivity Pressure, Strain gauge

Pump (SBE 5M)

050649

Voltage Delay Setting (standard)

(standard) 0 seconds


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Tel: (425) 643-9866 Email: seabird@seabird.com

## SBE 5M MINI SUBMERSIBLE PUMP CONFIGURATION SHEET for 4616

Serial Number:	0651
Job Number:	36026
Customer:	NOAA/PMC
Delivery Date:	6/14/2004

Single Connector Housing with Titanium screws

Pressure Case: 10,500 meters (titanium)

Maxon Motor Type:

P/N 90337, Motor PN 20130 (Low power 6 VDC, 2000 RPM MAX)	

P/N 90335, Motor PN 20130 (Low power 9 VDC, 2000 RPM MAX)

Vin 15V voltage across C2:	7 947	VDC	Current	<b>11.8</b> mA
Vin 9V voltage across C2:	7.948	VDC	Current	11.0 mA

Vin 6V voltage across C2: 5.868 VDC Current 10.2 mA

Pump submerged test, no load, Vin 12VDC Average current draw in water: 124 mA

✓



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Tel: (425) 643-9866 Email: seabird@seabird.com

## SBE 5M MINI SUBMERSIBLE PUMP CONFIGURATION SHEET for 4617

Serial Number:	0649
Job Number:	36026
Customer:	NOAA/PMC
Delivery Date:	6/14/2004

Single Connector Housing with Titanium screws

Pressure Case: 10,500 meters (titanium)

Maxon Motor Type:

P/N 90337, Motor PN 20130 (Low power 6 VDC, 2000 RPM MAX)	
P/N 90335, Motor PN 20130 (Low power 9 VDC, 2000 RPM MAX)	$\checkmark$

Vin 15V voltage across C2:	7.947	VDC	Current	<b>11.8</b> mA
Vin 9V voltage across C2:	7.948	VDC	Current	<b>11.0</b> mA
Vin 6V voltage across C2:	5.868	VDC	Current	<b>10.2</b> mA

Pump submerged test, no load, Vin 12VDC Average current draw in water: 124 mA

#### **IMPORTANT SOFTWARE & HARDWARE CONFIGURATION INFORMATION**

Sea-Bird supplies two versions of our software package for communication, real-time data acquisition, and data analysis and display:

• SEASOFT-Win32 - Windows software for PC running Win 95/98/NT/2000/XP

• SEASOFT-DOS - DOS software for IBM-PC/AT/386/486 or compatible computer with a hard drive Detailed information on the use of the **Windows** software follows:

#### SEASOFT-Win32

SEASOFT-Win32 software was supplied on a CD-ROM with your CTD. This software package is designed to run on a PC running Win 95/98/NT/2000/XP. The CD-ROM also contains software manuals that describe the appropriate applications for the various programs, the procedure for installing the software, and instructions on using the programs. There are three primary programs used with the CTD for setup, data collection and retrieval, data display, and data processing:

- SEATERM terminal program for setup of the CTD and uploading of data from the CTD memory (Note: If using the CTD with the 90208 Auto Fire Module or SBE 17*plus* V2 SEARAM, use SeatermAF instead of SEATERM)
- SEASAVE real-time data acquisition program
- SBE Data Processing data processing program

Instructions for using the software are found in their Help files.

To communicate with the CTD to set it up or to upload data from the CTD memory to the computer hard drive, **SEATERM** must have information about the CTD hardware configuration (communication parameters, internal firmware, etc.) and about the computer. To communicate with the CTD, double click on Seaterm.exe: 1. In the Configure menu, select the CTD. The Configuration Options dialog box appears.

- A. On the COM Settings tab, select the firmware version (if applicable), baud rate, data bits, and parity to match the CTD's configuration sheet. If necessary, change the com port to match the computer you are using.
  - B. On the Upload Settings tab, enter upload type (all as a single file, etc.) as desired.
     For the SBE 17 and 25 only: enter the serial number for the SBE 3 (temperature) and SBE 4 (conductivity) modular sensors, exactly as they appear in the configuration (.con) file.
- C. On the Header Information tab, change the settings as desired.
- Click OK when done. SEATERM saves the settings in a SEATERM.ini file.
- 2. On the Toolbar, click Connect to communicate with the CTD.
- 3. To set up the CTD prior to deployment: On the Toolbar, click Status. SEATERM sends the Status command and displays the response. Verify that the CTD setup matches your desired deployment. If not, send commands to modify the setup.
- 4. To upload data from the CTD: On the Toolbar, click Upload to upload data from the CTD memory to the computer.

Sea-Bird CTDs store and/or transmit data from their primary and auxiliary sensors in the form of binary or hexadecimal number equivalents of the sensors' frequency or voltage outputs. This is referred to as the *raw* data. The calculations required to convert from *raw* data to *engineering* units of the measured parameters (temperature, conductivity, pressure, dissolved oxygen, pH, etc.) are performed using the software, either in real time, or after the data has been stored in a file. SEASAVE creates the file in real time. As noted above, SEATERM uploads the recorded data and creates the file on the computer hard drive.

To successfully store data to a file on the computer and subsequently convert it to engineering units, the software must know the CTD type, CTD configuration, and calibration coefficients for the sensors installed on the CTD. This information is unique to each CTD, and is contained in a *configuration* file. The configuration file, which has a .con extension, was written onto a floppy disk and the CD-ROM shipped with the CTD. The .con file for a given CTD is named with the last four digits of the serial number for that CTD (e.g., 1234.con). The configuration file is created or modified (e.g., changing coefficients after recalibration, or adding another sensor) by using the Configure menu in **SEASAVE** or

**SBE Data Processing**. The configuration file is used by SEASAVE to convert raw data to engineering units when it acquires, stores, and displays real-time data. The configuration file is also used by some modules in SBE Data Processing (Data Conversion and Derive) that convert raw data to engineering units during data processing.

The instrument type and instrument configuration settings of the .con file and the required setup for the SEATERM.ini file for the CTD *as delivered* are documented below. The calibration coefficients for the CTD's sensors are contained in the calibration coefficient section of the CTD manual.

#### NOTE:

SEATERM will not upload data correctly without a properly configured SEATERM.ini file. SEASAVE and SBE Data Processing will not interpret the data correctly without the correct .con file.

#### **SEASOFT CONFIGURATION:**

The correct instrument type for your instrument is SBE 19plus SEACAT Profiler. The correct settings for the configuration of your instrument as delivered are documented below:

Configuration for the	SBE 19 Seacat plus CTD	×
ASCII file opened: Nor	ne	
Pressure sensor type	Strain Gauge	]
External voltage chann	nels 0 💌	
Mode	Profile	
Sample interval secon	ds 10	
Scans to average	1	
🗖 Surface PAR volta	ge added	
NMEA position dat	a added	
Channel	Sensor	New
1. Count	Temperature	
2. Frequency	Conductivity	
3. Count	Pressure, Strain Gauge	Save
		Save As
	-	Select
		Modify
Report Help	Exit	Cancel

# **SPECIFICATIONS**

1

SBE 19plus Specifications	
SBE 5M Pump	

# **SEACAT** Profiler

# SBE 19plus

The SBE 19*plus* is the next generation *Personal CTD*, bringing numerous improvements in accuracy, resolution (in fresh as well as salt water), reliability, and ease-of-use to the wide range of research, monitoring, and engineering applications pioneered by its legendary SEACAT predecessor. The 19*plus* samples faster (4 Hz vs 2), is more accurate (0.005 vs 0.01 in T, 0.0005 vs 0.001 in C, and 0.1% vs 0.25% — with *seven* times the resolution — in D), and has more memory (8 Mbyte vs 1). There is more power for auxiliary sensors (500 ma vs 50), and they are acquired at higher resolution (14 bit vs 12). Cabling is simpler and more reliable because there are four differential auxiliary inputs on two separate connectors, and a dedicated connector for the pump. All exposed metal parts are titanium, instead of aluminum, for long life and minimum maintenance.

The 19*plus* can be operated without a computer from even the smallest boat, with data recorded in non-volatile FLASH memory and processed later on your PC. Simultaneous with recording, real-time data can be transmitted over single-core, armored cable directly to your PC's serial port (maximum transmission distance dependent on number of auxiliary sensors, baud rate, and cable properties). The 19*plus'* faster sampling and pump-controlled TC-ducted flow configuration significantly reduces salinity spiking caused by ship heave, and allows slower descent rates for improved resolution of water column features. Auxiliary sensors for dissolved oxygen, pH, turbidity, fluorescense, PAR, and ORP can be added, and for moored deployments the 19*plus* can be set to *time-series* mode using software commands. External power and two-way real-time communication over 10,000 meters of cable can be provided with the SBE 36 CTD Deck Unit and Power and Data Interface Module (PDIM).

The 19*plus* uses the same temperature and conductivity sensors proven in 5000 SEACAT and MicroCAT instruments, and a superior new micro-machined silicon strain gauge pressure sensor developed by Druck, Inc. Improvements in design, materials, and signal acquisition techniques yield a low-cost instrument with superior performance that is also easy to use. Calibration coefficients, obtained in our computer-controlled high-accuracy calibration baths, are stored in EEPROM memory. They permit data output in ASCII engineering units (degrees C, Siemens/m, decibars, Salinity [PSU], sound velocity [m/sec], etc.). The 19*plus* can be factory-configured to emulate the .hex output format and 2 Hz data rate of old SEACATs for compatibility with existing software or instrument fleets.

Accuracy, convenience, portability, software, and support; compelling reasons why the 19plus is today's best low-cost CTD.

#### **CONFIGURATION AND OPTIONS**

A standard SBE 19plus is supplied with:

- · Plastic housing for depths to 600 meters
- Strain-gauge pressure sensor
- 8 Mbyte FLASH RAM memory
- 9 D-size alkaline batteries
- Impulse glass-reinforced epoxy bulkhead connectors: 4-pin I/O, 2-pin pump, and two 6-pin (two differential auxiliary A/D inputs each)
- SBE 5M miniature pump and T-C Duct

Options include:

- Titanium housing for depths to 7000 meters
- Sensors for oxygen, pH, fluorescence, light (PAR), light transmission, and turbidity
- SBE 5T pump in place of SBE 5M for use with dissolved oxygen and/or other pumped sensors
- Stainless steel cage
- MCBH Micro connectors
- · Ni-Cad batteries and charger

#### SOFTWARE

SEASOFT<sup>®</sup>-Win32, our complete Windows 95/98/NT/2000/XP software package, is included at no extra charge. Its modular programs include:

- SEATERM<sup>®</sup> communication and data retrieval
- SEASAVE<sup>®</sup> real-time data acquisition and display
- SBE Data Processing<sup>®</sup> filtering, aligning, averaging, and plotting of CTD and auxiliary sensor data and derived variables



#### Sea-Bird Electronics, Inc.

1808 136th Place NE, Bellevue, Washington 98005 USA Website: http://www.seabird.com



Email: seabird@seabird.com Telephone: (425) 643-9866 Fax: (425) 643-9954





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1808 136th Place NE, Bellevue, Washington 98005 USA Website: http://www.seabird.com

Email: seabird@seabird.com Telephone: (425) 643-9866 Fax: (425) 643-9954 The SBE 5M pump module consists of a centrifugal pump head and a long-life, DC ball bearing motor contained in a compact, titanium, pressure housing usable to 10,500 meters deep. The pump impeller and electric drive motor are coupled magnetically through the housing, providing high reliability by eliminating moving seals. Motor speed and pumping rate remain constant over the entire input voltage range. The motor drive electronics is intrinsically protected against accidental reversed polarity.

#### APPLICATIONS

The SBE 5M is standard on the SBE 19 and 19*plus* SEACAT Profiler CTD. It is optional on the SBE 16, 16*plus*, and 16*plus*-IM SEACAT C-T Recorder. The pump flushes water through the conductivity cell at a constant rate, independent of the CTD's motion, improving dynamic performance. For applications requiring pumping through additional sensors (for example, a dissolved oxygen sensor), use the SBE 5T pump instead.

Specify:

- Option 5M-1 for profiling (continuous duty) applications such as the SBE 19*plus*.
- Option 5M-2 for moored (pulsed duty) applications such as the SBE 16*plus* or 16*plus*-IM.

Contact Sea-Bird for use in other applications.

#### SPECIFICATIONS

Option 5M-1 (continuous duty): Input voltage range 9 - 18 VDC

Flow Rate 25 ml/s supply current 95 ma

Note: Supply current is independent of operating voltage.

#### Option 5M-2 (pulsed duty): Input voltage range 6 - 18 VDC

Pulse Duration	Flow Volume	Electrical Charge
0.5 seconds	15 ml	0.148 amp-seconds
1.0 seconds	21 ml	0.283 amp-seconds
1.5 seconds	31 ml	0.418 amp-seconds
2.0 seconds	40 ml	0.553 amp-seconds

#### Weight

In Air:	0.42 k
In Water:	0.28 k

).42 kg (0.91 lbs) ).28 kg (0.60 lbs)





SBE 5M

# LEICA NA2 · NAK2





Universal automatic level

# LEICA NA2 The classical level from Leica Geosystems

The NA2 universal automatic level meets all requirements regarding precision, convenience and reliability.

It was designed by surveyors and development engineers with years of experience and who know what a field instrument has to be able to do.

The NA2 soon pays for itself, because it can be used for all types of surveying job; on building sites for routine levelling, in engineering projects, and for geodetic control at all levels of accuracy.

#### **Universal application**

- Levelling of all types and all orders of accuracy
- Precise levelling and settlement determinations on buildings
- Routine heighting for the construction of roads, railways, pipelines, tunnels and so forth
- Setting-out work and control measurements on the construction site
- Area levelling of high accuracy

- Tacheometric levelling with the K-version on flat terrain by combining stadia and angular measurements with height readings
- Deformation measurement and monitoring of bridges



# Quickly set up, simple to use

#### Strong tripods

In principle, the NA2 can be set up on any Leica Geosystems tripod. In practice, for all-round purposes, we recommend the heavy-duty GST20 telescopic-leg tripod. For precise levelling the GST40 fixed-leg tripod is suitable because of its extreme rigidity.

The modular relationship between instrument and tripod is an advantage when transport space is limited.

#### Centring is easy

The circular level only needs to be centred approximately to bring the compensator well into its working range of ~30', and so setting-up goes quicker.

The bubble is viewed positively via a pentaprism and is monitored down the eyepiece.

#### **Play-free footscrews**

The pitch of the smoothrunning and backlash-free footscrews is such that the bubble can be centred in a very short time.

#### Independent of temperature

Unlike the tubular level of a traditional instrument, the NA2 universal automatic level is relatively insensitive to direct solar radiation and an umbrella need only be considered for the most precise levelling.



# Adjust the line of sight automatically

#### Easy to level up

The advantage of this instrument is that, as soon as the bubble is centred, the line of sight is horizontal for all pointings of the telescope. The observer is freed of the time-consuming centring procedure involved with the traditional tubular level, and can concentrate on the business of staff readings.

#### Robust and automatic

The compensator is essentially a pendulum with a prism (4).

The suspension system comprises four flexed tapes (1) made of a special alloy to ensure faultless functioning even at extreme temperatures. The compensator, which is located between the focusing lens and the crosshair reticle, is pneumatically damped against mechanical vibration and is screened against magnetic fields.

## Minimum maintenance

In the unlikely event that the compensator is damaged (and this can only happen as a result of extremely harsh treatment) it is replaced easily, being held only by three screws.

#### 2/NAK2 compensator

Suspension tapes System (fixed) Sompensator body Sendulum with prism ine of sight Sush-button Spring which taps pendulum Sneumatic damping mechanism



#### Push-button control – added security

With most automatics one taps the tripod or instrument to check if the compensator is functioning. Leica Geosystems offers a far more sophisticated solution.

Pressing the button under the NA2 eyepiece gives the compensator a gentle tap, so that you see the staff image swing smoothly away and then float gently back to give the horizontal line of sight. This check, which takes less than a second, is technically perfect, as the pendulum itself is activated and swings through its full range. It is also immediately apparent if the bubble is not centred.





# Top-class optics

#### **Top-class optics**

The telescope is of excellent quality and gives a bright, high-contrast, erect image, even in poor light - an essential for accurate levelling. With the standard eyepiece the magnification is 32×, the optimum for most applications of the instrument. Optional evepieces are available; the 40× may be preferred for precise levelling, the 25× in hot, shimmer conditions. Eyepiece exchange takes only a second or so.

The focusing knob has a coarse/fine movement: - coarse, for rapid setting with minimum turning

 fine, for the final delicate touch to give the perfect image.

#### Fatigue-free viewing

The reticle has:

- a single horizontal hair for reading normal staffs
- a wedge-shaped hair for use with invar staffs
- stadia hairs for distance measurement and threewire levelling.

The general layout of the controls, the smooth friction-braked rotation of the instrument, and the endless horizontal drive with bilateral knobs, all combine to make the instrument easy to use.



NA2 field of view with metric levelling staff Reading at horizontal hair: 1.143 m

#### At an advantage on unstable ground

If a tubular level is used on unstable ground it tilts out of range and has to be continuously reset. By contrast, the pendulum of the NA2 "compensates" and keeps the line of sight horizontal.

# Angle measurement with the NAK2

Civil engineers and contractors often require a circle for angle measurement and setting-out work. Even simple detail surveys, by taking angle, distance and height, and plotting with the polar method, can be done with a level.

The model NAK2 has an internal glass circle which is read via a scale microscope and which can be set to any value by turning the rim around the base of the instrument. NAK2 circle reading (400 gon) 392.66 gon





NAK2 circle reading (360°) 314°42'

# High-performance accessories for precise levelling

#### GPM3 parallel-plate micrometer

This optional accessory slips over the telescope objective and blends perfectly with the smooth lines of the NA2. With a compensator setting accuracy of ±0.3" (equivalent to 0.01 mm in 10 m) and a micrometer reading to 0.1 mm direct and 0.01 mm by estimation, the NA2 with GPM3 is an ideal combination for precise levelling, deformation studies, and even optical tooling. The micrometer drive for raising and lowering the line of sight is conveniently located and readings are taken on a glass scale viewed through an eyepiece just above the telescope eyepiece. This optical reading system, which is digital apart from the last and estimated figure in the metric and inch versions, is superior to the usual metal drum system.

#### GPM6 parallel-plate micrometer

There are tasks for which a micrometer is needed, yet for which the very high accuracy of the GPM3 is not essential.

To meet this requirement, a simpler micrometer attachment, the GPM6 with drum reading, is available for the NA2.

The GPM6 fits on to the telescope objective in the same manner as the GPM3, but the graduation is engraved on a metal drum.



#### **Evepiece** accessories for specialized tasks

Because of the bayonet fastening of the interchangeable eyepiece, all theodolite eyepiece accessories can be used with the NA2.





- Diagonal eyepiece for observing from above, below, and from the side; useful in cramped spaces
- Evepiece lamp for converting the NA2 into a horizontal collimator for laboratory work
- Autocollimation eyepiece for setting machine parts and instrument components precisely vertical

<u>Compact</u>	The rugged NA2 is indifferent to weather conditions and is extremely reliable in the rough world of the building site. The pendulum compen- sator is protected against knocks and shocks. There is a highly-effective vibration- damping mechanism.	
Precise	The high setting accuracy ensures that the line of sight stays put. The attach- able parallel-plate micro- meter renders the NA2 ideal for precise fine levelling.	
Reliable, automatic, maintenance-free	The instantaneous check facility with the push-button control not only makes work easier; it also promotes confidence.	
Easy handling	The convenient, well- arranged controls are designed for maximum convenience. The bilateral, endless horizontal drive promotes rapid fine-pointing.	
Quick levelling-up	The instrument is quickly set up with the three rapid- action footscrews. Their self-adjusting threads make subsequent resetting unnecessary.	
Superb telescope	Telescope with excellently- corrected optics for bright, high-contrast images. All optical components are coated on both sides.	
Effortless focusing	The erect image seen down the telescope is quickly and accurately brought into focus with the convenient rapid and fine focusing knob.	
Abundant accessories; many applications	Additional items such as the parallel-plate micro- meter, the laser eyepiece, or theodolite eyepiece accessories, offer almost unlimited possibilities.	





# LEICA NA2 · NAK2 Proven reliability ensures precise results

# Versatile accessories for demonstrable success

A comprehensive program of accessories enables you to expand the performance and applications range of each instrument. This way, you can match your equipment exactly to requirements.

The possibilities are described in brochure "Survey accessories" 710 883en.

#### Robust container for safe transport

The NA2 is supplied in a foam-padded container made of high performance synthetic material. The foam padding absorbs all jolts and shocks. The container provides perfect protection for the NA2.

#### Technical data

Standard deviation for 1 km levelling, depending on type	double-ru e of staff a	ın and on	
procedure With parallel-plate microme	eter		up to 0.7 mm 0.3 mm
Telescope Standard eyepiece FOK73 eyepiece (optional) FOK117 (optional) Clear objective aperture Field of view at 100 m Shortest focusing distance Multiplication factor Additive constant			erect image 32× 40× 25× 45 mm 2.2 m 1.6 m 100 0
Working range of compense Setting accuracy of comper Sensitivity of circular level	ator Isator (sta	ınd. dev.)	~30' 0.3" 8'/2 mm
Glass circle (K version) Graduation diameter Graduation interval Reading by estimation to		4	00 gon (360°) 70 mm 1 gon (1°) 10 mgon (1′)
Water- and dust resistance			IP53
Temperature range: Operation Storage	–20°C to –40°C to	+50°C (– +70°C (–4	4°F to 122°F) 40°F to 158°F)
Parallel-plate micrometer (optional accessory)	Range	Interval	Estimation
GPM3, with glass scale	10 mm	0.1 mm	0.01 mm
GPM6, with metal drum	10 mm	0.2 mm	0.05 mm



Total Quality Management – Our commitment to total customer satisfaction

Ask your local Leica Geosystems agent for more information about our TQM program.



Leica Geosystems AG CH-9435 Heerbrugg (Switzerland) Phone +41 71 727 31 31 Fax +41 71 727 46 73 www.leica-geosystems.com

## Carl Zeiss NI-2 Level





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## **Optical Data**

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Telescope with Zeiss T-coating 32 × Magnification 1 58 in (40 mm) Aperture 11 ft (33 m) Shortest sighting distance Field of view 23 ft at 1000 ft Estimation of 1/1000 ft. on 1/100 ft. graduation up to 120 ft (1 mm on a 1 cm graduation up to 120 m) **Circular Level** 15 per 2 mm Sensitivity Circle (on request) Material Glass Diameter 2 95 in (75 mm) 360° or 4009 Graduation 1° or 19 Graduation interval Readings through reading microscope Magnification 17× 10 or 0 19 Scale interval 1 or 0 01<sup>9</sup> Estimation to



Fig. 1 Ni 2 with horizontal circle (about 1/2 natural size)

- 1 Focus control with quick-fine movement
- 2 Viewing prism for circular level 3 Eyepiece of reading microscope for circle
- 4 Telescope eyepiece with
- dioptre scale 5 Screw cover over reticle
- adjusting screw 6 Lateral fine movement controls
- 7 Leveling screw 8 Knurled setting ring for circle orientation
- 9 Adjusting screw for tripod
- hinges 10 Adjusting screws for circular
- level 11 Clamping screw for tripod
- leg fitting

## Mechanical Data

Dimensions:		
Length of telescope	10.6 in. (27 cm.)	
Height of instrument .	5.1 in. (13 cm.)	
Diameter of base	5.1 in. (13 cm.)	
External dimensions of case	13×6.9×6.1 in.	
	(33×17.5×15.6 cm.)	
S 3 tripod extending from	3 ft. 5 in. to 5 ft. 7 in. (approx.)	
	(102-170 cm.)	
S 2 tripod extending from	3 ft. 5 in. to 5 ft. 7 in.	
	(approx.)	
	(102–170 cm.)	
Weights:		
Ni 2 without circle	4.6 lbs. (2.1 kg.)	
Ni 2 with circle	5.3 lbs. (2.4 kg.)	
Case for Ni 2 without circle	6.4 lbs. (2.9 kg.)	
Case for Ni 2 with circle,		
with plumb bob	6.6 lbs. (3.0 kg.)	1
Parallel plate micrometer		
in leather case	1.3 lbs. (0.6 kg.)	1
Torch with supports	0.7 lbs. (0.3 kg.)	
Leather case for torch	1.7 lbs. (0.7 kg.)	
S 3 tripod	11.6 lbs. (5.3 kg.)	- 1
S 2 tripod	13.6 lbs. (6.2 kg.)	
Leveling staff (03) 4 m. folding to 2 m.	12 lbs. (5.5 kg.)	
Leveling staff (05) 3 m.		1
folding to 1.5 m.	6.4 lbs. (2.9 kg.)	2
Invar staff (06) 3 m., rigid	9 lbs. (4.0 kg.)	
"Scotch light" staves,		
additional weight	0.45 lbs. (0.2 kg.)	

- 01 Tripod legs only, not n stiffness o (1 m.) apar tips modera
- 02 Lift instrum secure tigh
- 03 Center circ hairs on a the eyepiec
  - Caution: C over an ex dried with a allowed to of the conta
- 04 Aim telesco edge of the
- 05 For fine set the fine mo
- 06 Focus for focus conti matically in
- 07 Read staff necessary : slightly tap movement

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ng for or tripod for circular or tripod

#### **Mechanical Data**

Dimensions:			
Length of telescope		83	10.6 in. (27 cm.)
Height of instrument .		10	5.1 in. (13 cm.)
Diameter of base		÷	5.1 in. (13 cm.)
External dimensions of case		÷.	13×6.9×6.1 in.
			(33×17.5×15.6 cm.)
S 3 tripod extending from		æ	3 ft. 5 in. to 5 ft. 7 in.
			(approx.)
			(102-170 cm.)
S 2 tripod extending from		83	3 ft. 5 in. to 5 ft. 7 in.
			(approx.)
			(102 - 170  cm.)
Weights:			
Ni 2 without circle		÷	4.6 lbs. (2.1 kg.)
Ni 2 with circle			5.3 lbs. (2.4 kg.)
Case for Ni 2 without circle			6.4 lbs. (2.9 kg.)
Case for Ni 2 with circle,			
with plumb bob			6.6 lbs. (3.0 kg.)
Parallel plate micrometer			
in leather case	2	2	1.3 lbs. (0.6 kg.)
Torch with supports			0.7 lbs. (0.3 kg.)
Leather case for torch			1.7 lbs. (0.7 kg.)
S 3 tripod		25	11.6 lbs. (5.3 kg.)
S 2 tripod	6	÷	13.6 lbs. (6.2 kg.)
Loveling staff (03) 4 m. folding to 2	m.		12 lbs. (5.5 kg.)
Leveling staff (05) 3 m.			
folding to 1.5 m.	63	x:	6.4 lbs. (2.9 kg.)
Invar staff (06) 3 m., rigid	÷11		9 lbs. (4.0 kg.)
"Scotch light" staves,			
additional weight	28	÷	0.45 lbs. (0.2 kg.)

### Setting up, Reading

- 01 Tripod legs should be extended to a convenient height only, not necessarily to their maximum; observe correct stiffness of joints (see No. 43); spread legs about 3 ft. (1 m.) apart; level tripod head to eyesight; tread tripod tips moderately into ground.
- 02 Lift instrument slightly to find thread for center screw and secure tightly.
- 03 Center circular level with leveling screws. Focus crosshairs on a bright background by turning the milled ring of the eyepiece (4, fig. 1).

Caution: Do not store wet instrument in the container over an extended period of time. Instrument should be dried with a cloth on the outside as soon as possible and allowed to get completely dry overnight (to be taken out of the container for that purpose).

- 04 Aim telescope roughly onto target by viewing along one edge of the telescope housing.
- 05 For fine setting observe through telescope and use one of the fine movement screws (6).
- 06 Focus for a parallax-free staff image with dual speed focus control (1). Reversing the sense of rotation automatically introduces a slow motion (range: <sup>1</sup>/<sub>4</sub> turn).
- 07 Read staff graduation against horizontal crosshairs (if necessary also stadia lines, fig. 2). As a checking measure slightly tap the telescope with a pencil or operate the fine movement screw jerkily to and fro. After a small oscillat-

4

# Positioning Data Link

# **PDL**<sup>™</sup>

## High Performance Data Link

**Designed for Survey Systems** 

# 19,200 Baud Rate

Higher Over-the -Air Link Rate Extends Your Battery Life

## Enhanced User Interface

Change Channels in the Field View Status Information

## Compatible with GPS RTK Equipment Worldwide

Complete Kit Solutions Available for Your Application

**Reliable** Rugged, All Season Operation

#### **2 Year Warranty** Lower Cost of Ownership



Surveyors utilizing Global Positioning Systems require a rugged radio modem data link for precise positioning information. The PDL is compact and lightweight and offers power efficient operation. It is easy to use, and provides high performance and rugged dependability for the toughest survey environments.

PDL Products are designed to easily mount on all standard tripods and range poles. Complete kit solutions are available.



# Positioning Data Link<sup>™</sup>

	High Power Base	Low Power Base	Rover
<b>General Specifications</b>			'
DTE – DCE Interface		3 Wire, RS-232, 38.4k Baud Maximum.	
User Interface	On/Off Button. Channel Button with AutoBase and AutoRover. <sup>™</sup> Digital Display. Modem/Power Status Indicators. RF Power Select Toggle Switch.	On/Off Button. Channel Button with AutoBase and AutoRover. <sup>™</sup> Digital Display. Modem/Power Status Indicators.	On/Off Button. The second se
Power	1		1
External		9 – 16 VDC.	
Internal Battery	N/A	N/A.	Lithium Ion Battery Pack.
During TX (nominal)	110 Watts.	II Watts.	N/A.
During RX (nominal)	1.9 Watts.	0.9 Watts.	0.3 Watts.
Antenna	1		'
External	50 Ohm, BNC.	50 Ohm, NMO.	50 Ohm, NMO.
Modem Specifications	1		'
Link Rate/Modulation		19,200 bps/4 Level FSK. 9600 bps/4 Level FSK. 9600 bps/GMSK. 4800 bps/GMSK.	
Link Protocols	Transparent, Packet Switched, Digipeater, TRIMTALK.™	Transparent, Packet Switched, Digipeater, TRIMTALK.™	Transparent, Packet Switched, TRIMTALK.™
Forward Error Correction		Hamming Code (12, 8) with Data Interleaving.	
Radio Specifications	1		
Frequency Bands		Refer to price list for available frequency bands.	
Frequency Control		Synthesized 12.5k Hertz Resolution.	
		±2.5 ppm Stability.	
RF Power Select	Low/High. Factory Programmable.	N/A.	
RF Transmitter Output	3/35 Watts Maximum.	0.5 – 2 Watts.	0 Watt (Receive Only).
Sensitivity		-116 dBm (12 dB SINAD).	
Adjacent Channel Selectivity	>-60 dB.	>-70 dB at 9600 bps/GMSK.	>-60 dB.
		>-60 dB at 19,000 bps/4 Level FSK.	
Type Certification	All models are For detailed information conce	type accepted and certified for operation in the U.S erning your country's type certification, please cont	6. and Canada. act your sales representative.
Environmental Specificatio	ons		
Operating Temperature	-22 ° to +140° F (-30	° to +60 ° C).	-4° to +140° F (-20° to +85° C).
Storage Temperature	-67 ° to +185 ° F (-55	° to +85 ° C).	-4° to +185° F (-20° to +85° C).
Vibration/Shock		ANSI/ASAE EP455.	1
Enclosure		IEC 60529 I.P. 66. Water Tight and Dust Proof.	
Mechanical Specifications	·		
Dimensions	6.23" ₩ x 2.77" H x 6.58" L.	8.25" L × 2.40" Diameter.	8.25" L x 2.40" Diameter.
	(15.8 cm W x 7.0 cm H x 16.7 cm L).	(21.0 cm L x 6.1 cm Diameter).	(21.0 cm L x 6.1 cm Diameter).
Weight	2.96 lbs. (1.34 Kg).	0.65 lbs. (0.30 Kg).	0.75 lbs. (0.34 Kg).
Data/Power Connector	5 Pin LEMO #1 Shell.	5 Pin LEMO #0 Shell.	5 Pin LEMO #0 Shell.
Mount	Tripod Bracket.	5/8" – 11 Range Pole.	5/8" – 11 Range Pole.



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#### **INSTANT-RTK TECHNOLOGY**

## Z-Xtreme Survey System

#### **Z-XTREME**

The Ashtech<sup>®</sup> Z-Xtreme<sup>™</sup> from Thales Navigation professional products is a rugged, weather-proof, dual-frequency GPS receiver designed to provide surveyors with cost-effective, centimeter-accurate positions in a variety of system configurations.

The Z-Xtreme receiver begins with state-of-the-art satellite electronics coupled with patented Z-Tracking<sup>™</sup> to deliver the highest GPS signal reception level. A removable battery and flash memory card provide enough capacity to last all day for maximum utility. Components are completely integrated inside a weather-proof, high impact plastic housing, ensuring your investment is safe, rain or shine. Use the easy-to-operate interface on the front panel for important functions such as site information entry, survey status, and set-up of RTK base stations without the additional cost of a handheld controller. The result: Z-Xtreme with Instant-RTK<sup>®</sup> outperforms all other receivers in its class!

#### **ZX-SOLUTIONS**

The Z-Xtreme survey system from Thales Navigation provides a range of solutions designed for the vast array of positioning needs – from entry level static or kinematic post-processed surveys, all the way up to real-time functions such as stake out. The entry level ZX-Solutions<sup>™</sup> system dramatically increases your productivity for control surveys and other post-processed applications. Add an optional kinematic kit to make topographic feature collection more cost effective. Use Ashtech Solutions<sup>™</sup> software to easily process the field data, export results and



generate reports. Purchase only what you need for the job at hand because ZX-Solutions is fully upgradeable.

#### **ZX-SUPERSTATION**

Eclipse the productivity of optical instrument stake out with a ZX-SuperStation<sup>™</sup>. The ZX-SuperStation is a field-to-finish GPS surveying system that combines the Z-Xtreme receiver with a powerful data collector and wireless modems for centimeter accuracy in real-time. Instant-RTK gives you the ability to initialize the centimeter solution in a fraction of the time of conventional RTK systems. Powerful data collection software gives you the ability to efficiently perform GPS surveying techniques and to interface seamlessly with optical total stations.



#### **Z-XTREME**

#### **TECHNICAL SPECIFICATIONS**

#### Ashtech Technology

- 12 channel all-in-view operation
- Full-wavelength carrier on L1 and L2
- Z-Tracking
- Multipath mitigation
- · Dual-frequency smoothing for improved code differential
- Instant-RTK

#### **Performance Figures**<sup>1</sup>

#### Static, Rapid Static

- Horizontal: 0.005 m + 1 ppm (0.016ft+1ppm) • Vertical: 0.010 m + 1 ppm
- (0.033ft + 1ppm)

#### Post-Processed Kinematic

- Horizontal: 0.010 m + 1 ppm
- (0.033ft + 1ppm)
- Vertical: 0.020 m + 1 ppm (0.065ft+1ppm)

#### Real-Time Code Differential Position • <1 m (3.28 ft)

- Real-Time Z Kinematic Position (Fine Mode) Horizontal: 0.010 m + 2 ppm
- (0.033ft + 2 ppm)
- Vertical: 0.020 m + 2 ppm
- (0.065ft + 2 ppm)
- Azimuth (arc sec): 0.4 + 2.0/baseline (km)
- **RTK Occupation Time**
- · 2 seconds (typical sub-centimeter accuracy with longer occupation time)

#### Instant-RTK Initialization

- 99.9% reliability
- Typically <2 seconds with 6 or more satellites,</li> PDOP <5, baseline length <7 km (4.35 mi), open sky and low multipath conditions
- **RTK Operating Range**
- Recommended: 10 km (6.21 mi)
- Maximum: 40 km (24.85 mi)

#### **Standard Features**

- 16 MB PCMCIA removable memory card
- NMEA 0183 output
- · Selectable update rate from 999 sec to 10 Hz
- Event marker
- Point positioning
- 1 PPS timing signal
- Session programming

#### Thales Navigation, Inc.

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- · Wide array of coordinate transformations
- Removable internal battery
- · 8-character alphanumeric LED display with 4button interface
- 3 function LED display Radio, Memory, Satellites/Power
- Multi-function audible alarm
- · Quick reference card holder
- External mount capabilities
- · External power input
- 4 RS-232 ports (115200 baud max, 3 external, 1 internal)
- 1-year warranty
- Free factory technical support

#### **Standard Accessories**

- · Communications software
- · Padded system bag and hard case
- RS-232 data cable
- · Receiver operating manual
- Quick reference field card

#### **Technical Data**

#### Environmental

- Z-Xtreme Receiver
- Meets MIL-STD 810E for wind driven rain and dust
- Operating temperature: -30° to +55°C (-22° to 131°F)
- Storage temperature: -40° to +85°C
- (-40° to 185°F) Geodetic 4 Antenna
- Meets IPX7 specifications for submersion
- Operating temperature: -55 to +75°C
- (-40° to 149°F) • Storage temperature: -55° to +75°C (-67° to 167°F)

#### Physical

#### Weight

- Receiver: 1.59 kg (3.50 lb)
- Antenna: 0.82 kg (1.81 lb)
- Battery: 0.43 kg (0.95 lb)
- Dimensions
- 76.2 H x 196.85 W x 222.25 D mm
- (0.25 H x 0.646 W x 0.729 D ft)
- Power

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• 10 - 28 VDC, 6.0 W

#### Internal battery

- · Capacity: 6000 mAh
- >9 hours (typical) @ 25°C (77°F)
- Operating temperature: -30° to +55°C (-22° to 131°F)
- Storage temperature: -40 to +60°C
  - (-40° to + 140°F)

#### PC card

- ATA Type II PCMCIA memory card (16 MB standard)
- Temperature range: -40° to +85°C (-40° to 185°F)
- Data capacity: 4500 epochs per 2 MB\* \* Based on one session, eight satellites' data
- and full measurements. This number can vary significantly depending on the conditions of the session.

#### **Optional Features**

- Real-time kinematic (base and rover modes) for cm-accuracy
- RTCM 2.2 (Types 1, 2, 3, 9, 16, 18, 19, 20, 21, 22)
- · Internal UHF or spread spectrum radio for RTK rover operations
- External UHF or spread spectrum radio for RTK base and rover operations
- · Geodetic 4 antenna ground plane kit

**Optional Application Software** 

Land Surveying and Construction

Specifications assume operation follows all the

procedures recommended in the product manual utilizing Instant-RTK, post processing with Ashtech Solutions or Ashtech Office Suite for Survey. High-multipath areas, high PDOP values, low satellite visibility, and periods of adverse atmospheric conditions and/or other adverse

circumstances will degrade system performance. All

THALES

NAVIGATION

accuracy specifications are RMS values.

· Kinematic antenna kit Aircraft antenna kit

Long haul backpack kit

GPS data processing

Ashtech Survey Control II

Mining and Land Seismic

 Ashtech Mine Surveyor II Ashtech Seismark II

Ashtech GPS Fieldmate

Ashtech Solutions

TDS Survey Pro

Carlson SurvCE

1

AC power cable

All-on-a-pole kit

Choke ring antenna





# Valuable functions, superior cost-performance, longer battery life and enhanced software



Nikon has just taken the world-renowned Top Gun® DTM-300 total station to a whole new level. The new Top Gun® DTM-310's enhanced keyboard and on-board software enable easy code input in both alphabet and numbers, the way you've always wanted. It builds on existing features - such as the large four-line LCD and full numeric key pad — to improve overall convenience. And software upgrades make it easier to search and display data. In fact, the Top Gun® DTM-310 provides customers in any field - from civil construction to cadastral surveying and mapping — with greater ease of operation.

Ø

#### ENHANCED BASIC FUNCTIONS

Large four-line display with full alphanumeric input on both faces Meets basic requirements for distance and angle measurement Resume function for quick startup and power management Enhanced, powerful built-in programs 500-point on-board data storage function 7.3 hours continuous measuring with one on-board battery Compact and lightweight Quick access to the 20 most recently stored codes

## **CONVENIENT ALPHANUMERIC INPUT**

The inclusion of alphabetic input enables you to store codes in a combination of letters and numerals. Codes, target heights (HT) and point numbers are easily input for each new measurement. And codes can also be selected from the most recent 20 codes stored in the memory. eliminating the need to repeatedly input the same codes.



#### KEY DESCRIPTIONS

- MSR: Distance measurement in normal measurement mode
- DSP: Selects display item by scrolling display
- TRK: Distance measurement in high-speed measurement mode ANG: Horizontal angle zero-set, user-defined angle input or hold
- XYZ: Coordinate measurement
- RDM: Remote distance measurement (continuous or radial)
- **REM:** Remote elevation measurement
- STN: Station setup (known point, 2-point resection or 3-point resection)
- S-O: Stakeout by inputting angle distance or coordinates Illumination: Display illumination
- REC: Data record to internal memory
- ENT: Data entry or sending observation data to communication port in normal observation mode
- FNC: Input of temperature and barometric pressure, prism constant, and height of target; simple COGO calculation; settings; view/edit stored data; communication (internal memory); vertical collimation correction

# ENHANCED, POWERFUL BUILT-IN PROGRAMS

#### On-board data storage function

The DTM-310 memory stores up to 500 raw or coordinate records. Coordinate data can be manually input, measured or



uploaded from a PC. (Contact your Nikon distributor for download/upload and format conversion software.) Data can be instantly recalled and reviewed for station setup, stakeout and COGO.

#### Station setup

For station setups, in addition to the known station setup obtained by inputting the coordinate of backsight or direction angles, a more simplified default station setup is also possible. This can be obtained by setting the station point coordinates at zero



while maintaining the prior orientation intact. Two- and three-point resections are also available. In the case of a three-point resection, it is possible to transfer the elevation from a bench mark.

#### XYZ coordinate measurement

The coordinate system can be set to survey, mathematical or NEZ with indepen-

N:	1200.169	m
E:	1829.964	m
Z:	29.909	m
XV7	BOTH	

dent coordinate order settings. Azimuth zero-direction can be set to either north or south. Coordinate calculations are based on these settings. Point name, number, code and coordinate data can be stored in the data file. The target height can be changed at any time by pressing the FNC key.

#### Stakeout

Lets you perform stakeouts by inputting angle and distances, or coordinates. Co-



ordinates can be searched and retrieved from the built-in memory. Zero-direction countdown and delta displays (Left/Right, In/Out, Cut/Fill) make for fast and simple stakeouts. Stakeout data can be also recorded in the internal memory.

#### RDM

For continuous or radial remote distance measurement. Press the DSP key to se-



lect slope distance, elevation difference, horizontal distance, grade, legal grade ratio between two points, or azimuth from first to second points.

#### REM



#### COGO calculation

Enables point-to-point inverse calculations, plus azimuth and distance calculations. Coordinates can be searched and retrieved from the on-board memory, and calculated coordinates can be saved.

#### Data display

The DTM-310 enables you to search data by tracing back from the most recent record, from specific station points, or from a simple point number.



## 7.3 HOURS CONTINUOUS OPERATING TIME

Internal battery BC-60 provides about 7.3 hours (with full charge, at 20°C, for distance/angle measurements) of continuous operation. The remaining battery power is indicated by the LCD. As Ni-MH battery BC-60 contains no harmful substance, recycling is not necessary. Quick recharge can be performed in about 2 hours with standard battery charger Q-70U/Q-70E. The Q-70U/Q-70E's discharging function preserves the batteries' minimum power and protects against deterioration.

## **RESUME FUNCTION**

This resume function can automatically revert to the orientation prior to power OFF, or automatically display the previous horizontal angle. It guarantees the safety of all previous data settings.

## BASIC MEASUREMENT FUNCTIONS

- Built-in Automatic Vertical Compensation
- Vertical Angle Zero-Degree Set Handled in Three Modes
- Grade Display
- With Triple Prism, to 1.2km or 3,900 feet (under good conditions)
- ±(5 + 3ppm x D)mm Precision
- Automatic Environmental Compensation
- Selectable Angle Reading of 5/10", 0.5/1mgon, 0.02/0.05MIL
- Angle Measurement Accuracy of 5"/1.6mgon/ 0.02MIL (standard deviation based on DIN18723)

#### Standard Package

- DTM-310 main unit
- On-board battery BC-60
- Battery charger
- Q-70U/Q-70Ĕ
- Lens cap

#### **Optional Accessories**

- Diagonal eyepiece prism
- High-power (32x) and low-power (16x) eyepiece lenses

 Compass (tubular type) and compass adapter Zenith prismSolar filter

Plumb bob

Plastic case

Vinyl cover

Instruction manual

Tool set

- Solar reticle
- External battery B4





Ε

On-board battery BC-60 and battery charger Q-70U/Q-70E

Specifications			
Telescope Tube length Effective diameter of objective Magnification Field of view Resolving power Minimum focusing distance	150mm/5.9 in. 36mm/1.41 in. (EDM aperture 40mm/1.57 in.) 26x (standard) 1°30' 3.5" 1.0m/3.3 ft.	Measuring intervals Standard MSR mode Tracking mode Measuring mode Ambient temperature range Atmospheric correction range Temperature range Pressure range	4 sec. 1.2 sec. Continuous/Single/Average (2 - 99) -20°C to +50°C (-4°F to +122°F) -40°C to +60°C (-40°F to +140°F) 400 to 999mmHg (1mmHg step) 15.8 to 39.3 in Hg (0.1 in Hg step)
Angle measurement Reading system Unit of reading Least count (selectable)	Incremental encoder Degree/Gon/6400MIL	Display	533 to 1,332hPa (1hPa step) Dot-matrix LCD 16 characters x 4 lines
(360°) (400G) (6400MIL)	5" or 10" 0.5mgon or 1mgon 0.02MIL or 0.05MIL	Level vial Sensitivity of plate level vial Sensitivity of circular level vial	30"/2mm 10'/2mm
Accuracy (Standard deviation based on DIN 18723)	5"/1.6mgon/0.02MIL	Leveling base Tribrach	Detachable
Tilt sensor (Automatic Vertical Compensator) Working range	Liquid type ±3'	Optical plummet Image Magnification	Erect
Distance measurement Range (with Nikon prism)		Field of view Focusing range	5° 0.5m/1.6 ft. to ∞
(Normal conditions: ordinary haze, visibility 20km/12.5 miles) with mini prism with single prism with triple prism	380m/1,300 ft. 800m/2,600 ft. 1,100m/3,700 ft.	Power sources Type Continuous operating time	Ni-MH 7.2V DC 7.3 hrs. or 8,760 measurements (for distance/angle measurement) 22 hrs. (for angle measurement only)
(Good conditions: no haze, visibility 40km/25 miles) with mini prism	450m/1,500 ft.	Quick battery charger (Q-70U/Q-70E) Input voltage Recharging time	115V for Q-70U, 220/240V for Q-70E 1.5 hrs.
with single prism	1,200m/3,900 ft. +(5 + 3ppm x D)mm.	Dimensions (W x D x H) Main unit (with carrying handle)	164 x 177 x 335mm/6.5 x 7.0 x 13.2 in.
Maximum measurement display	-10°C to +40°C/+14°F to +104°F ±(5 + 5ppm x D)mm, -20°C to +50°C/-4°F to +122°F 1.230m/4.000 ft.	Weight Main unit w/battery Battery BC-60 Carrying case	5.5kg/12.1 lbs. 0.5kg/1.1 lbs. 2.5kg/5.5 lbs.
Least count Standard MSR mode Tracking mode	1mm/0.005 ft. 10mm/0.05 ft.		, Line and

These products (DTM-310 and battery charger Q-70U/E) are strategic products subject to Japanese/International export control regime. They should not be exported without authorization from the appropriate governmental authorities.



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# **V** . SPECIFICATIONS

## 1. Main Unit

#### • Telescope

Image	: Erect/unreversed
Magnification	:26×
Effective diameter of objective	: 36mm
Field of view	: 1°30′
Minimum focusing distance	: 1.0m
Resolving power	: 3.5″

#### • Distance Measurement

Distance range of Nikon prisms:	450m with mini prism
-	1000m with single prism
	1200m or longer with triple prism
	*With visibility 40km (25miles)
Precision :	$\pm$ (5mm + 3ppm × D)
	*With accurate measurement mode, at -10°C~+40°C/+14°F~+104°F
	±(5mm+5ppm×D) at -20°C≦t<-10°C/ -4°F≦t<+14°F and +40°C <t≦50°c <br="">+104°F<t≤+122°f< td=""></t≤+122°f<></t≦50°c>
Measuring time response	(MSR) mode: About 4sec.
in a coperior	(initial: about 5sec.)
	(TRK) mode (cm): About 1.2sec
	(initial: about 2.2sec.)
east count	· 1mm
Display	· Up to 1230m
Display unit	m/ft-INT/ft-US
Display unit	
Angle Measurement	
Accuracy	: 5" (Standard deviation based on DIN
Recuracy	18723)
Reading system	: Photoelectric detection by incremental encoder single-sided reading
Display unit	: Degree/Gon/MIL

#### **V** . SPECIFICATIONS

Automatic Vertical Comp	pensator	
System	: Liquid-electric detection	
Working range	: ±3′	
<ul> <li>Optical plummet</li> </ul>		
Image	: Erect	
Magnification	: 3×	
Field of view	: 5°	
Focusing range	:0.5m~∞	
Clamps/tangent screws	: Coaxial dual speed tangents	
Sensitivity of level vials		
Plate level vial	: 30 <b>'/</b> 2mm	
Circular level vial	: 10'/2mm	
● Tribrach	: Detachable	
• Dimensions and weight		
Main body	: 5.5kg (12lbs) including BC-6 battery	
	pack	
Case	: About 3.5kg (7.6lbs)	
• Operating temperature range:		

-20°C~50°C/-4°F~+122°F

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# SET5F Version 01-00 TOTAL STATION

Enhanced software with 3,000-point data memory.



# Flexible, Friendly and Featherweight

The SET5F's powerful EDM, dependable dual-axis compensator and 3,000-point data memory are conveniently packaged in a compact, lightweight body. Software [Version 01-00) has been enhanced for more effective survey work, and "softkey" assignments can be freely customized to suit all user needs.

# Dependable Hardware

#### Proven Dual-axis Compensator

•Since its introduction with the Series C total station in 1989, Sokkia's dual-axis compensator has proven its reliability and accuracy at survey sites all over the world. •The dual-axis tilt sensor monitors deviations of both the X and Y axes and the correct horizontal and vertical angle readings are automatically computed and applied. The result is easier and faster instrument leveling.



#### The High-performing EDM

•1,500m/4,900ft range with a single prism under good ambient conditions (40km/ 25miles visibility, with no haze, overcast, no scintillation).

•Outstanding precision;

 $\pm$ (3+2ppmxD)mm. This corresponds to a

deviation of a mere ±3.2mm at a distance of 100m and ±5mm at 1,000m.
Supreme speed; only 1.7 seconds initial measuring time in the rapid measurement mode.

	Average Conditions	Good Conditions
CP01 Compact Prism	700 m/2,300 ft.	
One AP01 Prism	1,200 m/3,900 ft.	1,500 m 4,900 ft.
Three AP01 Prisms	1,600 m/5,200 ft.	2,000 m 6,500 ft.

#### **Powerful Telescope**

Highest magnification in its class: 30x
Easy, accurate sighting of prisms or targets



#### **Outstanding Mobility**

•Total carrying weight (including instrument, tribrach, battery and hard case) is a mere 8 kg/18 lbs. The secret lies in the lightest and most compact carrying case of its kind



(W390 x D255 x H220mm / W15.3 x D10.0 x H8.6in.), making the SET5F supremely portable.

•A convenient shoulder strap is provided as standard. An optional back pack (SC94) is ideal for longer day treks.

# Enhanced Software

# The SET5F can be easily customized to your preferred key assignments.

•The SET5F offers optimum keyboard flexibility. Any keyboard layout can be configured. For example, functions can be assigned to any key position on any page, and unused functions can be temporarily deleted.

•A powerful "softkey" feature facilitates input of coordinate values, feature codes, etc.



#### Spacious 3,000-point Internal Memory

•The SET5F's internal memory is large holding a full 3,000 data points—and secure. For optimum convenience, measurements can be performed and recorded at the touch of a key. •Up to five (5) job files can be created to efficiently organize multiple survey tasks. •Forty (40) feature codes (max.13 characters each) can be kept in the memory for easy recall as needed.



Sophisticated Application Software Missing Line Measurement (MLM) •The SET5F measures horizontal distance, slope distance, height difference, and slope in percent (%) between two prisms, all at the touch of a key.

# The SET5F brings full freedom to survey work.





# Remote Elevation Measurement (REM)

•The SET5F can be used to easily determine the height of a point where a prism cannot be placed. The system sights a prism directly above or below the target point, and then sights the point desired.



#### **Angle Repetition**

•For enhanced accuracy in the horizontal angle measurement, the SET5F can measure in repetition. It then calculates and displays the average of the multiple angle measurements.

#### **Azimuth Angle Setting**

•Using the coordinates of the instrument station and a backlight point, the SET5F can automatically set the horizontal angle to the azimuth of the backlight.



#### Resection

•With 2 to 5 known points, the SET5F can be used to determine the azimuth and coordinates of the unknown instrument station.

•When using 2 known points, both angles and distances are measured. When using 3 or more points, the distance does not always have to be measured.



#### **3-D Coordinate Measurement**

The SET5F calculates 3-D coordinate values of measuring points.
The operator may choose display settings either of "N, E, Z" or "E, N, Z."



#### 3-D Setting-out

•The SET5F can be used to perform 3-dimensional setting-out with N, E and/or Z coordinates.



#### **Offset Measurements**

Two basic offset measurement methods are provided to measure the hidden points. One calls for input of the offset distance and the direction between the measuring point and the prism. The other uses a prism set on the left or right side of the measuring point at the same distance from the SET5F; the angles and distance to the prism are measured, and the measuring point is sighted. In both cases, the SET5F calculates the horizontal and vertical angles and distance, or the N, E, Z coordinates.





#### **Standard Configuration**

The SET5F comes with two (2) BDC25 rechargeable batteries EDC19 battery charging adapter CDC27, CDC31 or CDC31A quick charger, CP7 tubular compass, sunshade, lens cap, plumb bob, vinyl cover, tool kit, operator's manual, carrying case and shoulder strap.

# Electronic Field Books (SDR33/SDR31)

Thanks to its advanced two-way communications port, the SET5F's functions can all be accessed by external controller. For example, by connecting one of the Sokkia's acclaimed Electronic Field Books (SDR33 or SDR31), complex field operations such as traverse adjustment, intersection, area calculations and roading can be carried out with remarkable ease.



#### **Optional Accessories**

DE17A	<b>Diagonal Eyepiece</b>
OF1/OF1A	Solar Filters
SC94	Back Pack

Telescone		Fully transiting coavial FDM	
l enath		165mm (6 5in)	
Ohiective aperture		45mm (1.8in)	
Magnification image		30v Freet	
Resolving power		3.0"	
Field of view		1°30'(26m/1 000m)	
Minimum focus		1 3m (4 3ft )	
Reticle illumination		Bright or Dim selectable	
Angle measurement		Incremental encoder, diametrical detection	
Display resolution	H&V	1"/ 0.2 mgon/ 0.005 mil. 5"/1 mgon/ 0.02 mil	
Angle unit	H&V	Degree/Gon/Mil	
Accuracy	H&V	5" (1.5 mgon/ 0.02 mil) according to DIN18723	
Dual-axis compensator		Liquid dual-axis tilt sensor range: +3' (+55 mgon)	
Display mode	Ц	Clockwise/Counterclockwise Repetition Ocet Hold available	
Display mode	$\frac{11}{V}$	Zapith 0%/Llorizontal 0%/Llorizontal 0% 00%/Slope%	
	V		
Distance measurement	internes)	Electro-optical with modulated infrared LED.	
ivieasuring range (slope d	istance)	A: Average conditions; slight haze, visibility about 20km(12 miles),	
		sunny periods, weak scintillation.	
		G: Good conditions; no naze, visibility about 40km (25 miles),	
		overcast, no scintiliation.	
		Maximum ranges are achieved with Sokkia CP/AP prisms.	
With CPU1 compact prise	n	A: 1.3m (4.3ft.) to 700m (2,300ft.)	
With one AP01 prism		A: 1.3m (4.3ft.) to 1,200m (3,900ft.), G: 1,500m (4,900ft.)	
With three AP01 prism		A: 1.3m (4.3π.) to 1,600m (5,200π.), G: 2,000m (6,500π.)	
Distance unit		Meters of feet, selectable	
Accuracy (Fine measuren	nent)	±(3+2ppmxD)mm D=measuring range, unit=mm	
Measuring unit and time	Fine	0.001 m Every 3.2 seconds (initial 4.7 seconds)	
(slope distance)	Rapid	0.001 m 1.7 seconds	
	Tracking	0.01 m Every 0.3 seconds (initial 1.4 seconds)	
A	Average	0.0001 m (average of 2 to 9 times measurement)	
Atmospheric correction		Key-in the temperature and pressure, or -499 to +499ppm.	
Prism constant		-99 to 0mm (1 mm steps)	
Refraction & Earth-curvat	ure	On/off selectable (K=0.142)	
correction			
General			
Display		LCD dot matrix display (20 characters x 4 lines) on both faces with	
Keeleraud		back light.	
Keyboard		5 keys on both faces, free assignment of functions.	
Resume function		On/on selectable	
Sensitivity of levels		Plate level: 40 /2mm, Circular level: 10/2mm (in tribrach)	
		Image: erect, Magnification: 3X, Minimum focus: 0.5m (1.6ft.)	
Interface		Asynchronous serial, RS-2320 compatible, baud rate 1200/	
0		96000ps	
2-way communication		2 000 paint data mamany	
Data storage			
Operating temperature	L. (	$-20^{\circ}$ C to $+50^{\circ}$ C ( $-4^{\circ}$ F to $+122^{\circ}$ F)	
Tilting/Trunnion axis heigi	ht	236mm (9.3in) from tribrach bottom, 193mm (7.6in) from	
<u></u>		tribrach dish.	
Size with handle and battery		W150 X D165 X H353mm, W5.9 X D6.5 X H13.9In.	
Weight with handle and ba	attery	5.4Kg (11.9lbs)	
vveight of parts		BDC25 battery: 240g (8.5oz.), Handle: 100g (3.5oz.),	
Damas arms <sup>11</sup>		ribrach: 740g (1.6 lbs), Case:2.4kg (5.3lbs)	
Power supplies			
Battery level display		4 steps with warning message.	
Automatic power cut-off		Drivon selectable (30 minutes after the last operation)	
Power source	(770)	Dictored & engle measurement of built 5 hours of built 20	
working duration at 25°C	(//˘⊢)	Uistance & angle measurement: about 5 hours, about 600 points	
w/one BDC25 battery		(rine & single measurement with 30 seconds intervals).	
Charging time		Angle measurement only: about 9 hours.	
		CDC27/31: about 80 minutes, CDC31A: about 90 minutes	

**SET5F Specifications** 

Designs and specifications are subject to change without notice. SOKKIA CO.,LTD.

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Sokkia is a sponsor of the International Federation of Surveyors.



#### Vessel Reports, Offsets, and Diagrams

#### Launch 1010

Vessel Report

- 1\_HVF
- 2\_Offsets
- 3\_Patch Test
- 4\_DDSSM and Settlement & Squat
- 5\_POS Gams Calibration
- 6\_Wire Diagram

#### Launch 1018

- Vessel Report
- 1\_HVF
- 2\_Offsets
- 3\_Patch Test
- 4\_DDSSM and Settlement & Squat
- 5\_POS Gams Calibration
- 6\_Wire Diagram

#### S220

Vessel Report

- 1\_HVF
- 2\_Offsets
- 3\_Patch Test
- 4\_DDSSM and Settlement & Squat
- 5\_POS Gams Calibration
- 6\_Wire Diagram
- 7\_Correspondence

FA\_1010\_Reson8101\_end07.txt Vessel Name: FA\_1010\_Reson8101.hvf Vessel created: December 19, 2006

Depth Sensor:

	Sensor Class: Time Stamp:	Swath 2006-001	00: 00
	Transduer #1: Pitch Offset: Roll Offset: Azimuth Offset:	-1. 160 2. 250 0. 930	
	Del taX: 0.312 Del taY: -0.142 Del taZ: 0.397		
	Manufacturer: Model: Serial Number:	Reson sb8101 2701011	
Depth Sensor:			
	Sensor Class: Time Stamp:	Swath 2007-001	00: 00
	Transduer #1:		
	Pitch Offset: Roll Offset: Azimuth Offset:	-0. 280 2. 500 0. 600	
	Del taX: 0.247 Del taY: -0.138 Del taZ: 0.551		
	Manufacturer: Model: Serial Number:	Reson sb8101 2701011	
Depth Sensor:			
	Sensor Class: Time Stamp:	Swath 2007-119	00: 00
	Transduer #1: Pitch Offset: Roll Offset: Azimuth Offset:	-0. 280 3. 000 0. 600	
	Del taX: 0.247 Del taY: -0.138 Del taZ: 0.551		
	Manufacturer: Model: Serial Number:	Reson sb8101 2701011	

Depth Sensor:
		FA_10	10_Reson8101_end07.txt
	Sensor Class: Time Stamp:	Swath 2007-136	22: 07
	Transduer #1: Pitch Offset: Roll Offset: Azimuth Offset:	-0. 280 2. 710 0. 600	
	Del taX: 0.247 Del taY: -0.138 Del taZ: 0.551		
	Manufacturer: Model: Serial Number:	Reson sb8101 2701011	
Depth	Sensor:		
	Sensor Class: Time Stamp:	Swath 2007-150	00: 00
	Transduer #1: Pitch Offset: Roll Offset: Azimuth Offset:	-0. 280 3. 000 0. 600	
	Del taX: 0.247 Del taY: -0.138 Del taZ: 0.551		
	Manufacturer: Model: Serial Number:	Reson sb8101 2701011	
Depth	Sensor:		
	Sensor Class: Time Stamp:	Swath 2007-150	19: 04
	Transduer #1: Pitch Offset: Roll Offset: Azimuth Offset:	-0. 280 2. 710 0. 600	
	Del taX: 0.247 Del taY: -0.138 Del taZ: 0.551		
	Manufacturer: Model: Serial Number:	Reson sb8101 2701011	
Depth	Sensor:		
	Sensor Class: Time Stamp:	Swath 2007-151	00: 00
	Transduer #1: Pitch Offset:	-0. 280	Page 2

FA\_1010\_Reson8101\_end07.txt 3.070 Roll Offset: Azimuth Offset: 0.600 Del taX: 0.247 Del taY: -0.138 Del taZ: 0.551 Manufacturer: Reson Model: sb8101 Serial Number: 2701011 Depth Sensor: Sensor Class: Time Stamp: Swath 2007-172 00:10 Transduer #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: -0.280 Roll Offset: 2.620 Azimuth Offset: 0.600 Del taX: 0.247 Del taY: -0.138 Del taZ: 0.551 Manufacturer: Reson Model: sb8101 Serial Number: 2701011 Depth Sensor: Sensor Class: Swath Time Stamp: 2007-176 00:00 Transduer #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: -0.280 2.890 Roll Offset: Azimuth Offset: 0.600 Del taX: 0.247 Del taY: -0. 138 Del taZ: 0. 551 Manufacturer: Reson sb8101 Model: Serial Number: 2701011 Depth Sensor: Sensor Class: Swath Time Stamp: 2007-176 22:20 Transduer #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ -0.280 Pitch Offset: Roll Offset: 2.620 Azimuth Offset: 0.600 Del taX: 0.247 Del taY: -0.138 Del taZ: 0.550

Page 3

## FA\_1010\_Reson8101\_end07.txt

	Manufacturer: Model: Serial Number:	Reson sb8101 2701011	
Depth Se	ensor:		
	Sensor Class: Time Stamp:	Swath 2007-197 00	0: 00
	Transduer #1: Pitch Offset: Roll Offset: Azimuth Offset:	-1.040 2.910 0.890	
	Del taX: 0.247 Del taY: -0.138 Del taZ: 0.550		
	Manufacturer: Model: Serial Number:	Reson sb8101 2701011	
Depth Se	ensor:		
	Sensor Class: Time Stamp:	Swath 2007-252 00	0: 00
	Transduer #1: Pitch Offset: Roll Offset: Azimuth Offset:	-0. 570 2. 810 0. 570	
	Del taX: 0.247 Del taY: -0.138 Del taZ: 0.550		
	Manufacturer: Model: Serial Number:	Reson sb8101 2701011	
Navi gati	on Sensor:		
	Time Stamp:	2006-001 00	0: 00

Comments (null) Latency 0.000 DeltaX: 0.000 DeltaY: 0.000 DeltaZ: 0.000 Manufacturer: Applanix Model: POS/MV v320 Serial Number: 788

Time Stamp: 2007-001 00:00

Comments POS time mistakenly set to GPS time requiring a 14 sec time correction  $\hfill \ensuremath{\mathsf{C}}$ 

FA\_1010\_Reson8101\_end07.txt Latency 14.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Manufacturer: Appl ani x POS/MV v4 Model: Serial Number: 2564 Time Stamp: 2007-102 00:00 Comments Time changed in POS to UTC - 14 sec time correction deleted Latency 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Manufacturer: Appl ani x POS/MV v4 Model: Serial Number: 2564 Gyro Sensor: Time Stamp: 2006-001 00:00 Comments (null) Latency 0.000 2007-001 00:00 Time Stamp: Comments POS time mistakenly set to GPS time requiring a 14 sec time correcti on Latency 14.000 Time Stamp: 2007-102 00:00 Comments Time changed in POS to UTC - 14 sec time correction deleted Latency 0.000 Heave Sensor: 2006-001 00:00 Time Stamp: Comments True Heave Enabled Apply Yes Latency 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Offset: 0.000 Appl ani x POS/MV v320 Manufacturer:

> Time Stamp: 2007-001 00:00

788

Model:

Serial Number:

#### FA\_1010\_Reson8101\_end07.txt

Comments True Heave Enabled / POS time mistakenly set to GPS time requiring a 14 sec time correctionPOS time mistakenly set to GPS time requiring a 14 sec time correcti on Apply Yes

Latency 14.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Offset: 0.000 Manufacturer: Appl ani x POS/MV v4 Model: Serial Number: 2564 Time Stamp: 2007-102 00:00 Comments Time changed in POS to UTC - 14 sec time correction deleted Apply Yes Latency 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Offset: 0.000 Manufacturer: Appl ani x POS/MV v4 Model: Serial Number: 2564

Pitch Sensor:

Time Stamp: 2006-001 00:00

Comments (null) Apply Yes Latency 0.000 Pitch offset: 0.000

Manufacturer: Appl ani x POS/MV v320 Model: Serial Number: 788

Time Stamp: 2007-001 00:00

Comments POS time mistakenly set to GPS time requiring a 14 sec time correction

Apply Yes

Latency 14.000 Pitch offset: 0.000

Appl ani x Manufacturer: Model: POS/MV v4 Serial Number: 2564

Time Stamp: 2007-102 00:00

Comments Time changed in POS to UTC - 14 sec time correction deleted Apply Yes Latency 0.000 Pitch offset: 0.000

#### FA\_1010\_Reson8101\_end07.txt

Manufa	cturer:	Appl ani	х
Model:		POS/MV	v4
Seri al	Number:	2564	

Roll Sensor:

Time Stamp: 2006-001 00:00 Comments (null) Apply Yes Latency 0.000 Roll offset: 0.000 Manufacturer: Appl ani x Model: POS/MV v320 Serial Number: 788 Time Stamp: 2007-001 00:00 Comments POS time mistakenly set to GPS time requiring a 14 sec time correcti on Apply Yes Latency 14.000 Roll offset: 0.000 Manufacturer: Appl ani x Model: POS/MV v4 Serial Number: 2564 Time Stamp: 2007-102 00:00 Comments Time changed in POS to UTC - 14 sec time correction deleted Apply Yes Latency 0.000 Roll offset: 0.000 Manufacturer: Appl ani x POS/MV v4 Model: Serial Number: 2564 Draft Sensor: Time Stamp: 2006-001 00:00 Apply Yes Comments DDSSM Entry 1) Draft: 0.000 Entry 2) Draft: -0.070 Entry 3) Draft: -0.030 Speed: 0.000 Speed: 4.636 Speed: 6.230 Entry 4) Draft: -0.020 Speed: 8.164 Entrý 5) Draft: -0.010 Speed: 9.846 Entry 6) Draft: -0.030 Speed: 12.227 Time Stamp: 2007-001 00:00 Apply Yes

Comments DDSSM Entry 1) Draft: 0.000 Speed: 0.000 Page 7 FA\_1010\_Reson8101\_end07.txt Entry 2) Draft: -0.041 Speed: 5.015 Entry 3) Draft: -0.031 Speed: 6.026 Entry 4) Draft: 0.023 Speed: 7.737 Entry 5) Draft: 0.053 Speed: 8.942 Entry 6) Draft: 0.102 Speed: 10.050 Entry 7) Draft: 0.089 Speed: 10.438

TPE

Time Stamp: 2006-001 00:00 Comments **Offsets** Motion sensing unit to the transducer 1 X Head 1 0.312 Y Head 1 -0.142 Z Head 1 0.397 Motion sensing unit to the transducer 2 X Head 2 0.000 Y Head 2 0.000 Z Head 2 0.000 Navigation antenna to the transducer 1 X Head 1 1.209 Y Head 1 1.057 Z Head 1 3.538 Navigation antenna to the transducer 2 X Head 2 0.000 Y Head 2 0.000 Z Head 2 0.000 Roll offset of transducer number 1 0.000 Roll offset of transducer number 2 0.000 Heave Error: 0.050 or 5.000'' of heave amplitude. Measurement errors: 0.007 Motion sensing unit alignment errors Gyro: 0. 250 Pi tch: 0. 150 Rol I : 0. 150 Gyro measurement error: 0.020 Roll measurement error: 0.020 Pitch measurement error: 0.020 Navigation measurement error: 0.500 Tranšducer timing error: 0.005 Navigation timing error: 0.005 Gyro<sup>-</sup>timing erroř: 0.005 Heave timing error: 0.005 PitchTimingStdDev: 0.005 Roll timing error: 0.005 Sound Velocity speed measurement error: 0.000 Surface sound speed measurement error: 0.050 Ti de measurement error: 0.010 Ti de zoni ng error: 0.720 Speed over ground measurement error: 0.030 Dynamic loading measurement error: 0.000 Static draft measurement error: 0.050 Delta draft measurement error: 0.020 StDev Comment: `éƒJ Ï…J`õ…JPõ…J°ð…J €…J@í…J°k€JàZ€J€Ó…Ja Time Stamp: 2007-001 00:00

Comments Offsets

FA\_1010\_Reson8101\_end07.txt Motion sensing unit to the transducer 1 X Head 1 0.247 Y Head 1 -0.138 Z Head 1 0.551 Motion sensing unit to the transducer 2 X Head 2 0.000 Y Head 2 0.000 Z Head 2 0.000 Navigation antenna to the transducer 1 X Head 1 1.144 Y Head 1 1.061 Z Head 1 3.667 Navigation antenna to the transducer 2  $\begin{array}{cccc} X & Head & 2 & 0. \ 000 \\ Y & Head & 2 & 0. \ 000 \end{array}$ Z Head 2 0.000 Roll offset of transducer number 1 0.000 Roll offset of transducer number 2 0.000 Heave Error: 0.050 or 5.000'' of heave amplitude. Measurement errors: 0.007 Motion sensing unit alignment errors Rol I: 0. 130 Gyro: 0. 100 Pi tch: 0. 130 Gyro measurement error: 0.020 Roll measurement error: 0.020 Pitch measurement error: 0.020 Navigation measurement error: 0.500 Transducer timing error: 0.005 Navigation timing error: 0.005 Gyro timing error: 0.005 Heave timing error: 0.005 PitchTimingStdDev: 0.005 Roll timing error: 0.005 Sound Velocity speed measurement error: 0.000 Surface sound speed measurement error: 0.050 Tide measurement error: 0.010 Tide zoning error: 0.720 Speed over ground measurement error: 0.030 Dynamic Loading measurement error: 0.010 Static draft measurement error: 0.016 Delta draft measurement error: 0.007 StDev Comment: `éƒJ Ï…J`õ…JPõ…J°ð…J €…J@í…J°k€JàZ€J€Ó…Ja

Svp Sensor:

Time Stamp: 2006-001 00:00 Comments Svp #1: Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.312 Del taY: -0.142 Del taZ: 0.397 SVP #2: . . . . . . . . . . . . . Pitch Offset: 0.000 Roll Offset: 0.000

FA\_1010\_Reson8101\_end07.txt Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Time Stamp: 2007-001 00:00 Comments Svp #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.247 Del taY: -0. 138 Del taZ: 0.551 SVP #2: \_\_\_\_\_ Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Time Stamp: 2007-119 00:00 Comments Svp #1: \_ \_ \_ \_ \_ \_ 0.000 Pitch Offset: Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.247 Del taY: -0. 138 Del taZ: 0. 551 SVP #2: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Time Stamp: 2007-136 22:07 Comments Svp #1: Pitch Offset: 0.000 0.000 Roll Offset: Azimuth Offset: 0.000

Del taX: 0.247 Del taY: -0. 138 Del taZ: 0. 551 SVP #2: . . . . . . . . . . . . . Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Time Stamp: 2007-150 00:00 Comments Svp #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ 0.000 Pitch Offset: Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.247 Del taY: -0. 138 Del taZ: 0. 551 SVP #2: \_\_\_\_\_ Pitch Offset: 0.000 Rol I Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Time Stamp: 2007-150 19:04 Comments Svp #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.247 Del taY: -0. 138 Del taZ: 0. 551 SVP #2: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ 0.000 Pitch Offset: Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000

#### FA\_1010\_Reson8101\_end07.txt

Time Stamp: 2007-150 23:23 Comments Svp #1: . . . . . . . . . . . . . Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.247 Del taY: -0. 138 Del taZ: 0. 551 SVP #2: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Time Stamp: 2007-151 00:00 Comments Svp #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: 0.000 0.000 Roll Offset: Azimuth Offset: 0.000 Del taX: 0.247 Del taY: -0. 138 Del taZ: 0. 551 SVP #2: Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 2007-172 00:10 Time Stamp: Comments Svp #1: \_\_\_\_ Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.247 Del taY: -0.138 Del taZ: 0.551 SVP #2:

Pitch Offset: 0.000 0.000 Roll Offset: Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Time Stamp: 2007-176 00:00 Comments Svp #1: \_ \_ \_ \_ \_ Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.247 Del taY: -0. 138 Del taZ: 0. 551 SVP #2: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: 0.000 0.000 Roll Offset: Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Time Stamp: 2007-176 22:20 Comments Svp #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.247 Del taY: -0.138 Del taZ: 0.550 SVP #2: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 2007-197 00:00 Time Stamp: Comments Svp #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_

FA\_1010\_Reson8101\_end07.txt 0.000 Pitch Offset: Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.247 Del taY: -0.138 Del taZ: 0.550 SVP #2: -----Pitch Offset: 0.000 0.000 Roll Offset: Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 2007-252 00:00 Time Stamp: Comments Svp #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.247 Del taY: -0. 138 Del taZ: 0. 550 SVP #2: -----Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 WaterLine:

> Time Stamp: 2006-001 00:00 Comments Apply Yes WaterLine -0.240 Time Stamp: 2007-001 00:00 Comments Apply Yes WaterLine -0.243

## **1010 Offsets and Measurements - Summary**

2007 Measured Values

Measurement	IMU to RP*	8101 to RP*	IMU to 8101		Port Ant to 8101	RP* to Waterline
aka			SWATH1 x,y,z & MRU to Trans		Nav to Trans x,y,z	
Coord. Sys.	Caris	Caris	Caris		Caris	Caris
х	0.000	0.247	0.247	'	1.144	n/a
у	0.000	-0.138	-0.138	3	1.061	n/a
z	0.000	0.551	0.551		3.667	-0.243
				-		

\*IMU is RP (Reference Pt)

Vessel Offsets for 1010\_8101 are derived from the <u>Horizontal</u>, <u>Vertical</u> <u>& XYZ</u> worksheets in this spreadsheet.

Calculations Coord. Sys. Port Ant to 8101 8101 to RP\* IMU to 8101 **RP to Waterline** IMU (m) Theodolite 3.516 IMU (m) 3.516 IMU (m) 3.516 х Х х 0.011 0.011 0.011 У У у -1.183 -1.183 -1.183 z z z BM H x 3.271447 Port Antenna х 2.317 BM C х 0.000 y 0.425598 -0.886 0.000 у у z -1.37667 1.934 0.000 z z IMU -0.244 IMU to -1.199 BM C to IMU х Х to BM H 0.415 Port Antenna -0.897 у У х n/a -0.194 3.117 z z у n/a Ζ -1.183 BM H to 10.6 IMU to -0.138 х х Phase Ctr (cm) y Phase Ctr -16.8 У 0.247 BM C to Waterline -35.7 -0.551 measured z z measured х n/a у n/a BM H to 0.106 х z -0.940 Phase Ctr (m) У -0.168 Ζ -0.357 see Coord. Sys. IMU to 8101 Port Ant to 8101 **RP to Waterline** IMU to 8101 Theodolite IMU to -0.138 1.061 Х х х n/a 0.247 Phase Ctr У у 1.144 у n/a z -0.551 z -3.667 z 0.243 Coord. Sys. CARIS Coord. Sys. CARIS Coord. Sys. CARIS 0.247 1.144 n/a х Х Х -0.138 1.061 n/a У У У 0.551 z 3.667 -0.243 7

# 1010 Offsets and Measurements - Summary

Port Ant to Stb	Port Ant to Stbd Ant		IMU to Port Antenna		IMU to	Heave
		Caris	Pos/Mv		Caris	Pos/Mv
Scalar Distance	1.840	-0.897	-1.199		-0.011	-1.176
		-1.199	-0.897		-1.176	-0.011
		-3.117	-3.117		-0.243	-0.243
				•		

Port Ant t	o Stbd	Ant	IMU to Po	rt Anter	nna		IMU to Heav	е	
Port Ant (m)	х	2.317	IMU (m)	х	3.516	IMU (m)		у	0.011
	У	-0.886		У	0.011	x is n/a		Z	-1.183
	z	1.934		z	-1.183				
						Heave Pt	(m)		
Stbd Ant (m)	х	2.324	Port Ant (m)	х	2.317	(centerline)		У	0.000
	У	0.953		У	-0.886				
	z	1.878		z	1.934	BM C to Waterl	ine (m)		-0.940
						measured scala	ar dist		
						BM C			
						x&y are n/a		z	0.000
						BM C to Waterl	ine (m)		
						(Heave Pt)	- ( )	z	-0.940
						IMU to LCG		х	-1.176
							See IN	/U to F	leave tab

Port Ant to S	Stbd Ant	IMU to	Port Anten	na	IN	IU to Heave	
			х	-1.199		х	-1.176
Scalar Distance	1.840		У	-0.897		У	-0.011
			z	3.117		Z	0.243
		Coord. Sys.	Pos/Mv		Coord. Sys.	Pos/Mv	
			х	-1.199		× ×	-1.176
			У	-0.897		У	-0.011
			z	-3.117		z	-0.243
					See IMU to Heav	r <u>e tab</u>	

# **Description of Offsets for Launch 1010**

### All Values Shown are in CARIS Coordinates

The Ship Reference Frame (SRF) for Launch 1010 was based from benchmark (BM) C as the 0 point. Physical locations were measured with x,y,z offsets from this point. These locations were used to calculate offsets of items with respect to each other, as described for each offset.



IMU to 8101				
х	у	Z		
0.247	-0.138	0.551		

The physical positions of the IMU and the phase center of the 8101 with respect to the Ship Reference Frame were measured by NOAA personnel. These physical measurements were used to calculate the xyz offsets from the IMU to BM H. Measurements from BM H to the Phase Center of the 8101 were collected by NOAA personnel while the boat was secured in the davit and thought to be as level as possible. The measured offsets from BM H to the phase center were then added to the offset from the IMU to BM H. The result is the offset from the IMU to the phase center of the transducer. The values in the X and Y fields are transposed and the inverse of the Z value is used to give the offsets in CARIS coordinates.

Port Ant to 8101				
х	У	Z		
1.144	1.061	3.667		

NOAA personnel calculated the distance between the port antenna and the phase center of the port antenna subtracting the IMU to Port Antenna value from the IMU to Phase Center value.

RP to Waterline				
Х	У	Z		
N/A	N/A	-0.243		

The vertical distance from BM A and B to the waterline was measured by FAIRWEATHER personnel using a steel tape and bubble level. With the knowledge of the two BMs height above the IMU, the waterline height above the IMU could be calculated. On launch 1010, the IMU is used as the reference point.

Port Ant to Stbd Ant	
Scalar Distance	
1.840	

The location of the phase center of the port and starboard POS/MV antennas were measured by NOAA personnel with respect to the SRF. The scalar distance between the phase centers was then calculated.

IMU to Port Antenna				
х	у	Z		
-0.897	-1.199	-3.117		

The location of the IMU and the location of the port antenna were measured by NOAA personnel with respect to the Ship Reference Frame (SRF). The xyz offsets from the IMU to the port antenna could be calculated from these physical locations.

I	MU to Heav	e
х	у	Z
-0.011	-1.176	-0.243

The heave point was positioned differently on each of the axes. The distance for the longitundinal axis was determined as described in the "IMU to Heave" tab in this workbook. The athwart ships axis was the vessel centerline. Lastly, the waterline was used as the height of the heave point, which was calculated earlier in 'RP to Waterline'.

# 1010 Vessel Diagram

All Values Shown are in Theodolite Coordinates



# FAIRWEATHER

# Multibeam Echosounder Calibration

# Launch 1010

Vessel

7/17/2007	197	Kodiak, Womans Bay	
Date	Dn	Local Area	
8101			
MBES Syster	n	MBES System Location	Date of most recent EED/Factory Check
2701011			
Sonar Serial I	Number		Processing Unit Serial Number
Sonar Mounti	ng Confi	guration	Date of current offset measurement/verification
POSMV v.4			
Description of	f Positior	ing System	Date of most recent positioning system calibration

# Acquisition Log

7/17/2007 197	Kodiak		Flat calm		
Date Dn	Local Area		Wx		
			10-40m		
Bottom Type			Approximate Water Depth		
Dowling, Argento, Mo	rgan, Gonsalves				
Personnel on board					
Comments					
No Trueheave logged					
TrueHeave filename					
071971628	1628	57/43/38.3	152/31/23.73		22.8
SV Cast #1 filename	UTC Time	Lat	Lon	Depth	Ext. Depth (Cast#2 backtimed to 1
071972105	2105	57/42/53.6	152/31/56.3		27.6
SV Cast #2 filename	UTC Time	Lat	Lon	Depth	Ext. Depth
SV Cast #2 filename	UTC Time	Lat	Lon	Depth	Ext. Depth

# ROLL

SV Cast #	XTF Line Filename	Hd	Speed (kts)	Remarks
1	197-1705, 1709	035/215	7.0	
1	197-1714, 1719	035/215	6.0	Waked out at beginning of line 1719 (use for timing)
1	197-1725, 1729	035/215	6.5	Acquired post hard starbord turns
1	197-1734, 1739	035/215	6.5	Acquired post hard starbord turns
1	Port_Turn_2, Port_Turn_3	035/215	7.0	Acquired post hard port turns
1	Port_Turn_4, Port_Turn_5	035/215	7.2	Acquired post hard port turns
1	Jen_Roll_1, Jen_Roll_2	035/215	6.3	Transducer cranked down by Dowling
1	Jen_Roll_3, Jen_Roll_4	035/215	6.3	Transducer cranked down by Dowling
1	Jen_Roll_5, Jen_Roll_6	035/215	6.4	Acquired post hard port turns
1	Jen_Roll_7, Jen_Roll_8	035/215	7.2	Acquired post hard port turns
1	Jen_Roll_9, Jen_Roll_10	035/215	7.1	Acquired post hard starbord turns
1	Jen_Roll_11, Jen_Roll_12	035/215	6.5	Acquired post hard starbord turns
1	Adam_Roll_1, Adam_Roll_2	035/215		Transducer leisurely cranked down

## PITCH

SV Cast #	XTF Line Filename	Hd	Speed (kts)	Remarks
2	Pitch_2	247	5.5	
2	Pitch_4	066	5.5	
2	Pitch_5	245	5.3	
2	Pitch_6	065	5.3	

# HEADING/YAW

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
2	Z	245		
2	Pitch_8	065		
2	Pitch_9	242		
2	Pitch_10	066		

## **REFERENCE SURFACE**

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks

# Processing Log

7/17/2007 197 Argento		
Date Dn Personnel		
✓ Data converted> HDCS_Data	in CARIS	
TrueHeave applied	No trueheave logged	
SVP applied 🔽	previous in time	
Tide applied 🗹	Kodiak verified - foo	
Zone file	N/A	
Lines merged		
Data cleaned to remove gross fliers	✓ (mog)	
	Compute correctors in this order	
1. Precise Timing	2. Pitch bias 3. Heading bias 4.	Roll bias
Do not enter/app	ly correctors until all evaluations are complete and analyzed.	

Calibrating Hydrographer(s)

PATCH TEST RESU	JLTS/CORRECTOR	S			Yaw (deg)
Evaluators	Latency (sec)	Pitch (deg)	Roll (deg)		
adam/nick A	0.00		2.85		0.80
matt B	0.00	-1.10		2.97	0.94
brenna C	0.00		2.85		
pat/allison D	0.00	-1.05	2.94		0.93
mark/steph E	0.00	-1.22	2.87		0.90
toshi/cathleen F	0.00	-0.90		2.84	0.85
mog	0.00	-0.95	2.91		0.90
FOO (Post SmTide)	0.00		2.91		
Grayed out signifies	s outlier-not used in av	/erage			
			0.00		0.00
Averages	0.00	-1.04	2.89		0.89
Standard Deviation	0.00	0.13	0.04		0.05
FINAL VALUES		-1.04	2.91		0.89
<b>F</b> ired Malazza has a dam					
Final Values based on	Average minus outlie	rs (roll based on mog value based of	n dozens of roll lines)		
Final Values analyzed/c	compiled by:	mog/too			
Value from standard devi	ation of Heading offset \	/alues 0.	MRU Align Stal	Dev Gyro	11 - I-
value from sum of squ	ares standard deviatio	ons of pitch and roll offsets $0$ .	<b>13</b> MRU Aligh Sta	Dev Roll/P	itch
Results are	e for HVF File Named:	FA_1010_Reson8101			
✓ HVF Hyd	rographic Vessel File	created or updated with current offse	ts		
Name:				Date:	
NARRATIVE					

RPM	Speed (m/s)	Speed (knots)	mog-Ave	bj-Ave	kb-Ave	Std. Dev.	Average
0	0	0	0	0	0	0	0
620	2.58	5	-0.044685862	-0.040728915	-0.037282951	0.003704394	-0.040899243
790	3.10	6	-0.02870312	-0.039467254	-0.023804602	0.00801229	-0.030658325
1040	3.98	7.7	0.019162864	0.017309788	0.033217055	0.008698614	0.023229902
1235	4.60	8.9	0.048612724	0.048718001	0.060843062	0.007030995	0.052724596
1530	5.17	10	0.096159255	0.094792289	0.115960382	0.011846529	0.102303975
1696	5.37	10.4	0.083489759	0.080253529	0.101141624	0.011242583	0.088294971





Blue cells used in computation of Delta Draft StDev used in TPE

Ave. StDev 0.006862



# **NOAA POS/MV Calibration Report**

Ship:	FAIRWEATH	IER			Vessel:	1010				
Date:	3/30/2007		-		Dn:	08	9	_		
Personnel:	Walker, Gonsalve	s, Mills								
PCS Serial	#	2564			IMU Seria	I #		294		
IP Address	:	129.100.1.23	1			-				
POS contro	oller Version (Use	Menu Help >	About)		3.3.2.2					
POS Versio	on (Use Menu View Vers	<pre>&gt; Statistics)</pre>		MV320 v4						
	Primary Receiver			BD950 SN:462	4A70264					
	Secondary Receiv	ver		BD950 SN:462	2A68956					
Calibrat	ion area									
Location:	Nichols Passage,	AK								
Approxima	te Position:			Lat	55	1	7	3		
DGPS Beac Frequency:	con Station:		Annette Isla 323	Lon and	131	39	9	55		
Satellite	Constellatio	n		(Use View> GF	'S Data)					
Primary C	SPS				Second	ary GPS	6			
Sketch gene	eral SV configuratio	n			Note any o	difference	s from	Primary GPS	Receiver	
Primary GPS Se	condary GPS Auxiliary 1 GPS Au	oiliary 2 GPS			Primary GPS	Secondary GPS	Auxiliary 1	GPS Auxiliary 2 GPS		



1.600

PDOP

(Use View> GAMS Solution)



# POS/MV Configuration

Gams Parameter Setup

#### Settings

(Use Settings > Installation > GAMS Intallation)

Fwo Antenna Separation (m)	1.840
leading Calibration Threshold (deg)	0.100
Heading Correction (deg)	0.000
aseline Vector	
K Component (m)	0.000
Y Component (m)	0.000
7 Component (m)	0.000

**Configuration Notes:** 

### **POS/MV** Calibration

Calibration	Procedure:
-------------	------------

(Refer to POS MV V3 Installation and Operation Guide, 4-25)

0.1

Start time:	1947
End time:	1948
Heading acc	uracy achieved for calibration:

#### **Calibration Results:**

Gams Parameter	er Setup	(Use Settings	> Installation	n > GAMS Inta	Illation)
G	iAMS Parameter Setup	ip		1	хI
	Two Antenna Separation (m)	)	1.827		
	Heading Calibration Thresho	ld (deg)	0.100		
	Heading Correction (deg)		0.000		
	Baseline Vector		0.001		
	Y Component (m)		1.827		
	Z Component (m)		0.029		
		ose Ar	ply	View	
GAMS Status Online Save Settings	Yes Yes				
Save POS Settings on PC File Name: 1010_089_POS	MV	(Use File > Sto	ore POS Set	tings on PC)	

#### The POS/MV uses a Right-Hand Orthogonal Reference System

The right-hand orthogonal system defines the following:

- The x-axis is in the fore-aft direction in the appropriate reference frame.
- The y-axis is perpendicular to the x-axis and points towards the right (starboard) side in the appropriate reference frame.
- The z-axis points downwards in the appropriate reference frame.

#### The POS/MV uses a Tate-Bryant Rotation Sequence

Apply the rotation in the following order to bring the two frames of reference into complete alignment:

a) Heading rotation - apply a right-hand screw rotation θz about the z-axis to align one frame with the othε

b) Pitch rotation - apply a right-hand screw rotation θy about the once-rotated y-axis to align one frame with the other.

c) Roll rotation - apply a right-hand screw rotation  $\theta x$  about the twice-rotated x-axis to align one frame with the other.

#### SETTINGS

Input/Output Ports

COM1

COM2

COM3

(Use Settings > Input/Output Ports) Input/Output Ports Set-up COM1 COM2 COM3 COM4 COM5 Flow Control None Hardware XON/XOFF Baud Rate 9600 💌 Parity None Even Odd Stop Bits Data Bits C 7 Bits I Bit C 2 Bits 8 Bits NMEA Output 
 Striptic

 SPRDID

 SPRDID

 SPRDID

 SINGGK

 VISUTC

 INPPS
 Output Select Roll Positive Sense Port Up C Starboard Up Pitch Positive Sense Bow Up C Stern Up NMEA 💌 Heave Positive Sense • Heave Up • Heave Down Input Select None -Close Apply Input/Output Ports Set-up COM1 COM2 COM3 COM4 COM5 Flow Control C None C Hardware C XON/XOFF Parity © None C Even C Odd Data Bits Stop Bits Baud Rate C 7 Bits • 1 Bit 19200 💌 8 Bits C 2 Bits Binary Output Output Select Roll Positive Sense Port Up C Starboard Up Frame
 Image: Sensor 1
 Image: Sensor 2 Update Rate 25 Hz Binary 🔹 Formula Select -Input Select None 💌 Close Apply Input/Output Ports Set-up Y COM1 COM2 COM3 COM4 COM5 Parity None Even Odd Data Bits Flow Control None Hardware XON/XOFF Stop Bits • 1 Bit Baud Rate 9600 👻 C 7 Bits 8 Bits C 2 Bits Output Select None 💌 Input Select Base GPS Input Base 1 GPS 💌 Input Type RTCM 1 or 9 💌 Line
C Serial C Modern Modern Settings Close Apply put/Output Ports Set-up COM1 COM2 COM3 COM4 COM5 Parity None Even Odd Flow Control None Hardware XON/XOFF Data Bits Stop Bits Baud Rate I Bit 9600 -C 7 Bits 8 Bits C 2 Bits Output Select None 💌 Input Select None

Close

Apply

COM4

### **SETTINGS Continued**

### COM5

put/Uutput Ports Set-up	
сом1 сом2 сом3 сом4	СОМ5
Baud Rate 9600 💌	Parity         Data Bits         Stop Bits         Flow Con           © None         C 7 Bits         © 1 Bit         © None           C Even         © 8 Bits         C 2 Bits         C X0NX
Output Select	
Input Select	
	Close Apply
Use Settings > Heave	e)
Teave Filter	×
C Z Altitude	
<ul> <li>Heave Filter</li> <li>Heave Bandwidth (s</li> </ul>	sec) 20.000
Heave Filter     Heave Bandwidth (s	sec) 20.000
<ul> <li>Heave Filter</li> <li>Heave Bandwidth (s</li> <li>Damping Ratio</li> </ul>	sec) 20.000
<ul> <li>Heave Filter</li> <li>Heave Bandwidth (s</li> <li>Damping Ratio</li> <li>Ok</li> </ul>	Sec) 20.000
<ul> <li>Heave Filter</li> <li>Heave Bandwidth (s</li> <li>Damping Ratio</li> <li>Ok</li> </ul>	sec) 20.000 0.707 Close Apply
Heave Filter     Heave Bandwidth (s     Damping Ratio     Ok     Jse Settings > Events;	sec) 20.000 0.707 Close Apply
Heave Filter     Heave Bandwidth (s     Damping Ratio     Ok     Se Settings > Events     Events	sec) 20.000 0.707 Close Apply
<ul> <li>Heave Filter Heave Bandwidth (s Damping Ratio</li> <li>Ok</li> <li>Jse Settings &gt; Events;</li> <li>Events</li> </ul>	sec) 20.000 0.707 Close Apply )
Heave Filter Heave Bandwidth (s Damping Ratio Ok Jse Settings > Events Events Event 1 © Positive Edge	sec) 20.000 0.707 Close Apply )
Heave Filter Heave Bandwidth (s Damping Ratio Ok Jse Settings > Events; Events Event 1 © Positive Edge C Nexting Filter	e Trigger
Heave Filter Heave Bandwidth (s Damping Ratio Ok Jse Settings > Events Events Event 1 © Positive Edge © Negative Edge	sec) 20.000 0.707 Close Apply ) e Trigger ge Trigger
Heave Filter Heave Bandwidth (s Damping Ratio     Ok     Ok Jse Settings > Events Events Event 1      Positive Edge     Negative Edge Event 2	sec) 20.000 0.707 Close Apply e Trigger ge Trigger
Heave Filter Heave Bandwidth (s Damping Ratio Ok Jse Settings > Events Event 1 Event 1 © Positive Edge © Negative Edge Event 2	e Trigger
<ul> <li>Heave Filter Heave Bandwidth (s Damping Ratio</li> <li>Ok</li> <li>Ok</li> <li>Jse Settings &gt; Events</li> <li>Event 1</li> <li>Positive Edge</li> <li>Negative Edge</li> <li>Event 2</li> <li>Positive Edge</li> </ul>	e Trigger
<ul> <li>Heave Filter Heave Bandwidth (s Damping Ratio</li> <li>Ok</li> <li>Ok</li> <li>Jse Settings &gt; Events;</li> <li>Event 1</li> <li>Positive Edge</li> <li>Negative Edge</li> <li>Event 2</li> <li>Positive Edge</li> <li>Negative Edge</li> <li>Negative Edge</li> </ul>	sec) 20.000 0.707 Close Apply e Trigger ge Trigger ge Trigger ge Trigger
Heave Filter Heave Bandwidth (s Damping Ratio Ok Se Settings > Events Events Event 1 © Negative Edge Event 2 Event 2 © Negative Edge	e Trigger

#### Events

Heave Filter

#### INSTALLATION



#### User Parameter Accuracy

### (Use Settings > Installation > User Accuracy)

Attitude (deg)	0.050	
Heading (deg)	0.050	
Position (m)	2.000	
Velocity (m/s)	0.500	

### Frame Control

(Use Tools > Config)

Navigator Configuration	×
Frame Control	Auxiliary GPS Position
C User Frame	C Use regardless of status C Do not use
Primary GPS Measurement	GAMS Disable GAMS Solution
C Use regardless of status	
O Do not use	
Ok C	lose Apply

## **GPS** Receiver Configuration

(Use Settings> Installation> GPS Receiver Configuration)

Primary GPS Receiver

Secondary GPS Receiver

s Receiver Configuration			
Primary GPS Receiver Sec	condary GPS Rec	eiver	
Primary GPS GPS Output Rate 1 Hz	GPS 1 Port Baud Rate 9600	-	
Auto Configuration © Enabled © Disabled	Parity None Even Odd	Data Bits © 7 Bits © 8 Bits	Stop Bits © 1 Bit © 2 Bits
[	Ok	Close	Apply
s Receiver Configuration	condary GPS Pac	aivar ]	
Secondary GPS GPS Output Rate	GPS 2 Port Baud Rate 9600	•	
Auto Configuration © Enabled © Disabled	Parity None Even Odd	Data Bits © 7 Bits © 8 Bits	Stop Bits © 1 Bit © 2 Bits
		o 1	• • 1



FA\_1018\_Reson8101\_end07.txt Vessel Name: FA\_1018\_Reson8101.hvf Vessel created: December 19, 2006

Depth Sensor:

Sensor Class: Swath Time Stamp: 2007-001 00:00 Transduer #1: Pitch Offset: -0.240 Roll Offset: 2.890 Azimuth Offset: 0.260 Del taX: 0.286 Del taY: -0.141 Del taZ: 0.551 Manufacturer: Reson Model: sb8101 Serial Number: 35737 Depth Sensor: Sensor Class: Swath Time Stamp: 2007-224 00:00 Transduer #1: \_\_\_\_\_ Pitch Offset: -0.240 Roll Offset: 3.200 Azimuth Offset: 0.260 Del taX: 0.286 Del taY: -0.141 Del taZ: 0.551 Manufacturer: Reson sb8101 Model: Serial Number: 35737 Depth Sensor: Sensor Class: Swath Time Stamp: 2007-236 00:00 Transduer #1: Pitch Offset: -0.240 Roll Offset: 3.630 Azimuth Offset: 0.260 Del taX: 0.286 Del taY: -0.141 Del taZ: 0.551 Manufacturer: Reson Model: sb8101 Serial Number: 35737

Navigation Sensor:

#### FA\_1018\_Reson8101\_end07.txt

Time Stamp: 2007-001 00:00

Comments POS time mistakenly set to GPS time requiring a 14  $\sec$  time correction

Latency 14.000 Del taX: 0.000

Del taY: 0.000 Del taZ: 0.000

Manufacturer: Applanix Model: POS/MV v4 Serial Number: 2560

Time Stamp: 2007-102 00:00

Comments Time changed in POS to UTC - 14 sec time correction deleted Latency 0.000 DeltaX: 0.000 DeltaY: 0.000 DeltaZ: 0.000

Manufacturer: Applanix Model: POS/MV v4 Serial Number: 2560

Gyro Sensor:

Time Stamp: 2007-001 00:00

Comments POS time mistakenly set to GPS time requiring a 14 sec time correction

Latency 14.000

Time Stamp: 2007-102 00:00

Comments Time changed in POS to UTC - 14 sec time correction deleted Latency  $0.\,000$ 

#### Heave Sensor:

Time Stamp: 2007-001 00:00

Comments True Heave Enabled/POS time mistakenly set to GPS time requiring a 14 sec time correctionPOS time mistakenly set to GPS time requiring a 14 sec time correction

Apply Yes Latency 14.000 DeltaX: 0.000 DeltaY: 0.000 Offset: 0.000 Manufacturer: Applanix Model: POS/MV v4 Serial Number: 2560

Time Stamp:

#### FA\_1018\_Reson8101\_end07.txt

Comments Time changed in POS to UTC - 14 sec time correction deleted Apply Yes Latency 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Offset: 0.000 Manufacturer: Appl ani x POS/MV v4 Model: Serial Number: 2560 Pitch Sensor: Time Stamp: 2007-001 00:00 Comments POS time mistakenly set to GPS time requiring a 14 sec time correcti on Apply Yes Latency 14.000 Pitch offset: 0.000 Manufacturer: Appl ani x POS/MV v4 Model: Serial Number: 2560 Time Stamp: 2007-102 00:00 Comments Time changed in POS to UTC - 14 sec time correction deleted Apply Yes Latency 0.000 Pitch offset: 0.000 Manufacturer: Appl ani x POS/MV v4 Model: Serial Number: 2560 Roll Sensor: 2007-001 00:00 Time Stamp: Comments POS time mistakenly set to GPS time requiring a 14 sec time correction Apply Yes Latency 14.000 Roll offset: 0.000 Manufacturer: Appl ani x Model: POS/MV v4 Serial Number: 2560 Time Stamp: 2007-102 00:00 Comments Time changed in POS to UTC - 14 sec time correction deleted Apply Yes Latency 0.000 Roll offset: 0.000

	FA_1018_Reson8101_end07.txt
Manufacturer:	Appl ani x
Model:	PÖS∕MV ∨4
Serial Number:	2560

Draft Sensor:

Time Stamp: 2007-001 00:00 Apply Yes Comments DDSSM Entry 1) Entry 2) Draft: 0.000 Speed: 0.000 Draft: 0.039 Speed: 5.015 Entrý 3) Entry 4) Speed: 6.026 Draft: 0.061 Speed: 7.425 Draft: 0.110 Speed: 8.242 Entry 5) Draft: 0.151 Entry 6) Draft: 0.133 Speed: 9.350 Entry 7) Draft: 0.074 Speed: 10.341 Entry 8) Draft: 0.049 Speed: 11.955

TPE

Time Stamp: 2007-001 00:00 Comments **Offsets** Motion sensing unit to the transducer 1 X Head 1 0.286 Y Head 1 -0.141 Z Head 1 0.551 Motion sensing unit to the transducer 2 X Head 2 0.000 Y Head 2 0.000 Z Head 2 0.000 Navigation antenna to the transducer 1 X Head 1 1.184 Y Head 1 0.960 Z Head 1 3.711 Navigation antenna to the transducer 2 X Head 2 0.000 Y Head 2 0.000 Z Head 2 0.000 Roll offset of transducer number 1 0.000 Roll offset of transducer number 2 0.000 Heave Error: 0.050 or 5.000'' of heave amplitude. Measurement errors: 0.007 Motion sensing unit alignment errors Gyro: 0. 090 Pi tch: 0.060 Rol I: 0.060 Gyro measurement error: 0.020 Roll measurement error: 0.020 Pitch measurement error: 0.020 Navigation measurement error: 0.500 Transducer timing error: 0.005 Navigation timing error: 0.005 Gyro timing error: 0.005 Heave timing error: 0.005 PitchTimingStdDev: 0.005 Pable timing error: 0.005 Roll timing error: 0.005 Sound Velocity speed measurement error: 0.007 Surface sound speed measurement error: 0.007 Page 4

 $FA\_1018\_Reson8101\_end07.txt$ Ti de measurement error: 0.007 Ti de zoni ng error: 0.030 Speed over ground measurement error: 0.030 Dynamic Loadi ng measurement error: 0.010 Static draft measurement error: 0.016 Del ta draft measurement error: 0.050 StDev Comment: `éfJ Ï...J`õ...JPõ...J°Õ...J €...J@Í...J°k€JàZ€J€Ó...Ja

Svp Sensor:

Time Stamp: 2007-001 00:00 Comments Svp #1: Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.286 Del taY: -0. 141 Del taZ: 0. 551 SVP #2: 0.000 Pitch Offset: 0.000 Roll Offset: Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Time Stamp: 2007-224 00:00 Comments Svp #1: . . . . . . . . . . . . . . Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.286 Del taY: -0.141 Del taZ: 0.551 SVP #2: . . . . . . . . . . . . . Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 2007-236 00:00 Time Stamp: Comments Svp #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_

 FA\_1018\_Reson8101\_end07.txt

 Pitch Offset:
 0.000

 Roll Offset:
 0.000

 Azimuth Offset:
 0.000

 Del taX:
 0.286

 Del taY:
 -0.141

 Del taZ:
 0.551

 SVP #2:
 ---- 

 Pitch Offset:
 0.000

 Roll Offset:
 0.000

 Azimuth Offset:
 0.000

 Del taX:
 0.000

## WaterLine:

Time Stamp: 2007-001 00:00

Comments Apply Yes WaterLine -0.280
# 1018 Offsets and Measurements Summary

Measurement	IMU to RP*	8101 to RP*	IMU to 8101		Port Ant to 8101	1	RP* to Waterlin	е
aka			SWATH1 x,y,z & MRU to Trans		Nav to Trans x,y,z			
Coord. Sys.	Caris	Caris	Caris		Caris			Caris
х	0.000	0.286	0.286		1.184			n/a
у	0.000	-0.141	-0.141		0.960			n/a
Z	0.000	0.551	0.551		3.711			-0.276
				•				
•	*IMU is Reference	e Point						

Vessel Offsets for 1018\_8101 are derived from the <u>Horizontal</u>, <u>Vertical</u> <u>& XYZ</u> worksheets in this spreadsheet.

2007 Measured Value

Calculation	IS								
Coord. Sys.	8101 to RP*	IM	U to 8101		Port A	nt to 8101	RP to V	Vaterline	
<b>Theodolite</b>		IMU (m)	Х	3.54587	IMU (m)	x 3.545867	IMU (m)	Х	3.546
			у	-0.01516		y -0.01516		У	-0.015
			Z	-0.85883		z -0.85883		Z	-0.859
		BM H	х	3.30204	Port Ant (m)	x 2.445	BM C	х	0.000
			У	0.43081		y -0.913		У	0.000
			Z	-1.0485		z 2.302		Z	0.000
		IMU	х	-0.244	IMU to	x -1.101	BM C to IMU		
		to BM H	У	0.446	Port Antenna	y -0.898		Х	n/a
			Z	-0.190		z 3.161		У	n/a
								Z	-0.859
		BM H to	Х	10.3	IMU to	x -0.141			
		Phase Ctr	(cm) y	-16.0	Phase Ctr	y 0.286	BM C to Waterlin	ne (m)	
		measured	z	-36.1		z -0.551		z	-0.583
		BM H to	x	0.103					
		Phase Ctr	(m) y	-0.160					
			Z	-0.361					
Coord Sve	See	IM	LI to 8101		Port A	nt to 8101	RP to V	Vatorlino	
Theodolite		IMLI to	Y X	-0 141	IULA	x 0.960		Y	n/a
meddonte		Phase Ctr	v v	0.286		v 1 184		v	n/a
		1 11836 01	у –	0.200		y 1.104		у 7	0.276
			Z	-0.551		2 -3.711		Z	0.276
		Coord. Sys.	<b>CARIS</b>		Coord. Sys.	CARIS	Coord. Sys.		
			х	0.286		x 1.184		х	n/a
			У	-0.141		y 0.960		у	n/a
			z	0.551		z 3.711		z	-0.276

# 1018 Offsets and Measurements Summary

	Port Ant to Stbd Ant		IMU to Port Ant				IMU to Heave		
				Caris	Pos/M	V	Caris		Pos/My
	Scaler Distance	1.834		-0.898	-1.1	01	0.015		-1.114
				-1.101 -3.161	-0.8 -3.1	98 61	-1.114 -0.276		0.015 -0.276

Port Ant	to Stbd	Ant	IMU 1	to Port	Ant	IMU to	Heave	
Port Ant (m)	х	2.445	IMU (m)	х	3.546	IMU (m)	У	-0.015
	у	-0.913	2	у	-0.015	x is n/a	z	-0.859
	z	2.302	:	z	-0.859			
						Heave Pt (m)		
Stbd Ant (m)	х	2.445	Port Ant(m)	x	2.445	(centerline)	У	0.000
	У	0.921	2	у	-0.913		_	
	z	2.275	2	z	2.302	BM C to Waterlin	ne (m)	-0.583
						measured scalar	dist	
						BM C		
						x&y are n/a	Z	0.000
						BM C to Waterlir	ne (m)	
						(Heave Pt)	z	-0.583
						IMU to Hv	х	-1.114
						See	IMU to H	eave tab



# **Description of Offsets for Launch 1018**

#### All Values Shown are in CARIS Coordinates





IMU to 8101							
х	у	Z					
0.286	-0.141	0.551					

The physical positions of the IMU and the phase center of the 8101 with respect to the Ship Reference Frame were measured by NOAA personnel. These physical measurements were used to calculate the xyz offsets from the IMU to BM H. Measurements from BM H to the Phase Center of the 8101 were collected by NOAA personnel while the boat was secured in the davit and thought to be as level as possible. The measured offsets from BM H to the phase center were then added to the offset from the IMU to BM H. The result is the offset from the IMU to the phase center of the transducer. The values in the X and Y fields are transposed and the inverse of the Z value is used to give the offsets in CARIS coordinates.

Port Ant to 8101							
х	x y						
1.184	0.960	3.711					

NOAA personnel calculated the distance between the port antenna and the phase center of the port antenna subtracting the IMU to Port Antenna value from the IMU to Phase Center value.

RP to Waterline							
х	у	z					
N/A	N/A	-0.276					

The vertical distance from BM A and B to the waterline was measured by FAIRWEATHER personnel using a steel tape and bubble level. With the knowledge of the two BMs height above the IMU, the waterline height above the IMU could be calculated. On launch 1010, the IMU is used as the reference point.

Port Ant to Stbd Ant	
Scalar Distance	
1.834	

The location of the phase center of the port and starboard POS/MV antennas were measured by NOAA personnel with respect to the SRF. The scalar distance between the phase centers was then calculated.

IMU to Port Antenna							
х	у	z					
-0.898	-1.101	-3.169					

The location of the IMU and the location of the port antenna were measured by NOAA personnel with respect to the Ship Reference Frame (SRF). The xyz offsets from the IMU to the port antenna could be calculated from these physical locations.

IMU to Heave							
х	у	z					
0.015	-1.114	-0.276					

The heave point was positioned differently on each of the axes. The distance for the longitundinal axis was determined as described in the "IMU to Heave" tab in this workbook. The athwart ships axis was the vessel centerline. Lastly, the waterline was used as the height of the heave point, which was calculated earlier in 'RP to Waterline'.

# 1018 Vessel Diagram

#### All Values Shown are in Theodolite Coordinates



# FAIRWEATHER Multibeam Echosounder Calibration

Multibeam Echosounder Calibration			Launch 101	8	_			
				Vessel				
4/9/2007	099		Ketchikan					
Date	Dn		Local Area					
Gonsalves,	Johnston, Bro	wn, Froelich						
Calibrating I	Hydrographer(	s)						
Reson 8101	1		1		1			
MBES Syste	em		MBES System Location		Date of mos	t recent EED/F	actory Check	
35737					1			
Sonar Seria	al Number				Processing	Unit Serial Nun	nber	
Sonar Mour	nting Configura	ation			Date of curr	ent offset meas	surement/verif	ication
					1			
Description	of Positioning	System			Date of mos	t recent positio	ning system c	alibration
	-					·		
Acquisiti	on Log							
4/9/2	2007 099		Ketchikan		Calm			
Date	Dn		Local Area		Wx			
					40m			
Bottom Type	е				Approximate	Water Depth		
Consolves	Johnston Bro	wp Fraalich						
Personnel o	on board	wii, i ioelicii						
Comments								
<b>T</b> U 4040 <b>D</b>								
TH_1018_D	0N099 filename							
Thericave	mename							
07099171		17:11	55/19/59	-131/37/52		57.1		<u> </u>
SV Cast #1	filename	UTC Time	Lat	Lon		Ext. Depth	Bk time to	For lines
07099185		18:51	55/16/28	-131/40/26		77.2		1
SV Cast #2	filename	UTC Time	Lat	Lon		Ext. Depth	Bk time to	For lines
07099203		I	55/11/29	-131/37/36		81.1	I	1
SV Cast #3	filename	UTC Time	Lat	Lon		Ext. Depth	Bk time to	For lines

# ROLL

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
70991851.ex	Roll1	270	4.8	Kurt's
	Roll2	090	4.6	Kurt's
	Roll3	270	4.8	Bonnie's
	Roll4	090	4.6	Bonnie's
	Roll5	270	4.7	Mike's
	Roll6	090	4.6	Mike's

# PITCH

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
070991711.ex	pitch1	100	4.5	
	pitch2	292	4.5	
	pitch3	BAD	BAD	
	pitch4	292	4.5	
	pitch5	100	4.5	
	pitch6	295	4.5	
	-			-

### **HEADING/YAW**

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
070991711.ex	HEADING1	120	4.5	
	HEADING2	295	4.5	
	HEADING3	117	4.5	
	HEADING4	295	4.5	

# **REF SURFACE**

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
70992033	099-2053			Reference surface on 11fm shoal
70992033	099-2055 to 2101			

# Processing Log

Date	Dn	Personnel			
~	Data converted> HI	DCS_Data in CARIS			
$\checkmark$	TrueHeave applied	TH_1018_DN099.000	(kb)		
[	✓ SVP applied	kb			
	✓ Tide applied	kb - No zoning used fo	r patch lines over wreck - ou	utside zoning file	
		Zone file			
		Lines merged 🗸			
	Data alaonad				
	Data cleaned	to remove gross mers 💟			
		Compute c	orrectors in this order		
	1. Precise Timing	2. Pitch bias	3. Heading	bias 4. Roll	bias
PATCH TE Evaluators mog keb olj	ST RESULTS/CORRE	ECTORS Latency (sec) 14.00 14.00 14.00	Pitch (deg) -0.25 -0.30 -0.18	<b>Roll (deg)</b> 2.90 2.87 2.90	Yaw (deg) 0.20 0.22 0.36
	Averages	14.00	-0.24	2.89	0.26
St	andard Deviation FINAL VALUES	0.00 14.00	0.06 -0.24	0.02 2.89	0.09
Fin	al Values based on	Group Average			
Result	ting HVF File Name	FA_1018_Reson8101			
	MRU MRU Alig	J Align StdDev gyro 0. n StdDev Roll/Pitch 0.	09 Value from standard 06 Value from sum of s	deviation of Heading offset quares standard deviations of	values of pitch and roll offset

#### NARRATIVE

Time on the POSMV was mistakenly set to GPS time on launches for all data acquired prior to DN100. This resulted in a latency value of 14.00 seconds which is equivalent to the time difference between GPS and UTC time. GPS time is ahead 14 seconds. Following this discovery the POSMV was corrected to log UTC time on both launches. Two lines of offset values have been added to the HVFs for 1018. The first set of offsets include 14 seconds entered into the time correction field for Navigation, Gyro, Heave, Ptich, and Roll, and should be used for all data collected on and before DN100. The second set has the time correction field set to zero and should be used for all data collected on and after DN102. Values for Pitch, Roll and Yaw in both set of offsets were taken from the average bias values shown above.

HVF Hydrographic Vessel File created or updated with current offsets

Name:

Kurt Brown

Date: 04/12/2007

RPM	Speed (m/s)	Speed (knots)	mog-Ave	bj-Ave	kb-Ave	Std. Dev.	Average
	0	0	0	0	0	0	0
	2.58	5	-0.00585794	0.079715319	0.043122636	0.042935813	0.038993338
	3.10	6	0.025614878	0.079009483	0.076973913	0.030256894	0.060532758
	3.82	7.4	0.03839154	0.148848379	0.144137953	0.062456925	0.110459291
	4.24	8.2	0.08821736	0.151215298	0.214475233	0.063128982	0.15130263
	4.81	9.3	0.077429894	0.200576308	0.121471387	0.062399627	0.133159196
	5.32	10.3	0.016338694	0.109102998	0.095486417	0.050091565	0.073642703
	6.15	11.9	-0.01948801	0.099463807	0.0659994	0.061342615	0.048658399







# Blue cells used in computation of Delta Draft StDev used in TPE

Ave StDev 0.052236



# NOAA POS/MV Calibration Report

Ship:	FAIRWEATH	IER	_	Vessel:	1018	_
Date:	3/30/2007			Dn:	89	_
Personnel:	Froelich, Lewis, Ca	ampbell				
PCS Serial	#	2560	-	IMU Seria	I #	37
IP Address:		129.100.1.231			_	
POS contro	ller Version (Use I	Menu Help > About)		3.3.2.2		
POS Versio GPS Receiv	n (Use Menu View <sup>v</sup> ers	> Statistics)	MV320 v4			
	Primary Receiver		SN:4624A70243			
	Secondary Receiv	er	SN:4624A70263			
Calibrati Location: Approximat	On area Bostwick Inlet, AK e Position:		_ Lat	55	13	30
	an Clatian	Annata Ial	Lon	131	43	30
Frequency:	on Station:	323 kHz	anu			
Satellite	Constellatio	n	- (Use View> GPS [	Data)		
Primary G	PS			Seconda	ary GPS	
Sketch gene	ral SV configuration	1		Note any o	differences from	Primary GPS Receiver
Primary (PPS ] Seconda Primary (PPS ] Seconda Mode Mode HOCP VDOP Geodal Separation (P VDOP Geodal Separation (P PS-VTC Week Nam OPS-VTC Week N	y GPS   Austiany 1 GPS   Austiany 2 GPS 3-0 CIA mode 0.736 1.032 n) -7.385 Der 1420 1.1000 ((sec) 0.119 2000 2000 2000 2010 1.20000 1.20000 1.20000 1.20000 1.20000 1.20000 1.20000 1.20000 1.20000 1.20000 1.20000 1.20000 1.200000 1.200000 1.200000 1.200000 1.2000000 1.2000000 1.20000000 1.20000000 1.200000000 1.200000000 1.2000000000000000000000000000000000000	Citiz 2		Primary (PS) Secondar Pecelver Status Mode HCOP VDOP Geodal Separation (m CPS Time Offset (sec) Nut Metisage Latency Correction Latency (se SV 3 7 Status Lisble (pS) 770 Lisble (pS)	Y GPS         Austilary 1 GPS         Austilary 1 GPS           3-D CIA mode 0.736         0.736           0.738         0.7385           01         1.0000           1         0.000           1         1.0000           (sec)         0.077           kc)         0.000           1         1.840000           1         1.8400000           1 <th>22 CPS  </th>	22 CPS
						Close

PDOP

1.7 (Use View> GAMS Solution)

# POS/MV Configuration Settings

Gams Parameter Setup	(Use Settings > Installation > GAMS Intallation)
GAMS Parameter Setup	$\mathbf{X}$
Two Antenna Separation (m) Heading Calibration Threshold (deg) Heading Correction (deg)	1.834 0.500 0.000
Baseline Vector	
X Component (m)	0.000
Y Component (m)	0.000
Z Component (m)	0.000
Ok Close	Apply View

**Configuration Notes:** 

# **POS/MV** Calibration

#### **Calibration Procedure:**

(Refer to POS MV V3 Installation and Operation Guide, 4-25)

Start time:	1130	
End time:	1135	
Heading acc	uracy achieved for calibration:	

0.085

#### Calibration Results:

Gams Parameter Setup

(Use Settings > Installation > GAMS Intallation)

GAMS Parameter Setup	
Two Antenna Separation (m)	1.830
Heading Calibration Threshold (deg)	0.500
Heading Correction (deg)	0.000
	,
Baseline Vector	
X Component (m)	-0.008
Y Component (m)	1.830
Z Component (m)	0.025
Ok     Close	Apply View

#### The POS/MV uses a Right-Hand Orthogonal Reference System

The right-hand orthogonal system defines the following:

• The x-axis is in the fore-aft direction in the appropriate reference frame.

• The y-axis is perpendicular to the x-axis and points towards the right (starboard) side in the appropriate reference frame.

• The z-axis points downwards in the appropriate reference frame.

#### The POS/MV uses a Tate-Bryant Rotation Sequence

Apply the rotation in the following order to bring the two frames of reference into complete alignment:

a) Heading rotation - apply a right-hand screw rotation  $\theta z$  about the z-axis to align one frame with the other.

b) Pitch rotation - apply a right-hand screw rotation θy about the once-rotated y-axis to align one frame with the other.

c) Roll rotation - apply a right-hand screw rotation θx about the twice-rotated x-axis to align one frame with the other.

# SETTINGS

### COM1

Input/Output Ports (Use Settings > Input/Output Ports)

>	(Use Settings > input/Output Ports)
COM1	Input/Output Ports Set-up
	СОМ1 СОМ2 СОМ3 СОМ4 СОМ5
	Baud Rate Parity Data Bits Stop Bits Flow Control
	9600 CEven CHardware COdd C8 Bits C 2 Bits C XON/XOFF
	Output Select NMEA Output
	NMEA SPRDID
	SPRDID - TSS SINGGK Talker ID
	SINPPS ✓ IN ▼ Heave Up C Heave Down
	Input Select
	None
COM2	Input/Output Ports Set-up
002	СОМ1 СОМ2 СОМ3 СОМ4 СОМ5
	Baud Rate Parity Data Bits Stop Bits Flow Control
	9600 CEven CHardware COdd © 8 Bits C 2 Bits C XDMXDEF
	Output Select         Diminipation           Binary         Update Rate         Frame           Roll Positive Sense         © Port Up         © Starboard Up
	1 Hz C Sensor 2 Pitch Positive Sense © Bow Up C Stern Up
	Formula Select TSS1
	Input Select
	None
	CloseApply
· · · · · · · · · · · · · · · · · · ·	Input/Output Ports Set-up
COM3	COM1 COM2 COM3 COM4 COM5
	Baud Rate Parity Data Bits Stop Bits Flow Control
	9600 VICE Ven
	C Odd C Olits C 2013 C XON/XOFF
	Output Select
	None
	Innut Select Base GPS Innut
	Base 1 GPS  Input Type RTCM 1 or 9
	Line © Serial © Modern Modern Settings
	Close Apply

#### SETTINGS Continued Heave Filter

(Use Settings > Heave)	
Heave Filter	×
⊂ Z Altitude ∟	
Heave Bandwidth (sec) 20.000	
Damping Ratio 0.707	
Ok Close Appl	y

Events

#### Use Settings > Events)

Event 1		
<ul> <li>Positive</li> </ul>	Edge Trigger	
C Negative	e Edge Trigger	
ivent 2		
<ul> <li>Positive</li> </ul>	Edge Trigger	
C Negative	e Edge Trigger	
~ 1	Class	



In Navigation Mode , to change parameters go to Standby Mode !

#### **User Parameter Accuracy**

(Use Settings > Installation > User Accuracy)

User Parameter Ac	curacy	
-RMS Accuracy-		
Attitude (deg)	0.050	
Heading (deg)	0.050	
Position (m)	2.000	
Velocity (m/s)	0.500	
💣 Ok	Close	Apply

# **GPS Receiver Configuration**

(Use Settings> Installation> GPS Receiver Configuration)

Primary GPS Receiver

Gps Receiver Configuration			×
Primary GPS Receiver Sec Primary GPS GPS Output Rate	Condary GPS Rec GPS 1 Port Baud Rate 9600	eiver	
Auto Configuration © Enabled © Disabled	Parity None Even Odd	Data Bits 7 Bits 8 Bits	Stop Bits © 1 Bit © 2 Bits
[	Ok	Close	Apply

Secondary GPS Receiver

Gps Receiver Configurati	ion 🛛	K
Primary GPS Receiver Secondary GPS GPS Output Rate	Secondary GPS Receiver GPS 2 Port Baud Rate	
Auto Configuration © Enabled © Disabled	Parity Data Bits Stop Bits	
	Close Apply	



FA\_S220\_Reson8111\_end07.txt Vessel Name: FA\_S220\_Reson8111.hvf Vessel created: December 19, 2006

Depth Sensor:

Sensor Class: Swath Time Stamp: 2006-001 00:00 Transduer #1: Pitch Offset: -0.630 Roll Offset: -0.010 Azimuth Offset: -0.520 Del taX: 2.868 Del taY: 8.252 Del taZ: 4.753 Manufacturer: Reson Model: sb8111 Serial Number: Depth Sensor: Sensor Class: Swath Time Stamp: 2006-216 00:00 Transduer #1: \_\_\_\_\_ Pitch Offset: -0.630 Roll Offset: -0.010 Azimuth Offset: -0.520 Del taX: 2.868 Del taY: 8.252 Del taZ: 4.753 Manufacturer: Reson Model: sb8111 Serial Number: Depth Sensor: Sensor Class: Swath Time Stamp: 2007-001 00:00 Transduer #1: Pitch Offset: -0.590 Roll Offset: -0.020 Azimuth Offset: -0.380 Del taX: 2.868 Del taY: 8.252 Del taZ: 4.752

> Manufacturer: Reson Model: sb8111 Serial Number:

Navigation Sensor:

# FA\_S220\_Reson8111\_end07.txt

Time Stamp:	2006-001 00:00
Comments (null) Latency 0.000 DeltaX: 0.000 DeltaY: 0.000 DeltaZ: 0.000	
Manufacturer: Model: Serial Number:	Appl ani x POS/MV v320 846
Time Stamp:	2007-001 00:00
Comments (null)	
Latency 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000	

# Gyro Sensor:

Time Stamp:	2006-001	00: 00
Comments (null) Latency 0.000		
Time Stamp:	2007-001	00: 00
Comments (null)		

Comments (null) Latency 0.000

# Heave Sensor:

Time Stamp: 2006-001 00:00 Comments True Heave Enabled Apply Yes Latency 0.000 Del taX: 0.000 Del taZ: 0.000 Offset: 0.000 Manufacturer: Applanix Model: POS/MV v320 Serial Number: 846 Time Stamp: 2007-001 00:00 Comments True Heave Enabled Apply Yes Latency 0.000

Del taY: Del taZ: Offset:	0. 000 0. 000 0. 000	
Manufac Model : Seri al	turer: Number:	Appl ani x POS/MV v4 2411

 $Del taX \cdot 0.000$ 

### Pitch Sensor:

Time Stamp: 2006-001 00:00 Comments (null) Apply Yes Latency 0.000 Pitch offset: 0.000 Manufacturer: Applanix Model: POS/MV v320 Serial Number: 846

Time Stamp: 2007-001 00:00

Comments (null) Apply Yes Latency 0.000 Pitch offset: 0.000

Manufa	cturer:	Appl ani	Х
Model:		PÖS/MV	ν4
Seri al	Number:	2411	

# Roll Sensor:

Time Stamp: 2006-001 00:00 Comments (null) Appl y Yes Latency 0.000 Roll offset: 0.000 Manufacturer: Appl ani x POS/MV v320 Model: Serial Number: 846 2007-001 00:00 Time Stamp: Comments (null) Apply Yes Latency 0.000 Roll offset: 0.000 Manufacturer: Appl ani x POS/MV v4 Model: Serial Number: 2411

Draft Sensor:

\_

Time Stamp: 2006-001 00:00
Apply Yes Comments Entry 1) Draft: 0.000 Speed: 0.000 Entry 2) Draft: 0.090 Speed: 4.704 Entry 3) Draft: 0.075 Speed: 6.104 Entry 4) Draft: 0.064 Speed: 7.192 Entry 5) Draft: 0.046 Speed: 8.106 Entry 6) Draft: 0.095 Speed: 9.097 Entry 7) Draft: 0.170 Speed: 11.605 Entry 8) Draft: 0.189 Speed: 12.907
Time Stamp: 2007-001 00:00
Appl y Yes Comments Entry 1) Draft: 0.000 Speed: 0.000 Entry 2) Draft: -0.032 Speed: 4.024 Entry 3) Draft: 0.002 Speed: 5.618 Entry 4) Draft: 0.023 Speed: 8.339 Entry 5) Draft: 0.142 Speed: 10.400 Entry 6) Draft: 0.159 Speed: 11.857 Entry 7) Draft: 0.232 Speed: 13.860
Time Stamp: 2006-001 00:00
Comments Offsets
Motion sensing unit to the transducer 1 X Head 1 2.868 Y Head 1 8.252
Z Head 1 4.753 Motion sensing unit to the transducer 2 X Head 2 0.000 Y Head 2 0.000
Z Head 2 0.000 Navigation antenna to the transducer 1 X Head 1 2.993 Y Head 1 19 145
Z Head 1 16.253 Navigation antenna to the transducer 2 X Head 2 0.000 Y Head 2 0.000 Z Head 2 0.000
Roll offset of transducer number 1 0.000 Roll offset of transducer number 2 0.000
Heave Error: 0.050 or 5.000'' of heave amplitu Measurement errors: 0.003 Motion sensing unit alignment errors Gyro: 0.230 Pitch: 0.160 Roll: 0.160 Gyro measurement error: 0.020 Roll measurement error: 0.020 Pitch measurement error: 0.020

# TPE

ude. Navigation measurement error: 0.500 Transducer timing error: 0.005 Navigation timing error: 0.005 Page 4

FA\_S220\_Reson8111\_end07.txt Gyro timing error: 0.005 Heave timing error: 0.005 PitchTimingStdDev: 0.005 Roll timing error: 0.005 Sound Velocity speed measurement error: 0.003 Surface sound speed measurement error: 0.003 Tide measurement error: 0.003 Tide zoning error: 0.030 Speed over ground measurement error: 0.030 Dynamic loading measurement error: 0.030 Static draft measurement error: 0.050 Delta draft measurement error: 0.020 StDev Comment: `éfJ Ï...J`õ...JPõ...J°ð...J €...J@í...J°k€JàZ€J€Ó...Ja 2007-001 00:00 Time Stamp: Comments **Offsets** Motion sensing unit to the transducer 1 X Head 1 2.868  $\begin{array}{c} Y \ Head \ 1 \ 8. \ 252 \\ Z \ Head \ 1 \ 4. \ 752 \end{array}$ Motion sensing unit to the transducer 2 X Head 2 0.000 Y Head 2 0.000 Z Head 2 0.000 Navigation antenna to the transducer 1 X Head 1 1.691 Y Head 1 20.172 Z Head 1 17.756 Navigation antenna to the transducer 2 X Head 2 0.000 Y Head 2 0.000 Z Head 2 0.000 Roll offset of transducer number 1 0.000 Roll offset of transducer number 2 0.000 Heave Error: 0.050 or 5.000'' of heave amplitude. Measurement errors: 0.007 Motion sensing unit alignment errors Pi tch: 0. 110 Gyro: 0. 050 Rol I : 0. 110 Gyro measurement error: 0.020 Roll measurement error: 0.020 Pitch measurement error: 0.020 Navigation measurement error: 0.500 Transducer timing error: 0.005 Navigation timing error: 0.005 Gyro timing error: 0.005 Heave timing error: 0.005 PitchTimingStdDev: 0.005 Roll timing error: 0.005 Sound Velocity speed measurement error: 0.003 Surface sound speed measurement error: 0.003 Tide measurement error: 0.003 Tide zoning error: 0.030 Speed over ground measurement error: 0.030 Dynamic Loading measurement error: 0.020 Static draft measurement error: 0.022 Delta draft measurement error: 0.075 StDev Comment: `éfJ Ï…J`õ…JPõ…J°ð…J €…J@í…J°k€JàZ€J€Ó…Ja Svp Sensor:

2006-001 00:00 Time Stamp: Comments Svp #1: Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 2.868 Del taY: 8.252 Del taZ: 4.753 SVP #2: . . . . . . . . . . . . . Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 Time Stamp: 2006-216 00:00 Comments Svp #1: -----Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 2.868 Del taY: 8.252 Del taZ: 4.753 SVP #2: . . . . . . . . . . . . . Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000 2007-001 00:00 Time Stamp: Comments Svp #1: \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 2.868 Del taY: 8.252 Del taZ: 4.752

SVP #2: Pitch Offset: 0.000 Rol I Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000

### WaterLine:

Time Stamp: 2006-001 00:00 Comments Apply Yes WaterLine -0.010 Time Stamp: 2007-001 00:00 Comments Apply Yes WaterLine 0.000 FA\_S220\_Reson8160\_5to750\_end07.txt Vessel Name: FA\_S220\_Reson8160\_5to750.hvf Vessel created: December 19, 2006

Depth Sensor:

Sensor Class: Swath Time Stamp: 2007-001 00:00 Transduer #1: Pitch Offset: -0.290 Roll Offset: -0.040 Azimuth Offset: 0.100 Del taX: 0.493 Del taY: 7.665 Del taZ: 4.726 Manufacturer: Reson sb8160a Model: Serial Number:

# Navigation Sensor:

Time Stamp: 2007-001 00:00 Comments (null) Latency 0.000 DeltaX: 0.000 DeltaY: 0.000 DeltaZ: 0.000 Manufacturer: Applanix Model: POS/MV v4 Serial Number: 2411

# Gyro Sensor:

Time Stamp: 2007-001 00:00

Comments (null) Latency 0.000

#### Heave Sensor:

Time Stamp: 2007-001 00:00 Comments True Heave Enabled Apply Yes Latency 0.000 DeltaX: 0.000 DeltaY: 0.000 DeltaZ: 0.000 Offset: 0.000 Manufacturer: Applanix Model: POS/MV v4 Serial Number: 2411

#### Pitch Sensor: Time Stamp: 2007-001 00:00 Comments (null) Apply No Latency 0.000 Pitch offset: 0.000 Manufacturer: Appl ani x POS/MV v4 Model: Serial Number: 2411 Roll Sensor: Time Stamp: 2007-001 00:00 Comments (null) Apply No Latency 0.000 Roll offset: 0.000 Manufacturer: Appl ani x POS/MV v4 Model: Serial Number: 2411 Draft Sensor: Time Stamp: 2007-001 00:00 Apply Yes Comments DDSSM Entry 1) Draft: 0.000 Speed: 0.000 Entry 2) Entry 3) Speed: 4.024 Draft: -0.031 Speed: 5.618 Draft: 0.002 Speed: 8.339 Speed: 10.400 Speed: 11.857 Entry 4) Draft: 0.022 Entrý 5) Draft: 0.136 Entry 6) Draft: 0.153 Entry 7) Draft: 0.223 Speed: 13.860 TPE Time Stamp: 2007-001 00:00 Comments **Offsets** Motion sensing unit to the transducer 1 X Head 1 0.493 Y Head 1 7.665 Z Head 1 4.726 Motion sensing unit to the transducer 2 X Head 2 0.000 Y Head 2 0.000 Z Head 2 0.000 Navigation antenna to the transducer 1 X Head 1 1.691 Y Head 1 20.172 Z Head 1 17.756 Navigation antenna to the transducer 2 Page 2

FA\_S220\_Reson8160\_5to750\_end07.txt X Head 2 0.000 Y Head 2 0.000 Z Head 2 0.000 Roll offset of transducer number 1 0.000 Roll offset of transducer number 2 0.000 Heave Error: 0.050 or 5.000'' of heave amplitude. Measurement errors: 0.007 Motion sensing unit alignment errors Pi tch: 0. 260 Gyro: 0. 030 Rol I: 0. 260 Gyro measurement error: 0.020 Roll measurement error: 0.020 Pitch measurement error: 0.020 Navigation measurement error: 0.500 Transducer timing error: 0.005 Navigation timing error: 0.005 Gyro timing error: 0.005 Heave timing error: 0.005 PitchTimingStdDev: 0.005 Roll timing error: 0.005 Sound Velocity speed measurement error: 0.500 Surface sound speed measurement error: 0.100 Tide measurement error: 0.010 Tide zoning error: 0.000 Speed over ground measurement error: 0.030 Dynamic loading measurement error: 0.020 Static draft measurement error: 0.030 Delta draft measurement error: 0.075 StDev Comment: `éƒJ Ï…J`õ…JPõ…J°ð…J €…J@í…J°k€JàZ€J€Ó…Ja

Svp Sensor:

Time Stamp: 2007-001 00:00 Comments Svp #1: Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.493 Del taY: 7.665 Del taZ: 4.726 SVP #2: Pitch Offset: 0.000 Roll Offset: 0.000 Azimuth Offset: 0.000 Del taX: 0.000 Del taY: 0.000 Del taZ: 0.000

WaterLine:

Time Stamp: 2007-001 00:00

Comments Apply Yes FA\_S220\_Reson8160\_5to750\_end07.txt

WaterLine -0.002

#### S220\_8111 Measurements



Vessel Offsets for S220\_8111 are derived from Westlake-Survey-Report-NOAA-Fairweather-09-23-03.pdf

2006 Measured Values

Calculation	าร																			
Coord. Sys.		IMU to 8111			Port Ant to 81	11	Waterline to	RP*	F	Port Ant to Stbd	Ant		IMU t	o Port Ant				IMU to	Heave	
Westlake	IMU	easting	0.000	Port	easting	-35.739	IMU Base to baseline a	at Keel	Port	easting	-35.739	IMU		easting	0.000	IMU to Bulkho	(Frame) 5	2	IMU Base to baseline at	t Keel
	Base	northing	0.000	Ant	northing	-0.409	(ft) elevation	12.856	Ant	northing	-0.409	Base		northing	0.000	(ft)	easting	-11.638	(ft) elevation	12.856
		(ft/m) elevation	0.000		(ft) elevation	-38.283	IMU Base to baseline a	at Keel		(ft) elevation	-38.283		(ft/m)	elevation	0.000	(m)	easting	-3.547	(m) elevation	3.919
							(m) elevation	3.919												
	8111	easting	27.072	8111	easting	27.072			Stbd	easting	-35.866	Port		easting	-35.739	Frame 0 (FP)	to Frame 5	2	Top of IMU to Base of I	MU
		(ft) northing	9.410		(ft) northing	9.410	Waterline to Keel		Ant	northing	12.925	Ant		northing	-0.409	(m)	easting	-27.737	(m) elevation	0.168
		elevation	15.042		elevation	15.042	(ft) elevation	13.375		(ft) elevation	-38.209		(ft) (	elevation	-38.283				Top of IMU to Keel	
							Waterline to Keel									IMU to Frame	0 (FP)		(m) elevation	4.087
		8111 easting	8.252	Port A	nt to 8111		(m) elevation	4.077				Port		easting	-10.893	(m)	easting	24.1898		
		(m) northing	2.868		(ft) easting	62.811						Ant		northing	-0.125				Center of Gravity above	e baseline
		elevation	4.585		northing	9.819	Top of IMU to Base of	IMU					(m) (	elevation	-11.669	Heave Pt* to	Frame 0 (FI	<b>&gt;</b> )	(ft) elevation	16.37
					elevation	53.325	(m) elevation	0.168								(ft)	easting	102.42	Mean Metacentric heigh	nt
	Base	of IMU to Top of I	MU				Top of IMU to Keel					Base o	of IMU to	Top of IML	J	(m)	easting	31.218	(ft) elevation	3.88
	(inve	rse of measured	value)				(m)	4.087				(inver	rse of me	easured val	ue)					
		(m) elevation	-0.168										(m) (	elevation	-0.168	IMU to Cente	line		Heave Pt* to baseline a	t Keel
																(ft)	northing	6.122	(ft) elevation	20.25
																(m)	northing	1.866	(m) elevation	6.172
																Heave Pt* to	Contorlino		(*Heave Pt is Metacente	ar)
																(m)	northing	0	(FP is Forward Perpend	ticular)
																(11)	norunng	0	(if is i of ward i of poind	noulur)
		IMU to 8111			Port Ant to 81	11	Waterline to	RP*		Port Ant to Stbd	Ant		IMU t	o Port Ant		IM	I to Heave			
		(m) easting	8 252		(m) easting	19 145	(m) easting	N/A					(m)	easting	-10 893	(m)	easting	-7 0282		
	Top of	IMU northing	2.868		northing	2,993	Waterline northing	N/A	Scala	Distance (ft)	13.335	Top of	IMU	northing	-0.125	Top of IMU	northing	1.866		
	to 81	1 elevation	4 753		elevation	16 253	to IMU elevation	-0.010				to Por	t Ant i	elevation	-11 501	to Heave Pt*	elevation	-2.085		
		olovaloli			olovatori	10.200		0.010				10 1 01		olovalon		to riburo r t	oloration	2.000		
	Coord	Sys. CARIS		Coord	Sys. CARIS		Coord. Sys. CARIS					Coord	Sys. P	os/Mv		Coord. Sys.	Pos/Mv			
		x	2.868		x	2.993	×	N/A	Scala	r Distance (m)	4.064			х	-10.893		х	-7.028		
		v	8.252		v	19.145		N/A						v	-0.125		<b>.</b> v	1.866		
		z	4.753		z	16.253	× 2	-0.010						z	-11.501	/	/ z	-2.085		
		_					see Description Tab							_		see Description	on Tab			

#### S220\_8160 Measurements

Measurement	IMU to 8160 (MRU to Trans	)	Port Ant to 8160 (Nav to Trans)	Waterline to	RP*	Port Ant to Stb	od Ant		IMU t	o Port An	t		IN	IU to Heav	e
Coord. Sys.	Caris		Caris		Caris			(	aris		Pos/Mv		Caris		Pos/Mv
х	0.4	93	-0.684		n/a	Scaler Distance	1.995		1.177		-11.920		1.866		-7.028
у	7.6	65 <mark></mark>	19.585		n/a				11.920		1.177		-7.028		1.866
z	4.7	26	17.730		-0.002				13.004		-13.004		-2.086		-2.086
												-			
	*Top of IMU is RP (Reference	Pt)													

Vessel Offsets for S220\_8111 are derived from Westlake-Survey-Report-NOAA-Fairweather-09-23-03.pdf and Fairweather\_NGS\_Report\_Feb\_2007.doc Derivations

Donnation	°					
Coord. Sys.		IMU to 8160			Port Ant to 81	60
	<b>Westlake</b>			NGS		
	IMU	easting	0.000	Port	easting	-11.920
	Base	northing	0.000	Ant	northing	1.177
	(ft/m	) elevation	0.000		(m) elevation	-13.004
	Westlake			Westla	ake	
	8160	easting	25.149	8160	easting	7.665
	(ft	) northing	1.619		(m) northing	0.493
		elevation	14.956		elevation	4.559
	Westlake			NGS		
	8160	easting	7.665	8	3160 (as calculat	ed)
	(m	) northing	0.493		(m) easting	7.665
		elevation	4.559		northing	0.493
					elevation	4.726
	Base of IN	1U to Top of	IMU			
	(m	) elevation	-0.168			
		IMU to 8160			Port Ant to 81	60
	(m	) easting	7.665		(m) easting	19.585
	Top of IMU	J northing	0.493		northing	-0.684
	to 8160	elevation	4.726		elevation	17.730
	Coord Sys	: Caris		Coord	Sys Caris	
		x	0.493		x	-0.684
		У	7.665		у	19.585
		z	4.726		z	17.730

# **Description of Offsets for FAIRWEATHER S-220**

All Values Shown are in CARIS Coordinates



S220 Offset Descriptions



		i i an <i>sj</i>
х	У	Z
2.868	8.252	4.753
The lever arm	ns between	the IMU
and phase ce	nter of the	8160
ransducer ar	e taken fror	n the
Westlake repo	ort with the	addition
of the 0.168 n	n offset incl	uded for
he height of t	the IMU.	
Port Ant to 8	3111 (Nav t	o Trans)
Port Ant to 8	8 <b>111 (Nav t</b> y	o Trans) z
Port Ant to 8 x 2.993	<b>3111 (Nav t</b> y 19.145	<b>o Trans)</b> z 16.253
Port Ant to 8 x 2.993 This informati	111 (Nav t y 19.145 on comes o	<b>o Trans)</b> z 16.253 directly
Port Ant to 8 x 2.993 This informati rom the Wes	111 (Nav t y 19.145 on comes c tlake surve	o Trans) z 16.253 lirectly y.
Port Ant to 8 x 2.993 This informati from the Wes	111 (Nav t y 19.145 on comes c tlake surve	<b>o Trans)</b> z 16.253 lirectly y.
Port Ant to 8 x 2.993 This informati from the Wes	111 (Nav t y 19.145 on comes o tlake surve	o Trans) z 16.253 Jirectly y.
Port Ant to 8 x 2.993 This informati rom the Wes	111 (Nav t y 19.145 on comes o tlake surve	o Trans) z 16.253 Jirectly y.

0444 (MDLLA

IM	U to 8160	(MRU to T	rans)	
	Х	У	Z	
	0.493	7.665	4.727	
The I	ever arms	between t	he IMU	
and p	phase cent	ter of the 8	111	
rans	ducer are	taken from	the	
Vest	lake repor	t with the a	addition	
of the	e 0.168 m	offset inclu	ded for	
he h	eight of th	e IMU.		
D	A	00 (Name 1 -		
Port	Ant to 81	60 (Nav to	Trans)	
Port	Ant to 81 X	<b>60 (Nav to</b> y	<b>Trans)</b> Z	
Port	Ant to 81 x 0.618	<b>60 (Nav to</b> y 18.559	<b>Trans)</b> z 16.227	
Port This	Ant to 81 x 0.618 information	<b>60 (Nav to</b> y 18.559 n comes di	<b>Trans)</b> z 16.227 rectly	
Port This rom	Ant to 81 x 0.618 information the Westla	<b>60 (Nav to</b> y 18.559 n comes di ake survey	<b>Trans)</b> z 16.227 rectly	
Port This rom	Ant to 81 x 0.618 information the Westla	<b>60 (Nav to</b> y 18.559 n comes di ake survey	<b>Trans)</b> z 16.227 rectly	
Port This rom	Ant to 81 x 0.618 information the Westla	<b>60 (Nav to</b> y 18.559 n comes di ake survey	Trans) z 16.227 rectly	
Port This rom	Ant to 81 x 0.618 information the Westla	<b>60 (Nav to</b> y 18.559 n comes di ake survey	Trans) z 16.227 rectly	
Port This rom	Ant to 81 x 0.618 information the Westla	<b>60 (Nav to</b> y 18.559 n comes di ake survey	Trans) z 16.227 rectly	
Port This rom	Ant to 81 x 0.618 information the Westla	60 (Nav to y 18.559 n comes di ake survey	Trans) z 16.227 rectly	
Port This rom	Ant to 81 x 0.618 information the Westla	<b>60 (Nav to</b> y 18.559 n comes di ake survey	Trans) z 16.227 rectly	

# S220 Offset Descriptions

# Port Ant to Stbd Ant

Scaler Distance 4.064 From the Westlake survey it was determined that the vector for antenna separation was 4.064 m.

IMU to Port Ant				
х	У	Z		
-0.125	-10.893	-11.501		
This information comes directly				
from the Westlake survey.				

Waterline to RP*			
х	У	z	
n/a	n/a	-0.010	
The height of the IMU above the			
keel comes from the Westlake			
survey value of 3.919 m plus the			

measured value of 5.919 m pids the IMU to the base plate, to get an IMU height above the keel. The draft (waterline to keel) used for the FAIRWEATHER is based on repeated observations. Differencing the value of IMU to keel and waterline to keel gives the waterline to RP value.

IMU to Heave	IMU to Heave
x y z	From pg 3 of the Westlake Survey
1.866 -7.028 -2.085	
Key points on the IMU, from the Westlake survey, are its location with respect to the ship's reference frame. It is 4.087 m (3.919 m to base line + 0.168 m for IMU height above base plate)	<ul> <li>SUMMARY</li> <li>IMU foundation plate is level to within +/-0.001 feet.</li> <li>IMU foundation plate is located 12.856 feet above baseline established at the keel.</li> <li>IMU is parallel to ship's centerline to within +/- 0.001 feet. Location of scribed centerline intersection is 6.122 feet port of ship's centerline.</li> <li>IMU foundation plate centerline is located 11.638' feet forward of bulkhead 52.</li> </ul>
centerline and 3.547 m forward of frame 52. This information is needed to reference the IMU to the ship's Heave Measurement Location (Heave Point). *	

# S220 Offset Descriptions

#### IMU to Heave

\* From the Art Anderson inclination experiment the position of the metacenter was used as the position of the ship's Heave Point. (There may be a better way to determine the Heave Point, but this decision was based upon available information). The metacenter is defined by the center of buoyancy. As a vessel inclines through small angles, the center of buoyancy moves through the arc of a circle whose center is at the metacenter.

Important numbers and information determined from the Art Anderson report are the location of the metacenter and how it is positioned with respect to the vessel. The longitudinal location of the metacenter is defined as 102.42 feet (31.217 m) aft of the forward perpendicular. The height of the metacenter is 20.25 feet (6.172 m) above the keel. There is an assumption of the metacenter being on the centerline of the vessel. Similar values for the RAINIER's metacenter are 32.52 m aft of the forward perpendicular and 5.2 m above the keel. The difference in the height of the metacenter can be attributed to the difference between the FA's and RA's average draft which is 13.12 feet as opposed to approximately 14.5 feet respectively.

Referencing the metacenter (Heave Point, HP) to the IMU information requires information about the frame spacing of the vessel. From the Westlake survey, the IMU is located 3.547 m forward of frame 52. From Inclination document, the HP is 31.217 m aft of the forward perpendicular. From engineering drawings of the ship frame spacing is approximately 21 inches. The calculation for the longitudinal location of the HP with respect to frame zero, the Forward Perpendicular (FP) is as follows:

52 (frame) \* 21 (inches/frame)/12(inches/ft)\*.3048(m/ft)-3.547 m = 24.190 m from frame 0.

31.217 m (HP aft of FP) – 24.190 m (IMU aft of FP) = 7.027 m (HP aft of IMU)

The calculation for the vertical separation between the IMU and the HP is based on the height of the metacenter being 6.172m and the height of the IMU being 4.087 m above the keel. Differencing yields the metacenter being 2.085 m above the IMU.

The calculation for the athwartship separation is based upon the assumption that the HP is on the centerline and the knowledge that the IMU is 1.866 m to port of the centerline.
### Sources

Offset values for the ship were derived from three sources. A static offset survey, an inclination experiment, and values measured or approximated by ship's personnel.

On September 23, 2003 an offset survey of the NOAA Ship FAIRWEATHER was conducted by:

Westlake Consultants, Incorporated 15115 SW Sequoia Parkway, Suite 150 Tigard, Oregon 97224 Phone (503) 684-0652

These values relate the physical positions of one sensor to the next with the base plate of the IMU being the point of origin. All dimensions in the document are given in feet and decimal feet.

On July 16, 2004 an inclination experiment was conducted at MOC-P by:

Art Anderson Associates 202 Pacific Avenue Bremerton, WA 98337-1932

### Calculations

The values for the required lever arms are listed in the S220\_Offsets and Measurements spreadsheet. The reference point and the IMU are identical. Difference in documentation between Westlake and FA calculations are based off of measuring up from the IMU base (Westlake's origin) and the top of the IMU. The top center of the IMU for the POS/MV is the defined origin for the POS/MV and the origin that is being used on all FAIRWEATHER vessels. The distance from the base plate to the top of the IMU is 0.168 m, a value measured by ship's complement. Conversions factor from feet to meters is 0.3048 m/ft.

As a requirement for the TPE, the standard deviation for each position is 3 mm. This value is based upon a conversation with Elaine McDonald of Westlake and is followed up by an Email documenting that fact. The email is located at the end of this document.

























# **Definitions and Basis for Dimensions/Locations**

#### Northings

Northings (Port - Starboard) are with reference to the IMU Foundation Plate centerline scribe. Positive values are starboard of the IMU. Negative values are port of the IMU. *Calculated values are in italics.* 

#### Eastings

Eastings (Stern to Bow ) are with reference to the IMU Foundation Plate centerline scribe. Positive values are forward of the IMU. Negative values are aft of the IMU. *Calculated values are in italics.* 

#### Elevations

Elevations are with reference to the IMU Foundation Plate centerline scribe = 0 elevation. Positive values are below the IMU (toward the keel). Negative values are toward the topside.

#### Dimensions

All dimensions are in feet and decimal feet. All dimensions provided are "offsets" to IMU centerline.

#### Ship's Centerline Data

At project initiation, control was established to define the ship's centerline as a plane running from a point on the centerline of the keel at the stern through a point on the centerline of the keel near the bow, to a point on the bow splitting the bow chock.

#### **IMU Referenced Data - Procedure**

All data was originally referenced to the ship's geometry. Following location of the IMU, data was transformed to the IMU as point of origin for Northings, Eastings, and Elevation. All dimensions provided with reference to the IMU are "offsets."

# **Ship's Centerline - Control Measurements**

(Prior to location of IMU and referencing of data to IMU as point of origin (0,0,0)

Defined by measurements at the keel centerline					
	longitude	transverse	elevation		
near the bow	1190.674	1000.000	135.8672		
at the stern (point of origin)	1000.000	1000.000	100.0000		
along the keel (approx 180' forward)	1180.121	1000.000	116.6810		

### Ship's Baseline

Defined by measurements on the keel			
	longitude	transverse	elevation
at the stern (point of origin)	1000.000	1000.000	100.0000
and approx. 129' forward of stern	1129.120	999.985	100.0022

Report of Sonar Array Installation on NOAA Fairweather

# **IMU Foundation Plate**

	EASTING	NORTHING	ELEVATION
Horizontal alignment per scribed lines			
on IMU foundation plate		0.001	
		0.000	
Scribed lines - intersection/centerline c	of IMU plate		
	0.000	0.000	0.000
Elevation checks near four corners of I	MU Foundation	plate *	
* elevation check adjusted for target			0.001
that created 10 mm offset =.03281			-0.001
feet			0.000
			-0.001

### SUMMARY

- IMU foundation plate is level to within +/-0.001 feet.
- IMU foundation plate is located 12.856 feet above baseline established at the keel.
- IMU is parallel to ship's centerline to within +/- 0.001 feet. Location of scribed centerline intersection is 6.122 feet port of ship's centerline.
- IMU foundation plate centerline is located 11.638' feet forward of bulkhead 52.

# **Granite Block**

	EASTING	NORTHING	ELEVATION	
Horizontal alignment per scribed lines				
		1.584		
		1.583		
Scribed lines - intersection/centerline c	of granite block			
	-0.003	1.583		
				Deviation
Elevation checks near four corners of g	granite block			from level
* elevation check adjusted for target t	hat created 10		-0.217	-0.001
mm offset = 0.03281 fee	et		-0.217	-0.001
			-0.216	0.001
			-0.215	0.001

### SUMMARY

- Granite block is level to within +/-0.001 foot
  - of average elevation = -0.21632 feet
- Granite block is parallel to ship's centerline to within 0.001 foot
  - Location is 4.54 feet to port of ship's centerline and 1.583 feet starboard of IMU.
- Granite block is aligned with IMU to within 0.003 feet longitudinally.

# Array Acoustical Centers - Referenced to IMU

	EASTING	NORTHING	ELEVATION
PORT ARRAY (81-60)	25.149	1.619	14.956

### **Explanation of Calculations**

Acoustic center is defined as the center of the transmitter array with the elevation = 83 mm below mounting face of array.

### Easting

Center of array is defined by the foundation plate bolt centerlines (1/2 distance between bolts)

- 27.008 Forward edge of foundation as measured
- 0.104 Forward edge of foundation to centerline of forward bolt hole
- 1.755 Distance from bolt hole centerline to center of array
- 25.149 feet forward of IMU

### Northing

Center of array is defined as the mid-point between the bolt holes on the foundation.

- 1.369 Port edge of foundation as measured
- + 0.078 Port edge of foundation to centerline of bolt hole per Cascade General
- + 0.172 Distance from bolt hole centerline to array center
  - 1.619 feet starboard of IMU

### Elevation

Per Reson drawing 2148M011\_001 the elevation is 83 mm below array mounting surface

14.679 Array foundation elevation as measured.

0.005 Isolation "shim" added between foundation and array

0.272 83 mm below array mounting surface to acoustical center

14.956 feet below IMU

# Array Acoustical Centers - Referenced to IMU

	EASTING	NORTHING	ELEVATION
STARBOARD ARRAY (81-11)	27.072	9.41	15.042

### **Explanation of Calculations**

Acoustic center is defined as midpoint of the transmitter array in the longitudinal and transverse axes. The elevation is defined as the center of the receiving array.

### Easting

Center of array is defined as 0.235' aft of the forward bolt centerlines on transmitter array foundation

- 28.563 Forward edge of foundation fixture plate as measured (receiving plate forward edge)
  - 27.349 Forward edge of transmitter array foundation as calculated
  - 0.042 Forward edge of foundation to centerline of forward bolt hole per design
  - 0.235 Distance from bolt hole centerline to center of array per design

27.072 feet forward of IMU

### Northing

Center of array is defined as the mid-point between the bolt holes on the transmitter array foundation.

9.410 Centerline of array foundation as measured on scribe - aft section of fixture plate

9.410 feet starboard of IMU

### Elevation

Elevation is 0.401 feet above receiver array mounting surface

- 16.085 Mounting foundation fixture plate as measured.
- 15.447 Receiver foundation elevation as calculated
- + 0.005 Isolation "shim" added between foundation and array
- 0.410 Design distance from mounting surface of array to acoustic center
- 15.042 feet below IMU

	EASTING	NORTHING	ELEVATION	
Horizontal alignment measured at port	edge of array for	oundation		
		1.369		
		1.369		
Forward edge of array foundation - me	asured			
	27.008			
Horizontal alignment - calculated to an	ray centerline			
Foundation edge is 0.25 feet port of		1.619		
array centerline		1.619		
				deviation from
Elevation checks near four corners of a	array foundation			level (average)
			14.680	0.001
			14.681	0.002
			14.678	-0.001
			14.677	-0.002

# Longitudinal Array Foundation - Port Side

### SUMMARY

- Port longitudinal array foundation average elevation is 14.679 feet. Variation in elevation is +0.002 to -0.002 feet.
- Port longitudinal array foundation is parallel to ship's centerline and 1.369 feet starboard of IMU. Calculated array centerline is 1.619 feet starboard of IMU

Report of Sonar Array Installation on NOAA Fairweather

9/23/2003

	EASTING	NORTHING	ELEVATION	deviation from
Horizontal alignment measured on fixt	ure plate scribe	-		parallel
Design location is 3.292 feet		9.410		0.002
starboard of ship centerline		9.406		-0.002
Forward edge of array foundation fixtu	re plate - <i>measu</i>	red		
<b>C</b>	28.563			
				deviation from
Elevation checks near four corners of a	array foundation	"fixture plate"		average
			16.085	0.000
			16.085	0.000
			16.084	0.000
			16.085	0.000
Calculated locations of longitudinal and	d transverse arra	ay foundations		
Forward edge				
Receiver (transverse)	28.563			
Transmitter (longitudinal)	27.349			
difference = $1.2$	14			

# Longitudinal Array Foundation - Starboard Side

**NOTE:** On Transmitter array foundation - from forward edge to center of forward holes = 0.042' On Receiver array foundation distance from forward edge to center of forward holes = 0.076'

Calculated elevation of longitudinal and transverse array foundations	
Receiver/Transverse Foundation	15.446
Transmitter/Longitudinal Foundation	15.709
difference = 0.263	

### SUMMARY

- Starboard longitudinal array foundation (measured at fixture plate) average elevation is 16.085 feet. Deviation from level (average elevation) is less than 0.001 feet.
- Starboard longitudinal array foundation averages 9.408 feet starboard of IMU. Variation from parallel is from -0.002 feet to +0.002 feet from average.
- Starboard longitudinal array foundation forward edge is 28.563 feet forward of IMU.

	EASTING	NORTHING	ELEVATION	
Forward Edge - Transverse array foun	dation - measure	ed		
	28.343			
	28.338			
Port edge - Transverse array - measur	ed			
		-0.181		
Centerline of array - calculated				
Foundation forward edge minus	28.093			
0.25 feet to array centerline	28.088			
Port edge of foundation plus 1.806 fee	t	1.624		
to calculated array centerline				
				deviation from
Elevation checks near four corners of a	array foundation			level
			14.679	0.002
0 861 feet below baseline with 0 965			14.675	-0.001
foot offset = 98.180 feet average			14.675	-0.001
elevation			14.677	0.001

# **Transverse Array Foundation - Port Side**

### SUMMARY

- Transverse array foundation average measured elevation is 14.677 feet below IMU (0.006 feet above design location).
  - Deviation from level (average elevation) is 0.003 to -0.001 feet
- Transverse array foundation centerline (calculated) averages 28.090 feet forward of IMU. Variation from parallel to ship's centerline is from -0.003 to 0.003 feet (from average).
- Transverse array centerline is calculated to be 1.624 feet starboard of IMU.

Report of Sonar Array Installation on NOAA Fairweather

# **Transverse Array Foundation - Starboard Side**

NOTE: Direct Measurements were not taken to the transverse array because a single "fixture plate" covered be transmitter and receiver foundations. The data provided here is primarily "calculated".

	EASTING	NORTHING	ELEVATION
Forward edge - as measured or	n fixture plate		
Receiver - (transverse)	28.563		
as measured			
Transmitter (longitudinal)	27.349		
difference = 1.2	214		

**NOTE:** On Transmitter array foundation - from forward edge to center of forward holes = 0.042' On Receiver array foundation distance from forward edge to center of forward holes = 0.076'

Horizontal Alignment centerline scribe on fixture plate as measured - forward portion of plate (near receiver array)	9.406	
Average of measurements on fixture plate	9.408	
Elevation of longitudinal and transverse array for Receiver/Transducer Transverse Foundation	oundations	15.446
Transmitter/Longitudinal Foundation		15.709
difference = 0.263		

Based on measured elevations averaging 16.085 feet across fixture plate

### SUMMARY

- Transverse array foundation is calculated to be 15.446 feet below IMU calculated from measured elevation of 16.085 feet. Deviation in elevation measurements across the array fixture plate is less than 0.001 fe
- Transverse array foundation forward edge (measured) is 28.563 feet forward of IMU.
- Transverse array centerline is measured to be 9.406 feet starboard of IMU.

Variation from parallel of the fixture plate across entire starboard array is  $\pm 0.002$  feet (from average).

	EASTING	NORTHING	ELEVATION
Stbd POS MV Antenna -Location	-35.866	12.925	-38.209
Port POS MV Antenna - Location	-35.739	-0.409	-38.283
Foundation Plate Stack Antenna Align	ment	7.677	
Foundation Plate Stack Antenna Align	ment	7.677	
Port GYRO Foundation Plate Alignmer	nt	2.411	
Port GYRO Foundation Plate Alignment	2.411		
Stbd GYRO Foundation Plate Alignme	nt	3.866	
Stbd GYRO Foundation Plate Alignme	nt	3.867	

# Antennae

### SUMMARY

- Foundation plate stack antenna alignment is parallel to ship's centerline.
- Port GYRO Foundation Plate is aligned parallel to ship's centerline.
- Starboard GYRO Foundation Plate is aligned parallel to ship's centerline.

#### Email regarding Standard Deviation of Westlake Survey

Greetings Mark -

As promised I am writing to document our conversation of late yesterday afternoon regarding the reliability of measurements on the NOAA Fairweather.

We discussed your question here at Westlake and possible interpretations.

We believe the you can comfortably use plus/minus 3 mm as the standard error of any given distance between 2 measured/located points on the vessel. We are confident that given the same circumstances, were we to repeat the measurements, our inter-point distances would be within plus/minus 3 mm of data reported (standard error).

If the measurements were taken from a single instrument set up within a fairly close range the distance would be reliable to nearly plus/minus 1 mm. However, we had to take many measurements from a number of setups around, on, and inside the vessel, and we then tied all of these measurements to a common coordinate system. Consequently, it is not realistic to expect a 1 mm error.

As we discussed yesterday, there are many other factors that will impact the location of each point and, consequently, the distance between two or more points. Temperature, sun light, deformation of the vessel when it is in and out of the water, movement of the drydock, settlement, definition of the actual point to be measured relative to the identified structure etc. all impact the reliability or repeatability of measurements.

Nonetheless we appear to be in agreement that the 3 mm value will work in your software without introducing significant, additional variability.

If you have questions or require additional information, please give me a call - or email.

Best wishes,

Elaine for Derek Colclough, Director, Industrial Measurement Division

Elaine McDonald Director of Marketing Westlake Consultants, Inc. 15115 SW Sequoia Parkway (150) Tigard, Oregon 97224

 phone
 503-684-0652

 fax
 503-624-0157

 toll-free
 800-523-8750

 email
 emcdonald@westlakeconsultants.com

We invite you to visit our website www.westlakeconsultants.com

# STABILITY TEST:

7/25/2004 6:05 AM

# NOAA Ship FAIRWEATHER (16 Jul 2004 )

	FROM HYDROSTATIC FRO CURVES	OM INDEPENDENT CALCULATION
Corrected diaplacement	tons 1638.	79 tons
Mean virtual metacentric height obtained from plot of moment = 5987.252 / 1638.79 inclining moments versus tangents of angles of heel displacement x tangent	feet 3.6	5 feet
Correction for free surface = 374.0 / 1638.790	feet 0.2	3 feet
Mean metacentric height G.M. =	feet 3.8	8 feet
Transverse metacenter above base line corresponding to draft at LCF (corrected for hog or sag)	feet	
Transverse metacenter above base line corrected for trim, and hog or sag	feet	
C.G. above base line	feet 16.3	7 feet (from figure)
	16.3	6 feet (from GHS)
Longitudinal metacenter above C.G.	feet	
Moment to alter trim 1 foot, (Long GM x $\Delta$ ) / L	ft-tons	
Trim by stern	feet	
Trimming lever = (Trim x moment to trim) / displacement	feet	
Longitudinal center of buoyancy (LCB) from origin	feet	
C.G. from origin	feet 102.4	4 feet (from figure)
	102.4	<sup>2</sup> feet (from GHS)
		FP
Period of complete rollseconds		
Apparent radius of gyration of vessel $\alpha = \frac{T GM}{1.108}$ feet $\frac{3.88}{12.35}$	102.42	
Rolling constant $C = \frac{T GM}{B}$ WATERLINE	B 16.37	WATERLINE BASE LINE
TRAFELINE	102.44	

SHIP AT TIME OF STABILITY TEST--CONDITION

8

Page 8 of 31

Page 1 of 1



ISO 9002 Certified

**Certificate of Accuracy** 

Customer Name: MCMASTER-CARR SUPPLY CO. Customer Address: 200 AURORA IND. PARKWAY AURORA.OH 44202 Customer PO#: TA-28173060

0002"
0010
6
200

This product was inspected under environmentally controlled conditions. The electronic and optical gauging equipment used in inspecting this item has been calibrated and is traceable to the National Institute of Standards and Technology (NIST). Our calibration system is in compliance with ISO 10012-1.

Calibration Equipment Used in the Inspection of this Product:

Type of Equipment	ID Number	Instrument Uncertainty	NIST Traceability	Cal. Due Date
Autocollimator	IP 040	±0.5 arc sec	821/259488-97	6-03
.000020 Mahr Dial I	20990	50 µin	25894-1	6-03
	201 20 20		Q	

Laboratory Manager Signature:

Lan

Donald Schirmers, Lapping Manager Robert Golla, Accessories Supervisor

REWORK / RECALIBRATION (This section is completed for recertification orders only - accuracies upon receipt)

Date of Receipt:

Accuracy of Incoming Product:

Repeat Measurement of Incoming Product:

Was unable to read upon receipt due to poor condition of product

The results on this Certificate of Accuracy apply only to the item described above. This report shall not be reproduced except in full and with the written authorization of our laboratory.

Measurement Uncertainty is expressed at a confidence level of 95% (coverage factor k=2)

Procedure Number: QP 4.10.1

1101 Prosper Drive • Box 430 • Waite Park, MN 56387• PH: 320-251-7171 • Fax: 320-259-5073

Laboratory Name	STONE	
1101 Prosper Waite Par PH: 320-251-7171	Drive - Box 430 k. MN 56387	
Final Inspection	(1) Inspection Number:	0200851
(3) Date of Receipt (rework items):     (4) Repeat Reading of Received Item:     (5) Accuracy of Received (rework) Item:	(2) Inspection Date: (6) Customer Name:	8-23-02
Unable to Inspect - product in too poor o	f condition (7) Serial Number:	6961
(8) P.O. Number: 1- 22(13:060)	(9) Print/Part Number:	
10) Description of Item: 8x12x2 (	CB (11) Granite Type:	Impala
(12) Conditions at Time of Inspection: Ter	nperature: 69 OF Humid	ity: 51
(13) Test Equipment: <u>Type of Equipment</u> Serie	al Number Calibration Due Date	Uncertainty of IMTE
Autocollimator Mirror Size: Autocollimator G Repeat-o-meter G Electronic Level G Height Check G Amp & Gauge Head G Surfometer G Penta Prism Mikrokator G	190 <u>6-03</u> 190 <u>6-03</u>	tos are see 50 pin
Other (14) Grade: B A AA N/A (15) Overall Accuracy / Flatness (actual):	000075 (allowed): 0	002
(16) Repeat Measurement (actual):(FIM: (FIM: (17) Final Ir	Full Indicator Movement)	.000025" N/A
(18) Opinion / Interpretation (if applicable):	/	
(21) Thread Size, Quantity & Location to Print: (22) Insert / Hole / Slot Size, Quantity & Locati	Yes No on to Print: Yes No	19-23 Are Not Applicable - No
(23) In Existing inserts are not The results of this inspection apply only to the item de written approval of our laboratory. Measurement unce	inspector Signature: inspected on reworks and/or calibration items. escribed above. This report shall not be reprod ertainty is expressed at a confidence level of 95%	uced, except in full, with the (coverage factor k=2).

IMPORTANT DOCUMENT





Save

# Tru-Stone Technologies Instructions for Care of Granite Surface Plates

- Cleaning and Moisture: Plates shall be cleaned thoroughly and given adequate time to dry before testing for tolerance. Water based cleansers that have not dried will cause iron parts to rust if they are left in contact with the wet surface for an extended period of time. It is recommended that plates undergo drying time in a room with less than 50 percent relative humidity. Temperature and dirt have a direct correlation with measurement accuracy. Personal cleanliness will aid in eliminating one source of contamination.
- Temperature Soaking Time: Before granite surface plates are measured for work surface flatness, the granite should remain in the calibration area until it has reached room temperature, which may require 2 to 3 days. Large plates require more soak-out time than smaller ones.
- Scratches and Nicks: Whenever scratches and nicks appear on granite plates, the resulting rough edges should be removed with a flat granite dressing plate. Any bump that shatters the surface raises fractured material at the rim of the crater.
- 4. Rotation of Plates: When a specific work surface area receives prolonged usage, it is suggested that the plate and stand be rotated 180 degrees on a periodic basis to increase the wear life of the plate. The production of a contour map during calibration is particularly helpful in locating the parts of the plate that should be given the most use. This can be accomplished by requesting a long form certification when ordering the new surface plate or when the plate is being sent in for recalibration.
- 5. Periodic Recalibration: Periodic recalibration of granite surface plates is recommended to determine resurfacing or replacement needs. The interval between calibrations will vary with the grade of plate and the wear resistance of the granite. TRU-STONE CONFORMS TO ISO 9000 CERTIFICATION REQUIREMENTS FOR VENDORS. Frequent monitoring of the work surface by scanning it with the repeat gage is desirable. When these results differ from those marked on the replaceable sticker, you should recalibrate the plate. In addition to measuring the overall accuracy of a surface, smaller areas can be checked for localized variations often missed by the calibrating methods. Remember precision measurements are only as accurate as the measuring tools used.
- Torque on THREADED Inserts: Do not exceed the following maximum torque values when using a torque wrench to limit distorting the work surface and pulling the insert. The following torque values are the maximum level permissible by the Federal Specification GGG-P-463c.

#### PERMISSIBLE TORQUE CLAMPING ON THREDED INSERTS

Thread Size	Torque
.250 inch	7 ft. lbs.
.3125 inch	15 ft. lbs.
.375 inch	20 ft. lbs.
.500 inch	25 ft. lbs.

- 7. Clamping Ledges on Grade AA Surface Plates: There is danger of distorting the work surface flatness beyond tolerance when a heavy item rests on the ledge or an item is clamped to the ledge. Ledges are not only expensive, but a great cause of inaccuracy. Experimentation and research reveal that no-ledge plates retain their accuracy better than ledged plates.
- 8. Supports: There are working and loading conditions where the standard three point supports are not satisfactory. These cases should be individually engineered. When four or more supports are used, shims or adjusting screws are necessary for proper support. The supports could be spotted under the loading points and set to approximately equal the loading. Sometimes the work surface flatness can be improved by shifting support positions. Fulcrum, air and hydraulic supports are available. Whenever nonstandard supports are used, the surface plate shall be calibrated at the site for compliance to the flatness tolerance.

- 9. Care:
  - Utilize the full surface of a plate so the wear is distributed and not concentrated in one area.
  - The surface plate should not be overloaded.
  - Use extreme care in moving the item being measured and the gages being used.
  - Place on the surface ONLY what is required.
  - Particularly avoid heavy contact with the edges.
  - Don't leave metal objects on the surface longer than necessary.
  - Clean the surface before and after use.

Remember that the condition of this accurate plane is an integral factor in the measurement being made.

#### NOTE:

Surface plate cleaner can be purchased through your local Tru-Stone distributor or directly from Tru-Stone Technologies. Call for pricing and delivery information.

When the need for recalibration or rework of your surface plates and precision granite accessories arises, contact a Tru-Stone representative or call us directly for more details on restoring your inspection item to a "like new" condition. This service comes with new certification and plate labels.

One advantage of having your granite inspection equipment recalibrated by a manufacturer is the manufacturer's ability to take the time required to ensure the proper repeatability and overall shape of the inspection surface. Tru-Stone allows the item to normalize overnight prior to taking the final readings to indicate whether it is a good enough quality to certify and return to you.

Should you have any questions, please contact our customer service representatives at 320/251-7171 or fax us at 320/259-5073.

# **Important Notice**

Any streaks of color in the granite are not defects. These are created by the molten lava mixing with minerals prior to evolving into the granite you see today. Black streaks or spots are the result of a magnetite (black iron oxide) concentration. White streaks or spots are areas where the granite is lacking magnetite. The levels of magnetite in granite vary considerably, however the color of the granite in no way affects the functionality or guality of it.

# Our products are UNCONDITIONALLY Guaranteed

Please refer to the Federal Specification GGG-P-463c, which is followed by NIST (National Institute of Standards & Technology) for Granite Surface Plates.

- "3.7 Seams or Color Streaks: Seams are cause for rejection. Color streaks have no affect on the serviceability of the granite."
- "4.5.8 Seams or Color Streaks: Test for a seam is to wet the smooth surface of the granite where the color streak appears; then dry it off. If the streak remains wet or damp, it is a seam."

1101 Prosper Drive • P. O. Box 430 • Waite Park, MN 56387 • 1-800-959-0517 • PH: 320-251-7171 • Fax: 320-259-5073

# FAIRWEATHER Multibeam Echosounder Calibration

		Ves	sel
3/29/2007	088	Nichols Passage	
Date	Dn	Local Area	
Calibrating	Hydrograph	er(s)	
8111		S220	
MBES Syst	em	MBES System Location	Date of most recent EED/Factory Check
Sonar Seria	al Number		Processing Unit Serial Number
Sonar Mour	nting Configu	uration	Date of current offset measurement/verification
POS MV ve	ersion 4		29 March 2007
Description	of Positionir	ng System	Date of most recent positioning system calibration
Acquisiti	on Log		
3/29/200	07 088	Nichols Passage	Sunny, near calm seas
Date	Dn	Local Area	Wx
Bottom Typ	е		Approximate Water Depth
Personnel o	on board		

S220 8111

Comments

 TH\_S220\_088

 TrueHeave filename

 Batch #
 BOT Files (botXXX.???-???)

 1

 2

 SV Cast #1 filename
 UTC Time
 Lat
 Lon
 Depth
 Ext. Depth

Append to

day SV file

Copy files to

network

### ROLL

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks

# PITCH

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	PITCH1	359	3.9	18m shoal observed
	PITCH2	179	4.3	
	PITCH3	359	4.0	Good line
	PITCH4	168	4.0	Good line

# HEADING/YAW

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
	HEADING1	359	4.1	
	HEADING2	179	5.1	
	HEADING3	179	4.3	
	HEADING4	359	4.0	Good line

# NAV TIME LATENCY

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks

# **Processing Log**

4/2/2007	092			Froelich		
Date	Dn	Personnel				
	✓ Data converted	-> HDCS_Data in (	CARIS			
	TrueHeave applied	Trueheave file w	as corrupted not a	applied to calibration lines		
	SVP applied	Testing_s220_0	88.svp			
	✓ Tide applied	9450460.tid				
		Zone file <u>r</u>	oatch_test.zdf			
		Lines merged	$\checkmark$			
	Data cleaned to ren	nove gross fliers	$\checkmark$			
			Communita o ammo a fa	ve in this endor		
	1. Precise Timina		2. Pitch bias	3. Heading bias	4. Roll bias	
	Do not enter/apply correctors until all evaluations are complete and analyzed.					

# PATCH TEST RESULTS/CORRECTORS

Evaluators	Latency (sec)		Pitch (deg)	Roll (deg)	Yaw (deg)
Froelich	0.00		-0.70	-0.10	-0.40
Gonsalves	0.00		-0.55	0.00	-0.40
Brown	0.00		-0.50	0.05	-0.30
Johnston			-0.60	-0.04	-0.40
Averages	0.00		-0.59	-0.02	-0.38
Standard Deviation	0.00		0.09	0.06	0.05
FINAL VALUES	0.00		-0.59	-0.02	-0.38
Final Values based on	Group Average				
Resulting HVF File Name	FA_S220_Reson	8101.hvf			
MRU Ali	gn StdDev gyro	0.05	Value from standard	deviation of Heading offset	values
MRU Align St	dDev Roll/Pitch	0.11	Value from sum of se	quares standard deviations of	of pitch and roll offset v

NARRATIVE

 $\hfill \square$  HVF Hydrographic Vessel File created or updated with current offsets

Name: gonsalves

Date: 14-Apr-07

# FAIRWEATHER

Multibear	n Echosoun	der Calibra	tion	<b>S220 8160</b> Vessel				
4/16/2007	106	Ernest Sound						
Date	Dn	Local Area						
French, Froe	lich, Gonsalves,	Mills						
Calibrating F	lydrographer(s)							
Reson 8160		Hull mount						
MBES Syste	т	MBES System	Location		Date of most recent EED/F	actory Cheo	ck	
Sonor Sorial Number					Processing Unit Serial Nur	nher		
Sonar Moun	ting Configuration	ז			Date of current offset meas	surement/ve	rification	
Description of	of Positioning Sys	stem			Date of most recent position	oning system	n calibration	
• • •								
Acquisitio	on Log							
4/16/2007	106	Ernest Sound			Calm			
Date	Dn	Local Area			Wx			
					65 Fathoms			
Bottom Type	•				Approximate Water Depth			
Froelich Ma	rtin CO Gonsalı	ves French						
Personnel or	n board	00, 11011011						
Comments								
TH \$220 10	)6_2_000_(use_for	nitch lines). TH	1 8160 106 3	(use for head	ina)			
TrueHeave f	ilename		_0700_700_0	1000 101 110000	"'9 <i>'</i>			
		1	1		1			
SV Cast #1 1	ïlename	UTC Time	Lat		Lon	Depth	Ext. Depth	
					1			
SV Cast #2 1	ilename	UTC Time	Lat		Lon	Depth	Ext. Depth	
	lionalite		Lat		2011	Dopur		
POLI								
SV Cast #	XTF Line Filen	ame	Heading	Speed (kts)	Remarks			
			J		Use pitch lines			
			<b> </b>					
······								

#### PITCH

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
bot_106.001	PITCH1	207	5.5	
	PITCH2	032	4.8	
	PITCH3	207	5.6	
	PITCH4	035	4.7	Computer crashed near end of line.

### **HEADING/YAW**

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks
bot_106.001	HEADING1	210	5.7	missed the target - do not use
	HEADING2	029	4.8	may have been too far from target
	HEADING3	211	5.7	
	HEADING4	029	4.8	operator error, I may have blown out near the target (of all places)
	HEADING5	211	5.7	

### NAV TIME LATENCY

SV Cast #	XTF Line Filename	Heading	Speed (kts)	Remarks

# Processing Log

4/18/2007	108	Brown, Johnston, Gonsalves, Froelich
Date	Dn	Personnel
V	Data converted -	-> HDCS_Data in CARIS
🗸 Tr	ueHeave applied	TH_s220_106_2 and TH_8160_106_3
	SVP applied	bot_106_8160.svp
	✓ Tide applied	predicted - 09450460.tid
		Zone file 0119FA2007CORP.zdf
		Lines merged 🗸
D	ata cleaned to rem	ove gross fliers 🗸

		Compute correctors i	n this order	
1. Precise Ti	ming	2. Pitch bias	3. Heading bias	4. Roll bias
	Do not enter/app	ly correctors until all evalua	tions are complete and analyz	red.
ATCH TEST RESULTS	CORRECTORS			
valuators	Latency (sec)	Pitch (deg)	Roll (deg)	Yaw (deg)
эb	0.00	-0.30	-0.06	-0.15
j	0.00	-0.26	-0.03	0.35
og	0.00	-0.28	-0.06	0.30
df	0.00	-0.31	-0.02	-0.11
Averages	0.00	-0.29	-0.04	0.10
Standard Deviation	0.00	0.02	0.02	0.26
FINAL VALUES	0.00	-0.29	-0.04	0.10
Final Values based on	group average			
Resulting HVF File Name	FA_S220_Reson	3160_5to750 and1000to	1500 and1750to5000	
		0.06 Value from stor	dard daviation of Lloading offe	
	gn StaDev gyro	0.20 Value from star	iuaru ueviation of Heading offs	iteh and roll affect volues
WIKU Aligh St	ubev Koll/Pitch	0.03 value from ave	rayeu stanuaru ueviations of p	iten and foil offset values

NARRATIVE

☑ HVF Hydrographic Vessel File created or updated with current offsets

Name: FA\_S220\_Reson8160\_5to750

Date: <u>19-Apr-07</u>

RPM/Pitch	Speed (m/s)	Speed (knots)	mog-Ave	bj-Ave	kb-Ave	Std. Dev.
0	0	0	0	0	0	0
145/40%	2.07	4	-0.064982971	-0.013021726	-0.018728741	0.028495599
150/40%	2.89	5.6	-0.01867823	0.001391433	0.022948255	0.02081767
150/80%	4.29	8.3	-0.019780177	0.001593794	0.086367291	0.056140712
150/90%	5.35	10.35	0.132309505	0.045112313	0.247795069	0.101669862
155/100%	6.10	11.8	0.195134109	0.02426495	0.258779328	0.121273779
185/100%	7.13	13.8	0.241202363	0.09212141	0.361192291	0.134797288







Average	8160 Depth		
0	0	Heave to 8111(m)	15.28
-0.032244479	-0.0310205	Heave to 8160(m)	14.7
0.001887152	0.00181552	Lever arm ratio	0.962042
0.022726969	0.0218643		
0.141738962	0.13635882		
0.159392796	0.15334255		
0.231505354	0.22271785		

# Blue cells used in computation of Delta Draft StDev used in TPE



# **NOAA POS/MV Calibration Report**

Ship:	hip: FAIRWEATHER ate: 3/29/2007		Vessel:	S220	_		
Date:			Dn:	088	-		
Personnel:	Lewis, Evans, Mills, Froelich						
PCS Serial #	¥ <u>2411</u>		IMU Serial	#	292		
IP Address:	129.100.1.23	1					
POS contro	ller Version (Use Menu Help	o > About)	3.3.2.2				
POS Version GPS Receiv	n (Use Menu View > Statisti ers	cs) Version 4					
	Primary Receiver	BD950 SN:4	BD950 SN:4611A66708 v.00211				
	Secondary Receiver	BD950 SN:4	BD950 SN:4602A62806 v.00211				
	on area						
Approximat	e Position:	Lat	55	14	26		
		Lon	131	38	31		
DGPS Beacon Station: Annette Isl		Annette Island			<u> </u>		
Frequency: 323		323					

#### **Satellite Constellation**

(Use View> GPS Data)



Secondary GPS



PDOP

1.904

(Use View> GAMS Solution)

### POS/MV Configuration Settings

Gams Parameter Setup	(Use Settings > Installation > GAMS Intallation)
GAMS Parameter Setup	×
Two Antenna Separation (m)	1.995
Heading Calibration Threshold (deg)	0.100
Heading Correction (deg)	0.000
Baseline Vector	
Component (m)	0.000
Y Component (m)	0.000
Z Component (m)	0.000
Close	Apply View

**Configuration Notes:** 

#### **POS/MV** Calibration

#### Calibration Procedure:

(Refer to POS MV V4 Installation and Operation Guide, 4-25)

Start time:	1810	
End time:	1812	
Heading accuracy achieved for calibration:		

0.352

#### **Calibration Results:**

ams Parameter Setup	(Use Settings > Installation > GAMS Inta
AMS Parameter Setup	×
I wo Antenna Separation (m)	1.997
Heading Calibration Threshold (deg)	0.100
Heading Correction (deg)	0.000
Baseline Vector	
× Component (m)	0.011
Y Component (m)	1.997
Z Component (m)	0.010
Ok     Close	Apply View

GAMS Status Online Save Settings

Yes	
Yes	

#### **General Notes:**

#### The POS/MV uses a Right-Hand Orthogonal Reference System

The right-hand orthogonal system defines the following:

• The x-axis is in the fore-aft direction in the appropriate reference frame.

• The y-axis is perpendicular to the x-axis and points towards the right (starboard) side in the appropriate reference frame.

The z-axis points downwards in the appropriate reference frame.

#### The POS/MV uses a Tate-Bryant Rotation Sequence

Apply the rotation in the following order to bring the two frames of reference into complete alignment:

a) Heading rotation - apply a right-hand screw rotation  $\theta z$  about the z-axis to align one frame with the other.

b) Pitch rotation - apply a right-hand screw rotation θy about the once-rotated y-axis to align one frame with the other.

c) Roll rotation - apply a right-hand screw rotation  $\theta x$  about the twice-rotated x-axis to align one frame with the other.

#### SETTINGS

Input/Output Ports

COM1

COM2

(Use Settings > Input/Output Ports)

Output Select       NMEA Output         NMEA       Image: Select         Image: Select       Image: Select         None       Image: Select         Image: Select       Imag	Baud Rate 9600 💌		Parity None Even Odd	Data Bits C 7 Bits C 8 Bits	Stop Bits FI © 1 Bit © 2 Bits C	ow Control- None Hardware XON/XOFF
U/Output Ports Set-up         coM1       COM2       COM3       COM4       COM5         Baud Rate       Parity       Data Bits       Stop Bits       Flow Cr         19200       Com3       Com4       Com5       Com5       Com6       7 Bits       C1 Bit       C Non         19200       Com3       Com3       Com4       Com5       Com5       Com5       Com5         Output Select       Binary       Update Rate       Frame       C Sensor 1       Prot Up       C Starb         Formula Select       Formula Select       Formula Select       Heave Positive Sense       Prot Up       C Starb         Input Select       None       V       V       V       Heave	Output Select NMEA • Input Select	NMEA Output \$PASHR \$PRDID \$PRDID \$INGGK \$UTC \$INPPS	TSS V TSS TSS	pdate Rate 1 Hz 💌 alker ID IN 💌	Roll Positive Sense Port Up Pitch Positive Sens Bow Up Heave Positive Sens Heave Up	Starboard U e Stern Up se Heave Down
Duty Come     Come     Come     Parity     Data Bits     Stop Bits     Flow C       19200     Image: Stop Bits     Flow C     7 Bits     G 1 Bit     Non       19200     Image: Stop Bits     Flow C     7 Bits     G 1 Bit     Non       Output Select     Binary     Update Rate     Frame     G 2 Bits     C 2 Bits     C 2 Dits       Binary     Update Rate     Frame     Sensor 1     Port Up     Starb       Formula Select     Formula Select     G Bow Up     C Heave Up     Heave       Input Select     None     Image: Starb     Image: Starb     Heave Up     Heave	t/Output Ports Set-up				Close	Apply
Output Select     Binary Output     Frame     Roll Positive Sense       Update Rate     C Sensor 1     Pitch Positive Sense       Formula Select     Sensor 2     Pitch Positive Sense       Formula Select     Sensor 2     Heave Positive Sense       Input Select     Heave Up     Heave	THE COMPANY AND	lesson lesson l				
Input Select None	OM1 COM2 COM3 Baud Rate 19200 -	COM4   COM5	Parity	Data Bits C 7 Bits @ 8 Bits	Stop Bits C 1 Bit C 2 Bits C 2 Bits	ow Control None Hardware XON/XOFF
	OM1 COM2 COM3 Baud Rate 19200 V Output Select Binary V	Binary Output Update Rate 25 Hz Formula Select TSS1	Parity © None © Even © Odd Frat © S C S t	Data Bits 7 Bits 8 Bits 8 Bits 9 Sensor 1 Sensor 2 ¥	Stop Bits         Fk           1 Bit         C           2 Bits         C           Roll Positive Sense         Pont Up           Pitch Positive Sense         Bow Up           Heave Positive Sense         Genuty	ow Control None Hardware XON/XOFF Starboard Up Starboard Up stern Up e teave Down

COM3

Input/Output Ports Set-up × COM1 COM2 COM3 COM4 COM5 Flow Control None Hardware XON/XOFF Parity None Even Odd Data Bits Stop Bits Baud Rate 9600 💌 C 7 Bits I Bit • 8 Bits C 2 Bits Output Select None 💌 Input Select Base GPS Input Base 1 GPS 💌 Input Type RTCM 1 or 9 👻 Line Serial C Modem Modem Settings Close Apply Input/Output Ports Set-up × COM1 COM2 COM3 COM4 COM5 
 Parity
 Data Bits
 Stop Bits

 © None
 C 7 Bits
 © 1 Bit

 © Even
 © 8 Bits
 C 2 Bits
 Flow Control None C Hardware C XON/XOFF Baud Rate 9600 💌 Output Select Roll Positive Sense Port Up C Starboard Up Pitch Positive Sense Bow Up C Stern Up SGPGST SGPGGA SGPHDT SGPZDA SGPVTG SGPVTG SPASHR Update Rate
 I Hz NMEA 💌 Talker ID GP Heave Positive Sense • Heave Up C Heave Down Input Select None 💌 Close Apply Input/Output Ports Set-up × СОМ1 СОМ2 СОМ3 СОМ4 СОМ5 
 Data Bits
 Stop Bits
 Flow Control

 C 7 Bits
 C 1 Bit
 C None

 C 8 Bits
 C 2 Bits
 C XON/XOFF
 Parity None Even Odd Baud Rate 9600 💌 NMEA Output Output Select Roll Positive Sense • Port Up C Starboard Up SGPGGA SGPGGA SGPHDT SGPZDA SGPVTG SPASHR Update Rate NMEA 💌 Pitch Positive Sense © Bow Up C Stern Up Input Select None Close Apply

COM5

COM4

#### SETTINGS Continued Heave Filter

(Use Settings > Heave)	
Heave Filter	×
C Z Altitude Heave Filter Heave Bandwidth (sec) 20.000 Damping Ratio 0.707	
Close Apply	

#### Events

(Use Settings > Events)
Events 🔀
Event 1
<ul> <li>Positive Edge Trigger</li> <li>Negative Edge Trigger</li> </ul>
Event 2
<ul> <li>Positive Edge Trigger</li> <li>Negative Edge Trigger</li> </ul>
Ok Close Apply

### INSTALLATION

(Use Settings > Installation)

Lever Arms and Mounting Angles

(Use Settings > Installation > Lever Arms and Offsets)

Lever Arms & Mounting Angles	Sensor Mounti	ng 🛛 Tags, Multipath & AutoStart	
Ref. to IMU Lever Arm X (m) 0.000	IMU Frame X (deg)	w.r.t. Ref. Frame	
Y (m) 0.000	Y (deg)	0.000	
Z (m) 0.000	Z (deg)	0.000	
Ref. to Primary GPS Lever Arm	⊐ ⊢ ⊓ ⊢Ref. to Ves	sel Lever Arm	
X (m) -11.920	X (m)	0.000	
Y (m) 1.177	Y (m)	0.000	
Z (m) -13.004	Z (m)	0.000	
Notes:	Ref. to Cen	tre of Rotation Lever Arm	
1. Ref. = Reference	X (m)	-7.028	
3. Reference Frame and Vesse	Y (m)	1.866	
Frame are co-aligned	Z (m)	-2.086	
	L		

(Use Settings > Installation > Tags, Multipath and Auto Start)

Lever Arms & Mounting Angle	es Sensor Mounting Tags, Multipath & AutoStart
Time Tag 1 © POS Time	Multipath © Low
O GPS Time	O Medium
<ul> <li>UTC Time</li> </ul>	C High
Time Tag 2 POS Time GPS Time UTC Time USer Time	
AutoStart C Disabled Enabled	

#### Sensor Mounting

#### (Use Settings > Installation > Sensor Mounting)

Lever Arms & Mounting Angle	es (Sei	nsor Mountin	g Tags, Multipath & AutoStart	
Ref. to Aux. 1 GPS Lever Arm				
X (m) 0.000		X (m)	0.000	
Y (m) 0.000		Y (m)	0.000	
Z (m) 0.000		Z (m)	0.000	
Ref. to Sensor 1 Lever Arm		Sensor 1 Fra	ame w.r.t. Ref. Frame	
X (m) 0.000		X (deg)	0.000	
Y (m) 0.000		Y (deg)	0.000	
Z (m) 0.000		Z (deg)	0.000	
Ref. to Sensor 2 Lever Arm		Sensor 2 Fr	ame w.r.t. Ref. Frame	
X (m) 0.000		X (deg)	0.000	
Y (m) 0.000		Y (deg)	0.000	
Z (m) 0.000		Z (deg)	0.000	

#### **User Parameter Accuracy**

(Use Settings > Installation > User Accuracy)

User Parameter Accu	racy	×
-RMS Accuracy-		
Attitude (deg)	0.050	
Heading (deg)	0.050	
Position (m)	2.000	
Velocity (m/s)	0.500	
ef Ok	Close	Apply
#### Frame Control

### (Use Tools > Config)

Navigator Configuration	×
Frame Control	Auxiliary GPS Position
C IMU Frame	💿 Normal
© User Frame	C Use regardless of status C Do not use
Primary GPS Measurement	GAMS
💿 Normal	Disable GAMS Solution
C Use regardless of status	
C Do not use	
Ok	se Apply

## GPS Receiver Configuration

Primary GPS Receiver	Gps Receiver Configuration	×
	Primary GPS Receiver     Secondary GPS Receiver       Primary GPS     GPS 1 Port       GPS Output Rate     Baud Rate       1 Hz     9600	Ţ
	Auto Configuration © Enabled © Disabled Ok Close Auto Configuration © Enabled Ok Close Apply	

Secondary GPS Receiver	Gps Receiver Configuration	×
	Primary GPS Receiver Secondary GPS Receiver	
	Secondary GPS GPS 2 Port Baud Rate 1 Hz 9600	
	Auto Configuration     Parity     Data Bits     Stop Bits       C Enabled     C Disabled     C 2 Bits       Ok     Close     Apply	





# SeaBat 8111 Noise Analysis

# 1.0 Overview

For mid and deep water sonar systems, noise emanating from the vessel on which the sonar is mounted is a major determinant in the performance of the sonar. In addition to sources such as echosounders and other acoustic devices, such as doppler logs, mechanical noise from the engines and drive trains, and flow noise will also affect performance, with the magnitude of the noise varying with vessel speed.

This document describes the noise analysis test done on the RESON SeaBat 8111 installed on the NOAA S/V Fairweather, on 11 October 2004.

# 2.0 Test Conduct

The following is a description of the system setup and test protocol used to test the SeaBat 8111 multibeam sonar.

## 2.1 Sonar Setup

To determine the amount of in-band noise seen by the sonar, the system was configured as follows:

Setting	Value
Power	Off
Gain	Manual Fixed 20
Range	100 meters

Data collection was done using a RESON engineering utility, which collects the full amplitude and phase time series data from the sonar. Figure 1 shows a sample screen capture, in this case one of the data sets taken at six knots, with a shaft speed of 140 RPM. At least ten (10) collections were done for each test case, and the results for first 10 measurements each test case were averaged for the report.

# 2.2 Vessel Operation

Normal survey speed for the vessel is approximately 10 knots. To bracket this range, and to check at possible lower survey speeds, the test protocol was defined to cover the range of 2 to 12 knots, in 2 knot steps. The tests were conducted at shaft speeds of 120 to 170 RPM, in 10 RPM steps, with the speed adjusted by changing the pitch on the propellers. For each RPM value, the speeds that could be achieved at that shaft speed were tested. A log of data collections for the tests is provided in Appendix A.



All the underway data collections were done in water depths of 120 to 160 fathoms. The zero speed data collections, with the engines on, were done at anchor in about 30 meters of water, and out in the bay, at water depths of about 130 fathoms.



Figure 1 - Snapshot Utility Screen Capture

# 2.3 Data Analysis

The data from each of the test cases were collated in an Excel spreadsheet, shown in Appendix B. A graph of the measured noise levels, as a function of vessel speed and shaft RPM is shown in Figure 2. The noise level is a unitless value that represents the average of all the amplitude samples, from all the beams for the sampled sonar ping. This value represents a combination of the electrical noise in the sonar, and the response to all acoustic energy, within the bandwidth of the sonar, impinging on the receive array.

For each the tests, the plot shows the noise level as a function of vessel speed. Again, the tests were run at the speeds that could be achieved at the selected shaft RPM.

In an effort to resolve the cause of the high noise levels at anchor seen in the 8160 tests, noise tests with the engines at idle (110 shaft RPM, 0 pitch) in both shallow and deep water. In deeper



water, much lower noise levels were observed, apparently due to the greater attenuation of the noise from the various acoustic sources on the ship over the greater range.



Figure 2 - Noise Plot

# 3.0 Conclusions

- a. It appears that the best survey speed for the 8111, from a noise perspective, is in the range of 8 to 10 knots. Both lower and higher speeds correlate with higher noise levels.
- b. It would be desirable to use shaft speeds of 140 RPM, or lower, to minimize the noise level seen by the sonar.
- c. Significantly increased levels of reverberation from acoustic sources on the vessel are seen in shallower water. If this causes any degradation in the quality of the soundings in the 8111, increased power levels, higher than those recommended in the sonar settings guide, should be used to compensate.



# Appendix A – Test Logs

🗐 s	urvey Log -	8111 Noise	e Test.xls										
	A	В	C	D	E	F	G	Н	1	J	K	L	M
1						RE	ESON I	nc.					
2	Date:	10/11	1/2004			Survey	Area:	Ru	dyerd Ba	y, AK	Page /	Pages:	1 of 2
3	Survey I	Name:	8111 No	se Test		Surveyo	ors:	B Bridg	е		TimeZo	ne:	-9
4	Survey '	Vessel:	NOAA F	airweathe	r	Client:		NOAA					
5	Offset	t Inforr	nation			51. S.							
6			X	Y	z	Latency	Roll	Pitch	Yaw		SVP File		
7	Sounder										Tide File		
8	DGPS								_	_			
9	Motion S	ensor				- D-44	of Details	<b>T</b> 4	-			I otal Pole	
10	Other			8.		Date	or Paten	Test			minus	Droft (7)	
												Drait (2)	
12	Start	Stop		Line		Dir.	Speed			сом	MENTS		
13			8111-00	<t-engon-< td=""><td>0001</td><td></td><td>0</td><td>Gain M</td><td>=20, Pow</td><td>er 0, Rar</td><td>nge 100, at</td><td>anchor, 1</td><td>10 RPM</td></t-engon-<>	0001		0	Gain M	=20, Pow	er 0, Rar	nge 100, at	anchor, 1	10 RPM
14			8111-00	<u> </u>	~ .	a. a	0	110 RP	M 0 Pitch	1			
15			8111-02	<u>4-120-00</u>	01		2	120 RP	M 1.0 Pit	ch 0.4 Do	oppler		
16			8111-04	4 120-00	01	2	4	120 RP	MEDDIE		oppier		
17			8111-00	4-120-00	01	\$1 <mark></mark>	8	120 RF	M 8 5 Pit	ch 6 7 Dr	oppler		
19			8111-10	d-120-00	01	2) 2)	9	120 RP	M 10.0 P	itch 7.2 F	Doppici Doppler		
20			8111-10	t-130-00	01		10	130 RPM 10.0 Pitch 8.2 Doppler					
21			8111-08	t-130-00	01		8	3 130 RPM 7.0 Pitch 6.2 Doppler					
22			8111-06	8111-06kt-130-0001			6	6 130 RPM 5.0 Pitch 4.5 Doppler					
23			8111-04	d-130-00	01		4	130 RP	M 3.0 Pit	ch 2.2 Do	oppler		
24			8111-02	<u> </u>	01		2	130 RP	M 1.5 Pit	ch 0.5 Do	oppler		
25			8111-04	<u> </u>	01		4	140 RP	M 2.5 Pit	ch 2.5 Do	oppler	<u></u>	
26			8111-06	<u> 4 4 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 </u>	01	3 2	6	140 RP	M 4.75 P	Itch 4.3 L	oppler I o	o Shallow	
2/			9111-00	8111-06kt-140-0002				140 KP	N 7 4 Dit	01 0.2 D(	uppier		
20	20		8111-00	140-00 1140-00	01	3) 3)	10	140 RP	M 9 N Pit	ch 8 5 D(	oppier oppler		
30				- 1 <del>-1</del> 0-00	01		10	14010	141 O.O.I. IL	01 0.0 D(	pploi		
31			2										
32	Survey N	lanager:				28	Client R	epresent	tative:				
33	Signature	e:					Signatur	e:					
34							12:25						
35	▶ ▶ \She	et1 / Sheel	:2 / Sheet3 /	· · · · ·					•				



📑 S	urvey Log -	8111 Noise	e Test Pg2.xl	5									
	A	В	C	D	E	F	G	Н	1	J	K	L	M
1						RE	ESON I	nc.					
2	Date:	10/1	1/2004			Survey	Area:	Ru	dyerd Bay	y, AK	Page / I	Pages:	2 of 2
3	Survey	Name:	8111 Noi	ise Test		Surveyo	ors:	B Bridg	e		TimeZor	ne:	-9
4	Survey '	Vessel:	NOAA Fa	ainweathe	er	Client:		NOAA					
5	Offset	t Inforr	nation										
6			X	Y	z	Latency	Roll	Pitch	Yaw		SVP File		
7	Sounder										Tide File		
8	DGPS												
9	Motion S	ensor					6.0.4.1	-				Fotal Pole	
10	Other		5	55		Date	of Patch	lest	-		minus	Dry Pole	
		10.11	-				1277 - 17					Draft (Z)	-
12	Start	Stop		Line		Dir.	Speed			сомі	MENTS		
13			8111-10	<t-150-00< th=""><th>101</th><th>0</th><th>10</th><th>Gain MF</th><th>F20, Pow</th><th>er 0, Rang</th><th>ge 100, 15</th><th>i0, 8.2, 7.</th><th>4</th></t-150-00<>	101	0	10	Gain MF	F20, Pow	er 0, Rang	ge 100, 15	i0, 8.2, 7.	4
14			8111-08	kt-150-00	102		8	150 RP	M 6.1 Pite	ch 6.3 Do	ppler		
15			8111-06	<u>kt-150-00</u>	101		6	150 RP	M 4.3 Pit	ch 4.4 Do	ppler		
16			8111-04	<u>- 150-00</u>	101	<u>.</u>	4	150 RP	M 3.0 Pit	ch 2.8 Do	ppler		
17	2		8111-06	<1-160-00	101	2 2	6	160 RP	M 4.0 Piti	ch 5.2 Do	ppler		
18			0111-00	4-100-00	01	* *	10	160 RP	M Q 2 Dit.	ch 9 9 Do	ppier pplor		
20			8111-12	4-160-00	101	2	11 7	160 RP	M 10 Pit	ch 9 9 Do	ppiei nnler		
21			8111-12	d-170-00	01	n n	12	170 RP	M 9.0 Pit	ch 10.4 D	oppler		
22			8111-06	kt-170-00	101	20 21	6	170 RP	M 4.0 Pit	ch 4.8 Do	ppler		
23			8111-08	kt-170-00	01		8	170 RP	M 5.9 Pite	ch 6.8 Do	ppler		
24			8111-10	kt-170-00	101		10	170 RP	M 7.0 Pit	ch 8.3 Do	ppler		
25													
26						<u>.</u>							
27			8			2 2							
28			-			<u>.</u>							
29			2			2. 2							
31						2							
32	Survev N	l 1anader:				-	Client R	epresent	ative:				
33	Signature	e:	8				Signatur	'е:					
34													
35	▶ ▶ \She	et1 / Sheel	t2 / Sheet3 /	r					•				



# Appendix B – Noise Analysis Spreadsheet

Eng On Shallow Eng On Deep 120 RPM	Concernance of	Pitch (ft)					rest Case						Average
Eng On Shallow Eng On Deep 120 RPM			-	2	m	4	Ś	9	2	8	0	9	
Eng On Deep	0	0	707.5	740.2	754.1	711.4	728.1	710.6	691.5	747.9	813.7	722.1	732.7
120 RPM	0	0	209.0	208.4	208.6	207.2	205.6	211.2	206.3	208.8	210.9	210.0	208.6
	2.0	1.0	382.8	363.0	363.6	330.6	447.5	315.2	389.0	322.1	371.9	371.1	365.7
	4.0	3.0	552.7	431.0	555.9	480.0	517.9	448.0	472.8	500.7	583.6	499.2	504.2
	6.0	6.0	325.5	332.9	302.5	322.9	324.8	364.2	325.8	384.3	409.1	407.4	349.9
	8.0	8.5	253.8	244.0	250.3	253.0	248.4	241.0	241.7	252.4	253.5	259.1	249.7
	9.0	10.0	298.8	296.8	277.4	306.1	284.1	274.0	274.1	290.1	287.5	291.9	288.1
130 RPM	2.0	1.5	316.9	363.0	366.1	429.6	317.1	313.9	303.7	315.5	315.5	289.4	333.1
	4.0	3.0	671.0	657.4	700.4	632.7	602.6	631.0	552.5	605.8	537.9	523.7	611.5
	6.0	5.0	488.2	471.1	410.9	497.2	387.7	390.9	431.0	448.9	361.3	393.5	428.1
	8.0	7.0	285.2	279.1	276.7	266.2	287.8	268.3	271.0	262.5	283.4	249.9	273.0
	10.0	10.0	362.8	396.1	378.8	378.2	370.2	391.7	354.6	369.9	334.3	374.0	371.1
RPM 140	4	2.5	763.9	725.6	669.0	723.3	759.5	751.5	773.5	750.6	689.0	785.7	739.2
	9	5.3	487.1	551.5	605.3	596.4	444.3	480.0	416.2	500.0	452.6	478.9	501.2
	8	7.4	261.5	257.6	260.7	273.1	259.8	274.8	255.0	252.1	248.7	270.6	261.4
	10	9.0	301.5	365.3	328.4	360.1	359.9	328.4	326.2	315.0	302.7	300.4	328.8
RPM 150	4	3.0	775.2	766.3	916.9	809.7	815.4	860.6	710.5	801.1	892.1	928.6	827.6
	9	4.3	1058.7	926.7	737.5	1015.6	1028.1	1086.3	1048.8	1133.8	997.3	931.8	996.5
	80	6.1	507.8	567.2	535.4	486.4	507.3	443.4	460.9	537.6	461.0	406.4	491.3
	10	8.2	299.2	294.1	315.8	306.5	308.4	323.2	348.8	336.8	332.8	344.5	321.0
160 RPM	9	4.0	1488.4	1551.6	1328.3	1454.8	1456.9	1518.9	1256.4	1146.3	1089.5	1005.8	1329.7
	8	6.1	740.7	777.4	926.5	904.7	851.6	817.7	886.5	801.0	1005.7	1015.9	872.8
	10	8.2	339.9	330.9	335.0	329.4	300.6	326.7	316.9	311.6	313.7	300.9	320.6
	12	10.0	581.4	396.6	351.5	360.6	344.6	410.5	466.2	357.1	389.6	386.4	404.5
170 RPM	9	4.0	1240.1	1173.3	1016.2	1346.1	1301.8	1391.5	1520.2	1327.6	1320.2	1176.3	1281.3
	80	5.9	961.9	1096.9	1229.4	1017.2	1041.2	1168.9	1176.6	1060.5	1117.9	1112.2	1098.3
	10	7.0	756.2	751.3	747.9	640.1	769.5	844.8	714.6	795.6	787.4	709.4	751.7
	12	0.6	396.2	360.1	552.7	339.9	348.5	339.3	352.6	356.5	502.1	351.7	390.0

## Total Propagated Error (TPE)

## **TPE Values**

Standard Deviation

FAIRWEATHER SURVEY	Doc. No. REP-6XX	Appendix IV	Process Owner Survey
Documents Title	Last update	Version	Approval Date
FA_TPE_Values_2007	Apr 23, 2007	2006.2	

Offsets					
	Vessel	FAIRWEATHER-S220	FAIRWEATHER-S220	1010	1018
	Sonar System	Reson 8111	Reson 8160	Reson 8101	Reson 8101
	Positioning System	POS/MV	POS/MV	POS/MV	POS/MV
		Model 320	Model 320	Model 320	Model 320
	MRU to Trans X	2.868	0.493	0.247	0.286
	MRU to Trans Y	8.252	7.665	-0.138	-0.141
	MRU to Trans Z	4.752	4.726	0.551	0.551
Offsets	Nav to Trans X	1.691	-0.684	1.144	1.184
	Nav to Trans Y	20.172	19.585	1.061	0.96
	Nav to Trans Z	17.756	17.730	3.667	3.711
	Trans Roll	0.00	0.00	0.00	0.00

Standard	Deviation						
	Vessel	FAIRWEATHER-S220	FAIRWEATHER-S220	1010	1018		
	Sonar System	Reson 8111	Reson 8160	Reson 8101	Reson 8101		
	Positioning System	POS/MV	POS/MV	POS/MV	POS/MV		
		Model 320 V4	Model 320 V4	Model 320 V3	Model 320 V3		Status
	Motion Gyro (deg)	0.02	0.02	0.02	0.02		Finalized
	Heave% Amp	5	5	5	5		Finalized
Motion	Heave (m)	0.05	0.05	0.05	0.05		Finalized
Sonsor	Roll (deg)	0.02	0.02	0.02	0.02		Finalized
3611301	Pitch (deg)	0.02	0.02	0.02	0.02		Finalized
	Position Nav (m)	0.5*	0.5	0.5	0.5	e	Finalized
	Vessel Speed (m/s)	0.03	0.03	0.03	0.03	Ξ	Finalized
	Timing Trans (s)	0.005	0.005	0.005	0.005	5	Finalized
	Nav Timing (s)	0.005	0.005	0.005	0.005	atio	Finalized
Latency	Gyro Timing (s)	0.005	0.005	0.005	0.005	- n	Finalized
Latency	Heave Timing (s)	0.005	0.005	0.005	0.005	ıfig	Finalized
	Pitch Timing (s)	0.005	0.005	0.005	0.005	Lo Lo	Finalized
	Roll Timing (s)	0.005	0.005	0.005	0.005	0	Finalized
Vessel	Offset X (m)	0.007	0.007	0.007	0.007	sse	Finalized
Offecte	Offset Y (m)	0.007	0.007	0.007	0.007	jë	Finalized
Onsets	Offset Z (m)	0.008	0.008	0.007	0.007	-	Finalized
	Loading	0.02	0.02	0.01	0.01		Finalized
Waterline	Draft (m)	0.022	0.022	0.016	0.016		Finalized
	DeltaDraft (m)	0.075	0.075	0.007	0.05		Finalized
MRU	MRU alignStdev gyro	0.05	0.26	0.10	0.09		Finalized
Alignment	MRU align roll/pitch	0.11	0.03	0.13	0.06		Finalized
Tides	Tide Meas (m)	0.01	0.01	0.01	0.01	9	Project Dependent
Tides	Tide Zoning (m)	0.1	0.1	0.1	0.1	리 뛰 일 경	Project Dependent
Sound	SV Meas (m/s)	0.5	0.5	1.0	1.0	E H E	Finalized
Velocity	Surface SV (m/s)	0.5	0.5	1.0	1.0		Finalized

\*Position Nav adjusted in the HVF to 5m when acquiring in Coarse Acquisition mode, additional information will be submitted in the DAPR and/or the DR.

## **Additional Calibration Reports**

## Control

- Ashtech
  - Positioning Equipment Confidence Check
  - OPUS solution
- Tides
  - . Kukkamakis 2006
  - · Vertical Control Equipment Testing
- Trimble
  - Positioning Equipment Confidence Check
  - OPUS solution
  - See SAND1.ssf attached in digital separates

## Diver Least Depth Gauge (DLDG)

• See cal files attached in digital separates

## Laser Level

## Leadlines

SV

- MVP
  - Penetrometer
- SBE
  - SBE 19plus
    - SBE 19plus 4585
    - SBE 19plus 4616
    - SBE 19*plus* 4617
  - SBE 45 TSG



Subject: OPUS solution : USCG0732.070 000106232 From: opus@ngs.noaa.gov Date: Mon, 02 Apr 2007 12:07:31 -0400 (EDT) To: horcon.fairweather@noaa.gov FILE: USCG0732.070 000106232 NGS OPUS SOLUTION REPORT \_\_\_\_\_ USER: horcon.fairweather@noaa.gov DATE: April 02, 2007 RINEX FILE: uscg073s.07o TIME: 16:07:30 UTC START: 2007/03/14 18:06:00 SOFTWARE: page5 0612.06 master29.pl EPHEMERIS: igs14183.eph [precise] STOP: 2007/03/14 20:36:00 OBS USED: 6385 / 6511 : 98% NAV FILE: brdc0730.07n ANT NAME: ASH701975.01AGP NONE # FIXED AMB: 30 / 32 : 94% ARP HEIGHT: 2.0 OVERALL RMS: 0.018(m) REF FRAME: NAD 83(CORS96)(EPOCH:2003.0000) ITRF00 (EPOCH: 2007.1995) -2415359.692(m) 0.013(m) x: -2415358.884(m) 0.013(m) Y: -2718046.175(m) 0.012(m) -2718045.070(m) 0.012(m) 5222559.312(m) 0.016(m) 5222559.510(m) 7: 0.016(m) 0.010(m) 55 19 58.66133 0.010(m) 55 19 58.67266 LAT: E LON: 228 22 28.18023 0.007(m) 228 22 28.10433 131 37 31.89567 0.007(m) W LON: 131 37 31.81977 0.007(m) 0.007(m)EL HGT: 3.781(m) 0.023(m) 3.780(m) 0.023(m) ORTHO HGT: 9.656(m) 0.034(m) [Geoid06 NAVD88] UTM COORDINATES STATE PLANE COORDINATES UTM (Zone 09) SPC (5001 AK 1) Northing (Y) [meters] 6134983.221 0.000 Easting (X) [meters] 333464.469 0.000 Convergence [degrees] -2.15989540 0.0000000 Point Scale 0.99994023 0.00000000 0.99993963 Combined Factor 0.00000000 US NATIONAL GRID DESIGNATOR: 9UUB3346434983(NAD 83) BASE STATIONS USED PID DESIGNATION LATITUDE LONGITUDE DISTANCE(m) AI5022 BIS1 BIORKA ISLAND 1 CORS ARP N565116.162 W1353221.387 296620.8 AJ4430 LEV1 LEVEL ISLAND 1 CORS ARP N562756.438 W1330533.935 155968.5 AF9530 AIS1 ANNETTE ISLAND 1 CORS ARP N550408.647 W1313558.255 29425.1

NEAREST NGS PUBLISHED CONTROL POINT AI4914 BM NO 37 N551958.659 W1313731.820 0.0

### BASE STATION INFORMATION

STAT	ION NAME: bisl	a 5 (BIORKA 1	[SLAND 1; Bior]	ka Island, Alaska, U.S.A.)
ANT	ENNA: ASH700829	.3 SNOW		S/N=xxxx
XYZ	-2494921.0213	-2448390.9324	5317113.5289	MON @ 1997.0000 (M)
XYZ	-0.0164	0.0037	0.0005	VEL (M/YR)
NEU	0.0000	0.0000	0.0000	MON TO ARP (M)
NEU	-0.0000	0.0000	0.0877	ARP TO L1 PHASE CENTER (M)
NEU	-0.0000	0.0000	0.0598	ARP TO L2 PHASE CENTER (M)
XYZ	-0.1673	0.0377	0.0051	VEL TIMES 10.1982 YRS
XV7	0 0000	0 0000		MON TO ARP
XV7	_0_0342	-0.0336	0.0000	APD TO I.1 DHASE CENTER
XIZ VV7	-2404021 2220	-2448390 9283	5217112 6074	I DUG CEN @ 2007 1995
XIZ VV7		0 0014	0 0005	
XV7	_2494921 2228	-2448390 9269	5317113 6080	NEW 11 DHS CEN @ 2007 1995
XV7	2494921.2220 2404021.1006	2440300.0200	5317113.0000 5217112 5245	NEW ADD @ 2007 1005
AIA VV7	-2494921.1000	-2440390.0933	551/115.5545	NEW ARP @ 2007.1995
	-2494921.1000		$\frac{531}{113.5545}$	NEW MON @ 2007.1995
ЦЦН Т Т Т ТТ	50 51 10.17228			NEW LI PHS CEN @ 2007.1995
LLH	56 51 16.1/228		7 66.5910 7 66.5910	NEW ARP @ 2007.1995
ЦЦΗ	56 51 16.1/228	224 27 38.5326	66.5910	NEW MON @ 2007.1995
		0 (7 ] 7		
STAT	ION NAME: LEVI	a 8 (Level 19	sland 1; Level	Island, Alaska USA)
AN'I'	ENNA: ASH700829	.3 SNOW		S/N=CG11936
XYZ	-2412828.4670	-2579056.1235	5293283.3535	MON @ 1997.0000 (M)
XYZ	-0.0190	0.0003	-0.0044	VEL (M/YR)
NEU	0.0000	0.0000	0.0000	MON TO ARP (M)
NEU	-0.0000	0.0000	0.0877	ARP TO L1 PHASE CENTER (M)
NEU	-0.0000	0.0000	0.0598	ARP TO L2 PHASE CENTER (M)
XYZ	-0.1938	0.0031	-0.0449	VEL TIMES 10.1982 YRS
XYZ	0.0000	0.0000	0.0000	MON TO ARP
XYZ	-0.0331	-0.0354	0.0731	ARP TO L1 PHASE CENTER
XYZ	-2412828.6939	-2579056.1558	5293283.3817	L1 PHS CEN @ 2007.1995
XYZ	-0.0002	0.0006	0.0002	+ XYZ ADJUSTMENTS
XYZ	-2412828.6941	-2579056.1552	5293283.3819	NEW L1 PHS CEN @ 2007.1995
XYZ	-2412828.6610	-2579056.1198	5293283.3088	NEW ARP @ 2007.1995
XYZ	-2412828.6610	-2579056.1198	5293283.3088	NEW MON @ 2007.1995
LLH	56 27 56.44916	226 54 25.98578	3 25.2831	NEW L1 PHS CEN @ 2007.1995
LLH	56 27 56.44916	226 54 25.98578	3 25.1954	NEW ARP @ 2007.1995
LLH	56 27 56.44916	226 54 25.98578	3 25.1954	NEW MON @ 2007.1995
STAT	ION NAME: aisl	a 7 (ANNETTE	ISLAND 1; Anne	ette Island, Alaska, U.S.A.)
ANT	ENNA: ASH700829	.3 SNOW		S/N=11276
XYZ	-2430153.7846	-2737192.8996	5205816.6147	MON @ 1997.0000 (M)
XYZ	-0 0151	0 0008	-0 0082	VEL (M/YR)
NEII	0 0000	0 0000	0 0000	MON TO ARP $(M)$
NEU	-0.0000	0 0000	0.0000	ARD TO I.1 DHASE CENTER $(M)$
NEII	-0.0000	0.0000	0.0077	ARE TO BE PHASE CENTER $(M)$
XV7	-0.1540	0.0000	-0.0836	VEL TIMES 10 1082 VPS
AIA VV7	0.1040	0.0002	0.0030	MON TO ADD
AIL VV7		0.0000	0.0000	MUNIUARP
AIL VV7	-0.0333	-0.03/0		ARF IU LI FHASE CENIER
AIZ XXZ	-2430153.9/19	-2/3/192.9290	0.000.0102020	LI PHS CEN @ 200/.1995
AIZ XXZ	U.UUUL	-U.UUUL 2727100 0001		+ AIZ ADJUSIMENTS
ΧYΖ	-2430153.9/18	-2/3/192.9291	5∠058⊥0.6030	NEW LI PHS CEN @ 2007.1995

XYZ	-2430153.9385	-2737192.8915	5205816.5311	NEW ARP @ 2007.1995
XYZ	-2430153.9385	-2737192.8915 5	5205816.5311	NEW MON @ 2007.1995
LLH	55 4 8.65871	228 24 1.66998	32.2471	NEW L1 PHS CEN @ 2007.1995
ЦЦН Т Т Т Т	55 4 8.658/1	228 24 1.66998	32.1594	NEW ARP @ 2007.1995
НЦЦ	55 4 8.058/1	228 24 1.00998	32.1594	NEW MON @ 2007.1995
		REMOTE STATIC	ON INFORMATIC	DN
STAT	ION NAME: uscg	1		
ANT	ENNA: ASH701975	.01AGP NONE		S/N=UNKNOWN
XYZ	-2415360.3793	-2718045.5588 5	5222561.1762	MON @ 2007.1993 (M)
NEU	0.0000	-0.0000	2.0000	MON TO ARP (M)
NEU	-0.0000	0.0000	0.0637	ARP TO LI PHASE CENTER (M)
NEU XV7	-0.0000	-0.8504	1 6449	MON TO ARD
XYZ	-0 0241	-0.0271	0 0524	ARP TO L1 PHASE CENTER
XYZ	-2415361.1590	-2718046.4363	5222562.8735	L1 PHS CEN @ 2007.1995
BASE	LINE NAME: bi	sl uscg		
XYZ	0.6817	0.4813	-1.6607	+ XYZ ADJUSTMENTS
XYZ XV7	-2415360.4774		5222561.2128	NEW LI PHS CEN @ 2007.1995
XIZ VV7	-2415300.4533 -2415350.6076	-2/18045.92/8	5222561.16U4 5222550 5155	NEW ARP @ 2007.1995 NEW MON @ 2007 1995
T.T.H	55 19 58 67251	278 22 28 10438	5 8533	NEW MON @ 2007.1995 NEW L1 PHS CEN @ 2007 1995
TTTH	55 19 58.67251	228 22 28.10438	5.7896	NEW ARP @ 2007.1995
LLH	55 19 58.67251	228 22 28.10438	3.7896	NEW MON @ 2007.1995
BASE	LINE NAME: le	vl uscg	1	
XYZ	0.6864	0.4936	-1.6609	+ XYZ ADJUSTMENTS
XYZ XV7	-2415360.4/2/	-2/18045.942/ 5	5222561.212/	NEW LI PHS CEN @ 2007.1995
AIZ VV7	-2415360.4466	-2718045.9150	5222501.1003	NEW ARP @ 2007.1995 NEW MON @ 2007 1995
T.T.H	55 19 58 67284	278 22 28 10412	5 8462	NEW MON @ 2007.1995 NEW L1 PHS CEN @ 2007 1995
LLH	55 19 58.67284	228 22 28.10412	5.7825	NEW ARP @ 2007.1995
LLH	55 19 58.67284	228 22 28.10412	3.7825	NEW MON @ 2007.1995
BASE	LINE NAME: ai	sl uscg	1 (5)	
XYZ	0.6951	0.4928	-1.6769	+ XYZ ADJUSTMENTS
XYZ	-2415360.4639	-2/18045.9435	5222561.1967	NEW LI PHS CEN @ 2007.1995
AIZ VV7	-2415360.4396 -2415359.6842	-2718045.9164	5222501.1445	NEW ARP @ 2007.1995 NEW MON @ 2007 1995
TTH	55 19 58 67268	228 22 28 10452	5.8300	NEW L1 PHS CEN @ 2007.1995
LLH	55 19 58.67268	228 22 28.10452	5.7663	NEW ARP @ 2007.1995
LLH	55 19 58.67268	228 22 28.10452	3.7663	NEW MON @ 2007.1995
		G-I	FILES	
∆xx20	07 314 7 314			
B2007	31418 5 7 31	42035 1 page5 v061	12.06IGS	222 1 2 27NGS 2007 4 2IFDDFX
Iant	info.003	NGS 20070320		
C0009	0001 -795614910	19 2696541842	21 9455401	.90 39 X0737AUSCGX0737ABIS1
D 1	2 7550588 1	3 -9307589 2 3	-7806480	
700				
AXX20	21/10 F 7 21	12025 1 page	12 06709	200 1 0 07MCC 2007 4 01
BZUU/ Tant	info 003	NGS 20070320	17.00102	ZZZ I Z Z/INGO ZUU/ 4 ZIFDDFX
C0009	0002 25310319	17 1389889454	20 7072379	35 38 X0737AUSCGX0737ALEV1
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## D 1 2 8189618 1 3 -9202066 2 3 -7448116

Axx2007 314 7 314 B2007 31418 5 7 3142035 1 page5 v0612.06IGS 222 1 2 27NGS 2007 4 2IFDDFX Iant\_info.003 NGS 20070320 C00090003 -147942543 19 -191478255 22 -167429683 36 X0737AUSCGX0737AAIS1 D 1 2 9369495 1 3 -7883557 2 3 -7554607

#### POST-FIT RMS BY SATELLITE VS. BASELINE

	OVERALL	03	06	07	10	16	18	19	21
bis1-uscg	0.017	0.018	0.016	0.018	0.014	0.019	0.013	0.015	
	22	24	25	26	29	30			
bis1-uscg	0.018	0.015		0.022	0.019				
	OVERALL	03	06	07	10	16	18	19	21
lev1-uscg	0.018	0.017	0.018	0.019	0.017	0.022	0.017	0.015	
	22	24	26	29	30				
lev1-uscg	0.018	0.013	0.018	0.021					
	OVERALL	03	06	07	10	16	18	19	21

aisl-uscg 0.018 0.020 0.018 0.018 0.012 0.022 0.016 ... ... 22 24 26 29 30 aisl-uscg 0.015 0.017 0.015 0.016 ...

## OBS BY SATELLITE VS. BASELINE

	OVERALL	03	06	07	10	16	18	19	21
bis1-uscg	2148	155	203	279	102	296	245	28	
	22	24	25	26	29	30			
bis1-uscg	118	284		200	238				
	OVERALL	03	06	07	10	16	18	19	21
lev1-uscg	2087	155	182	225	106	296	247	28	
	22	24	26	29	30				
lev1-uscg	117	284	200	247					
	OVERALL	03	06	07	10	16	18	19	21
ais1-uscg	2150	152	207	284	105	295	239		
	22	24	26	29	30				
aisl-uscg	119	283	213	253	• • •				

Covariance Matrix	for the xyz OPU	S Position (meters2).
0.000022467	0.000002159	-0.000004052
0.000002159	0.0000029444	-0.000004008
-0.000004052	-0.000004008	0.000094689
Covariance Matrix	for the enu OPU	S Position (meters2).
0.000023402	-0.000002845	0.000001534
-0.000002845	0.0000044782	0.000029060
0.000001534	0.0000029060	0.000078416
Horizontal network	accuracy =	0.00458 meters.
Vertical network a	accuracy =	0.00549 meters.

Derivation of NAD 83 vector components

Position of reference station ARP in NAD\_83(CORS96)(EPOCH:2003.0000). Xa(m) Ya(m) Za(m) BIS1 -2494920.37852 -2448391.99956 5317113.26406 2003.00 LEV1 -2412827.84636 -2579057.21856 5293283.07789 2003.00 AIS1 -2430153.14737 -2737194.00189 5205816.33593 2003.00 Position of reference station monument in NAD\_83(CORS96)(EPOCH:2003.0000). Xr(m) Yr(m) Zr(m) BIS1 -2494920.37852 -2448391.99956 5317113.26406 2003.00 LEV1 -2412827.84636 -2579057.21856 5293283.07789 2003.00 AIS1 -2430153.14737 -2737194.00189 5205816.33593 2003.00 Velocity of reference station monument in NAD\_83(CORS96)(EPOCH:2003.0000). Vx (m/yr) Vy (m/yr) Vz (m/yr) BIS1 0.00490 0.00450 0.00990 LEV1 0.00220 0.00120 0.00480 0.00170 AIS1 0.00580 0.00110 Vectors from unknown station monument to reference station monument in NAD 83(CORS96)(EPOCH:2003.0000). Yr-Y= DY(m) Xr-X= DX(m) Zr-Z=DZ(m)-79561.49452 269654.17544 94553.95206 2003.00 BIS1 LEV1 2531.03764 138988.95644 70723.76589 2003.00

This position and the above vector components were computed without any knowledge by the National Geodetic Survey regarding the equipment or field operating procedures used.

-16742.97607

2003.00

-14794.26337 -19147.82689

AIS1

## Kukkamaki March 13 & 14, 2007

On March 13, 2007 (Dn072) LTJG Lewis, ST Mills and ENS Morgan performed a Kukkamaki on both Carl Zeiss NI2 (stadia: 333) levels (S/N 103267 and S/N 100056).

The Kukkamaki course was set up at the NOAA base in Ketchikan, AK in the early afternoon. The sky was overcast with occasional snow showers passing intermixed with occasional rain. A 40 meter straight line was set up on relatively level ground and divided into 10 meter intervals. The level was then set up on the 30 meter mark and a backsight and foresight were shot to the 20 and 40 meter marks respectively. Next, the level was set up at the 0 meter mark, and a backsight and foresight were shot to the 20 and 40 meter marks, respectively. (See *fig. 1*)

The Carl Zeiss level S/N 103267 had a collimation error of 0.0066, which is within tolerance. The Carl Zeiss level S/N 100056 had a collimation error of -0.176, which is not within tolerance. The kukkamaki was run 2 more times on that level and still did not pass within tolerance. An adjustment was made to the level to calibrate it for the error recorded during the kukkamaki. After the level S/N 100056 was re-calibrated, another kukkamaki was run on March 14, 2007 (Dn073) and the level was within tolerance with a collimation error of 0.02.



Fig 1. Diagram of Kukkamaki setup.

NOAA	IOAA FORM 75-29 U.S. DEPARTMENT OF COMMER						ON			NUMBER	SHEET	OF
(12-			ΝΛΤ									
(12- 75)			INAT	ATMOS	PHERIC							
				ADMINIST	RATION	FROM B M				ТОВМ		
	PREC	SISE LEV	ELING									
		THREE-WIR	F				Kukk	amak		ТІМЕ	DATE: DN 072, 13	March 2007
						WEATHER	Overcast with	n snow showe	ers			
	FORWARD	RUN (See re	verse for BAC	CKWARD RUN	1)							
		BAC	SIGHTS				FORE	SIGHTS		3 ORDER, CL/	ASS1	
Setup	THREAD READING	MEAN	THREAD INTERVAL	SUM OF INTERVALS	ROD TEMP	THREAD READING	MEAN	THREAD INTERVAL	SUM OF INTERVALS	REMARKS	3	
	1558	BS1				1602	FS1			$C = (\Delta h1 - \Delta 2)$	<u>- 0.2mm</u>	
1	<mark>1543</mark>	1543				1588	1587.67			20 m		
	1528					1573				where BS1 - FS1	l = ∆h1	
	4629					4763				BS2 - FS2	= Δh2	
											T	
	1220	20mS				1295	40mS			<u>Δh1-</u>	-44.67	
2	1190	1190				1235	1235			<u>Δh2</u>	-45	
	1160					11/5				Δh1-Δh2 =	0.33	
	3570					3705				- 0.2 (CR)	0.13	
										÷20m	0.00666667	
										<b>C</b> -	0.0000007	
				abada								
				snaded	a cei	IS.				"C" must be < +	0.05mm/m	
										Instrument SN: 103267		
										Rod SN: B		
										Party Chief: Beaver		
<u> </u>										Observer: Mills		
<u> </u>										Recorder. Lewis		
<u> </u>												

NOAA	IOAA FORM 75-29 U.S. DEPARTMENT OF COMMERCE					TIDE STATI	ON			NUMBER	SHEET	OF
(10												
(12- 75)			NAT	IONAL OCEAN ATMOS	NIC AND							
- /				ADMINIST	RATION							
	PREC					FROM B.M.				IO B.M.		
							Kuld	omok		TIME	DATE DN 072.13	March 2007
		THREE-WIR	E				NUKK	amak			- , -	
	FORWARD	RUN (See re	verse for BAC	KWARD RUN	Ŋ	WEATHER	Overcast with	n snow showe	ers			
		BAC	SIGHTS				FORE	SIGHTS		3 ORDER, CLASS1		
Setup	tup THREAD MEAN THREAD SUM OF ROD THRE READING MEAN THREAD INTERVALS TEMP READ						MEAN	THREAD INTERVAL	SUM OF INTERVALS	REMARKS	3	
	1588	BS1				1634	FS1			C = (Δh1 - Δ2)	- 0.2mm	
1	1573	1573.33				1618	1618.67			20 m		
	1559					1604				where BS1 - FS1	l = ∆h1	
	4720					4856				BS2 - FS2 :	= Δh2	
	1278	20mS				1350	40mS			Δh1-	-45.33	
2	1248	1248				1290	1290			Δh2	-42	
	1218					1230				Δh1-Δh2 =	-3.33	
	3744					3870				- 0.2 (CR)	-3.53	
				1	1					÷20m	-0.17666667	
										C =	-0.17666667	
<u> </u>												
	Fi	ll in YE	LLOW	shade	d cel	ls.				"C" must bo < + (	0.05mm/m	
										o must be < i t	0.001111/11	
<u> </u>										Instrument SN: 100056		
<u> </u>										Rod SN: B		
<u> </u>										Party Chief: Beaver		
										Observer: Lewis		
									Recorder: Mills			
									Rod Person: Morgan			

NOAA	IOAA FORM 75-29 U.S. DEPARTMENT OF COMMERCI					TIDE STATI	ON			NUMBER	SHEET	OF
(10												
(12- 75)			INAT	ATMOS								
,				ADMINIST	RATION	FROM R M						
	PREC					FROM B.M.				ТО В.М.		
			_				Kukk	amak		TIME	DATE DN 072, 13	March 2007
		IHREE-WIR	E				NUNN	allian		4		
	FORWARD	RUN (See re	verse for BAC	CKWARD RUN	I)	WEATHER	Overcast with	n snow showe	ers			
		BAC	KSIGHTS				FORE	SIGHTS		3 ORDER, CLASS1		
Setup	up     THREAD READING     MEAN     THREAD INTERVAL     SUM OF INTERVALS     ROD THREAD INTERVALS     THREAD READING						MEAN	THREAD INTERVAL	SUM OF INTERVALS	REMARKS	6	
	1587	BS1				1631	FS1			C = <u>(Δh1 - Δ2)</u>	<u>- 0.2mm</u>	
1	1572	1572				1617	1616.33			20 m		
	1557					1601				where BS1 - FS1	l = Δh1	
	4716					4849				BS2 - FS2 :	= Δh2	
	1307	20mS				1380	40mS			Δh1-	-44.33	
2	1277	1277				1320	1320			<u>Δh2</u>	-43	
	1247					1260				Δh1-Δh2 =	-1.33	
	3831					3960				- 0.2 (CR)	-1.53	
			1	-						÷20m	-0.07666667	
										C =	-0.07666667	
	Fi	ll in YE	LLOW	shade	d cel	ls.				"O" must be < 1	0.05.000/00	
	Fin in TELEOW Shaded cens.								C must be < +	0.05mm/m		
										Instrument SN: 100056		
										Rod SN: B		
<u> </u>										Party Chief: Beaver		
										Observer: Lewis		
										Recorder: Mills		
									Rod Person: Morgan			
								_				

NOAA	OAA FORM 75-29 U.S. DEPARTMENT OF COMMER						ON			NUMBER	SHEET	OF
(12			ΝΑΤ									
(12- 75)			INAT	ATMOS	PHERIC							
				ADMINIST	RATION	FROM B M				ТОВМ		
	PREC	SE LEV	ELING			TROW D.W.				TO D.M.		
		THREE-WIR	F				Kukk	amak		TIME	DATE DN 072, 13	3 March 2007
						WEATHER	Overcast with	n snow showe	ers			
	FORWARD	RUN (See re	verse for BAC	CKWARD RUN	1)							
		BAC	SIGHTS				FORE	SIGHTS		3 ORDER, CLAS	SS1	
Setup	THREAD READING	MEAN	THREAD INTERVAL	SUM OF INTERVALS	ROD TEMP	THREAD READING	MEAN	THREAD INTERVAL	SUM OF INTERVALS	REMARKS		
	1585	BS1				1630	FS1			C = <u>(Δh1 - Δ2)</u> -	0.2mm	
1	1570	1570				1615	1615			20 m		
	1555					1600				where BS1 - FS1	= Δh1	
	4710					4845				BS2 - FS2 =	Δh2	
												I
	1278	20mS				1350	40mS			<u>Δh1-</u>	-45.00	
2	1248	1248				1290	1290			Δh2	-42	
	1218					1230				<u>Δh1-Δh2 =</u>	-3.00	
	3744	_				3870	_			- 0.2 (CR)	-3.20	
				I	1					÷20m	-0.16	
										<b>C</b> -	-0.10	
	<b>C</b> :			ahada								
				snaue	a cei	15.				"C" must be < + 0	.05mm/m	-
										Instrument SN: 100056		
				ļ						Rod SN: B		
										Party Chief: Beaver		
										Observer: Lewis		
	<u> </u>			<u> </u>					ļ	Rod Person: Morgan		

NOAA	OAA FORM 75-29 U.S. DEPARTMENT OF COMMER						ON			NUMBER	SHEET	OF
(12			ΝΑΤ									
(12- 75)			INAT	ATMOS	PHERIC							
				ADMINIST	RATION	FROM B M				ТОВМ		
	PREC		ELING			T ICON D.IVI.				TO D.M.		
		THREE-WIR	F				Kukk	amak		TIME	DATE DN 072, 13	3 March 2007
						WEATHER	Overcast with	n snow showe	ers			
	FORWARD	RUN (See re	verse for BAC	CKWARD RUN	1)							
		BAC	SIGHTS				FORE	SIGHTS		3 ORDER, CLA	SS1	
Setup	THREAD READING	MEAN	THREAD INTERVAL	SUM OF INTERVALS	ROD TEMP	THREAD READING	MEAN	THREAD INTERVAL	SUM OF INTERVALS	REMARKS		
	1480	BS1				1700	FS1			C = <u>(Δh1 - Δ2)</u> -	0.2mm	
1	1465	1465				1685	1685			20 m		
	1450					1670				where BS1 - FS1	= Δh1	
	4395					5055				BS2 - FS2 =	Δh2	
												T
	2210	20mS				2462	40mS			<u>Δh1-</u>	-220.00	
2	2180	2180				2402	2402			<u>Δh2</u>	-222	
	2150					2342				<u>Δh1-Δh2 =</u>	2.00	
	6540					7206	_			- 0.2 (CR)	1.80	
				ſ	1					÷20m	0.09	
										C -	0.03	
	<b>E</b> :			ahada								
				snaue	a cei	15.				"C" must be < + 0	.05mm/m	-
										Instrument SN: 100056		
L				ļ						Rod SN: B		
<u> </u>										Party Chief: Beaver		
<u> </u>		ļ								UDServer: Lewis		
<u> </u>										Recorder. Willis Rod Person: Morgan		
<u> </u>												

NOAA	OAA FORM 75-29 U.S. DEPARTMENT OF COMMERC					TIDE STATION				NUMBER	SHEET	OF
(12- 75)			NAT	IONAL OCEAN								
73)				ADMINIST	RATION							
						FROM B.M.				TO B.M.		
	PREC	SISE LEV	ELING								DATE DU 070 40	M 1 0007
		THREE-WIR	E				Kukk	amaki		IIME	DATE DN 072, 13	March 2007
						WEATHER	Overcast with	n snow showe	ers			
	FORWARD	RUN (See re	verse for BAC	CKWARD RUN	1)							
		BAC	<b>(SIGHTS</b>				FORE	SIGHTS		3 ORDER, CLA	NSS1	
Setup	THREAD READING	MEAN	THREAD INTERVAL	SUM OF INTERVALS	ROD TEMP	THREAD READING	MEAN	THREAD INTERVAL	SUM OF INTERVALS	S		
	1483	BS1				1705	FS1			C = <u>(Δh1 - Δ2)</u>	<u>- 0.2mm</u>	
1	1469	1468.67				1689	1689.33			20 m		
	1454					1674				where BS1 - FS1	= Δh1	
	4406					5068				BS2 - FS2 =	= Δh2	
		-										
	2234	20mS				2485	40mS			Δh1-	-220.67	
2	2204	2203.67				2425	2425			<u>Δh2</u>	-221.333333	
	2173					2365				Δh1-Δh2 =	0.67	
	6611	-				7275				- 0.2 (CR)	0.47	
										÷20m	0.02333333	
										C =	0.02333333	
	Fi	ll in YF		shade	d cel	Is						
	- Fill in YELLOW shaded cells.									"C" must be < + (	0.05mm/m	
										Instrument SN: 100056		
										Rod SN: B		
										Party Chief: Beaver		
										Observer: Lewis		
										Recorder: Mills		
										Koa Person: Morgan		
1												

NOAA	IOAA FORM 75-29 U.S. DEPARTMENT OF COMMERCI					TIDE STATI	ON			NUMBER	SHEET	OF
(10												
(12- 75)			INAT	ATMOS								
- /				ADMINIST	RATION							
	PREC					FROM B.M.				то в.м.		
			-				Kukk	amak		TIME	DATE DN 356, 200	5
		THREE-WIR	E				NUKK	amak			,	
	FORWARD	RUN (See re	verse for BAC	CKWARD RUN	Ŋ	WEATHER	Overcast with	n occasional i	ain showers			
		BAC	SIGHTS				FORE	SIGHTS		3 ORDER, CLASS1		
				1								
Setup	THREAD READING	MEAN	THREAD INTERVAL	SUM OF	ROD TEMP	THREAD READING	MEAN	THREAD INTERVAL	SUM OF	REMARKS	3	
	1544	BS1				1538	FS1			C = <u>(Δh1 - Δ2)</u>	- 0.2mm	
1	1559	1559				1554	1553.67			20 m		
	1574					1569				where BS1 - FS1	l = ∆h1	
	4677					4661				BS2 - FS2 :	= Δh2	
	1584	20mS				1550	40mS			Δh1-	5.33	
2	1615	1614.67				1609	1609.67			<u>Δh2</u>	5	
	1645					1670				Δh1-Δh2 =	0.33	
	4844					4829				- 0.2 (CR)	0.13	
					T					÷20m	0.00666667	
										C =	0.00666667	
-												
											ļ	
	Fi	ll in YE	LLOW	shaded	d cel	ls.						
	Fill III TELEOW shaded cells.				1				C must be < +	0.05mm/m		
										Instrument SN: 100056		
<u> </u>										Rod SN: B		
										Party Chief: Beaver		
										Observer: Morgan		
									Recorder: Mills			
								Rod Person: Lewis				



Subject: OPUS solution : USCG0732.070 000106232 From: opus@ngs.noaa.gov Date: Mon, 02 Apr 2007 12:07:31 -0400 (EDT) To: horcon.fairweather@noaa.gov FILE: USCG0732.070 000106232 NGS OPUS SOLUTION REPORT \_\_\_\_\_ USER: horcon.fairweather@noaa.gov DATE: April 02, 2007 RINEX FILE: uscg073s.07o TIME: 16:07:30 UTC START: 2007/03/14 18:06:00 SOFTWARE: page5 0612.06 master29.pl EPHEMERIS: igs14183.eph [precise] STOP: 2007/03/14 20:36:00 OBS USED: 6385 / 6511 : 98% NAV FILE: brdc0730.07n ANT NAME: ASH701975.01AGP NONE # FIXED AMB: 30 / 32 : 94% ARP HEIGHT: 2.0 OVERALL RMS: 0.018(m) REF FRAME: NAD 83(CORS96)(EPOCH:2003.0000) ITRF00 (EPOCH: 2007.1995) -2415359.692(m) 0.013(m) x: -2415358.884(m) 0.013(m) Y: -2718046.175(m) 0.012(m) -2718045.070(m) 0.012(m) 5222559.312(m) 0.016(m) 5222559.510(m) 7: 0.016(m) 0.010(m) 55 19 58.66133 0.010(m) 55 19 58.67266 LAT: E LON: 228 22 28.18023 0.007(m) 228 22 28.10433 131 37 31.89567 0.007(m) W LON: 131 37 31.81977 0.007(m) 0.007(m)EL HGT: 3.781(m) 0.023(m) 3.780(m) 0.023(m) ORTHO HGT: 9.656(m) 0.034(m) [Geoid06 NAVD88] UTM COORDINATES STATE PLANE COORDINATES UTM (Zone 09) SPC (5001 AK 1) Northing (Y) [meters] 6134983.221 0.000 Easting (X) [meters] 333464.469 0.000 Convergence [degrees] -2.15989540 0.0000000 Point Scale 0.99994023 0.00000000 0.99993963 Combined Factor 0.00000000 US NATIONAL GRID DESIGNATOR: 9UUB3346434983(NAD 83) BASE STATIONS USED PID DESIGNATION LATITUDE LONGITUDE DISTANCE(m) AI5022 BIS1 BIORKA ISLAND 1 CORS ARP N565116.162 W1353221.387 296620.8 AJ4430 LEV1 LEVEL ISLAND 1 CORS ARP N562756.438 W1330533.935 155968.5 AF9530 AIS1 ANNETTE ISLAND 1 CORS ARP N550408.647 W1313558.255 29425.1

NEAREST NGS PUBLISHED CONTROL POINT AI4914 BM NO 37 N551958.659 W1313731.820 0.0

### BASE STATION INFORMATION

STAT	ION NAME: bisl	a 5 (BIORKA 1	[SLAND 1; Bior]	ka Island, Alaska, U.S.A.)
ANT	ENNA: ASH700829	.3 SNOW		S/N=xxxx
XYZ	-2494921.0213	-2448390.9324	5317113.5289	MON @ 1997.0000 (M)
XYZ	-0.0164	0.0037	0.0005	VEL (M/YR)
NEU	0.0000	0.0000	0.0000	MON TO ARP (M)
NEU	-0.0000	0.0000	0.0877	ARP TO L1 PHASE CENTER (M)
NEU	-0.0000	0.0000	0.0598	ARP TO L2 PHASE CENTER (M)
XYZ	-0.1673	0.0377	0.0051	VEL TIMES 10.1982 YRS
XV7	0 0000	0 0000		MON TO ARP
XV7	_0_0342	-0.0336	0.0000	APD TO I.1 DHASE CENTER
XIZ VV7	-2404021 2220	-2448390 9283	5217112 6074	I DUG CEN @ 2007 1995
XIZ VV7		0 0014	0 0005	
XV7	_2494921 2228	-2448390 9269	5317113 6080	NEW 11 DHS CEN @ 2007 1995
XV7	2494921.2220 2404021.1006	2440300.0200	5317113.0000 5217112 5245	NEW ADD @ 2007 1005
AIA VV7	-2494921.1000	-2440390.0933	551/115.5545	NEW ARP @ 2007.1995
	-2494921.1000		$\frac{531}{113.5545}$	NEW MON @ 2007.1995
ЦЦН Т Т Т ТТ	50 51 10.17228			NEW LI PHS CEN @ 2007.1995
LLH	56 51 16.1/228		7 66.5910 7 66.5910	NEW ARP @ 2007.1995
ЦЦΗ	56 51 16.1/228	224 27 38.5326	66.5910	NEW MON @ 2007.1995
		0 (7 ] 7		
STAT	ION NAME: LEVI	a 8 (Level 19	sland 1; Level	Island, Alaska USA)
AN'I'	ENNA: ASH700829	.3 SNOW		S/N=CG11936
XYZ	-2412828.4670	-2579056.1235	5293283.3535	MON @ 1997.0000 (M)
XYZ	-0.0190	0.0003	-0.0044	VEL (M/YR)
NEU	0.0000	0.0000	0.0000	MON TO ARP (M)
NEU	-0.0000	0.0000	0.0877	ARP TO L1 PHASE CENTER (M)
NEU	-0.0000	0.0000	0.0598	ARP TO L2 PHASE CENTER (M)
XYZ	-0.1938	0.0031	-0.0449	VEL TIMES 10.1982 YRS
XYZ	0.0000	0.0000	0.0000	MON TO ARP
XYZ	-0.0331	-0.0354	0.0731	ARP TO L1 PHASE CENTER
XYZ	-2412828.6939	-2579056.1558	5293283.3817	L1 PHS CEN @ 2007.1995
XYZ	-0.0002	0.0006	0.0002	+ XYZ ADJUSTMENTS
XYZ	-2412828.6941	-2579056.1552	5293283.3819	NEW L1 PHS CEN @ 2007.1995
XYZ	-2412828.6610	-2579056.1198	5293283.3088	NEW ARP @ 2007.1995
XYZ	-2412828.6610	-2579056.1198	5293283.3088	NEW MON @ 2007.1995
LLH	56 27 56.44916	226 54 25.98578	3 25.2831	NEW L1 PHS CEN @ 2007.1995
LLH	56 27 56.44916	226 54 25.98578	3 25.1954	NEW ARP @ 2007.1995
LLH	56 27 56.44916	226 54 25.98578	3 25.1954	NEW MON @ 2007.1995
STAT	ION NAME: aisl	a 7 (ANNETTE	ISLAND 1; Anne	ette Island, Alaska, U.S.A.)
ANT	ENNA: ASH700829	.3 SNOW		S/N=11276
XYZ	-2430153.7846	-2737192.8996	5205816.6147	MON @ 1997.0000 (M)
XYZ	-0 0151	0 0008	-0 0082	VEL (M/YR)
NEII	0 0000	0 0000		MON TO ARP $(M)$
NEU	-0.0000	0 0000	0.0000	ARD TO I.1 DHASE CENTER $(M)$
NEII	-0.0000	0.0000	0.0077	ARE TO BE PHASE CENTER $(M)$
XV7	-0.1540	0.0000	-0.0836	VEL TIMES 10 1082 VPS
AIA VV7	0.1040	0.0002	0.0030	MON TO ADD
AIL VV7		0.0000	0.0000	MUNIUARP
AIL VV7	-0.0333	-0.03/0		ARF IU LI FHASE CENIER
AIZ XXZ	-2430153.9/19	-2/3/192.9290	0.000.0102020	LI PHS CEN @ 2007.1995
AIZ XXZ	U.UUUL	U.UUUL- 0727100 0001		+ AIZ ADJUSIMENTS
ΧYΖ	-2430153.9/18	-2/3/192.9291	5∠058⊥6.6030	NEW LI PHS CEN @ 2007.1995

XYZ	-2430153.9385	-2737192.8915	5205816.5311	NEW ARP @ 2007.1995
XYZ	-2430153.9385	-2737192.8915 5	5205816.5311	NEW MON @ 2007.1995
LLH	55 4 8.65871	228 24 1.66998	32.2471	NEW L1 PHS CEN @ 2007.1995
ЦЦН Т Т Т Т	55 4 8.658/1	228 24 1.66998	32.1594	NEW ARP @ 2007.1995
НЦЦ	55 4 8.058/1	228 24 1.00998	32.1594	NEW MON @ 2007.1995
		REMOTE STATIC	ON INFORMATIC	DN
STAT	ION NAME: uscg	1		
ANT	ENNA: ASH701975	.01AGP NONE		S/N=UNKNOWN
XYZ	-2415360.3793	-2718045.5588 5	5222561.1762	MON @ 2007.1993 (M)
NEU	0.0000	-0.0000	2.0000	MON TO ARP (M)
NEU	-0.0000	0.0000	0.0637	ARP TO LI PHASE CENTER (M)
NEU XV7	-0.0000	-0.8504	1 6449	MON TO ARD
XYZ	-0 0241	-0.0271	0 0524	ARP TO L1 PHASE CENTER
XYZ	-2415361.1590	-2718046.4363	5222562.8735	L1 PHS CEN @ 2007.1995
BASE	LINE NAME: bi	sl uscg		
XYZ	0.6817	0.4813	-1.6607	+ XYZ ADJUSTMENTS
XYZ XV7	-2415360.4/74		5222561.2128	NEW LI PHS CEN @ 2007.1995
XIZ VV7	-2415300.4533 -2415350.6076	-2/18045.92/8	5222561.16U4 5222550 5155	NEW ARP @ 2007.1995 NEW MON @ 2007.1995
T.T.H	55 19 58 67251	278 22 28 10438	5 8533	NEW MON @ 2007.1995 NEW L1 PHS CEN @ 2007 1995
TTTH	55 19 58.67251	228 22 28.10438	5.7896	NEW ARP @ 2007.1995
LLH	55 19 58.67251	228 22 28.10438	3.7896	NEW MON @ 2007.1995
BASE	LINE NAME: le	vl uscg	1	
XYZ	0.6864	0.4936	-1.6609	+ XYZ ADJUSTMENTS
XYZ XV7	-2415360.4/2/	-2/18045.942/ 5	5222561.212/	NEW LI PHS CEN @ 2007.1995
AIZ VV7	-2415360.4466	-2718045.9150	5222501.1003	NEW ARP @ 2007.1995 NEW MON @ 2007 1995
T.T.H	55 19 58 67284	278 22 28 10412	5 8462	NEW MON @ 2007.1995 NEW L1 PHS CEN @ 2007 1995
LLH	55 19 58.67284	228 22 28.10412	5.7825	NEW ARP @ 2007.1995
LLH	55 19 58.67284	228 22 28.10412	3.7825	NEW MON @ 2007.1995
BASE	LINE NAME: ai	sl uscg	1 (5)	
XYZ	0.6951	0.4928	-1.6769	+ XYZ ADJUSTMENTS
XYZ	-2415360.4639	-2/18045.9435	5222561.1967	NEW LI PHS CEN @ 2007.1995
AIZ VV7	-2415360.4396 -2415359.6842	-2718045.9164	5222501.1445	NEW ARP @ 2007.1995 NEW MON @ 2007 1995
TTH	55 19 58 67268	228 22 28 10452	5.8300	NEW L1 PHS CEN @ 2007.1995
LLH	55 19 58.67268	228 22 28.10452	5.7663	NEW ARP @ 2007.1995
LLH	55 19 58.67268	228 22 28.10452	3.7663	NEW MON @ 2007.1995
		G-I	FILES	
∆xx20	07 314 7 314			
B2007	31418 5 7 31	42035 1 page5 v061	12.06IGS	222 1 2 27NGS 2007 4 2IFDDFX
Iant	info.003	NGS 20070320		
C0009	0001 -795614910	19 2696541842	21 9455401	.90 39 X0737AUSCGX0737ABIS1
D 1	2 7550588 1	3 -9307589 2 3	-7806480	
700				
AXX20	21/10 F 7 21	12025 1 page	12 06709	200 1 0 07MCC 2007 4 01
BZUU/ Tant	info 003	NGS 20070320	17.00102	ZZZ I Z Z/INGO ZUU/ 4 ZIFDDFX
C0009	0002 25310319	17 1389889454	20 7072379	35 38 X0737AUSCGX0737ALEV1
-				

## D 1 2 8189618 1 3 -9202066 2 3 -7448116

Axx2007 314 7 314 B2007 31418 5 7 3142035 1 page5 v0612.06IGS 222 1 2 27NGS 2007 4 2IFDDFX Iant\_info.003 NGS 20070320 C00090003 -147942543 19 -191478255 22 -167429683 36 X0737AUSCGX0737AAIS1 D 1 2 9369495 1 3 -7883557 2 3 -7554607

#### POST-FIT RMS BY SATELLITE VS. BASELINE

	OVERALL	03	06	07	10	16	18	19	21
bis1-uscg	0.017	0.018	0.016	0.018	0.014	0.019	0.013	0.015	
	22	24	25	26	29	30			
bis1-uscg	0.018	0.015		0.022	0.019				
	OVERALL	03	06	07	10	16	18	19	21
lev1-uscg	0.018	0.017	0.018	0.019	0.017	0.022	0.017	0.015	
	22	24	26	29	30				
lev1-uscg	0.018	0.013	0.018	0.021					
	OVERALL	03	06	07	10	16	18	19	21

aisl-uscg 0.018 0.020 0.018 0.018 0.012 0.022 0.016 ... ... 22 24 26 29 30 aisl-uscg 0.015 0.017 0.015 0.016 ...

## OBS BY SATELLITE VS. BASELINE

	OVERALL	03	06	07	10	16	18	19	21
bis1-uscg	2148	155	203	279	102	296	245	28	
	22	24	25	26	29	30			
bis1-uscg	118	284		200	238				
	OVERALL	03	06	07	10	16	18	19	21
lev1-uscg	2087	155	182	225	106	296	247	28	
	22	24	26	29	30				
lev1-uscg	117	284	200	247					
	OVERALL	03	06	07	10	16	18	19	21
ais1-uscg	2150	152	207	284	105	295	239		
	22	24	26	29	30				
aisl-uscg	119	283	213	253					

Covariance Matrix	for the xyz OPU	S Position (meters2).
0.000022467	0.000002159	-0.000004052
0.000002159	0.0000029444	-0.000004008
-0.000004052	-0.000004008	0.000094689
Covariance Matrix	for the enu OPU	S Position (meters2).
0.000023402	-0.0000002845	0.000001534
-0.000002845	0.0000044782	0.000029060
0.000001534	0.0000029060	0.000078416
Horizontal network	accuracy =	0.00458 meters.
Vertical network a	accuracy =	0.00549 meters.

Derivation of NAD 83 vector components

Position of reference station ARP in NAD\_83(CORS96)(EPOCH:2003.0000). Xa(m) Ya(m) Za(m) BIS1 -2494920.37852 -2448391.99956 5317113.26406 2003.00 LEV1 -2412827.84636 -2579057.21856 5293283.07789 2003.00 AIS1 -2430153.14737 -2737194.00189 5205816.33593 2003.00 Position of reference station monument in NAD\_83(CORS96)(EPOCH:2003.0000). Xr(m) Yr(m) Zr(m) BIS1 -2494920.37852 -2448391.99956 5317113.26406 2003.00 LEV1 -2412827.84636 -2579057.21856 5293283.07789 2003.00 AIS1 -2430153.14737 -2737194.00189 5205816.33593 2003.00 Velocity of reference station monument in NAD\_83(CORS96)(EPOCH:2003.0000). Vx (m/yr) Vy (m/yr) Vz (m/yr) BIS1 0.00490 0.00450 0.00990 LEV1 0.00220 0.00120 0.00480 0.00170 AIS1 0.00580 0.00110 Vectors from unknown station monument to reference station monument in NAD 83(CORS96)(EPOCH:2003.0000). Yr-Y= DY(m) Xr-X= DX(m) Zr-Z=DZ(m)-79561.49452 269654.17544 94553.95206 2003.00 BIS1 LEV1 2531.03764 138988.95644 70723.76589 2003.00

This position and the above vector components were computed without any knowledge by the National Geodetic Survey regarding the equipment or field operating procedures used.

-16742.97607

2003.00

-14794.26337 -19147.82689

AIS1

## NOTE

# Trimble – Additional Calibration Reports

See SAND1.ssf attached as digital separates

#### NOAA Ship FAIRWEATHER LASER LEVEL Accuracy test 3.8 sn# 000676 Laser Technology, Inc. Impulse 200 laser ranging instrument

### Testing date: 02/27/2006

	Actual	LL	Actual	LL
Trial	Distance	Distance	Height	Height
1	10	10.0	2.0	2.0
2	10	10.0	2.0	2.0
3	10	10.0	2.0	2.0
4	20	20.0	2.0	1.9
5	20	19.9	2.0	2.0
6	20	20.0	2.0	2.0
7	50	50.1	2.0	2.0
8	50	50.1	2.0	2.1
9	50	50.1	2.0	2.1
10	100	100.1	2.0	2.1
11	100	100.1	2.0	1.9
12	100	100.1	2.0	1.8

LL = Laser Level

all distances are measured in meters

### Comparison Testing Lasers 000676 and i0929 and Trimble

### Testing date: 03/03/2006

	Trial	Trimble Distance	000676 Distance	i0929 Distance	000676 Height	i0929 Height	Actual Height		
	1.0	30.0	32.8	33.0	2.1	2.4	2.0	2.8	
	2.0	23.5	27.3	27.8	2.0	1.9	2.0	3.8	
	3.0	20.2	24.0	24.2	2.2	2.0	2.0	3.8	
	4.0	34.0	31.9	32.4	2.6	2.3	2.0	2.1	
	5.0	26.8	26.2	25.8	2.1	2.0	2.0	0.6	
	7.0	30.6	28.5	28.5	2.0	2.4	2.0	2.1	
	6.0	51.9	38.7	38.5	2.0	2.3	2.0	13.2	
sum		217.0	209.4	210.2	15.0	15.3	14.0	28.4	15.2
mean		31.0	29.9	30.0	2.1	2.2	2.0	4.1	2.5
standard deviation		10.3	5.0	4.9	0.2	0.2	0.0		

Lead Line & Sounding Pole Calibration Report								
Field unit: FA								
Lead Line / Sounding Pole I (Unique Identifier, with equipn	Lead Line / Sounding Pole Identification Number: Leadline 10_01_05 (Unique Identifier, with equipment type, date made, etc.)							
Date of Calibration: 3/6/2007	Date of Calibration: 3/6/2007							
Method of Calibration: X Steel tape Permanent graduation marks Other								
Location: Ketchikan, Alaska	3							
Chief of Party: Cdr. Andrew	Beaver, NOAA, FA							
Lead Line / Sounding Pole I	Jnit of Measure: Meters							
Measured by: BC	Recorded by: BC	Checked by: BC						
Graduated Marking (a)	Calibration Measuremen	t Lead Line Corrector (c = b - a)						
1	0.96	0.04						
2	1.96	0.04						
3	2.96	0.04						
4	3.97	0.03						
5	4.97	0.03						
6	5.97	0.05						
7	6.95	0.05						
8	7.97	0.03						
9	8.97	0.03						
10	9.95	0.05						
	Average Correction	0.039						
	Standard Deviation 0.0088							

Correction Values Lead Line 10\_01\_05



Lead Line &	Lead Line & Sounding Pole Calibration Report							
Field unit: FA								
Lead Line / Sounding Pole lo (Unique Identifier, with equipm	Lead Line / Sounding Pole Identification Number: Leadline 20_01_05 (Unique Identifier, with equipment type, date made, etc.)							
Date of Calibration: 3/20/200	Date of Calibration: 3/20/2007							
Method of Calibration: X Steel tape Permanent graduation marks Other								
Location: Ketchikan, Alaska	Location: Ketchikan, Alaska							
Chief of Party: Brenna Campbell								
Lead Line / Sounding Pole U	nit of Measure: Meters							
Measured by: BC/DJ	Recorded by: BC	Checked by: BC						
Graduated Marking	Calibration Measuremen	t Lead Line Corrector						
(a)	(b)	(c = b - a)						
1	1.003	0.003						
2	1.988	0.012						
3	2.981	0.019						
4	3.979	0.021						
5	4.978	0.022						
6	5.983	0.017						
7	6.981	0.019						
8	7.981	0.019						
9	8.981	0.019						
10	9.983	0.017						
11	10.984	0.016						
12	11.983	0.017						
13	12.983	0.017						
14	13.983	0.017						
15	14.983	0.017						
16	15.986	0.014						
17	16.984	0.016						
18	17.99	0.01						
19	19 18.99 0.01							
20	20 19.993 0.007							
-	Average Correction 0.015							
	Standard Deviation	0.005						
Correction Values Lead Line 20\_01\_05



Lead Line & Sounding Pole Calibration Report				
Field unit: FA				
Lead Line / Sounding Pole Identification Number: Leadline 20_02_05 (Unique Identifier, with equipment type, date made, etc.)				
Date of Calibration: 4/09/2007				
Method of Calibration: X Steel tape Permanent graduation marks Other				
Location: Ketchikan, Alaska	3			
Chief of Party: CDR Andrew	Beaver/NOAA Ship Fairweather			
Lead Line / Sounding Pole U	Jnit of Measure: Meters			
Measured by: BC/DJ	Recorded by: BC	Checked by: BC		
Graduated Marking	Calibration Measurement	Lead Line Corrector		
(a)	(b)	(c = b - a)		
1	0.99	0.01		
2	1.987	0.013		
3	3 2.985 0.015			
4	3.979	0.021		
5	4.977 0.023			
6	5.977	0.023		
7	6.973	0.027		
8	7.973	0.027		
9	8.968	0.032		
10	9.966	0.034		
11	10.966	0.034		
12	11.964	0.036		
13	12.965	0.035		
14	13.965	0.035		
15	14.967	0.033		
16	15.965	0.035		
17	16.969	0.031		
18	17.973	0.027		
19	18.978	0.022		
20	19.982	0.018		
	Average Correction	0.02655		
	Standard Deviation	0.00810117		

Correction Values Leadline 20\_02\_05



Lead Line & Sounding Pole Calibration Report				
Field unit: FA				
Lead Line / Sounding Pole Identification Number: Leadline 20_03_05 (Unique Identifier, with equipment type, date made, etc.)				
Date of Calibration: 3/26/2007				
Method of Calibration: X Steel tape Permanent graduation marks Other				
Location: Ketchikan, Alaska	Location: Ketchikan, Alaska			
Chief of Party: Cdr. Andrew	Beaver/NOAA Ship Fairweather			
Lead Line / Sounding Pole U	nit of Measure: Meters			
Measured by: BC/DJ	Recorded by: BC	Checked by: BC		
Graduated Marking	Calibration Measurement	Lead Line Corrector		
(a)	(b)	(c = b - a)		
1	0.985	0.015		
2	1.978	0.022		
3	2.973	0.027		
4	3.969	0.031		
5	4.966	0.034		
6	5.961	0.039		
7	6.962	0.038		
8	7.962	0.038		
9	8.956	0.044		
10	9.952	0.048		
11	10.946	0.054		
12	11.949	0.051		
13	12.951	0.049		
14	13.95	0.05		
15	14.946	0.054		
16	15.942	0.058		
17	16.941	0.059		
18	17.938	0.062		
19	18.939	0.061		
20	19.934	0.066		
	Average Correction	0.045		
	Standard Deviation	0.014		

Correction Values Leadline 20\_03\_05



Lead Line & Sounding Pole Calibration Report					
Field unit: FA					
Lead Line / Sounding Pole (Unique Identifier, with equipr	Lead Line / Sounding Pole Identification Number: Leadline 30_01_05 (Unique Identifier, with equipment type, date made, etc.)				
Date of Calibration:					
Method of Calibration: Other	Method of Calibration:XSteel tapePermanent graduation marksOther				
Location: Ketchikan, Alaska	a				
Chief of Party: CO Andrew	Beaver/NOAA Ship Fairweathe	r			
Lead Line / Sounding Pole	Unit of Measure: Meters				
Measured by: BC/ACA	Measured by: BC/ACA         Recorded by: BC         Checked by: BC				
Graduated Marking (a)	Calibration Measurement (b)	Lead Line Corrector (c = b - a)			
1	1.015	0.015			
2	1.992	0.008			
3	2.991	0.009			
4	3.979	0.021			
5	4.974	0.026			
6	5.965	0.035			
7	6.963	0.037			
8	7.949	0.051			
9	8.942	0.058			
10	9.937	0.063			
11	10.937	0.063			
12	11.923	0.077			
13	12.921	0.079			
14	13.907	0.093			

Graduated Marking (a)	Calibration Measurement (b)	Lead Line Corrector (c = b - a)
15	14.905	0.095
16	15.903	0.097
17	16.898	0.102
18	17.898	0.102
19	18.908	0.092
20	19.91	0.09
21	20.912	0.088
22	21.882	0.118
23	22.879	0.121
24	23.874	0.126
25	24.872	0.128
26	25.868	0.132
27	26.862	0.138
28	27.862	0.138
29	28.855	0.145
30	29.857	0.143
	Average Correction	0.083
	Standard Deviation	0.043

Correction Values Leadline 30\_01\_05



# APPLIED Because it's not just MICROSYSTEMS

# 4986 Certificate of Calibration

Customer:

NOAA - Pacific Marine Center

Instrument Serial Number: INS-04986

Instrument Type: Smart SV&P

Instrument Description:

Real-time instrument with sound velocity (invar) and pressure

Calibrated Pressure Range:

Certification Date:

19/01/2007

1000 dBar

Certified By:

Robert Haydock, General Manager Applied Microsystems

Applied Microsystems certifies that the equipment described above has been calibrated with equipment referenced to traceable standards. Any repairs / calibrations completed on this instrument were approved by the instrument owner under purchase order.

This instrument has been recalibrated. Please be sure to update your records. Please also ensure that you update the instrument's coefficient values in any post-processing software (ie. Smart Talk) that you use. Instrument configuration files are available at our Client Service & Support Portal (see web address below).

For a complete service history of this instrument, please consult our on-line Client Service & Support Portal at <u>http://www.appliedmicrosystems.com/customers/index.htm</u>

Applied Microsystems 2071 Malaview Avenue Sidney, B.C. V8L 5X6 CANADA Tel: +1-250-656-0771 Fax: +1-250-655-3655

### **Smart Pressure Calibration**



# Smart SV Calibration





APPLIED Because it's not just for MICROSYSTEMS

# **Certificate of Calibration**

Customer:

Brooke Ocean Technology Ltd.

Reference: Job#: 11232 PO#: credit card

Part No: Smart SV & Pressure

Serial No: 4986

Comments: New invar rods for SV sensor, new zinc, re-calibration of sound velocity and pressure.

Date: 402 13/06

Jeff Bosma Electronics Technologist

APPLIED MICROSYSTEMS LTD. CERTIFIES THAT THE ABOVE DESCRIBED EQUIPMENT HAS BEEN CALIBRATED WITH EQUIPMENT REFERENCED TO TRACEABLE STANDARDS. ANY REPAIRS/CALIBRATIONS PERFORMED ON THIS INSTRUMENT WERE APPROVED BY THE CONTRACT/PURCHASE ORDER NAMED ABOVE.

#### AML Calibration Equipment

#### **Temperature Calibrations**

Performed using either of two Hart Scientific "Black Stack" Model 1560 Power Bases with attached Hart Scientific Model 2563 Thermistor Modules connected to a Thermometrics AS125 4 Wire Thermistor Standard

1: Hart Scientfic Power Base 1560 S/N 79263 / Thermistor Module 2563 S/N 79039 / Thermometrics AS125 4 Wire Thermistor Standard S/N 2131 2: Hart Scientfic power Base 1560 S/N A05690 / Thermistor Module 2563 S/N A05693 / Thermometrics AS125 4 Wire Thermistor Standard S/N 2128

Temperature calibration equipment is calibrated yearly and verified bi-monthly as per Applied Microsystems Ltd. Calibration Schedule T11.2 utilizing a Hart Scientific Model 5901 Triple Point of Water Cell. All temperature calibrations and verifications are ITS-90 and NIST traceable

#### Pressure Calibrations

Performed using a Budenburg Model 380D S/N 18564 Range 0-8000 psi Deadweight Tester. Calibrations and verifications are implemented as per Applied Microsystems Ltd. Calibration Schedule T11.2. All pressure calibrations and verifications are NIST traceable.

#### Conductivity Calibrations

Performed using either of two Guildline 8400B S/N 59251 or Guildline 8400 S/N 43385 Autosals. Both Conductivity Calibrators are calibrated and verified using Ocean Scientific International IAPSO Standard Seawater as per Applied Microsystems Itd. Calibration Schedule T11.2. All Conductivity Calibrations and verifications are NIST traceable

#### **Battery Channel Calibrations**

Performed using a Precision Fluke Model 45 Multimeter S/N 4720162. Calibrations and verifications are implemented as per Applied Microsystems Ltd. Calibration Schedule T11.2 All calibrations and verifications are NIST traceable.

#### Sound Velocity Calibrations

Performed using an Applied Microsystems Ltd Temperature Standard S/N 9998 in distilled water, <5 ppm TDS, and sound velocity reference is Del Grosso and Mader's Pure Water Equation. Calibrations and verifications are implemented as per Applied Microsystems Ltd. Calibration Schedule T11.2 All temperature calibrations and verifications are ITS-90 and NIST traceable.

# Calibration Coefficients Smart SV & Pressure 4986

01-13-2006

Brooke Ocean Technology Ltd.

NOTE: This instrument has been re-calibrated. Please update your records and any post-processing software you may be using.

# Applied Microsystems Ltd.

2071 Malaview Ave. West, Sidney, British Columbia, Canada V8L 5X6 Phone: (250) 656-0771 Fax: (250) 655-3655 Canada & USA: 800-663-8721

Email: info@AppliedMicroSystems.com Web: http://www.aml.bc.ca

## Smart SV Calibration

01-12-2006
11232
Brooke Ocean Technology Ltd.
AML
Time of Flight
166-1
1400 to 1550 m/s
1
JB
Smart T 9998



### Smart Pressure Calibration

Job Informatio

JOD IIIOIIIduoII		
Date	01-06-2006	
Job Number	11232	
Customer	Brooke Ocean Technology Ltd.	
Sensor Information		
Manufacturer	Keller	
Model Number	PA-10TAB/100BAR/8838.4	
Serial Number	YZ138	
Range	1000 DBar	
Channel	2	
Calibrated By	JB	
Standards	Budenburg Deadweight	





# **Conformity Certificate**

Customer:	Brooke Ocean Technology Ltd.
	50 Thornhill Drive, Unit 11
	Dartmouth

- **Reference:** Job#: 4337 PO#: 04653-0449M
- Part No: Smart SV & Pressure
- Serial No: 4987
- **Description:** Direct measurement of sound velocity and pressure.
- **Comments:** This stainless steel, right angle end cap instrument operates as a stand alone unit with a fixed 19200 baud rate, RS-485 communications interface. Maximum depth, 1000 meters.

Certification Date: 12-08-2004

Justin Romito Technologist

APPLIED MICROSYSTEMS LTD. CERTIFIES THAT THE ABOVE DESCRIBED EQUIPMENT HAS BEEN TESTED IN ACCORDANCE WITH THE CONDITIONS AND REQUIREMENTS OF THE CONTRACT/PURCHASE ORDER. UNLESS OTHERWISE NOTED ABOVE, THE EQUIPMENT CONFORMS IN ALL RESPECTS TO THE SPECIFICATIONS AND/OR RELEVANT DRAWINGS.

# **Smart SV Calibration**

Job Information	
Date	11-30-2004
Job Number	4337
Customer	Brooke Ocean Technology Ltd.
Sensor Information	
Manufacturer	AML
Model Number	Time of Flight
Serial Number	166-2
Range	1400 to 1550 m/s
Channel	2
Calibrated By	JR
Standards	Smart T 9998



# **Smart Pressure Calibration**

Date Job Number	12-06-2004 4337
Customer	Brooke Ocean Technology Ltd.
Sensor Information	
Manufacturer	Keller
Model Number	PA-10TAB/100BAR/8838.4
Serial Number	YZ136
Range	1000 Dbar
Channel	1
Calibrated By	JR
Standards	Budenburg Deadweight

Deviation (% of full scale) vs. Pressure (dbars) +0.1 +0.050.0 -0.05 -0.1 0 200 400 600 800 1000 Pressure (dbars) Coefficients A = -1.529758E+03 B = -4.856953E-01 C = -3.189672E-03D = 3.215278E-04E = 4.733318E-02 F = 2.070545E-05G = 4.684017E-07 H = -1.831440E-08 I = 3.933418E-08 J = -1.141085E-10 K = -9.489968E-12 L = 2.280363E-13=A+B\*T+C\*T^2+D\*T^3+(E+F\*T+G\*T^2+H\*T^3)\*Raw+(I+J\*T+K\*T^2+L\*T^3)\*Raw^2 RMS = 0.0963

MVP cfg - no\_con\_needed.txt Subject: [Fwd: Re: AML SV+P .cfg file] Date: Tue, 18 Apr 2006 15: 49: 46 +0000 From: "grant froelich" <grant.froelich@noaa.gov> To: chi efst fai rweather <chi efst. fai rweather@noaa.gov>, foo fairweather <foo.fairweather@noaa.gov>, mike castle <mike.castle@noaa.gov> - -------Grant Froelich Senior Survey Technician NOAA Ship FAIRWEATHER (907)254-2842 Cell (808)659-0054 At Sea \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_\_\_\_\_ Subject: RE: AML SV+P .cfg file Date: Tue, 18 Apr 2006 09:45:18 -0300 From: Murray Eisan <meisan@brooke-ocean.com> To: "'grant froelich'" <grant.froelich@noaa.gov> CC: "'Darrell Groom'" <dgroom@brooke-ocean.com>

Hi Grant,

The calibration coefficients have been applied to the sensor at AML. The MVP software logs the corrected data being outputted from the sensor. The AML configuration file does not need to be applied to the MVP software.

Regards,

Murray Eisan

\_\_\_\_\_

From: grant froelich [mailto:grant.froelich@noaa.gov] Sent: Monday, April 17, 2006 2:02 PM To: support@brooke-ocean.com Subject: AML SV+P .cfg file

Hello,

We recently sent our AML SV+P sensor out for calibration and when it returned we also received a .cfg file. Is this something that the MVP software needs to correct the sound velocity files produced? If so, how is that done?

thanks grant

--

p.2

**ENVIRONMENTAL SIMULATION LABS** 

**Division of Composites Atlantic Limited** 

# HYDROSTATIC PRESSURE TEST REPORT

JOB/REPORT #: ESL-06-025

DATE: February 20, 2006

CLIENT:Brooke Ocean Technology LTD. 50 Thornhill Drive, Unit 11 Dartmouth, Nova Scotia B3B 1S1 PO #: 06261-0578 CONTACT: Mark Smith

### TEST ARTICLE DESCRIPTION: Free Fall Cone Penetrator Model No: FFCPT-35-1

STANDARD USED: Autoclave Engineers 0-5000 PSIG Pressure TransducerMODEL #: TSW-6-5000-PE30INVENTORY #: 1127-TF1CALIBRATION DUE: July 4, 2006

The IUT was placed in the 1,200 PSIG Pressure Vessel, Inventory # 1142-TF1. The pressure was increased to 1,000 psig and maintained for one (1) hour. The pressure was then relieved and the IUT removed for inspection. Brocke Ocean Technology personnel performed an onsite inspection for any signs of water infiltration, none was found. The IUT was returned to Brooke Ocean Technology for final inspection.

THIS IS TO CERTIFY THAT THE ABOVE TESTING WAS PERFORMED ACCORDING TO REQUIREMENTS SET FORTH IN THE REFERENCED PURCHASE ORDER IN A MANNER CONSISTENT WITH STANDARD PRACTICES AND ANY SPECIFICATIONS REFERENCED HEREIN.

Tested by:

Conrad Tulk CET Lab Technologist

Approved By:

Neil Richter P.Eng, Manager, ESL



Brooke Ocean Technology 50 Thornhill Drive, Unit 11 Dartmouth, Nova Scotia. Canada. B3B 1S1

### Free Fall Cone Penetrometer and MVP Upgrades NOAA Field Acceptance Test Project No.: 0578 Homer, Alaska, June 9 – 13, 2006

### 1 Line Puller Installation

	Test	Result	Accept
1.1 Confirm Specifications			FAT
Danfoss Hydraulic Motor OMM8:151G00493	Check ID Tag	orc	KU
Relief valve setting of 1,500 psi	Check Pump B Gauge	1600 cold	-ES.I
Verify Line Speed of 12 - 13 m/s	RPM Gauge	13115	EN.
1.2 Installation			
Hydraulic System Upgrades	Check for leaks	OK	EM
Sheave wheel alignment	Wheel driven in outboard direction	or	BM
1.3 Performance and Operation			
Verify proper line puller operation	Observe that line puller is throwing line over-the-side after impact and that no slack cable has occurred on the drum.	QK	ENE
Verify FFCPT terminal velocity	Confirm from data that it is in the 7.5 – 11 m/s range in no more than 100m of water	6.3-7.8 m/s Fwidepth	AB
Verify that standard SVP fish operations are unaffected by line puller installation	Conduct deployments and check data.	OK	- Alfor

#### 2 Inner Sheave Load Cell Installation

	Test	Result	Accept
Confirm load cell installation			BNZ
Confirm proper calibration and functioning	Load cell reads approximately 115 lbs with FFCPT hanging or use calibration load cell and come- along to generate loads.	$(1)R^{2} = .99$ $(2)R^{2} = 1$ $(3)R^{2} = 1$	301

#### 3 Free Fall Cone Penetrometer (FFCPT)

	Test	Result	Accept
Overall Instrument Quality (fit and finish)	Visual inspection	OK	100
3.1 Confirm physical specifications	Diameter of 3.47"	OK	-Part
	Length of 73*	ok	FAN
	Weight of 115 lbs in-air	ox_	1 22
	Material of 316 Stainless	ok?	TAT
3.2 Confirm System Specifications			1
Rated Depth of 660m	BOT pressure test record		
Data Sampling rate of 2,000 HZ	Check data files	or	For
Battery Voltage	Verify fully charged voltage of 13.5V	14.4 unloaded	For
Accelerometers: [+3g/-2g]; [+20g/-5g]; [+90g/- 10g]	Confirm through data the presence of 3 accelerometers.	ok	EN
Drop Capacity of ~200 Drops on a 128 mb flash		~ 600 KB ER	Far

3.3 Confirm Function of Principal Components			Accept
Accelerometers	Check data to confirm proper operation and verify saturation points (if high enough peak acceleration has occurred)	Low cupped 035 His cupped 0206	Ð
Pressure Sensors	Compare output in water column with independent measure of depth	2-04 =	M
Optical Mudline Sensor	View mudline output using low speed data and trigger on mudline.	ok	FA
Sound Velocity Sensor	Compare SV data with highly calibrated CTD or other independent measure of SV.	OK	TA 1
FfcptView Features and Functionality	Software demo and post- processing analysis.	eK	EM
Communications Interface Box	Verify connectivity and communications between PC and FFCPT.	OK	EM
Instrument Status LED	Confirm LED is working flashes regularly when instrument is armed (bench top test)	OK.	EN

## 4 MVP200/FFCPT Integration and Deployment

	Test	Result	Accept
Deployment and Recovery	Deployment and recovery in soft mud (2.5m penetration).	¢K_	FSM
Multi-drop Capability	Complete multiple drops and verify collection of data.	QK	EAN !!
Asymmetrical tail fin	Confirm that cable twisting is minimized.	ox	AN
Log Single Drop Mode	Demonstrate and log a single drop	A/M	ADV.

### 5 Evaluate Geotechnical Performance

	Test	Result	Accept
5.1 Penetration Depth			
Typical Penetrations (2.5 in soft mud, 1m in silt, 0.25 – 0.5 m in gravel/sand)	Check penetration depth in various sediment types through post-processed data and through physical observation of FFCPT.	2.3 - clary 11-14 cm - grave 1-(.3 - sandy sitt	Ð
5.2 Sediment Classification			
Consistency	Demonstrate consistent SBT classifications at one site.	OV_ =	EDA
Discrimination	Demonstrate ability to distinguish between variable sediment types at different locations.	or	TAT
Independent Validation	Compare SBT classification to core of grab samples.	ov	1AB

#### 6 Final Deliverables Verification

Deliverable	Check	Action
FFCPT with 660m depth rating for on-station work	1.	
Communications interface box	1,	
Data processing and presentation software (FfcptView)	1,	
Shipping Crate	1	
Service Tools and spares (see attached packing list)	U/	
Wire rope extension (mechanical)	1	
Electrical extension	)	send longer extension
Users manual and documentation	1	J
Line Puller and associate MVP upgrades	J,	
Load Cell	1	

#### FAT Test Action Items

1. Replace faulty dummy plug.

2. BOT to provide software upgrade by July 15, 2006 with full operations manual.

3. BOT to provide communication interface box schematic.

4. BOT to send longer E/M cable extension.

5. FFCPT Quick Start Guide (cheat sheet).

BOT to provide appendices drawings as PDFs (Manual and appendices already provided, with the exception of drawings).

7. BOT to provide pressure test record.

001 10 P	F	10-1 1 0 to	-	
8.				
9.				
10.				
11.				
12.				
13.				
14.				
15.				
16.				
17.				
18.				

BOT Representative: Dan Cunningham

NOAA Representative: Bob McConnaughey

Date: 6/14/06 1/0 Signed: Date: 6/14/06 Signed

# SBE 19plus SEACAT PROFILER

Conductivity, Temperature, and Pressure Recorder with RS-232 Interface



# Serial Number: 19P36026-4585

Sea-Bird Electronics, Inc. 1808 136<sup>th</sup> Place NE Bellevue, Washington 98005 USA Tel: 425/643-9866 Fax:425/643-9954

# SEA-BIRD ELECTRONICS, INC.

1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

#### SENSOR SERIAL NUMBER: 4585 CALIBRATION DATE: 28-Nov-06

SBE19plus TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

#### **ITS-90 COEFFICIENTS**

a0 = 1.152047e-003 a1 = 2.774008e-004 a2 = -1.305731e-006 a3 = 1.956257e-007

BATH TEMP (ITS-90)	INSTRUMENT OUTPUT(n)	INST TEMP (ITS-90)	RESIDUAL (ITS-90)
1.0000	686658.716	1.0001	0.0001
4.5000	613981.973	4.4998	-0.0002
15.0000	430447,473	15,0001	0.0001
18.4999	380354.081	18.4999	0.0000
24.0000	311743.365	23.9999	-0.0001
29.0000	259025.784	28.9999	-0.0001
32.5000	226964.392	32,5001	0.0001

MV = (n - 524288) / 1.6e+007

$$R = (MV * 2.900e+009 + 1.024e+008) / (2.048e+004 - MV * 2.0e+005)$$
  
Temperature ITS-90 = 1/{a0 + a1[ln(R)] + a2[ln<sup>2</sup>(R)] + a3[ln<sup>3</sup>(R)]} - 273.15 (°C)

Residual = instrument temperature - bath temperature



Date, Delta T (mdeg C)

# SEA-BIRD ELECTRONICS, INC. 1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 \_ 0866 Eax (425) 642 \_ 0054 Empile apphird @apphird ear

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4585 CALIBRATION DATE: 28-Nov-06

SBE19plus CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

#### COEFFICIENTS:

- g = -1.030197e+000h = 1.491063e-001 i = -1.948610e-004
- j = 3.642440e-005

CPCOT	=	-9.5700e-008	
CTcor	=	3.2500e-006	

BATH TEMP (ITS-90)	BATH SAL (PSU)	BATH COND (Siemens/m)	INST FREO (Hz)	INST COND (Siemens/m)	RESIDUAL (Siemens/m)
22.0000	0.0000	0.00000	2630.82	0.0000	0.00000
1.0000	34.7657	2.97205	5181.45	2.9721	0.00001
4.5000	34.7458	3.27873	5375.65	3.2787	-0.00001
15.0000	34.7032	4.25920	5953.51	4.2592	-0.00001
18.4999	34.6940	4.60388	6143.50	4.6039	0.00001
24.0000	34.6839	5.16110	6438.51	5.1611	0.00000
29.0000	34.6777	5.68217	6702.35	5.6822	0.00000
32.5000	34.6738	6.05395	6884.23	6.0539	-0.00000

f = INST FREQ / 1000.0

Conductivity =  $(g + hf^{2} + if^{3} + jf^{4}) / (1 + \delta t + \epsilon p)$  Siemens/meter

t = temperature[°C)]; p = pressure[decibars]; δ = CTcor; ε = CPcor;

Residual = instrument conductivity - bath conductivity



# SEA-BIRD ELECTRONICS, INC. 1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4585 CALIBRATION DATE: 16-Nov-06 SBE19plus PRESSURE CALIBRATION DATA 5076 psia S/N 5433

#### COEFFICIENTS:

PA0 =	5.395719e-001
PA1 =	1.544973e-002
PA2 =	-6.597195e-010
PTEMPA0	= -6.655452e+003
PTEMPA1	= 5.245122e+001
PTEMPA2	= -5.873641e-001

PTCAO	=	5.087765e+005
PTCA1	=	-1.437990e+000
PTCA2	=	1.066827e-001
PTCBO	=	2.398063e+001
PTCB1	=	-2.075000e-003
PTCB2	=	0.000000e+000

PRESSUR	E SPAN CAL	IBRATION			THERM	<b>AL CORREC</b>	TION
PRESSURI	E INST T	HERMISTOR	COMPUTE	D ERROR	TEMP T	HERMISTO	R INST
PSIA	OUTPUT	OUTPUT	PRESSURE	%FSR	ITS90	OUTPUT	OUTPUT
14,62	509685.9	1.6	14.46	-0.00	32.50	1.93	509747.27
1026.60	575274.6	1.7	1026.49	-0.00	29.00	1.86	509725.26
2039.16	641253.6	1.7	2038.83	-0.01	24.00	1.76	509699.82
3051.47	707615.1	1.7	3051.25	-0.00	18.50	1.65	509690.89
4063.65	774362.2	1.7	4063.70	0.00	15.00	1.58	509683.62
5075.85	841475.1	1.7	5075.75	-0.00	4.50	1.38	509674.14
4063.51	774357.9	1.7	4063.66	0.00	1.00	1.31	509676.42
3051.17	707619.8	1.7	3051.38	0.00			
2038.70	641248.6	1.7	2038.81	0.00	TEMP(IT	S90) SP	AN(mV)
1026.22	575271.0	1.7	1026.47	0.00	-5.0	0 2	3.99
14.63	509708.3	1.7	14.76	0.00	35.0	0 2	3.91

y = thermistor output; t = PTEMPA0 + PTEMPA1 \* y + PTEMPA2 \*  $y^{2}$ 

x = pressure output - PTCA0 - PTCA1 \* t - PTCA2 \* 
$$t^2$$

$$n = x * PTCB0 / (PTCB0 + PTCB1 * t + PTCB2 * t2)$$

pressure (psia) =  $PA0 + PA1 * n + PA2 * n^{2}$ 



Date, Avg Delta P %FS

16-Nov-06 0.00



# **Temperature Calibration Report**

Customer:	Pacific Marine Center / NOAA					
Job Number:	44764	Date of Report:	11/29/2006			
Model Number	SBE 19Plus	Serial Number:	19P36026-4585			

Temperature sensors are normally calibrated 'as received', without adjustments, allowing a determination sensor drift. If the calibration identifies a problem, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or non-functional, or by customer request.

An 'as received' calibration certificate is provided, listing coefficients to convert sensor frequency to temperature. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'offset' allows a small correction for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair apply only to subsequent data.

'AS RECEIVED CALIBRATION'	✓ Per	Not Performed	
Date: 11/28/2006	Drift since last cal:	00103	Degrees Celsius/year
Comments:			

'CALIBRATION AFTER REPAIR'	Performed	~	Not Performed
Date:	Drift since Last cal:		Degrees Celsius/year

Comments:



# **Conductivity Calibration Report**

Customer:	Pacific Marine Center / NOAA				
Job Number:	44764	Date of Report:	11/29/2006		
Model Number	SBE 19Plus	Serial Number:	19P36026-4585		

Conductivity sensors are normally calibrated 'as received', without cleaning or adjustments, allowing a determination of sensor drift. If the calibration identifies a problem or indicates cell cleaning is necessary, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or non-functional, or by customer request.

An 'as received' calibration certificate is provided, listing the coefficients used to convert sensor frequency to conductivity. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'slope' allows small corrections for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair or cleaning apply only to subsequent data.

'AS RECEIVED CALIBRATION'		✓ Perfor	med	Not	Performed
Date: 11/28/2006	Drift since las	t cal:	0001	0	PSU/month*
Comments:					
'CALIBRATION AFTER CLEANING & REPLA	ATINIZING'	Perfor	med	✓ Not	Performed
Date:	Drift since La	st cal:			PSU/month*
Comments:					

\*Measured at 3.0 S/m

Cell cleaning and electrode replatinizing tend to 'reset' the conductivity sensor to its original condition. Lack of drift in post-cleaning-calibration indicates geometric stability of the cell and electrical stability of the sensor circuit.

# SBE 19plus SEACAT PROFILER

Conductivity, Temperature, and Pressure Recorder with RS-232 Interface



# Serial Number: 19P36026-4616

Sea-Bird Electronics, Inc. 1808 136<sup>th</sup> Place NE Bellevue, Washington 98005 USA Tel: 425/643-9866 Fax:425/643-9954



# **Temperature Calibration Report**

Customer:	Pacific Marine Center / N	NOAA	
Job Number:	44765	Date of Report:	11/29/2006
Model Number	SBE 19Plus	Serial Number:	19P36026-4616

Temperature sensors are normally calibrated 'as received', without adjustments, allowing a determination sensor drift. If the calibration identifies a problem, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or non-functional, or by customer request.

An 'as received' calibration certificate is provided, listing coefficients to convert sensor frequency to temperature. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'offset' allows a small correction for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair apply only to subsequent data.

 'AS RECEIVED CALIBRATION'
 ✓ Performed
 Not Performed

 Date:
 11/28/2006
 Drift since last cal:
 -.00276
 Degrees Celsius/year

 Comments:

'CALIBRATION AFTER REPAIR'

Performed 🖌 Not Performed

Degrees Celsius/year

Date:

Drift since Last cal:

Comments:

# SEA-BIRD ELECTRONICS, INC.

1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4616 CALIBRATION DATE: 28-Nov-06 SBE19plus CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

#### COEFFICIENTS:

- g = -1.045668e+000h = 1.453942e-001
- i = -2.957046e 004
- j = 4.199194e-005

CPcor = -9.5700e-008CTcor = 3.2500e-006

BATH TEMP (ITS-90)	BATH SAL (PSU)	BATH COND (Siemens/m)	INST FREO (Hz)	INST COND (Siemens/m)	RESIDUAL (Siemens/m)
22.0000	0.0000	0.00000	2686.32	0.0000	0.00000
1.0000	34.7657	2.97205	5263.87	2.9721	0.00001
4.5000	34.7458	3.27873	5460.51	3.2787	-0.00001
15.0000	34.7032	4.25920	6045.75	4.2592	-0.00001
18.4999	34.6940	4.60388	6238.19	4.6039	0.00001
24.0000	34.6839	5.16110	6537.03	5.1611	0.00001
29.0000	34.6777	5.68217	6804.29	5.6822	-0.00000
32.5000	34.6738	6.05395	6988.55	6.0539	-0.00000

f = INST FREQ / 1000.0

Conductivity =  $(g + hf^{2} + if^{3} + jf^{4}) / (1 + \delta t + \epsilon p)$  Siemens/meter

t = temperature[°C)]; p = pressure[decibars]; δ = CTcor; ε = CPcor;

Residual = instrument conductivity - bath conductivity



Date, Slope Correction

# SEA-BIRD ELECTRONICS, INC. 1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4616 CALIBRATION DATE: 20-Nov-06 SBE19plus PRESSURE CALIBRATION DATA 1450 psia S/N 5512

#### COEFFICIENTS:

PAO =	(	5.8	81	52	64	e-	001	
PA1 =	4	1.	42	52	95	e-	003	
PA2 =	-]	1.2	2.0	24	69	e-	011	
PTEMP	= 0A	-'	7.	70	17	95	e+0	Q1,
PTEMP	A1 =	4	4.	98	98	90	e+0	01
PTEMP	A2 =	- 2	4.	24	86	17	e-0	01

PTCA0 = 5.204411e+005 PTCA1 = 1.323211e+001 PTCA2 = -2.756389e-001 PTCB0 = 2.473825e+001 PTCB1 = 5.000000e-005 PTCB2 = 0.000000e+000

PRESSURI PRESSURI PSIA	E SPAN CAL E INST T OUTPUT	IBRATION HERMISTOR OUTPUT	COMPUTEI PRESSURE	D ERROR %FSR	THERMA TEMP TI ITS90	L CORRECT HERMISTOR OUTPUT	TION L INST OUTPUT
14.60	523731.0	2.0	14.55	-0.00	32.50	2.24	523800.43
301.14	588511.0	2.0	301.15	0.00	29.00	2.17	523810.10
587.96	653320.7	2.0	587.79	-0.01	24,00	2.06	523813.00
874.50	718131.9	2.0	874.32	-0.01	18.50	1.95	523803.73
1161.10	782945.4	2.0	1160.77	-0.02	15.00	1.87	523798.40
1447.47	847858.4	2.0	1447.56	0.01	4.50	1.66	523724.90
1160.85	783006.0	2.0	1161.04	0.01	1.00	1.59	523661.67
874.07	718109.8	2.0	874.22	0.01			
587.12	653216.1	2.0	587.32	0.01	TEMP (ITS	590) SPA	AN (mV)
300.59	588415.5	2.0	300.73	0.01	-5.00	) 24	1.74
14.59	523729.7	2.0	14.54	-0.00	35.00	) 24	1.74

y = thermistor output; t = PTEMPA0 + PTEMPA1 \* y + PTEMPA2 \*  $y^2$ 

$$n = x * PTCB0 / (PTCB0 + PTCB1 * t + PTCB2 * t2)$$

pressure (psia) =  $PA0 + PA1 * n + PA2 * n^{2}$ 







# SEA-BIRD ELECTRONICS, INC.

1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

#### SENSOR SERIAL NUMBER: 4616 CALIBRATION DATE: 28-Nov-06

SBE19plus TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

#### **ITS-90 COEFFICIENTS**

- a0 = 1.270073e-003a1 = 2.575893e-004a2 = 5.463437e-007
- a3 = 1.270161e 007

BATH TEMP (ITS-90)	INSTRUMENT OUTPUT(n)	INST TEMP (ITS-90)	RESIDUAL (ITS-90)
1.0000	622362.833	1.0000	-0.0000
4.5000	552569.850	4.5001	0.0001
15.0000	379385.467	14.9999	-0.0001
18.4999	332894.733	18.4999	0.0000
24.0000	269791.750	24.0001	0.0001
29.0000	221775.083	29.0000	-0.0000
32.5000	192778.933	32.5000	-0.0000

MV = (n - 524288) / 1.6e+007

R = (MV \* 2.900e+009 + 1.024e+008) / (2.048e+004 - MV \* 2.0e+005)Temperature ITS-90 = 1/{a0 + a1[*ln*(R)] + a2[*ln*<sup>2</sup>(R)] + a3[*ln*<sup>3</sup>(R)]} - 273.15 (°C)

Residual = instrument temperature - bath temperature



Date, Delta T (mdeg C)



# **Conductivity Calibration Report**

Customer:	Pacific Marine Center / NOAA				
Job Number:	44765	Date of Report:	11/29/2006		
Model Number	SBE 19Plus	Serial Number:	19P36026-4616		

Conductivity sensors are normally calibrated 'as received', without cleaning or adjustments, allowing a determination of sensor drift. If the calibration identifies a problem or indicates cell cleaning is necessary, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or non-functional, or by customer request.

An 'as received' calibration certificate is provided, listing the coefficients used to convert sensor frequency to conductivity. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'slope' allows small corrections for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair or cleaning apply only to subsequent data.

'AS RECEIVED CALIBRATION'	✓ Perfor	rmed No	t Performed
Date: 11/28/2006	Drift since last cal:	00020	] PSU/month*
Comments:			
		true 1	
'CALIBRATION AFTER CLEANING & I	REPLATINIZING' Perfor	rmed 🗹 No	t Performed
Date:	Drift since Last cal:		] PSU/month*
Comments:			

\*Measured at 3.0 S/m

Cell cleaning and electrode replatinizing tend to 'reset' the conductivity sensor to its original condition. Lack of drift in post-cleaning-calibration indicates geometric stability of the cell and electrical stability of the sensor circuit.
## SBE 19plus SEACAT PROFILER

Conductivity, Temperature, and Pressure Recorder with RS-232 Interface



## Serial Number: 19P36026-4617

Sea-Bird Electronics, Inc. 1808 136<sup>th</sup> Place NE Bellevue, Washington 98005 USA Tel: 425/643-9866 Fax:425/643-9954

## SEA-BIRD ELECTRONICS, INC. 1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4617 CALIBRATION DATE: 20-Nov-06 SBE19plus PRESSURE CALIBRATION DATA 1450 psia S/N 5513

### COEFFICIENTS:

PA0 =	-6.818889e-001
PAl =	4.441786e-003
PA2 =	-1.461601e-011
PTEMPAO	= -7.808315e+001
PTEMPA1	= 4.830529e+001
PTEMPA2	= -1.963775e-001

PTCAU	=	5.192316e+005
PTCA1	=	-1.293709e+001
PTCA2	=	2.841324e-001
PTCBO	=	2.460838e+001
PTCB1	=	6.750000e-004
PTCB2	-	0 0000000+000

PRESSURI	E SPAN CAL	IBRATION			THERN	AAL CORREC	CTION
PRESSURI	E INST I	HERMISTOR	COMPUTER	D ERROR	TEMP	THERMISTO	OR INST
PSIA	OUTPUT	OUTPUT	PRESSURE	%FSR	ITS90	OUTPUT	OUTPUT
14.60	522522.3	2.1	14.57	-0.00	32.50	2.31	522606.59
301.14	587037.6	2.1	300.91	-0.02	29.00	2.24	522606.93
587.96	651734.5	2.1	587.92	-0.00	24.00	2.13	522594.90
874.50	716289.7	2.1	874.19	-0.02	18.50	2.02	522596.96
1161.10	780935.2	2.1	1160.73	-0.03	15.00	1.94	522599.38
1447.47	845673.7	2.1	1447.55	0.01	4.50	1.72	522670.83
1160.85	781013.3	2.1	1161.07	0.02	1.00	1.65	522733.56
874.07	716327.5	2.1	874.35	0.02			
587.12	651602.8	2.1	587.33	0.01	TEMP(I	(TS90) S	PAN (mV)
300.59	587008.6	2.1	300,78	0.01	-5.	00	24.61
14.59	522526.1	2.1	14.59	0.00	35.	0.0	24.63

y = thermistor output; t = PTEMPA0 + PTEMPA1 \* y + PTEMPA2 \*  $y^{2}$ 

x = pressure output - PTCA0 - PTCA1 \* t - PTCA2 \*  $t^2$ 

$$n = x * PTCB0 / (PTCB0 + PTCB1 * t + PTCB2 * t2)$$

pressure (psia) =  $PA0 + PA1 * n + PA2 * n^{2}$ 

Date, Avg Delta P %FS



Date, Tryg Dena 1 7015

20-Nov-06 0.00

## SEA-BIRD ELECTRONICS, INC.

1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

SENSOR SERIAL NUMBER: 4617 CALIBRATION DATE: 28-Nov-06

SBE19plus CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

### COEFFICIENTS:

- g = -9.992894e-001h = 1.278604e-001
- i = -2.890367e-004
- j = 3.593846e-005

CPcor = -9.5700e-008 CTcor = 3.2500e-006

BATH TEMP (ITS-90)	BATH SAL (PSU)	BATH COND (Siemens/m)	INST FREO (Hz)	INST COND (Siemens/m)	RESIDUAL (Siemens/m)
22.0000	0.0000	0.00000	2801.40	0.0000	0.00000
1.0000	34.7657	2.97205	5583.94	2.9721	0.00000
4.5000	34.7458	3.27873	5794.98	3.2787	-0.00000
15.0000	34.7032	4.25920	6422.55	4.2592	0.00000
18.4999	34.6940	4.60388	6628.77	4.6039	0.00001
24.0000	34.6839	5.16110	6948.88	5.1611	-0.00001
29.0000	34.6777	5.68217	7235.05	5.6822	-0.00000
32.5000	34.6738	6.05395	7432.30	6.0539	0.00000

f = INST FREQ / 1000.0

Conductivity =  $(g + hf^{2} + if^{3} + jf^{4}) / (1 + \delta t + \varepsilon p)$  Siemens/meter

t = temperature[°C)]; p = pressure[decibars];  $\delta$  = CTcor;  $\varepsilon$  = CPcor;

Residual = instrument conductivity - bath conductivity



Date, Slope Correction

## SEA-BIRD ELECTRONICS, INC.

1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

#### SENSOR SERIAL NUMBER: 4617 CALIBRATION DATE: 28-Nov-06

SBE19plus TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

### **ITS-90 COEFFICIENTS**

a0 = 1.263742e-003 a1 = 2.634287e-004 a2 = 7.176289e-008 a3 = 1.504204e-007

-90)
001
002
001
002
001
002
001
1 1 1 1 1 1

MV = (n - 524288) / 1.6e+007

$$R = (MV * 2.900e+009 + 1.024e+008) / (2.048e+004 - MV * 2.0e+005)$$
  
Temperature ITS-90 = 1/{a0 + a1[*ln*(R)] + a2[*ln*<sup>2</sup>(R)] + a3[*ln*<sup>3</sup>(R)]} - 273.15 (°C)

Residual = instrument temperature - bath temperature





## **Temperature Calibration Report**

Customer:	Pacific Marine Center / N	IOAA	
Job Number:	44636	Date of Report:	11/29/2006
Model Number	SBE 19Plus	Serial Number:	19P36026-4617

Temperature sensors are normally calibrated 'as received', without adjustments, allowing a determination sensor drift. If the calibration identifies a problem, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or non-functional, or by customer request.

An 'as received' calibration certificate is provided, listing coefficients to convert sensor frequency to temperature. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'offset' allows a small correction for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair apply only to subsequent data.

'AS RECEIVED CALIBRATION'

Date.	11/28/2006
Dall.	1112012000

✓ Pe	rformed	Not Performed
Drift since last cal:	00207	Degrees Celsius/year

Comments:

'CALIBRATION AFTER REPAIR'

Performed 🗹 Not Performed

Date:

Drift since Last cal: Degrees Celsius/year

Comments:



## **Conductivity Calibration Report**

Customer:	Pacific Marine Center / NO	AAC	
Job Number:	44636	Date of Report:	11/29/2006
Model Number	SBE 19Plus	Serial Number:	19P36026-4617

Conductivity sensors are normally calibrated 'as received', without cleaning or adjustments, allowing a determination of sensor drift. If the calibration identifies a problem or indicates cell cleaning is necessary, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or non-functional, or by customer request.

An 'as received' calibration certificate is provided, listing the coefficients used to convert sensor frequency to conductivity. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'slope' allows small corrections for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair or cleaning apply only to subsequent data.

'AS RECEIVED CALIBRATION'		✓ Perform	ned	Not Performed
Date: 11/28/2006	Drift since la	st cal:	00030	PSU/month*
Comments:				
'CALIBRATION AFTER CLEANING & REP	LATINIZING'	Perform	ned 🗸	Not Performed
Date:	Drift since La	ast cal:		PSU/month*
Comments:				

\*Measured at 3.0 S/m

Cell cleaning and electrode replatinizing tend to 'reset' the conductivity sensor to its original condition. Lack of drift in post-cleaning-calibration indicates geometric stability of the cell and electrical stability of the sensor circuit.



### **APPLICATION NOTE NO. 42**

## **Revised September 2001**

### **ITS-90 TEMPERATURE SCALE**

Beginning January 1995, Sea-Bird temperature calibration certificates list a new set of coefficients labeled g, h, i, j, and F0. These coefficients correspond to ITS90 (T90) temperatures and should be entered by those researchers working with SEASOFT-DOS Versions 4.208 and higher (and all versions of SEASOFT-Win32). For the convenience of users who prefer to use older SEASOFT versions, the new certificates also list a, b, c, d, and F0 coefficients corresponding to IPTS68 (T68) temperatures as required by SEASOFT-DOS versions older than 4.208.

It is important to note that the international oceanographic research community will continue to use T68 for computation of salinity and other seawater properties. Therefore, following the recommendations of Saunders (1990) and as supported by the Joint Panel on Oceanographic Tables and Standards (1991), SEASOFT-DOS 4.200 and later and all versions of SEASOFT-Win32 convert between T68 and T90 according to the linear relationship:

### $T_{68} = 1.00024 * T_{90}$

The use of T68 for salinity and other seawater calculations is automatic in all SEASOFT programs. However, when selecting **temperature** as a display/output variable, you will be prompted to specify which standard (T90 or T68) is to be used to compute temperature. SEASOFT recognizes whether you have entered T90 or T68 coefficients in the configuration (.con) file, and computes T90 temperature directly or calculates it from the Saunders linear approximation, depending on which coefficients were used and which display variable type is selected.

For example, if *g*, *h*, *i*, *j*, *F0* coefficients (T90) are entered in the .con file and you select temperature variable type as T68, SEASOFT computes T90 temperature directly and multiplies it by 1.00024 to display T68. Conversely, if *a*, *b*, *c*, *d*, and *F0* coefficients (T68) are entered in the .con file and you select temperature variable type as T90, SEASOFT computes T68 directly and divides by 1.00024 to display T90.

**Note:** The CTD configuration (.con) file is edited using the Configure menu (in SEASAVE or SBE Data Processing in our SEASOFT-Win32 suite of programs) or SEACON (in SEASOFT-DOS).

Also beginning January 1995, Sea-Bird's own temperature metrology laboratory (based upon water triple-point and gallium melt cell, SPRT, and ASL F18 Temperature Bridge) converted to T90. These T90 standards are now employed in calibrating *all* Sea-Bird temperature sensors, and as the reference temperature used in conductivity calibrations. Accordingly, all calibration certificates show T90 (g, h, i, j) coefficients that result directly from T90 standards, and T68 coefficients (a, b, c, d) computed using the Saunders linear approximation.

## SEA-BIRD ELECTRONICS, INC.

1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

### SENSOR SERIAL NUMBER: 0117 CALIBRATION DATE: 03-Dec-05

SBE 45 TEMPERATURE CALIBRATION DATA ITS-90 TEMPERATURE SCALE

#### **ITS-90 COEFFICIENTS**

a0 = -2.052604e-004 a1 = 3.017581e-004 a2 = -4.020330e-006 a3 = 1.929919e-007

BATH TEMP (ITS-90)	INSTRUMENT OUTPUT	INST TEMP (ITS-90)	RESIDUAL (ITS-90)
1.0000	825534.5	1.0000	-0.0000
4.5000	707891.5	4.5000	0.0000
15.0000	454957.4	15.0000	-0.0000
18.5000	395012.3	18.5000	0.0000
24.0000	318215.6	24.0000	-0.0000
29.0000	262997.6	29.0000	-0.0000
32.5000	230900.3	32.5000	0.0000

Temperature ITS-90 =  $1/{a0 + a1[ln(n)] + a2[ln^2(n)] + a3[ln^3(n)]} - 273.15$  (°C)

Residual = instrument temperature - bath temperature





BE SEA-BIRD ELECTRONICS, INC. 1808 - 136th Place Northeast, Bellevue, Washington 98005 USA

1808 - 136th Place Northeast, Bellevue, Washington 98005 USA Phone: (425) 643-9866 Fax: (425) 643-9954 www.seabird.com

## **Temperature Calibration Report**

Customer:	Pacific Marine Center / NOAA		
Job Number:	41336	Date of Report:	12/5/2005
Model Number:	SBE 45	Serial Number:	4536628-0117

Temperature sensors are normally calibrated 'as received', without adjustments, allowing a determination sensor drift. If the calibration identifies a problem, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or non-functional, or by customer request.

An 'as received' calibration certificate is provided, listing coefficients to convert sensor frequency to temperature. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'offset' allows a small correction for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair apply only to subsequent data.

'AS RECEIVED CALIBRATION'	✓ Pe	rformed	Not Performed
Date: 12/3/2005	Drift since last cal:	+.00114	Degrees Celsius/year
Comments:			

'CALIBRATION AFTER REPAIR'	Performed	✓ Not Performed	
Date:	Drift since Last cal:	Degrees Celsius/year	
Comments:			

## SEA-BIRD ELECTRONICS, INC.

1808 136th Place N.E., Bellevue, Washington, 98005 USA

Phone: (425) 643 - 9866 Fax (425) 643 - 9954 Email: seabird@seabird.com

#### SENSOR SERIAL NUMBER: 0117 CALIBRATION DATE: 03-Dec-05

#### SBE 45 CONDUCTIVITY CALIBRATION DATA PSS 1978: C(35,15,0) = 4.2914 Siemens/meter

#### COEFFICIENTS:

g = -1.0	29977e+000
----------	------------

- h = 1.264651e-001i = -1.493348e-004
- j = 2.835643e-005

CPcor	=	-9.5700e-008
CTcor	=	3.2500e-006
WBOTC	=	-3.1803e-006

BATH TEMP (ITS-90)	BATH SAL (PSU)	BATH COND (Siemens/m)	INST FREQ (Hz)	INST COND (Siemens/m)	RESIDUAL (Siemens/m)
22.0000	0.0000	0.00000	2856.14	0.00000	0.00000
1.0000	34.9437	2.98581	5633.80	2.98582	0.00001
4.5000	34.9237	3.29386	5845.07	3.29385	-0.00001
15.0000	34.8803	4.27863	6473.56	4.27862	-0.00001
18.5000	34.8714	4.62489	6680.21	4.62489	0.00000
24.0000	34.8613	5.18458	7001.01	5.18461	0.00003
29.0000	34.8563	5.70813	7287.93	5.70810	-0.00003
32.5000	34.8533	6.08171	7485.76	6.08172	0.00001

f = INST FREQ \* sqrt(1.0 + WBOTC \* t) / 1000.0

Conductivity =  $(g + hf^{2} + if^{3} + jf^{4}) / (1 + \delta t + \epsilon p)$  Siemens/meter

t = temperature[°C)]; p = pressure[decibars];  $\delta$  = CTcor;  $\epsilon$  = CPcor;

Residual = instrument conductivity - bath conductivity



Date, Slope Correction



BE SEA-BIRD ELECTRONICS, INC. 1808 - 136th Place Northeast, Bellevue, Washington 98005 USA

1808 - 136th Place Northeast, Bellevue, Washington 98005 USA Phone: (425) 643-9866 Fax: (425) 643-9954 www.seabird.com

## **Conductivity Calibration Report**

Customer:	Pacific Marine Center / NOAA					
Job Number:	41336	Date of Report:	12/5/2005			
Model Number:	SBE 45	Serial Number:	4536628-0117			

Conductivity sensors are normally calibrated 'as received', without cleaning or adjustments, allowing a determination of sensor drift. If the calibration identifies a problem or indicates cell cleaning is necessary, then a second calibration is performed after work is completed. The 'as received' calibration is not performed if the sensor is damaged or non-functional, or by customer request.

An 'as received' calibration certificate is provided, listing the coefficients used to convert sensor frequency to conductivity. Users must choose whether the 'as received' calibration or the previous calibration better represents the sensor condition during deployment. In SEASOFT enter the chosen coefficients using the program SEACON. The coefficient 'slope' allows small corrections for drift between calibrations (consult the SEASOFT manual). Calibration coefficients obtained after a repair or cleaning apply only to subsequent data.

'AS RECEIVED CALIBRATION'	✓ Perfe	ormed 🗆 N	Not Performed
Date: 12/3/2005	Drift since last cal:	00210	PSU/month*
Comments:			

'CALIBRATION AFTER CL	EANING & REPLATINIZING' Perf	formed 🗹 Not Performed
Date:	Drift since Last cal:	PSU/month*
Comments:		

\*Measured at 3.0 S/m

Cell cleaning and electrode replatinizing tend to 'reset' the conductivity sensor to its original condition. Lack of drift in post-cleaning-calibration indicates geometric stability of the cell and electrical stability of the sensor circuit.



# BE SEA-BIRD ELECTRONICS, INC. 1808 - 136th Place Northeast, Bellevue, Washington 98005 USA

Phone: (425) 643-9866 Fax: (425) 643-9954 www.seabird.com

## **Pressure Test Certificate**

Customer	Pacific Marine Center / NOAA
Job Number	41336
Date	12/6/2005
<u>Technician</u>	JS
<u>Serial Number</u>	4536628-0117
Low Pressure (PSI)	2 45 PSI
Time (Minutes)	45 Minutes
High Pressure (PSI	) N/A* PSI
<u>Time (Minutes)</u>	Minutes
Pass 🔽	
Fail	
Comments	
Replaced the main	piston "O"-Rings.
*This unit is not des	igned for high pressure applications.
Pressure	High pressure is generally equal to the maximum depth rating of the instrument.
	Time

**Typical Test Profile** 

医弗里克氏 网络马克斯特拉克 网络马克拉斯特拉 网络克克吉

n sa ng sang sang sa ng ng sa sang sa ng sa n

TSG-Data.txt

S>ds SBE45 V 1.1 SERIAL NO. 0117508, 1.52891, 10.3145, 1489 not logging data sample interval = 1 seconds898, 10.3150, 1489.601 output conductivity with each sample18.5508, 1.52905, 10.3155, 1489.601 output salinity with each sample 18.5509, 1.52912, 10.3160 S>dc SBE45 V 1.1 0117 temperature: 03-dec-05 TAO = -2.052604e-04 TA1 = 3.017581e-04 TA2 = -4.020330e-06TA3 = 1.929919e-07conductivity: 03-dec-05 G = -1.029977e+00H = 1.264651e-01I = -1.493348e-04 J = 2.835643e-05 CPCOR = -9.570000e-08 CTCOR = 3.250000e-06 WBOTC = -3.180305e-06 

 S>
 18.5870,
 1.52912,
 10.3071,
 1489.703

 18.5872,
 1.52913,
 10.3071,
 1489.704

 18.5874,
 1.52914,
 10.3072,
 1489.705

 18.5875,
 1.52919,
 10.3075,
 1489.706

 18.5876,
 1.52920,
 10.3076,
 1489.706

 18.5874,
 1.52920,
 10.3076,
 1489.706

 18.5874,
 1.52920,
 10.3076,
 1489.705

 18.5874,
 1.52920,
 10.3076,
 1489.705

 19.5870,
 1.52920,
 10.3076,
 1489.705

 18. 5870, 1.5291,
18. 5872, 1.52913,
18. 5874, 1.52914,
18. 5875, 1.52919,
18. 5876, 1.52920,
18. 5874, 1.52920,
18. 5870, 1.52919, 10.3076



## Certificate of Calibration

Model: Nikon DTM310

Serial Number: 842575

This certifies that the above instrument has been inspected and calibrated by the GeoLine Positioning Systems Inc. Service Department. At the time of completion of this service, GeoLine Positioning Systems, Inc. certifies that the above stated product meets all factory specifications and tolerances for product parameters and performance of this product model.

All product calibration and specification parameters were tested and/or adjusted using applicable factory calibration jigs, precision optical collimation systems and electronic test equipment. All collimation systems have been properly checked and calibrated according to industry standard practices. All electronic test equipment used have had current calibration.

Date of Calibration: 6/28/04

Next Recommended Calibration Date: 12/28/04

whe Signed:

\_\_\_\_\_ Date: <u>6/28/04</u>

Title: Service Technician

GeoLine Positioning Systems, Inc. 1331 118th Avenue SE, Suite 400 Bellevue, WA 98005 425.452.2711 • 425.452.2703 fax



## Certificate of Calibration

Model: Sokkia SET 5F

Serial Number: 16288

This certifies that the above instrument has been inspected and calibrated by the GeoLine Positioning Systems Inc. Service Department. At the time of completion of this service, GeoLine Positioning Systems, Inc. certifies that the above stated product meets all factory specifications and tolerances for product parameters and performance of this product model.

All product calibration and specification parameters were tested and/or adjusted using applicable factory calibration jigs, precision optical collimation systems and electronic test equipment. All collimation systems have been properly checked and calibrated according to industry standard practices. All electronic test equipment used have had current calibration.

Date of Calibration: 7/19/04

Next Recommended Calibration Date: 7/19/05

Signed: Sean Value

Date: 7/19/04

Title: Service Technician

GeoLine Positioning Systems, Inc. 1331 118th Avenue SE, Suite 400 Bellevue, WA 98005 425.452.2711 • 425.452.2703 fax

## Appendix VI

Maintenance and Periodic Testing

CTD Care, Maintenance and Testing

DLDG Daily DQA

### SV Maintenance & Testing 2007

Date	Project	Maintenance	Notes	Results	Location
				_	_
3/29/2007	HSRR	Performed DQA between 4616 and 4617	Velocwin 8.83 installed on O-lab computer and 1010	ОК	Blank Inlet - Ketchikan Shakedown
4/14/2007	O119 Ernest Sound	Performed DQA between 4585 and MVP		ОК	Fools Inlet
4/25/2007	O119 Ernest Sound	Performed DQA between 4585 and 4617		ОК	Menefee Inlet
5/2/2007	O119 Ernest Sound	DQA between 4585 and 4617		ОК	Seward Passage
5/2/2007	O119 Ernest Sound	Attempted DQA with MVP and 4616	see note in folder	n/a	Seward Passage
5/12/2007	O119 Ernest Sound	DQA between 4585 and MVP		ОК	S of Sunny Bay
5/14/2007	O119 Ernest Sound	DQA between 4617 and 4616		ОК	S of Sunny Bay
5/22/2007	O119 Ernest Sound	DQA between 4616 and 4585		ОК	S of Sunny Bay
5/22/2007	O119 Ernest Sound	DQA between 4617 and MVP	Failed. Reattempt on 5/24, Results OK	N/A	S of Sunny Bay
5/24/2007	O119 Ernest Sound	DQA between 4617 and MVP		ОК	Warm Springs Bay
6/2/2007	P183 Shumagin Is	DQA b/w MVP and 4585		ОК	Big Koniuji
6/2/2007	P183 Shumagin Is	DQA b/w 4617 and 4616		ОК	Big Koniuji
6/19/2007	P183 Shumagin Is	DQA between 4616 and 4585		ОК	Big Koniuji
7/27/2007	P183 Shumagin Is	DQA between 4617 and 4585		ОК	Sand Point
7/27/2007	P183 Shumagin Is	DQA between 4616 and MVP	BOT file processed OK; Seacat error (too few points); reattempt	failed	Sand Point
7/30/2007	P183 Shumagin Is	DQA reattempted for 4616 and MVP	vbatt low on Seacat, changed out D batteries	ок	Bendel Is
8/15/2007	P183 Shumagin Is	4617 and MVP		ОК	Mist Harbor
8/15/2007	P183 Shumagin Is	4616 and 4585		ОК	Mist Harbor
8/24/2007	P132 NE PWS	4585 and MVP	POSMV wasn't on so BOT files did not have positions and could not be processed	failed	Two Moon Bay
8/27/2007	P132 NE PWS	4616 and 4617		ОК	Two Moon Bay
8/27/2007	P132 NE PWS	4585 and MVP		ОК	Two Moon Bay
9/12/2007	P132 NE PWS	4617 and 4585		ОК	Two Moon Bay
9/12/2007	P132 NE PWS	4616 and MVP		ОК	Two Moon Bay
9/20/2007	P132 NE PWS	4616 and 4585		ОК	Two Moon Bay
9/20/2007	P132 NE PWS	4617 and MVP		ОК	Two Moon Bay
10/8/2007	P132 NE PWS	4585 and MVP		ОК	Sunny Bay
10/8/2007	P132 NE PWS	4616 and 4617		ОК	Two Moon Bay
10/25/2007	O168 Endicott Arm	4616 and MVP		ОК	Sanford Cove
10/25/2007	O168 Endicott Arm	4617 and 4585			Sanford Cove

Subject: [Fwd: [Fwd: DGPS: P-checks & Nav DQA]]
Date: Mon, 12 Sep 2005 18:22:20 -0800
From: "foo fairweather" <foo.fairweather@noaa.gov>
To: chiefst.fairweather@noaa.gov

\_\_\_\_\_

Abigail,

I assume you're checking FOO-FA now, so sorry if you get this twice. Anyway, here's the email from Gerd from the spring about P-checks. Looks like it was a question from Lynn which prompted it in the first place.

Ben

----- Original Message -----Subject: DGPS: P-checks & Nav DQA Date: Wed, 25 May 2005 17:01:38 -0400 From: Gerd Glang <Gerd.Glang@noaa.gov> Organization: NOAA Hydro Systems & Technology Programs (301-713-2653, x152) To: holly.dehart.atsea@noaa.gov CC: Jack Riley <Jack.Riley@noaa.gov>, "Lynnette V. Morgan" <Lynnette.V.Morgan@noaa.gov>, "Holly A. Dehart" <Holly.A.Dehart@noaa.gov>, Benjamin K Evans <Benjamin.K.Evans@noaa.gov>, Guy Noll <Guy.Noll@noaa.gov> References: <793c68e7.68e7793c@fairweather.nmao.noaa.gov>

Hi Holly (I hear my train leaving),

Your "atsea" e-mail keeps getting bounced back...so I'm copying Lynn on this.

Short answer - No.

USCG Beacons are subject to their own rigorous integrity monitoring. If the beacon signal is being received w/ good signal strength, it should be valid for correcting your position (simple answer). The Specs and Deliverables requirements assume this.

What we need to do is check that our receivers are working properly and no bogus antenna offsets were entered. Probably adequate to do this once per season as part of the system cert, or when you suspect a problem. Our MB data (and side scan data) are spatially dense enough that any problems would be apparent in the data right away. Also, the several GPS failures we've experienced this year have all been pretty catastrophic, i.e., there was no doubt the POS GPS had failed. Bottom line, it's not in the current draft FPM, its not in the Specs and Deliverables. Should be a reqt for the System Cert process. So the two things I would require:

 During data acquisition, conscientious monitoring of all sensor data (POS controller window, POS CPU lights, USCG Beacon Receiver display/lights, Isis display, etc).
 During daily post-processing, a systematic and careful review of the data - treat as a directed editing problem.

Of course, we often fiddle with acquisition system configurations, both hardware and software, for one reason or another (or some gremlin gets into the system). It would be prudent to have a system cert-like checklist to run thru on Monday mornings after a long inport to prompt the briefly-befuddled or newly-trained OIC and chase Mr. Murphy away. Sort of like a pre-flight checklist. You may recall, we once had a case on the WH where an entire launch day (+4 hrs OT) of data was hosed because the Isis config was messed up the night before, and the JO's (who shall remain nameless but were nevertheless well qualified) didn't pay attention to #1.

(The complacent hydrographer will soon go aground - GFG).

BTW - RA has SonarPro for SSS (haven't used it much lately). NRTs use SonarPro.

#### G2

Holly DeHart atsea wrote:

> Hi Gerd,

> Lynn was asking me about comparing differential beacons, where you > take coincident positions w/ two systems on different beacons. Sounds > like WH's old p-check system. Do we still need to do these? If so at > what frequency? They've been doing it weekly all season w/ no errors, > is this still necessary? > > Holly > --LT Ben Evans, NOAA Field Operations Officer NOAA Ship RAINIER (s221) NOAA Marine Operations Center, Pacific 1801 Fairview Ave. E Seattle, WA 98102 Thank you so much - this was indeed the project we were discussing. Could you tell me, is that 0.14 total tide error is a one-sigma or two-sigma error estimate?

Thank you for your time.

~~ mike.q.

Monica Cisternelli wrote:

> I computed an error estimation for OPR-O119-FA-2007, between historic > Thoms Point and Ketchikan, and the total tide error came out to be 0.14 > m ( including datum error). I am not sure if this is even the project > you are concerned about, but it is the only one where we did not include > an error estimation in our project instructions. So I guessed this is > the one your talking about. So please use this value rather than a 0.4. > Thanks

>

> Monica

Thank you for the info Rick, it was ~exactly~ what I was looking for ..

While it is a shame to watch our data collapse in the face of IHO Order 1, it might just be the sad truth of Alaskan surveying: given the tidal uncertainties, a definitive depth cannot be ascertained without an appreciable error envelope.

I wish we could re-create your 14m IHO error in the field. As I mentioned earlier, we were unable to survey past 48m and maintain IHO Order 1. We'd used the exact error values suggested for the POS M/V and time latency suggested in HSTD-2; Our offset erors are on the order of 7 mm; Loading and Draft 3 and 4cm respectively; we low-balled the SV at 1 m/s and left the Delta Draft, and MRU align errors as zero (since we had yet to compute the patch test). This configuration blanked our swath in waters shoaler than 48m when filtered against IHO - but then, as you suggested, perhaps it is unrealistic to be expected to survey to IHO order 1 under these conditions. If that's the case, I feel like there should have been a disclaimer presented to everyone during the west coast hydro training, "Hey gang, while we strive to satisty IHO, the reality is you won't be able to get there while surveying in the shallow waters. How shallow? Well, anything shoaler than the Statue of Liberty is tall (46.84m - base to torch)."

The picture will not improve when the delta draft and MRU errors are added to the model.

I have attached a copy of our TPE spread sheet. Do any of the values appear inordinately high to you that keeps us from reaching your 14m glass ceiling (or would it be a glass floor)?

Is RAINIER having better luck than we?

Thank you for your time, all.

Regards,

~~ mike.g. Richard T Brennan wrote: > Hi Mike, > Not sure if you saw my response to Ben, but I agree, the MRU alignment > error is too big. My recommendation was that the guidance should say > "The MRU alignment error should be approximately the smallest unit of > change in the HIPS calibration window which produces no noticeable > change in the point cloud alignment." I think this would yield a > similar result to the method you are employing and not require a field > party to have six people, or have six people look at their patch test. > As for the zoning error, this value wraps up a lot of sins in one > place and thus I would not suggest altering this without consulting > CO-OPS. The goal of populating the error model with the various > system uncertainties is not to tweak them until they are "within > spec", it is to give us an honest assessment of how good our > measurements are. The zoning model does not account for changes in > the shape of the tide curve across the survey area (i.e. diurnal to > semi-diurnal, or semi-diurnal to mixed, etc...), differences between > the rate an area floods and ebbs, uncertainties in the datum, and > inaccuracies induced by the interpolation method itself. While CO-OPS > may not be able to supply a definitive zoning error value for your > survey area, they do use some judgment based on experience, and > experience has shown that 0.4 is not an unrealistic value, > particularly in Alaska. While 0.4m for zoning error is not unheard > of, it is larger than normal, so I would confirm with CO-OPS that this > is indeed the correct value. While your data may appear to be > internally consistent (no stereotypical tide artifacts), errors > induced by uncertainties in the datum would not cause a visual > artifact. That said my computations show that you should be able to > survey up to 14 m of water and still maintain IHO Order 1 with a 0.4m > combine tidal uncertainty (that is the rms of measurement uncertainty > and zoning uncertainty). I have attached a spreadsheet with my > numbers in it. Let me know if you have any questions regarding these > values. Hope this helps... > > Rick > > michael gonsalves wrote: >> \*\* This e'mail is longer than the attention span of the average JO >> and ST - thus I present the summary at the beginning: An MRU align >> error of 1.0 is too large; something on the order of 0.20 is a >> better estimate (want to know why ... then read on); A tidal zoning >> of 0.40 is also too large, it makes it impossible to acquire IHO >> Order 1 data in waters shoaler than ~45m), I propose 0.10 as a >> better upper bound until CO-OPS commits to something better. >> ...and now for the message -- mog \*\* >> >> Wait, we can haggle over HSTD 2007-2? >> >> ITEM #1 - MRU Alignment >> FAIRWEATHER had identical problems to those described by LT Evans at

>> the end of the previous field season. An incorrect calculation led >> to MRU alignment errors ~0.5 degrees which led to 2/3 or our swath >> being rejected as not satisfying IHO Order 1. >> >> I believe the spirit of the error is to report your reliability in >> the operator's ability to perform a successful patch test. RAINIER >> has struck upon the proper approach having several people >> independently perform the patch test. At that point, the Standard >> Deviation of the patch test values can be used as a valid >> approximation of the MRU alignment errors. This is the technique >> suggested by Dr. Calder to FA around this time last year. The only >> caveat I would suggest is that the multiple evaluations of the patch >> test data must be performed in tandem; that is, all processors must >> agree on a value in the timing error before the group proceeds to >> calibrating for pitch (and so on). Such a simultaneous approach is >> necessary due to the confounding of the various alignment errors >> (i.e. a pitch-induced artifact can be removed by adjusting timing). >> >> By the end of the field season, FA had settled on MRU align values >> of 0.25 for gyro and 0.15 for roll/pitch. In my opinion, these >> values may still be on the conservative side. But, with these >> values inserted into the hvf, filtering the data against IHO Order 1 >> resulted in all the wacky outbeams being rejected while the smooth >> continuous bottom was preserved. Any parameters that leads to >> "poor" data being rejected while retaining the "good" is a step in >> the right direction. >> >> The redundancy in having multiple eyes view a patch test can only be >> taken so far however. Sea state, speed of the vessel, validity of >> sound velocity profile, whether that pitch line was run ~exactly~ on >> top of the sonar-conspicious target will dictate how valid a given >> set of patch lines are for accurately determining the sonar >> calibration. It's like we're trying to calculate the average weight >> of any given Oreo by having a dozen people measure the weight of one >> specific Oreo. Sure, you'll get a great estimate of the weight of >> Oreo-X, and sure Nabisco strives to make all Oreos equal -- but can >> that single (though repeated) measurement ~really~ be extrapolated >> to all cookies? In magnitude, I would say yes (your single set of >> patch test values are valid), but I would say the error estimates of >> the patch values will be smaller than they really are. Anyone feel >> like doing a week of patch tests to estimate the variability? >> >> SUMMARY #1: 1-degree is an inordinately large estimate of the MRU >> alignment errors. Instead, compute the Std. Dev. of the values >> found during the patch test and those should give you a good low-end >> estimate. Values in the ballpark of 0.25 for gyro and 0.15 for >> pitch/roll are reasonable estimates of a field units ability to >> accurately conduct a patch test. >> >> ITEM #2 - Tide values >> I'm curious how the field units are coping with the errors >> associated with tide measured and tide zoning. The tide measured >> component is straight-forward and can be computed directly from the >> observed data (looking at past FA projects, 0.01m is a reasonable >> median). However I feel the tidal zoing error of 0.01 to 0.40 is >> too large. HSTD 2007-2 claims we will be given values in the Letter

>> Instructions, but the reality of Alaskan survey work is there will

```
>> seldom be enough historic data for CO-OPS to commit to a zoning
>> error. Speaking with the CST, we elected to high ball the error and
>> use 0.40m when computing TPE (the thought process being, "Well ...
>> it sure is a long way to the primary tide gauge."
>>
>> I do not know the exact equations involved when it comes to the
>> assimilation of the various components of error in the TPE model,
>> but a qualitative comparison can be made by varying the zoning error
>> (ZE) and examining the changes in the Dp TPE for a subset of pings.
>> Incrementally increasing the ZE causes the vertical TPE (Dp TPE) of
>> a given ping at nadir to converge on twice the value of the ZE,
>> regardless of the initial Dp TPE. See attached picture.
>>
>> It is worth repeating: regardless of the Dp TPE of a given sounding
>> with a zero ZE, inputting a ZE of 0.40 will lead to a Dp TPE for
>> that same sounding to change to 0.80.
>>
>> Using the IHO error estimate (Sqrt[a<sup>2</sup> + bd<sup>2</sup>]), this would imply
>> all soundings collected in waters shoaler than 48m will
>> automatically be rejected as having not satisfied IHO Order 1. I
>> wish I had a cookie analogy I could insert here.
>>
>> As of now, FA is proceeding with a zoning error of 0.10, since the
>> pings still appear to retain an essence of the other uncertainties
>> associated with the pings (alignment, POS/MV, precise timing,
>> etc.). Once we begin acquiring data in earnest, we will likely
>> re-evaluate if we're again suffereing from a lack of "IHO-ness".
>>
>> SUMMARY #2 - A zoning estimate of 0.40m is harsh and will render a
>> surveying platform incapable of acquiring data in waters shoaler
>> than 48m that will satisfy IHO Order 1. FA is proceeding with a
>> value of 0.10m and is standing by for changes. Likely someone from
>> CO-OPS would be in a better position to provide such an estimate
>> vice a group of JO's with their fingers orange from eating Cheetos.
>> Thus far, CO-OPS has punted claiming lack of data - but that doesn't
>> help our error model.
>>
>> This e'mail is long and I have a sudden urge for junk food.
                                                                I will
>> close with also stating I believe sound speed error estimates
>> suggested in HSTD 2007-2 are larger than necessary; however, since
>> it does not result in greater than half of my data being deleted ...
>> I will champion that cause another day.
>>
>> Opinions? I would love to hear them (I've got a hundred screen
>> shots I'm ~dying~ to share).
>>
>> ~~ mike.g.
>>
>> foo fairweather wrote:
>>
>> > ----- Original Message ------
>> >
         Subject: MRU allignment error estimates
     Resent-Date: Wed, 11 Apr 2007 18:40:18 GMT
     Resent-From: FOO.Fairweather@noaa.gov
            Date: Wed, 11 Apr 2007 18:32:59 +0000
```

		<pre>From: FOO Rainier <foo.rainier@noaa.gov> To: hydro.geek@noaa.gov CC: ChiefST Rainier <chiefst.rainier@noaa.gov>, Jake Yoos <jake.yoos@noaa.gov>, Olivia Hauser <olivia.hauser@noaa.gov>, Samuel Greenaway <samuel.greenaway@noaa.gov>, CO Rainier <co.rainier@noaa.gov>, _NMAO MOP FOO Fairweather <foo.fairweather@noaa.gov>, _NMAO MOA FOO Thomas Jefferson <foo.thomas.jefferson@noaa.gov>, _OMAO MOA FOO Rude <foo.rude@noaa.gov>, Mark Van Waes <mark.vanwaes@noaa.gov></mark.vanwaes@noaa.gov></foo.rude@noaa.gov></foo.thomas.jefferson@noaa.gov></foo.fairweather@noaa.gov></co.rainier@noaa.gov></samuel.greenaway@noaa.gov></olivia.hauser@noaa.gov></jake.yoos@noaa.gov></chiefst.rainier@noaa.gov></foo.rainier@noaa.gov></pre>
>>	>	
>>	>	Good morning,
>>	>	T believe that the MDH alignment error estimated regenmended by
>>	>	HSTD 2007-2 are too high. The directive suggests that the MRU
>>	>	alignment fields in the TPE section of the HVF be set to a values
>>	>	with "similar magnitude to patch test values," with recommended
>>	>	default values of 1 degree for both gyro and roll/pitch alignment.
>>	>	In accordance with this guidance, RA set the gyro MRU alignment
>>	>	error estimate to 0.5 degrees, and the Roll/Pitch estimate to 1
>>	>	degree for all Reson-equipped launches prior to the beginning of
>>	>	data acquisition. We immediately found that $\sim 2/3$ of our swath
>>	>	width was rejected by the IHO Order I TPE filter.
~~	Ś	I've attached an Excel worksheet showing examples of this effect
>>	>	for a Reson 8101 operating in 15-20m of water. The left-hand plot
>>	>	shows a representative example of TPE values as a function of beam
>>	>	number with MRU alignment errors set to 0.5 and 1.0 degree as
>>	>	described above. The right-hand plot shows a similar sample (not
>>	>	the exactly the same soundings, but the same line and depth regime) $% \left( {{{\left( {{{\left( {{{\left( {{{c}}} \right)}} \right.} \right)}}}} \right)$
>>	>	with the MRU alignment error estimates values set to 0 (which is
>>	>	what we previously used).
>>	>	
>>	>	ODVIOUSLY, zero error for alignment measurement is unrealistic;
~~	$\langle$	depth measurement error estimation. It seems that the HSTD was
>>	Ś	written with the understanding that the MRU alignment error
>>	>	estimate should be an estimate of the alignment error itself, not
>>	>	an estimate of the error in the measurement of that alignment. I
>>	>	believe this interpretation is incorrect. The alignment error
>>	>	estimate is already taken care of by the patch test bias values in
>>	>	the Swath entry. High bias values, if carefully measured, are not
>>	>	necessarily incorrect. Thus, entering the alignment errors as
>>	>	alignment measurement errors can result in incorrect TPE
>>	>	estimation, as in the example attached.
>>	>	Ttla containly difficult to actimate the mulitur of a match toot
>>	~	but it seems to me that a more accurate estimate would be to use
>>	Ś	the standard deviation of the values computed by the various
>>	>	personnel computing the test. This would decouple alignment
>>	>	measurement precision from the alignment accuracy itself, and
>>	>	assign each to its correct place in the data reduction and error
>>	>	estimation process. On RAINIER, we have ~6 people looking at each
>>	>	vessel's patch test, so that gives us a reasonable sample size.
>>	>	Preliminary results of our patch testing indicate that this will
>>	>	produce much smaller (though non-zero) alignment measurement error

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>> > estimates. At this point, I plan to use these values instead of
>> > those recommended in HSTD 2007-2; we will, of course, document
>> > this in the reports of those patch tests included with the affected
>> > DAPRs. However, I wanted to make others aware this potential
>> > problem- it took us a while to figure out why our swath width had
>> > mysteriously shrunk. I also recommend that HSD consider re-wording
>> > the HSTD to suggest this approach to the estimation of this value.
>> >
>> > Thanks,
>> >
>> > Ben
>> >
>> >
>> > --
>> > LT Ben Evans, NOAA
>> > Field Operations Officer
>> > NOAA Ship RAINIER (s221)
>> > NOAA Marine Operations Center, Pacific
>> > 1801 Fairview Ave. E
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>> > LT Jennifer Dowling, NOAA
>> > Field Operations Officer
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>> > Ketchikan, Alaska 99901
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>> > 907 255-1807 or 1809 Ketchikan phone
>> > 907 255-1808 Ketchikan fax
>> >
>> > 808 659 0054 at sea phone
>> >
>> > foo.fairweather@noaa.gov
>> > at sea email size limit: 200k
>> >
>>
      _____
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                              [Image]
>>
> --
>
> ------
> LCDR Richard Brennan, NOAA
  Chief, Hydrographic Systems and Technology Program
>
> 1315 East-West Highway, SSMC3
> N/CS11, Station 7853
> Silver Spring, MD, 20910
> Work: 301-713-2653 x152
> Cell: 443-994-3301
>
```

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Thank you for the info Rick, it was ~exactly~ what I was looking for..

While it is a shame to watch our data collapse in the face of IHO Order 1, it might just be the sad truth of Alaskan surveying: given the tidal uncertainties, a definitive depth cannot be ascertained without an appreciable error envelope.

I wish we could re-create your 14m IHO error in the field. As I mentioned earlier, we were unable to survey past 48m and maintain IHO Order 1. We'd used the exact error values suggested for the POS M/V and time latency suggested in HSTD-2; Our offset erors are on the order of 7 mm; Loading and Draft 3 and 4cm respectively; we low-balled the SV at 1 m/s and left the Delta Draft, and MRU align errors as zero (since we had yet to compute the patch test). This configuration blanked our swath in waters shoaler than 48m when filtered against IHO - but then, as you suggested, perhaps it is unrealistic to be expected to survey to IHO order 1 under these conditions. If that's the case, I feel like there should have been a disclaimer presented to everyone during the west coast hydro training, "Hey gang, while we strive to satisty IHO, the reality is you won't be able to get there while surveying in the shallow waters. How shallow? Well, anything shoaler than the Statue of Liberty is tall (46.84m - base to torch)."

The picture will not improve when the delta draft and MRU errors are added to the model.

I have attached a copy of our TPE spread sheet. Do any of the values appear inordinately high to you that keeps us from reaching your 14m glass ceiling (or would it be a glass floor)?

Is RAINIER having better luck than we?

Thank you for your time, all.

Regards,

~~ mike.g.

Richard T Brennan wrote:

#### Hi Mike,

Not sure if you saw my response to Ben, but I agree, the MRU alignment error is too big. My recommendation was that the guidance should say "The MRU alignment error should be approximately the smallest unit of change in the HIPS calibration window which produces no noticeable change in the point cloud alignment." I think this would yield a similar result to the method you are employing and not require a field party to have six people, or have six people look at their patch test.

As for the zoning error, this value wraps up a lot of sins in one place and thus I would not suggest altering this without consulting CO-OPS. The goal of populating the error model with the various system uncertainties is not to tweak them until they are "within spec", it is to give us an honest assessment of how good our measurements are. The zoning model does not account for changes in the shape of the tide curve across the survey area (i.e. diurnal to semi-diurnal, or semi-diurnal to mixed, etc...), differences between the rate an area floods and ebbs, uncertainties in the datum, and inaccuracies induced by the interpolation method itself. While CO-OPS may not be able to supply a definitive zoning error value for your survey area, they do use some judgment based on experience, and experience has shown that 0.4 is not an unrealistic value, particularly in Alaska. While 0.4m for zoning error is not unheard of, it is larger than normal, so I would confirm with CO-OPS that this is indeed the correct value. While your data may appear to be internally consistent (no stereotypical tide artifacts), errors induced by uncertainties in the datum would not cause a visual artifact. That said my computations show that you should be able to survey up to 14 m of water and still maintain IHO Order 1 with a 0.4m combine tidal uncertainty (that is the rms of measurement uncertainty and zoning uncertainty). I have attached a spreadsheet with my numbers in it. Let me know if you have any questions regarding these values. Hope this helps...

Rick

michael gonsalves wrote:

\*\* This e'mail is longer than the attention span of the average JO and ST - thus I present the summary at the beginning: An MRU align error of 1.0 is too large; something on the order of 0.20 is a better estimate (want to know why ... then read on); A tidal zoning of 0.40 is also too large, it makes it impossible to acquire IHO Order 1 data in waters shoaler than ~45m), I propose 0.10 as a better upper bound until CO-OPS commits to something better. ...and now for the message -- mog \*\*

Wait, we can haggle over HSTD 2007-2?

#### ITEM #1 - MRU Alignment

FAIRWEATHER had identical problems to those described by LT Evans at the end of the previous field season. An incorrect calculation led to MRU alignment errors  $\sim 0.5$  degrees which led to 2/3 or our swath being rejected as not satisfying IHO Order 1.

I believe the spirit of the error is to report your reliability in the operator's ability to perform a successful patch test. RAINIER has struck upon the proper approach having several people independently perform the patch test. At that point, the Standard Deviation of the patch test values can be used as a valid approximation of the MRU alignment errors. This is the technique suggested by Dr. Calder to FA around this time last year. The only caveat I would suggest is that the multiple evaluations of the patch test data must be performed in tandem; that is, all processors must agree on a value in the timing error before the group proceeds to calibrating for pitch (and so on). Such a simultaneous approach is necessary due to the confounding of the various alignment errors (i.e. a pitch-induced artifact can be removed by adjusting timing).

By the end of the field season, FA had settled on MRU align values of 0.25 for gyro and 0.15 for roll/pitch. In my opinion, these values may still be on the conservative side. But, with these values inserted into the hvf, filtering the data against IHO Order 1 resulted in all the wacky outbeams being rejected while the smooth continuous bottom was preserved. Any parameters that leads to "poor" data being rejected while retaining the "good" is a step in the right direction. The redundancy in having multiple eyes view a patch test can only be taken so far however. Sea state, speed of the vessel, validity of sound velocity profile, whether that pitch line was run ~exactly~ on top of the sonarconspicious target will dictate how valid a given set of patch lines are for accurately determining the sonar calibration. It's like we're trying to calculate the average weight of any given Oreo by having a dozen people measure the weight of one specific Oreo. Sure, you'll get a great estimate of the weight of Oreo-X, and sure Nabisco strives to make all Oreos equal -- but can that single (though repeated) measurement ~really~ be extrapolated to all cookies? In magnitude, I would say yes (your single set of patch test values are valid), but I would say the error estimates of the patch values will be smaller than they really are. Anyone feel like doing a week of patch tests to estimate the variability?

SUMMARY #1: 1-degree is an inordinately large estimate of the MRU alignment errors. Instead, compute the Std. Dev. of the values found during the patch test and those should give you a good low-end estimate. Values in the ballpark of 0.25 for gyro and 0.15 for pitch/roll are reasonable estimates of a field units ability to accurately conduct a patch test.

#### ITEM #2 - Tide values

I'm curious how the field units are coping with the errors associated with tide measured and tide zoning. The tide measured component is straight-forward and can be computed directly from the observed data (looking at past FA projects, 0.01m is a reasonable median). However I feel the tidal zoing error of 0.01 to 0.40 is too large. HSTD 2007-2 claims we will be given values in the Letter Instructions, but the reality of Alaskan survey work is there will seldom be enough historic data for CO-OPS to commit to a zoning error. Speaking with the CST, we elected to high ball the error and use 0.40m when computing TPE (the thought process being, "Well ... it sure is a long way to the primary tide gauge."

I do not know the exact equations involved when it comes to the assimilation of the various components of error in the TPE model, but a qualitative comparison can be made by varying the zoning error (ZE) and examining the changes in the Dp TPE for a subset of pings. Incrementally increasing the ZE causes the vertical TPE (Dp TPE) of a given ping at nadir to converge on twice the value of the ZE, regardless of the initial Dp TPE. See attached picture.

It is worth repeating: regardless of the Dp TPE of a given sounding with a zero ZE, inputting a ZE of 0.40 will lead to a Dp TPE for that same sounding to change to 0.80.

Using the IHO error estimate (Sqrt[a<sup>2</sup> + bd<sup>2</sup>]), this would imply all soundings collected in waters shoaler than 48m will automatically be rejected as having not satisfied IHO Order 1. I wish I had a cookie analogy I could insert here.

As of now, FA is proceeding with a zoning error of 0.10, since the pings still appear to retain an essence of the other uncertainties associated with the pings (alignment, POS/MV, precise timing, etc.). Once we begin acquiring data in earnest, we will likely re-evaluate if we're again suffereing from a lack of "IHO-ness".

SUMMARY #2 - A zoning estimate of 0.40m is harsh and will render a surveying platform incapable of acquiring data in waters shoaler than 48m that will satisfy IHO Order 1. FA is proceeding with a value of 0.10m and is standing by for changes. Likely someone from CO-OPS would be in a better position to

provide such an estimate vice a group of JO's with their fingers orange from eating Cheetos. Thus far, CO-OPS has punted claiming lack of data - but that doesn't help our error model.

This e'mail is long and I have a sudden urge for junk food. I will close with also stating I believe sound speed error estimates suggested in HSTD 2007-2 are larger than necessary; however, since it does not result in greater than half of my data being deleted ... I will champion that cause another day.

Opinions? I would love to hear them (I've got a hundred screen shots I'm ~dying~ to share).

~~ mike.g.

foo fairweather wrote:

----- Original Message ------

Subject: MRU allignment error estimates
Resent-Date: Wed, 11 Apr 2007 18:40:18 GMT
Resent-From: FOO.Fairweather@noaa.gov
Date: Wed, 11 Apr 2007 18:32:59 +0000
From: FOO Rainier <foo.rainier@noaa.gov>
To: hydro.geek@noaa.gov
CC: ChiefST Rainier <chiefst.rainier@noaa.gov>, Jake Yoos <Jake.Yoos@noaa.gov>,
Olivia Hauser <olivia.hauser@noaa.gov>, Samuel Greenaway
<samuel.greenaway@noaa.gov>, CO Rainier <co.rainier@noaa.gov>, \_NMAO MOP FOO
Fairweather <FOO.Fairweather@noaa.gov>, \_NMAO MOA FOO Thomas Jefferson
<FOO.Thomas.Jefferson@noaa.gov>, \_OMAO MOA FOO Rude <FOO.Rude@noaa.gov>, Mark
Van Waes <Mark.Vanwaes@noaa.gov>

Good morning,

I believe that the MRU alignment error estimates recommended by HSTD 2007-2 are too high. The directive suggests that the MRU alignment fields in the TPE section of the HVF be set to a values with "similar magnitude to patch test values," with recommended default values of 1 degree for both gyro and roll/pitch alignment. In accordance with this guidance, RA set the gyro MRU alignment error estimate to 0.5 degrees, and the Roll/Pitch estimate to 1 degree for all Reson-equipped launches prior to the beginning of data acquisition. We immediately found that ~2/3 of our swath width was rejected by the IHO Order 1 TPE filter.

I've attached an Excel worksheet showing examples of this effect for a Reson 8101 operating in 15-20m of water. The left-hand plot shows a representative example of TPE values as a function of beam number with MRU alignment errors set to 0.5 and 1.0 degree as described above. The right-hand plot shows a similar sample (not the exactly the same soundings, but the same line and depth regime) with the MRU alignment error estimates values set to 0 (which is what we previously used).

Obviously, zero error for alignment measurement is unrealistic; however, the recommended values appear to result in absurdly high depth measurement error estimation. It seems that the HSTD was written with the understanding that the MRU alignment error estimate should be an estimate of the alignment error itself, not an estimate of the error in the measurement of that alignment. I

believe this interpretation is incorrect. The alignment error estimate is already taken care of by the patch test bias values in the Swath entry. High bias values, if carefully measured, are not necessarily incorrect. Thus, entering the alignment errors as alignment measurement errors can result in incorrect TPE estimation, as in the example attached.

It's certainly difficult to estimate the quality of a patch test, but it seems to me that a more accurate estimate would be to use the standard deviation of the values computed by the various personnel computing the test. This would decouple alignment measurement precision from the alignment accuracy itself, and assign each to its correct place in the data reduction and error estimation process. On RAINIER, we have ~6 people looking at each vessel's patch test, so that gives us a reasonable sample size. Preliminary results of our patch testing indicate that this will produce much smaller (though non-zero) alignment measurement error estimates. At this point, I plan to use these values instead of those recommended in HSTD 2007-2; we will, of course, document this in the reports of those patch tests included with the affected DAPRs. However, I wanted to make others aware this potential problem- it took us a while to figure out why our swath width had mysteriously shrunk. I also recommend that HSD consider re-wording the HSTD to suggest this approach to the estimation of this value.

Thanks,

Ben

--LT Ben Evans, NOAA Field Operations Officer NOAA Ship RAINIER (s221) NOAA Marine Operations Center, Pacific 1801 Fairview Ave. E Seattle, WA 98102

--

LT Jennifer Dowling, NOAA Field Operations Officer NOAAS FAIRWEATHER 1010 Stedman Street Ketchikan, Alaska 99901

907 255-1807 or 1809 Ketchikan phone 907 255-1808 Ketchikan fax

808 659 0054 at sea phone

foo.fairweather@noaa.gov
at sea email size limit: 200k

## Diver Least Depth Gauge DQA 2006

OPR-P158-FA-06 Approaches to Cordova, Alaska

Date	UTC Time	DLDG reading	Sea Level Pressure	Gauge ID	Results
08-31-2006	20:44:14	14.39	993	68332	Good
09-01-2006	21:46:49	14.51	1007	68332	Good
09-05-2006	19:14:18	14.67	1020	68332	Good

\*\*Gauge 68322 stopped working after the 5 September reading and no new DLDG were obtained prior to the end of the field season\*\*

## Appendix VII

Correspondence

Shoreline Guidance

Tides – Gravina River

**Courtesy Letters** 

System Check Correspondence

Launch 1018 IMU Tumble Test