

Cover Sheet (NOAA Form 76-35A)

NOAA FORM 76-35A
NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION NATIONAL OCEAN SERVICE
Data Acquisition and Processing Report
Field No OPR-0322-KR-07
Registry No. H11696, H11697, H11698, H11699, H11700
H11701. H11702. H11703. H11704. H11705. H11706.
H11707. & H11708
LOCALITY
State ALASKA
General Locality CHATHAM STRAIT
Sublocality NE OF ERESHWATER BAY TO MURDER COVE
2007
2001
CHIEF OF PARTY
DEAN MOYLES
LIBRARY & ARCHIVES
DATE

U.S. GOV. PRINTING OFFICE: 1985-566-054



## Title Sheet (NOAA Form 77-28)

NOA A FORM 77-28	U.S. DEPARTMEN	T OF COMMERCE	DECISTED NO		
(11-72) NA	TIONAL OCEANIC AND ATMOSPHERIC A	ADMINISTRATION	H11696, H11697, H11698, H11699, H11700, H11701, H11702, H11703, H11704, H11705, H11706, H11707		
			& H11708		
HYDROGRAPHIC TI	TLE SHEET				
<b>INSTRUCTIONS</b> – The Hydrog completely as possible, when the	raphic Sheet should be accompanied by t sheet is forwarded to the Office	his form, filled in as	FIELD NO.		
State <u>Alaska</u>					
General Locality Chatham	n Strait				
Locality Freshwater Bay to	Murder Cove				
Scale 1.10000 & 1.20000		Data of Survey 05	05/07 06/10/07 & 08/02/07 00/15/07		
Scale <u>1.10000 &amp; 1.20000</u>		Date of Survey <u>05</u>	$105/07 = 00/10/07 \approx 08/02/07 = 09/15/07$		
Instructions dated June 15	, 2006	Project No. OPR-C	0322-KR-07		
Vessel <u>R/V Davidson (10</u>	66485), R/V R2 (623241), R/V D2	(647782), Shoreli	ne Skiff (WN6739NW)		
Chief of party DEAN MO	YLES				
Surveyed by <u>ORTHMANN</u>	I, REYNOLDS, GILL, MOUNT, ST	OCK, FARLEY, B	RIGGS, POECKERT, ET AL		
Soundings taken by echo so <u>HULL MOUNT</u> ) and RES	ounder, hand lead, pole <u>RESON 8101</u> ON 8125 (SKIFF - POLE MOUNT)	l (R2 & D2 - HULI	<u>, MOUNT), RESON 8111 (DAVIDSON -</u>		
Graphic record scaled by <u>F</u>	UGRO PELAGOS, INC. PERSON	NEL			
Graphic record checked by	FUGRO PELAGOS, INC. PERSON	NNEL			
Protracted by N/A Automated plot by N/A					
Verification by		in the second			
Soundings in	METERS at MLLW				
<u>REMARKS</u> : The purpose Southeastern Alaskan Penin	of this work is to provide NOAA wit nsula that extends from Freshwater B	h modern and accur ay to Murder Cove	rate hydrographic survey data for the areas in		
ALL TIMES ARE RECORDED IN UTC.					
Fugro Pelagos, Inc.	John Oswald & Associates LL	.C Stabber	t Maritime		
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NUAA FURINI 11-20 SUPERSI		J.S. GOVERNIVIEN	FRIMING OFFICE. 1900 - 032-007/41215		



## A – Equipment

The R/Vs Davidson, R2, D2, and Shoreline Skiff acquired all of the sounding data during the course of this survey. The R/V Davidson collected multibeam data and sound velocity profiles in medium to deep water depths, the R/Vs R2 & D2 collected multibeam data and sound velocity profiles in shallow to medium water depths, and the Shoreline Skiff collected multibeam data and sound velocity profiles in shallow to redium water depths. The equipment list and vessel descriptions are included in Appendices I and II.

## SOUNDING EQUIPMENT

The R/V Davidson was equipped with a hull mounted Reason 8111 multibeam system during the OPR-O322-KR-07 project. The Reson 8111 system operates at a frequency of 100 kHz, with 101 horizontal beams centered 1.5° apart (150° across-track beam width) and 1.5° along-track beam width. It transmits and receives a sonar signal to measure the relative water depth over the 150° swath. The range scale, gain, power level, ping rate, etc., were a function of water depth and data quality. Any changes to these parameters were noted on the survey line logs (see Separate 1).

The line orientation for the Davidson was generally parallel to the coastline and bathymetric contours in the area. The line spacing was dependent on the water depth and data quality, but never exceeded three times the water depth.

The R/V R2 was equipped with a hull mounted Reson SeaBat 8101 multibeam system during the OPR-O322-KR-07 project. The Reson 8101 system operates at a frequency of 240 kHz, with 101 horizontal beams centered 1.5° apart (150° across-track beam width) and 1.5° along-track beam width. It transmits and receives a sonar signal to measure the relative water depth over the 150° swath. The range scale, gain, power level, ping rate, etc., were a function of water depth and data quality. Any changes to these parameters were noted on the survey line logs (see Separate 1).

The line orientation for R2 was generally parallel to the bathymetric contours in the area. The line spacing depended on the water depth and data quality, but never exceeded three times the water depth.

The R/V D2 was equipped with a hull mounted Reson SeaBat 8101 multibeam system during the OPR-O322-KR-07 project. The Reson 8101 system operates at a frequency of 240 kHz, with 101 horizontal beams centered 1.5° apart (150° across-track beam width) and 1.5° along-track beam width. It transmits and receives a sonar signal to measure the relative water depth over the 150° swath. The range scale, gain, power level, ping rate, etc., were a function of water depth and data quality. Any changes to these parameters were noted on the survey line logs (see Separate 1).



The line orientation for D2 was generally parallel to the bathymetric contours in the area. The line spacing depended on the water depth and data quality, but never exceeded three times the water depth.

The Shoreline Skiff was equipped with a pole mounted Reson 8125 multibeam system (rotated 30 Degrees) during the OPR-O322-KR-07 project. The Reson 8125 system operates at a frequency of 455 kHz, with 240 horizontal beams centered 0.5° apart (120° across-track beam width) and 1.5° along-track beam width. It transmits and receives a sonar signal to measure the relative water depth over the 120° swath. The range scale, gain, power level, ping rate, etc., were a function of water depth and data quality. Any changes to these parameters were noted on the survey line logs (see Separate 1).

The line orientation for the Shoreline Skiff was generally parallel to the shoreline. The line spacing depended on the water depth and data quality.

The Shoreline Skiff was also used to perform shoreline verification. The Shoreline Skiff was equipped with a CSI GBX-PRO DGPS receiver, WinFrog (v3.7.0) data acquisition system, Laser range finder binoculars (with built-in compass), and a Sony digital camera. NOAA nautical charts, Remote Sensing Division (RSD) features, and multibeam coverages were displayed as layers in WinFrog for reference. All soundings on submerged features were collected by one of the multibeam systems.

Heights were taken on features awash or above the water level by visual estimation, using simultaneous comparison to a known reference (the vessel's bow).

## SIDE SCAN SONAR

Towed Side Scan Sonar (SSS) operations were not required by this contract. Backscatter data collected by the Reson 8111, 8101, and 8125 multibeam systems were logged, but used only to facilitate data cleaning.

## POSITIONING EQUIPMENT

Each vessel was equipped with an Applanix Position and Orientation System for Marine Vessels (POS/MV) to measure and calculate each position. Position was determined in real time using a Trimble Zephyr L1/L2 GPS antenna, which was connected to a Trimble BD950 L1/L2 GPS card residing in the POS/MV. The POS/MV was configured to accept differential corrections, which were output from a CSI MBX-3S Coast Guard beacon receiver. This unit also provided the position and velocity values to the POS/MV's Inertial Measurement Unit (IMU). The inertial navigation system implemented by the POS/MV computes a position by way of complex dead reckoning using GPS position, heading, and motion of the IMU.

An MBX-S differential receiver that used the U.S. Coast Guard (USCG) network of differential beacons was the main source of RTCM (Radio Technical Commission for



Maritime Services). It was also necessary to acquire dual frequency GPS data at known locations on the ground so that a Post-Processed Kinematic (PPK) solution could be used for final positioning. Sub-contractor John Oswald & Associates LLC (JOA) established two local control points: stations "Angoon A" and "Angoon B" located on the Inner Passage Electric Cooperative (IPEC) fuel shed in Angoon, AK. Refer to Appendix II of the OPR-O322-KR-07 "Horizontal and Vertical Control Report" for procedures and results.

The numerous real time displays of the POS/MV controller software were monitored throughout the survey to ensure that the positional accuracies specified in the NOS Hydrographic Survey Specifications and Deliverables (April 2007) were achieved. These include, but are not limited to the following: GPS Status, Position Accuracy, Receiver Status (which included HDOP), and Satellite Status. During periods of high HDOP and/or low number of available satellites, survey operations were suspended.

## SOFTWARE

## **Acquisition**

The primary data sets were collected with Isis Sonar (v 7.1428.53) from Triton Imagining, Inc. Isis Sonar operated on an Athlon 2800 Dual Processor PC running Windows XP Pro and logged data in the XTF file format. The XTF files contain all multibeam bathymetry, position, attitude, heading, and UTC time stamp data required by CARIS to process the soundings. Delph Map was utilized on the same computer to assist with real time QC of the acquired data.

The following display windows are available in Isis & Delph Map for operators to monitor data quality:

- 1. Parameter Display: The display window shows navigation, attitude, and heading information. It gives the user the ability to switch files during data acquisition and also displays important information on ping count and file size.
- 2. View 2-D and 3-D: The 2-D window displays the current multibeam profile. The 3-D window displays a 3-D mesh of the current line of profiles. The data in both windows have attitude data applied for quality control purposes.
- 3. Waterfall: The Waterfall displays backscatter data.
- 4. Graph Window: The user can display the sensor data in a graphical format, which aids in determining heave filter settings for the POS M/V.
- 5. Delph Map: Delph Map displays binned soundings in plan view or 3-D. The bin size is user defined and can be filtered by beam number and sounding quality.



The Davidson, R2, D2, and Shoreline Skiff were all equipped with an additional computer running WinFrog (v3.7.0).

WinFrog offers the following display windows for operators to monitor data quality:

- 1. Devices: The Devices window shows the operator which hardware is attached to the PC. It also allows the operator to configure the devices, determine whether they are functioning properly, and to view received data.
- 2. Graphic: The Graphic window shows navigation information in plan view. This includes vessel position, survey lines, background vector plots, and raster charts.
- 3. Vehicle: The Vehicle window can be configured to show any tabular navigation information required. Typically, this window displays position, time, line name, heading, HDOP, speed over ground, distance to start of line, distance to end of line, and distance off line. Many other data items are selectable.
- 4. Calculation: The Calculation window is used to look at specific data items in tabular or graphical format. Operators look here to view the status of the GPS satellite constellation and position solutions.

In addition to monitoring position, attitude, and heading accuracies, the Applanix POS/MV controller software was used to log raw POS/MV data—the standard POSPac logging groups, along with groups 3 (Primary GPS Data), and 102 (Sensor 1 Data). These data were collected via the Ethernet to the WinFrog computer at an update rate of 50 Hz and later post-processed and applied in CARIS HIPS.

MBSurvey Tools was used to aid in file administration and reporting during data acquisition. This program created a daily file that contained survey line, SVP, and static draft logs. These files were stored digitally, thus eliminating the constant printing and manual input of items such as line start and end times, Reson settings, etc., on each log sheet.

## Processing

All Soundings were processed using CARIS (Computer Aided Resource Information System) HIPS (Hydrographic Information Processing System) (v6.1).

AutoDesk Map R 5.0 and ESRI ArcMap (v9.2) were utilized for general survey planning, reviewing coverage plots, creating fill-in lines, tielines, etc.

ESRI ArcMap (v9.2) with the Shoreline Correlator add-on was utilized for processing the additional item investigations, such as Detached Positions (DPs).

Applanix POSPac (v4.3) was utilized for post-processing the dual frequency GPS data sets acquired by the survey vessels and the base stations. For every survey day and vessel, a new project was set up in POSPac. The software then extracted the POS data collected on the



survey vessel into the POSPac project; separating it into component data sets such as (IMU), primary GPS, and secondary GPS.

Using POSGPS—part of the POSPac suite—dual frequency GPS data from the vessels and ground control base stations were converted from their native format (Trimble), to the POS GPS .gpb format. The PPK data sets were then post-processed using the John Oswald & Associates LLC (JOA) antenna phase center positions given in Appendix II of the Horizontal and Vertical Control Report.

The POSPac module POSProc then used the post-processed PPK positions to post-process the POSMV attitude data and refine the inertial solution. The final solution was exported to an sbet.out file, which was then used by an in-house converter program that extracted the PPK positions to be used in the CARIS Generic Data Parser (GDP) program.

MBSurvey Tools was used to extract True Heave data from the raw POS data collected on the survey vessels. This text file was parsed to a format acceptable by the CARIS Generic Data Parser using MBSurvey Tools. This was utilized only on days when the GPS rollover week became problematic. Otherwise the True Heave was applied via CARIS HIPS & SIPS (v6.1).

A complete summary of the GPS post processing accuracy estimates can be found in Appendix III of the Horizontal and Vertical Control Report.

## Sound Velocity Profiles

Sound velocity profile (SVP) data from the Applied Microsystems Ltd. (AML) Smart Probes were acquired using Windows' Hyper Terminal. MBSurvey Tools was used to split the profile into up and down components, decimate the data, and write a CARIS format that contained time and position. A complete list of software and versions used on this project is included in Appendix I. Refer to the "2007-NOAAProcessing Procedures" document for a detailed processing routine with procedures used.

## **B**-Quality Control

With the implementation of the Combined Uncertainty and Bathymetry Estimator (CUBE) in CARIS, a different approach is taken in the analysis of data sets. In the HIPS vessel configuration file (HVF) we now input or create an error model of our survey sensors that is used to calculate the Total Propagated Error (at the 95% Confidence Interval for the horizontal and vertical components) for each individual sounding collected during data acquisition. The values that were input into the CARIS HVF for the survey sensors are the specified manufacturer accuracy values and can be downloaded from the CARIS website @ <a href="http://www.caris.com/tpe/">http://www.caris.com/tpe/</a>. The following is a breakdown on the manufacturer and Fugro Pelagos derived values used in the error model (which are entered into the CARIS HVF and Fugro\_CUBEParams.xml files):



• Navigation – In the CARIS HVF a value of 0.25m was entered for the Positional accuracy. Vessels were equipped with an Applanix POS MV 320 and all raw positions were post-processed and the PPK solution was parsed back into the data set. The accuracies yielded from the PPK routine were usually less than ten centimeters.

• Gyro/Heading – As mentioned above, the vessels were equipped with a POS MV 320 and had a baseline of about 3m, so therefore a value of 0.020 degrees was entered in the HVF.

• Heave – The heave percentage of amplitude was set to 5%, and the Heave was set to 0.05m, as per the manufacturer accuracy values.

• Pitch and Roll - As per the manufacturer accuracy values, both were set to 0.020 degrees.

• Precise Timing – All data were time stamped when created, not when logged, using a single clock/epoch. Position, attitude, (including True Heave) and heading, are all time stamped in the POS MV on the UTC epoch. This UTC string was also sent to the Reson processors and ISIS software via a serial string, yielding timing accuracies better than one millisecond.

• All vessel and sensor offsets were derived via conventional surveying techniques while the vessels were in dry dock. The results yielded a standard deviation of 0.025m.

- Tide values and Zoning were both set to 0.05m during TPE computing.
- Sound Speed Values were set to 1 m/s and 2.5 m/s for the Surface.
- IMU Align StdDev for the Gyro and Roll/Pitch were set to zero.

The calculated horizontal and vertical uncertainty or Total Propagated Error (TPE) values were then used to:

- filter the data to IHO Order 1 specifications
- create a CUBE surface used during subset cleaning stages
- create the final combined Bathymetric with Associated Statistical Error (BASE) surfaces.

The discussion that follows is an overview of our processing flow:

In order for the XTF files collected by ISIS to be used in CARIS, they must be converted to HDCS format using an XTF converter routine. Prior to the XTF files being converted using the XTF to HDCS function, vessel offsets, patch test calibration values, TPE values, and static draft were entered into the vessel configuration file.

Once converted, the SVP, Dynamic Draft, True Heave, and PPK data were loaded into each line and then SVP corrected in CARIS HIPS. Once SVP corrected, the TPE was computed for each sounding in CARIS HIPS. The attitude, navigation, and bathymetry data for individual lines were examined for noise, as well as to ensure the completeness and correctness of the data set. Filter setting files used during processing of the Reson 8111 and 8101 lines were: TPE-60-012.hft and TPE-65-012.hft, which rejected beams outside IHO Order 1, beams greater than 60 and 65 degrees past nadir, and all soundings with a quality flag other than 3 (a quality flag is assigned to each sounding by the multibeam system). The filter setting file used during processing of the Reson 8125 lines was 012.hft, which rejected



beams with a quality flag other than 3. Data quality determined which filter setting file was applied. Note: "Rejected" does not mean the sounding data point was deleted, but that it was flagged as being bad. Data flagged as rejected due to the angle from nadir parameters, did contain valid data, but the routine was conducted to flag noise and speed the processing flow. Valid data could have been reinserted into the data set during the line and subset editing phase to fill data gaps. The filter settings used were noted on each corresponding line log (refer to Separate 1).

In high noise areas additional filters may have been applied to specific sections or entire lines. In these instances, the additional filters were noted on the line logs (refer to Separate 1).

After each individual line was examined and cleaned in CARIS HIPS the tide zone file was loaded and the lines merged. Combined Uncertainty and Bathymetry Estimator (CUBE) surfaces were then created at varying resolutions depending on the depth range. For example:

- Depth Threshold: 0 to 20 meters, resolution = 1m
- Depth Threshold: 10 to 60 meters, resolution = 2m
- Depth Threshold: 40 to 70 meters, resolution = 4m
- Depth Threshold: 50 to 150 meters, resolution = 5m
- Depth Threshold: 130 to 500 meters, resolution = 10m
- Depth Threshold: 400 to Max depth, resolution = 15m

Subsets Tiles were then created in CARIS HIPS and adjacent lines of data were examined to identify tidal busts, sound velocity and roll errors, as well as to reject any remaining noise in the data set that adversely affected the CUBE surface.

While examining the data in subset mode, soundings were designated wherever the CUBE surface did not adequately depict the shoalest point of a feature. Soundings were designated when they met or exceeded the criteria for designation set forth in the NOS Hydrographic Survey Specifications and Deliverables (April 2007). Designation ensured that soundings were carried through to the finalized BASE surfaces.

A statistical analysis of the sounding data was conducted via the CARIS Quality Control Report (QCR) routine. Cross lines were run in each sheet and were compared with main-scheme lines wherever applicable. The Quality Control Reports are located in Separate 4.

Sounding data that passed the required quality assurance checks were used in the final BASE surfaces via CARIS HIPS. Due to the high volume of data, some of the near shore sheets were sub-divided into smaller overlapping FieldSheets. For each of these FieldSheets a series of BASE surfaces were created. On each BASE surface, CUBE surfaces were generated at different resolutions (1m, 2m, 5m, 10m & 15m). These surfaces were then finalized in CARIS with the specified parameters outlined in Sections 5.1.1.3 and 5.1.4.4 of the NOS Hydrographic Survey Specifications and Deliverables (April 2007) to produce the final surfaces.



To ensure sufficient overlap between these surfaces the follow parameters were used:

- Depth Threshold: 0 to 15 meters, resolution = 1m
- Depth Threshold: 10 to 45 meters, resolution = 2m
- Depth Threshold: 40 to 60 meters, resolution = 4m
- Depth Threshold: 50 to 150 meters, resolution = 5m
- Depth Threshold: 130 to 500 meters, resolution = 10m
- Depth Threshold: 400 to Max depth, resolution = 15m

Note: It should be noted that these resolutions may vary on a sheet by sheet basis due to extreme slopes, but variations are documented in the Descriptive Reports.

For the final product a single FieldSheet that covered the entire sheet was created and the finalized surfaces for each resolution were combined. Refer to Fugro Pelagos Inc. Document titled "2007-NOAAProcessingProcedures".

Features that were awash or above the waterline were tide corrected using verified zones and tides in Fugro Pelagos' Shoreline Correlator utility, imported into CARIS Notebook, edited where necessary, and exported as S57 Feature Files.

The Shoreline Skiff was used to perform shoreline verification and could generally safely navigate in any area where it could maintain 1-2 meters of keel clearance. Exceptions were made for areas with heavy swells near shore. The Shoreline Skiff was equipped with a CSI GBX-PRO DGPS receiver, WinFrog (v3.7.0) data acquisition system, Laser range finder binoculars (with built-in compass), and a Sony digital camera. NOAA nautical charts, Remote Sensing Division (RSD) features, and multibeam/LiDAR coverages were displayed as layers in WinFrog for reference. All soundings on submerged features were collected by one of the multibeam systems. Detached Positions (DPs) and their corresponding hydrographer's remarks were digitally recorded in WinFrog and digital photographs were taken of features when feasible.

ArcMap (v9.2), with the Shoreline Correlator add-on, written by the Fugro Pelagos Inc. GIS department, aided in the processing of the investigation results. The Correlator utilized the WinFrog log files to create an individual DP form for all acquired DPs. The Correlator was mapped to the WinFrog log file, tide file, corresponding photo, NOAA Chart (largest scale available) and multibeam coverage file to calculate and display the desired information for each DP. Figure 1 shows an example of a DP form produced from the Correlator.





**Figure 1 - DP Correlator Sheet** 

Correlator also utilized the final tide zones and verified tidal data to tide-correct all DP features. The tide-corrected feature information was exported to text file and then imported as a marker layer in to CARIS Notebook.

In Notebook, the marker layer was reviewed in context of all available data, including multibeam coverages, raster / ENC charts, RSD source shoreline, and LIDAR photo-mosaics (when available). New features and features that differed from the chart(s) or RSD source were assigned appropriate S57 object acronyms and attributes and saved in the feature file.

Features above MLLW found by multibeam instead of DP were also reviewed in CARIS HIPS and their multibeam depth and position used to place the feature in the feature file.

Changes to a sheet's source (RSD) Data were noted in the Descriptive Report for that sheet, as well as significant deviations or disapprovals of previously charted features. When complete, an S57 Feature File was exported.



## **C** - Corrections to Soundings

#### SOUND VELOCITY PROFILES

Sound velocity casts were normally performed every two to three hours. The AML Smart Probes used to determine sound velocities for the survey sampled at a rate of eight velocity and pressure observation pairs a second. For each cast, the probes were held at the surface for two minutes to achieve temperature equilibrium. The probes were then lowered and raised slowly (no greater then 1 meter per second) to maintain equilibrium. Between casts, the sound velocity sensors were stored in a barrel of fresh water to minimize salt-water corrosion and to hold them at ambient water temperatures. Refer to Appendix III for Calibration Reports.

#### SETTLEMENT CURVE

The squat settlement tests for the R/V R2 were conducted in Southeast Alaska on June 8, 2007 (Julian Day 159).

To perform the squat settlement test, the R/V R2 needed to log dual frequency (L1/L2) data on the POS/MV. The squat settlement test began by first establishing a 500 meter line in the direction of the current. The survey vessel then occupied the south end of the line for two minutes logging 'static' L1/L2 GPS data. Next, the line was run north at a constant engine speed of 300 RPM, then south at the same 300 RPMs. Stopping at the south end of the line, the survey vessel obtained an additional two minutes of 'static' L1/L2 GPS data, then repeated the scenario at incrementing engine RPMs.

All measurements were corrected for heave, pitch, and roll and then reduced to the vessel's Common Reference Point (CRP) and subsequently to the multibeam transducer. Static measurements observed at the end of lines were used to establish tidal correctors to apply to the squat settlement test data. A settlement curve for R2, with the Reson 8101 installed, was calculated from the corrected PPK derived altitude data.





Figure 2 - R/V R2 Settlement Curve

The results of the squat settlement test for the Reson 8101 on R/V R2 are shown below.

R2-8101				
	CALCULATED SETTLEMENT			
RPM	Squat Value (m)			
300	0.024			
400	0.025			
500	0.025			
600	0.032			
700	0.038			
800	0.043			
900	0.051			
1000	0.077			
1100	0.077			
1200	0.076			
1300	0.076			
1400	0.075			

## Table 1 - R/V R2 Squat Settlement Results

Note: Vessel speed was recorded on the survey line logs (refer to Separate 1).

The squat settlement test for the R/V D2was conducted in Southeast Alaska on June 8, 2007 (Julian Day 159).



To perform the squat settlement test, the R/V D2 needed to log dual frequency (L1/L2) data on the POS/MV. The squat settlement test began by first establishing a 500 meter line in the direction of the current. The survey vessel then occupied the south end of the line for two minutes logging 'static' L1/L2 GPS data. Next, the line was run north at a constant engine speed of 700 RPMs, then south at the same 700 RPMs. Stopping at the south end of the line, the survey vessel obtained an additional two minutes of 'static' L1/L2 GPS data, and then repeated the scenario at incrementing engine RPMs.

All measurements were corrected for heave, pitch, and roll and then reduced to the vessel's Common Reference Point (CRP) and subsequently to the multibeam transducer. Static measurements observed at the end of lines were used to establish tidal correctors to apply to the squat settlement test data. A settlement curve for D2, with the Reson 8101 installed, was calculated from the corrected PPK derived altitude data.



Figure 3 - R/V D2 Settlement Curve



The results of the squat settlement test for the Reson 8101 on R/V D2 are shown below.

	D2-8101				
	CALCULATED SETTLEMENT				
RPM	Squat Value (m)				
700	0.038				
800	0.041				
900	0.043				
1000	0.045				
1100	0.047				
1200	0.049				
1300	0.058				
1400	0.067				
1500	0.076				
1600	0.085				
1800	0.070				

Table 2 -	R/V	<b>D2</b> Squat	Settlement	<b>Results</b>
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Note: Vessel speed was recorded on the survey line logs (refer to Separate 1).

The squat settlement tests for the Shoreline Skiff were conducted in Southwest Alaska on June 7, 2007 (Julian Day 158).

To perform the squat settlement test, the Shoreline Skiff logged dual frequency (L1/L2) data on the POS/MV. The squat settlement tests were performed by first establishing a 500 meter line in the direction of the current. The survey vessel occupied the south end of the line for two minutes logging 'static' L1/L2 GPS data. The line was run north at an engine rate of 1000 RPMs, then south at 1000 RPMs. Stopping at the south end of the line, the survey vessel obtained an additional two minutes of 'static' L1/L2 GPS data, and then repeated the scenario at incrementing engine RPMs.

All measurements were corrected for heave, pitch, and roll and then reduced to the vessel's Common Reference Point (CRP) and subsequently to the multibeam transducer. Static measurements observed at the end of lines were used to establish tidal correctors to apply to the squat settlement test data. A settlement curve for the Shoreline Skiff, with the Reson 8125 installed, was calculated from the corrected PPK derived altitude data.





## Figure 4 – R/V Shoreline Skiff Settlement Curve

The results of the squat settlement test for the Reson 8125 on R/V Shoreline Skiff are shown below.

	Shoreline Skiff-8125			
	CALCULATED SETTLEMENT			
RPM	Squat Value (m)			
1000	0.005			
1100	0.026			
1200	0.046			
1300	0.052			
1400	0.058			
1500	0.055			
1600	0.052			

Table 3 – R/V Shoreline Skiff Squat Settlement Results

Note: Vessel speed was recorded on the survey line logs (refer to Separate 1).



The squat settlement test for the R/V Davidson was conducted in Puget Sound, WA on June 7, 2007 (Julian Day 158).

To perform the squat settlement test, the R/V Davidson logged dual frequency data on the POS/MV. The squat settlement tests were performed by first establishing a 500 meter line in the direction of the current. The survey vessel occupied the south end of the line for two minutes logging 'static' L1/L2 GPS data. The line was then run north with a propeller pitch of 4, then south with a pitch of 4. Stopping at the south end of the line, the survey vessel obtained an additional two minutes of 'static' L1/L2 GPS data, and then repeated the scenario at incrementing propeller pitch.

All measurements were corrected for heave, pitch, and roll and then reduced to the vessel's Common Reference Point (CRP) and subsequently to the multibeam transducer. Static measurements observed at the end of lines were used to establish tidal correctors to apply to the squat settlement test data. A settlement curve for the Davidson with the Reson 8111 installed, was calculated from the corrected PPK derived altitude data.



Figure 5 - R/V Davidson Settlement Curve



The results of the squat settlement test for the Reson 8111 on R/V Davidson are shown below.

Davidson-8111 CALCULATED SETTLEMENT			
Pitch	Squat Value (m)		
4	-0.022		
5	-0.004		
6	-0.007		
7	0.02		
8	0.042		

## Table 4 - R/V Davidson Squat Settlement Results

Note: Vessel speed was recorded on the survey line logs (refer to Separate 1).

## STATIC DRAFT

Static draft was measured from tabs on both sides of the vessels, the average was taken, and then the correction to the common reference point was applied. The table below shows the draft values for the R/V R2 used in data processing.

DRAFT #	JULIAN DAY	DATE (UTC)	TIME (UTC)	DEPTH (m)
1	125	5/5/2007	20:39	-0.30
2	126	5/6/2007	15:08	-0.30
3	127	5/7/2007	14:54	-0.28
4	128	5/8/2007	15:07	-0.28
5	129	5/9/2007	15:36	-0.28
6	130	5/10/2007	15:52	-0.29
7	131	5/11/2007	15:45	-0.29
8	132	5/12/2007	15:06	-0.29
9	133	5/13/2007	15:40	-0.29
10	134	5/14/2007	15:16	-0.29
11	135	5/15/2007	15:40	-0.29
12	136	5/16/2007	15:00	-0.28
13	137	5/17/2007	14:58	-0.28
14	138	5/18/2007	16:32	-0.29
15	139	5/19/2007	15:06	-0.28
16	140	5/20/2007	16:23	-0.28

## Table 5 - Draft Measurements for the R/V R2 (Reson 8101)



DRAFT #	JULIAN DAY	DATE (UTC)	TIME (UTC)	DEPTH (m)
17	141	5/21/2007	16:17	-0.28
18	142	5/22/2007	15:23	-0.29
19	143	5/23/2007	15:27	-0.28
20	144	5/24/2007	15:05	-0.29
21	145	5/25/2007	15:10	-0.29
22	146	5/26/2007	15:00	-0.29
23	147	5/27/2007	15:00	-0.29
24	148	5/28/2007	15:09	-0.28
25	149	5/29/2007	15:10	-0.28
26	150	5/30/2007	15:24	-0.28
27	151	5/31/2007	17:24	-0.28
28	152	6/1/2007	15:11	-0.28
29	153	6/2/2007	15:10	-0.28
30	154	6/3/2007	15:05	-0.28
31	155	6/4/2007	15:05	-0.28
32	156	6/5/2007	15:02	-0.29
33	157	6/6/2007	14:55	-0.28
34	158	6/7/2007	14:35	-0.28
35	159	6/8/2007	15:07	-0.28
36	215	8/3/2007	15:05	-0.28
37	216	8/4/2007	14:54	-0.27
38	217	8/5/2007	14:49	-0.28
39	218	8/6/2007	15:06	-0.27
40	219	8/7/2007	15:06	-0.28
41	220	8/8/2007	15:19	-0.28
42	221	8/9/2007	14:50	-0.27
43	222	8/10/2007	15:02	-0.28
44	223	8/11/2007	14:58	-0.27
45	224	8/12/2007	14:57	-0.28
46	225	8/13/2007	14:44	-0.27
47	226	8/14/2007	14:57	-0.28
48	227	8/15/2007	16:13	-0.28
49	228	8/16/2007	15:11	-0.26
50	229	8/17/2007	15:03	-0.26
51	230	8/18/2007	15:11	-0.28
52	231	8/19/2007	15:06	-0.28
53	232	8/20/2007	15:02	-0.27
54	233	8/21/2007	15:30	-0.28



DRAFT #	JULIAN DAY	DATE (UTC)	TIME (UTC)	DEPTH (m)
55	234	8/22/2007	14:57	-0.28
56	235	8/23/2007	15:10	-0.29
57	236	8/24/2007	15:07	-0.29
58	237	8/25/2007	15:07	-0.28
59	238	8/26/2007	14:56	-0.27
60	239	8/27/2007	15:05	-0.27
61	240	8/28/2007	15:28	-0.28
62	241	8/29/2007	15:03	-0.28
63	242	8/30/2007	15:37	-0.28
64	243	8/31/2007	15:20	-0.28
65	244	9/1/2007	15:00	-0.27
66	245	9/2/2007	15:04	-0.29
67	246	9/3/2007	15:05	-0.28
68	247	9/4/2007	15:12	-0.27
69	248	9/5/2007	14:58	-0.27
70	249	9/6/2007	15:03	-0.27
71	250	9/7/2007	15:00	-0.27
72	254	9/11/2007	20:30	-0.28

The table below shows the draft values for the R/V D2 used in data processing.

Table 6 -	Draft I	Measurements	for the	D2 (	Reson	8101)
Table 0 -	Dian	vicasui cincino	IUI UIIC		ILCOUL	0101)

DRAFT #	JULIAN DAY	DATE (UTC)	TIME (UTC)	DEPTH (m)
1	125	5/5/2007	19:50	-0.28
2	126	5/6/2007	16:02	-0.28
3	127	5/7/2007	14:56	-0.26
4	128	5/8/2007	16:17	-0.25
5	129	5/9/2007	16:34	-0.24
6	130	5/10/2007	15:38	-0.32
7	131	5/11/2007	16:09	-0.24
8	132	5/12/2007	15:34	-0.22
9	133	5/13/2007	15:58	-0.26
10	134	5/14/2007	16:25	-0.25
11	135	5/15/2007	16:08	-0.26
12	136	5/16/2007	15:16	-0.24
13	137	5/17/2007	15:20	-0.26
14	138	5/18/2007	16:55	-0.25

Project: OPR-0322-KR-07



DRAFT #	JULIAN DAY	DATE (UTC)	TIME (UTC)	DEPTH (m)
15	139	5/19/2007	15:52	-0.25
16	140	5/20/2007	16:36	-0.24
17	141	5/21/2007	15:59	-0.24
18	142	5/22/2007	15:21	-0.26
19	143	5/23/2007	15:32	-0.23
20	144	5/24/2007	15:28	-0.27
21	145	5/25/2007	15:12	-0.25
22	146	5/26/2007	16:25	-0.28
23	147	5/27/2007	15:25	-0.28
24	148	5/28/2007	15:09	-0.26
25	149	5/29/2007	15:12	-0.26
26	150	5/30/2007	15:22	-0.28
27	151	5/31/2007	16:58	-0.25
28	152	6/2/2007	15:18	-0.28
29	153	6/2/2007	15:10	-0.27
30	154	6/3/2007	15:49	-0.26
31	155	6/4/2007	15:06	-0.26
32	156	6/5/2007	15:10	-0.28
33	157	6/6/2007	14:55	-0.26
34	158	6/7/2007	15:09	-0.26
35	215	8/3/2007	16:01	-0.24
36	216	8/4/2007	15:50	-0.24
37	217	8/5/2007	15:40	-0.26
38	218	8/6/2007	16:04	-0.25
39	219	8/7/2007	15:43	-0.26
40	220	8/8/2007	16:49	-0.25
41	221	8/9/2007	15:37	-0.23
42	222	8/10/2007	20:32	-0.22
43	223	8/11/2007	15:09	-0.23
44	224	8/12/2007	20:51	-0.21
45	225	8/13/2007	14:58	-0.23
46	227	8/15/2007	17:14	-0.20
47	229	8/17/2007	15:54	-0.22
48	230	8/18/2007	15:55	-0.23
49	231	8/19/2007	17:18	-0.22
50	232	8/20/2007	15:57	-0.24
51	233	8/21/2007	15:59	-0.23
52	234	8/22/2007	15:10	-0.22



DRAFT #	JULIAN DAY	DATE (UTC)	TIME (UTC)	DEPTH (m)
53	235	8/23/2007	15:32	-0.27
54	235	8/23/2007	15:32	-0.27
55	236	8/24/2007	15:04	-0.26
56	236	8/24/2007	15:04	-0.26
57	237	8/25/2007	15:49	-0.24
58	237	8/25/2007	15:49	-0.24
59	238	8/26/2007	15:15	-0.23
60	238	8/26/2007	15:15	-0.23
61	239	8/27/2007	15:47	-0.24
62	239	8/27/2007	15:47	-0.24
63	240	8/28/2007	15:07	-0.25
64	240	8/28/2007	15:07	-0.25
65	241	8/29/2007	15:40	-0.22
66	242	8/30/2007	15:07	-0.21
67	242	8/30/2007	15:07	-0.21
68	243	8/31/2007	16:02	-0.28
69	243	8/31/2007	16:02	-0.28
70	244	9/1/2007	15:00	-0.26
71	244	9/1/2007	15:00	-0.26
72	245	9/2/2007	15:02	-0.26
73	246	9/3/2007	15:18	-0.23
74	247	9/4/2007	15:18	-0.26
75	248	9/5/2007	15:29	-0.23
76	249	9/6/2007	15:00	-0.23
77	250	9/7/2007	15:06	-0.24
78	251	9/8/2007	15:48	-0.26
79	252	9/9/2007	15:06	-0.27

The table below shows the draft values for the Shoreline Skiff used in data processing.

Table / - Draft Measurements for the K/V Shoreline (Keson 8125)	Table 7	- Draft	<b>Measurements</b>	for the	R/V S	Shoreline	(Reson	8125)
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DRAFT #	JULIAN DAY	DATE (UTC)	TIME (UTC)	DEPTH (m)
1	132	5/12/2007	16:45	1.38
2	133	5/13/2007	14:55	1.39
3	134	5/14/2007	15:00	1.41
4	135	5/15/2007	15:00	1.40
5	137	5/17/2007	20:25	1.43



<b>DRAFT</b> #	JULIAN DAY	DATE (UTC)	TIME (UTC)	DEPTH (m)
6	138	5/18/2007	22:33	1.40
7	140	5/20/2007	21:57	1.36
8	148	5/28/2007	17:40	1.37
9	151	5/31/2007	19:34	1.35
10	153	6/2/2007	21:27	1.34
11	156	6/5/2007	22:30	1.38
12	224	8/12/2007	23:37	1.30
13	225	8/13/2007	19:32	1.31
14	226	8/14/2007	20:12	1.31
15	227	8/15/2007	20:13	1.31
16	232	8/20/2007	17:46	1.18
17	233	8/21/2007	15:00	1.37
18	234	8/22/2007	23:00	1.35
19	235	8/23/2007	19:04	1.38
20	236	8/24/2007	15:41	1.37
21	237	8/25/2007	17:11	1.37
22	239	8/27/2007	19:40	1.37
23	240	8/28/2007	18:40	1.37
24	242	8/30/2007	1:07	1.36
25	242	8/30/2007	23:15	1.37
26	243	8/31/2007	19:54	1.36
27	244	9/1/2007	16:05	1.35
28	247	9/4/2007	21:04	1.37
29	250	9/7/2007	21:35	1.36
30	252	9/9/2007	19:18	1.39
31	254	9/11/2007	21:30	1.36
32	256	9/13/2007	21:30	1.37
33	257	9/14/2007	22:13	1.36
34	258	9/15/2007	20:42	1.39

The table below shows the draft values for the R/V Davidson used in data processing.

 Table 8 - Draft Measurements for the Davidson (Reson 8111)

DRAFT #	JULIAN DAY	DATE (UTC)	TIME (UTC)	DEPTH (m)
1	125	5/5/2007	23:00	-2.33
2	126	5/6/2007	2:10	-2.38
3	127	5/7/2007	15:15	-2.39



DRAFT #	JULIAN DAY	DATE (UTC)	TIME (UTC)	DEPTH (m)
4	128	5/8/2007	15:05	-2.36
5	129	5/9/2007	19:37	-2.40
6	131	5/11/2007	20:31	-2.38
7	132	5/12/2007	16:14	-2.35
8	133	5/13/2007	15:51	-2.35
9	135	5/15/2007	15:43	-2.37
10	136	5/16/2007	15:25	-2.34
11	137	5/17/2007	14:49	-2.35
12	138	5/18/2007	16:29	-2.33
13	139	5/19/2007	16:29	-2.30
14	140	5/20/2007	16:24	-2.34
15	142	5/22/2007	15:27	-2.31
16	143	5/23/2007	15:31	-2.29
17	144	5/24/2007	15:39	-2.31
18	145	5/25/2007	15:04	-2.30
19	148	5/28/2007	15:02	-2.32
20	148	5/28/2007	2:36	-2.31
21	149	5/29/2007	15:30	-2.30
22	150	5/30/2007	15:27	-2.32
23	151	5/31/2007	16:49	-2.31
24	151	5/31/2007	16:47	-2.31
25	155	6/4/2007	15:27	-2.31
26	156	6/5/2007	15:22	-2.30
27	158	6/7/2007	15:09	-2.30
28	159	6/8/2007	18:59	-2.29
29	215	8/3/2007	15:36	-2.42
30	216	8/4/2007	15:52	-2.39
31	217	8/5/2007	15:31	-2.43
32	218	8/6/2007	15:54	-2.39
33	219	8/7/2007	16:04	-2.40
34	220	8/8/2007	16:46	-2.38
35	221	8/9/2007	15:27	-2.37
36	222	8/10/2007	15:16	-2.35
37	223	8/11/2007	15:15	-2.36
38	224	8/12/2007	15:14	-2.42
39	225	8/13/2007	15:12	-2.37
40	226	8/14/2007	15:11	-2.32
41	227	8/15/2007	16:51	-2.28



DRAFT #	JULIAN DAY	DATE (UTC)	TIME (UTC)	DEPTH (m)
42	228	8/16/2007	15:22	-2.29
43	229	8/17/2007	15:53	-2.34
44	230	8/18/2007	15:59	-2.27
45	231	8/19/2007	16:28	-2.25
46	232	8/20/2007	16:21	-2.32
47	233	8/21/2007	16:07	-2.26
48	234	8/22/2007	15:18	-2.29
49	235	8/23/2007	15:16	-2.29
50	236	8/24/2007	14:45	-2.28
51	237	8/25/2007	14:47	-2.20
52	238	8/26/2007	14:42	-2.28
53	239	8/27/2007	15:03	-2.25
54	240	8/28/2007	14:56	-2.27
55	241	8/29/2007	19:16	-2.31
56	247	9/4/2007	23:55	-2.26
57	247	9/4/2007	2:46	-2.27

## TIDES

All sounding data were reduced to MLLW initially using unverified tidal data from three tide stations located in Warm Springs Bay, False Bay, and Mitchell Bay, AK. Tidal data for a twenty-four hour period UTC, (Alaska Daylight Time to UTC was +8 hours) was assembled by JOA and emailed to the Davidson at the end of every Julian Day. A cumulative file in a CARIS format was updated each day by appending the new data. Refer to the OPR-O322-KR-07 Horizontal and Vertical Control Report for additional tidal information and station descriptions.

The tidal zoning was modified by JOA, providing a more elaborate zoning scheme from those zones issued in the Statement of Work. For additional information, refer to JOA's Final Technical Report.

November 5, 2007, JOA issued verified tidal data and final zoning for H11696, H11697, H11698, H11699, H11702, H11703, H11704, H11705, H11706, H11707, & H11708 of OPR-O322-KR-07. On January 2, 2008, JOA issued verified tidal data and final zoning for H11700 & H11701 of OPR-O322-KR-07. All sounding data were then re-merged using CARIS HIPS and SIPS tide routine. Verified tidal data were used for all final Navigation BASE surfaces and S57 Feature files.

## VESSEL ATTITUDE: HEADING, HEAVE, PITCH, AND ROLL

Vessel heading and dynamic motion were measured by the POS/MV for the OPR-O322-KR-07 project. The system calculated heading by inversing between two Trimble GPS generated antenna positions. An accelerometer block (the IMU), which measured vessel attitude, was mounted directly over the multibeam transducer on each vessel. The operational accuracy specifications for this system, as documented by the manufacturer, are as follows:

POS/MV Accuracy			
Pitch and Roll 0.035°			
Heading	0.05°		
Heave	5% or 5-cm over 20 seconds		

## CALIBRATIONS

#### <u>Multibeam</u>

A patch test was conducted to identify alignment errors (timing, pitch, heading, and roll) between the motion sensor and the multibeam transducer.

On July 1, 2007, during Survey operations in Dutch Harbor for project OPR-Q191-KR-07, the R/V R2 struck a submerged object. Review of the data on July 1, 2007 after the incident revealed a shift in sonar to IMU alignment parameters. An additional patch test was conducted the next day to obtain new parameters. It was apparent that the new alignment parameters were static and valid after 01:07 on July 1 (the time of the incident).

On August 1, 2007, before deployment of the pole on the Shoreline Skiff, it was noticed that during the transit to Dutch Harbor, the A-Frame had decompressed. An inspection revealed the A-Frame had come to rest on the pole, tweaking its alignment. An additional patch test was conducted later that day to obtain new parameters. It was apparent that the new alignment parameters were static and valid for data collected after August 1, 2007.

Additional patch tests were conducted during the course of the survey for quality control and testing purposes, but the derived values were not entered into the vessel configuration file, hence, not used in processing. Patch test calibration values used to correct all soundings for the survey were as follows:



Patch Test Results for R/V R2 Reson 8101 May 5th, 2007 (2007-125)					
Test	CARIS Session	Mean Correction			
Navigation Timing Error	Patch_125_Nav	0.00 seconds			
Pitch Offset	Patch_125_Pitch	-2.200°			
Azimuth Offset	Patch_125_Yaw	-2.400°			
Roll Offset	Patch_125_Roll	0.040°			

## Table 10 - Patch Test Results for R/V R2 Reson 8101

## Table 11 - Patch Test Results for R/V R2 Reson 8101

Patch Test Results for R/V R2 Reson 8101 July 1st, 2007 (2007-182)				
Test	CARIS Session	Mean Correction		
Navigation Timing Error	Patch_182_Nav	0.00 seconds		
Pitch Offset	Patch_182_Pitch	-2.000°		
Azimuth Offset	Patch_182_Yaw	-2.300°		
Roll Offset	Patch_182_Roll	-0.380°		

## Table 12 - Patch Test Results for R/V D2 Reson 8101

Patch Test Results for R/V D2 Reson 8101 May 5th, 2007 (2005-125)			
Test	CARIS Session	Mean Correction	
Navigation Timing Error	Patch_128_Nav	0.00 seconds	
Pitch Offset	Patch_128_Pitch	-0.680°	
Azimuth Offset	Patch_128_Yaw	0.750°	
Roll Offset	Patch_128_Roll	1.670°	

Table 13 - Patch	Test Results f	or Shoreline Skiff	<sup>°</sup> Reson 8125
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Patch Test Results for Shoreline Skiff Reson 8125 May 12th, 2007 (2007-132)				
Test	CARIS Session	Mean Correction		
Navigation Timing Error	Patch_132_Nav	0.00 seconds		
Pitch Offset	Patch_132_Pitch	0.450°		
Azimuth Offset	Patch_132_Yaw	0.000°		
Roll Offset	Patch_132_Roll	0.200°		

Patch Test Results for Shoreline Skiff Reson 8125 August 1st, 2007 (2007-213)				
Test	CARIS Session	Mean Correction		
Navigation Timing Error	Patch_213_Nav	0.00 seconds		
Pitch Offset	Patch_213_Pitch	-0.100°		
Azimuth Offset	Patch_213_Yaw	0.600°		
Roll Offset	Patch_213_Roll	0.200°		

## Table 14 - Patch Test Results for Shoreline Skiff Reson 8125

## Table 15- Patch Test Results for the R/V Davidson Reson 8111

Patch Test Results for Davidson Reson 8111 May 5th, 2007 (2007-125)				
Test	CARIS Session	Mean Correction		
Navigation Timing Error	Patch_142_Nav	0.00 seconds		
Pitch Offset	Patch_142_Pitch	0.00°		
Azimuth Offset	Patch_142_Yaw	-0.400°		
Roll Offset	Patch_142_Roll	0.780°		

## Additional Sounding Techniques

No additional sounding techniques were used throughout the course of the survey.



## **D** - Approval Sheet

## **Approval Sheet**

For

# H11696, H11697, H11698, H11699, H11700, H11701 & H11702, H11703, H11704, H11705, H11706, H11707, & H11708

Standard field surveying and processing procedures were followed in producing this survey in accordance with the following documents:

OPR-O322-KR-07 Statement of Work and 2007 Specifications & Deliverables; Fugro Pelagos, Inc. Acquisition Procedures (2007- NOAA Acquisition Procedures); Fugro Pelagos, Inc. Processing Procedures (2007-NOAA Processing Procedures);

The data were reviewed daily during acquisition and processing.

This report has been reviewed and approved. All records are forwarded for final review and processing to the Chief, Pacific Hydrographic Branch.

Approved and forwarded,

Dean Moyles, Lead Hydrographer Fugro Pelagos, Inc. Survey Party



Equipment

UGRO

System	Manufacturer	Model	Serial No.
Multibeam Sounder	Reson	SeaBat 8101 Processor	12945
		SeaBat 8101 Transducer	1600001
		8101 Firmware Dry: 8101-2-07-2D4D	
		Wet: 8101-1-06-2F6B	
Multibeam Sounder	Reson	SeaBat 8101 Processor	37127
		SeaBat 8101 Transducer	
		8101 Firmware Dry: 8101-2-09-E34D	
		Wet: 8101-1-08-C215	
Multibeam Sounder	Reson	SeaBat 8125 Processor	36746
		SeaBat 8125 Transducer	0802100
		8125 Firmware Dry: 8125-2-10-A50F	
		Wet: 8125-1-08-9E98	
Multibeam Sounder	Reson	SeaBat 8111 Processor	Multibeam Sounder
		SeaBat 8111 Transducer Array	Transmit/Receive
		8111 Firmware Dry: 8111-E2.09-6114	
		Wet:8111-E1.01-AFAA	
POS/MV	Applanix	Firmware Model 320: Ver 4	2161
POS/MV	Applanix	IMU	231
POS/MV	Applanix	Firmware Model 320: Ver 4	2640
POS/MV	Applanix	IMU	241
POS/MV	Applanix	Firmware Model 320: Ver 4	2354
POS/MV	Applanix	IMU	78
POS/MV	Applanix	Firmware Model 320: Ver 4	2355
POS/MV	Applanix	IMU	49
GPS Antenna	Trimble	L1/L2	4435A43274
GPS Antenna	Trimble	L1/L2	4435A43283
GPS Antenna	Trimble	L1/L2	4644A74185
GPS Antenna	Trimble	L1/L2 4644A74186	
GPS Antenna	Trimble	L1/L2	4541A61043
GPS Antenna	Trimble	L1/L2 4541A61	
GPS Antenna	Trimble	L1/L2	4541A61044
GPS Antenna	Trimble	L1/L2	4533A9383
Smart Sensor	Applied Microsystems Ltd.	Smart Sound Velocity and Pressure	4655
Smart Sensor	Applied Microsystems Ltd.	Smart Sound Velocity and Pressure	5282
Smart Sensor	Applied Microsystems Ltd.	Smart Sound Velocity and Pressure	4820
Smart Sensor	Applied Microsystems Ltd.	Smart Sound Velocity and Pressure	5283
Smart Sensor	Applied Microsystems Ltd.	Smart Sound Velocity and Pressure	4703 (not used)
Smart Sensor	Applied Microsystems Ltd.	Smart Sound Velocity and Pressure	4966
Smart Sensor	Applied Microsystems Ltd.	Smart Sound Velocity and Pressure	4932
Smart Sensor	Applied Microsystems Ltd.	Smart Sound Velocity and Pressure	4431
Smart Sensor	Applied Microsystems Ltd.	Smart Sound Velocity and Pressure	4656
Smart Sensor	Applied Microsystems Ltd.	Smart Sound Velocity and Pressure	5284
CTD Profiler	Sea-Bird Electronics	CTD- 12	727
RTCM	CSI Inc.	CSI MBX-3	9834-2211-0001
RTCM	CSI Inc.	CSI-MBX-3	9920-3754-0002
RTCM	CSI Inc.	CSI MBX-3	9833-2166-0001
RTCM	CSI Inc.	CSI-MBX-3	9913-3442-0001

# Table 16 - Equipment List

Project: OPR-0322-KR-07



System	Manufacturer	Model	Serial No.
RTCM	CSI Inc.	CSI MBX-3	9830-2023-0001
RTCM	CSI Inc.	CSI-MBX-3	9834-2211-0001
RTCM	CSI Inc.	CSI-MBX-3	9834-2211-0020
DGPS	CSI Inc.	GBX PRO	0124-8517-0001
Digital Camera	Kodak	Kodak	KCKDP43503807
Digital Camera	Sony	Sony	0947524
Digital Camera	Sony	Sony	0947522
Control Station	Novatel	Novatel DL4 Receiver	0001
Control Station	Novatel	Novatel DL4 Receiver	0009
Control Station	Novatel	Novatel GPS 702 Rev 3 Ant.	NVH06140007
Control Station	Novatel	Novatel GPS 702 Rev 3 Ant.	NVH05230012
Automatic Level	Trimble	AL228	801241
Total Station	Topcon	GTS 211D	LG4090

## Software

Triton Isis v 7.1428.53 Delph Map v2.9.0.21 WinFrog v 3.7.0 CARIS Hips/Sips v 6.1 (w/ Service Pack 1) CARIS GIS v 4.4a (w/ Service Pack 5) MapInfo Professional v 5.0 AutoDesk Map R 5.0 MBSurvey Tools v2.00.05.00 POS/MV v4 Controller v3.2.2.2 & 3.4.0.0 (firmware dependent) ESRI Arc Map v9.2 Correlator v1.0 POSConv v1.4 POSPac 4.3 & 4.31



## **Appendix II – Vessel Descriptions**

## <u>R/V R2</u>

The R/V R2 (Figure 6) was modified to accommodate a survey crew and acquisition hardware. The keel was cut just aft of mid-ship and Reson 8101 multibeam sonar was installed. A conical cowling protected the sonar head forward and aft by a crescent shaped skid (Figure 8). The accelerometer package for a POS/MV was mounted in the hull of the vessel just over the 8101 multibeam transducer head.

Two Trimble L1/L2 antennas were mounted above the 8101 and accelerometer for positioning and heading (Figure 7). The two POS/MV antennas were offset 1.0m to the port and starboard. The port side antenna (L1/L2) functioned as the POS/MV master antenna; the starboard side antenna functioned as the POS/MV secondary.

The AML Smart Probe SV&P sensors and the CTD were deployed from an A-Frame on the stern using a small hydraulic winch.

Offset values were applied to the data in CARIS HIPS as specified in the vessel configuration file (VCF). Vessel offsets used are shown in the following table. Note that the VCF does not contain navigation offsets because the position provided by the POS/MV is already corrected to the CRP.

R2 Vessel Offsets				
From To		X	Y	Z
CRP	IMU - POS/MV	0.000	0.00	0.00
CRP	Reson 8101 Transducer	0.009	-0.614	0.632
CRP	GPS1 – Master Antenna	-0.998	-0.005	-3.071
CRP	GPS2 – Slave Antenna	1.010	-0.020	-3.035
CRP	Draft Measuring Point, Port	-1.795	-3.527	-1.503
CRP	Draft Measuring Point, Starboard	1.771	-3.560	-1.460

Table 17 - Vessel Offsets (R2)

Note: All units are meters.

CRP is the top-center of the IMU. Axis used: X positive toward Starboard Y positive toward Bow Z positive in to the water



Survey Launch	R2
Official Number	623241/647782
Owner	Stabbert Maritime Yacht & Ship
Year Built	1980/1982
Length	28.9 ft
Beam	12 ft
Draft	5.7 ft
Gross Ton	15
Net Ton	13
Mechanical Power	Caterpillar 3208
Electrical	Northern Lights

# Table 18 - Vessel Specifications (R2)



Figure 6 - R/V R2





Figure 7 - Differential and POS/MV Antennas (R/V R2)



Figure 8 – Hull Mounted Reson 8101 (R/V R2)



The R/V D2 (Figure 9) was modified to accommodate a survey crew and acquisition hardware. The keel was cut just aft of mid-ship and Reson 8101 multibeam sonar was installed. A conical cowling protected the sonar head forward and aft by a crescent shaped skid. The accelerometer package for a POS/MV was mounted in the hull of the vessel just over the 8101 multibeam transducer head.

Two Trimble L1/L2 antennas were mounted above the 8101 and accelerometer for positioning and heading (Figure 10). The two POS/MV antennas were offset 1.06m to the port and starboard. The port side antenna (L1/L2) functioned as the POS/MV master antenna; the starboard side antenna functioned as the POS/MV secondary.

The AML Smart Probe SV&P sensors and the CTD were deployed from an A-Frame on the stern using a small hydraulic winch.

Offset values were applied to the data in CARIS HIPS as specified in the vessel configuration file (VCF). Vessel offsets used are shown in the following table. Note that the VCF does not contain navigation offsets because the position provided by the POS/MV is already corrected to the CRP.

D2 Vessel Offsets				
From To		X	Y	Z
CRP	IMU – POS/MV	0.000	0.00	0.00
CRP	Reson 8101 Transducer	-0.016	-0.879	0.548
CRP	GPS1 – Master Antenna	-1.002	-0.064	-3.095
CRP	GPS2 – Slave Antenna	0.991	-0.048	-3.046
CRP	Draft Measuring Point, Port	-1.794	-2.535	-1.397
CRP	Draft Measuring Point, Starboard	1.846	-2.521	-1.331

 Table 19 - Vessel Offsets (D2)

Note: All units are meters.

CRP is the top-center of the IMU.

Axis used: X positive toward Starboard

Y positive toward Bow

Z positive in to the water



Survey Launch	D2	
Official Number	623241/647782	
Owner	Stabbert Maritime Yacht & Ship	
Year Built	1980/1982	
Length	28.9 ft	
Beam	12 ft	
Draft	5.7 ft	
Gross Ton	15	
Net Ton	13	
Mechanical Power	Caterpillar 3208	
Electrical	Northern Lights	

# Table 20 - Vessel Specifications (D2)



Figure 9 - R/V D2





Figure 10 - Differential and POS/MV Antennas (R/V D2)



## Shoreline Skiff

The Shoreline Skiff (Figure 11) was modified to accommodate survey crew and acquisition hardware. The vessel was fitted with a rugged pole configuration just aft of the wheelhouse on the starboard side. This housed the 8125 multibeam transducer head including SVP and the accelerometer package for a POS/MV (Figure 12).

Two Trimble L1/L2 antennas were mounted on the roof of the cabin for positioning and heading (Figure 13). The two POS/MV antennas were offset 1.5m to the port and starboard. The port side antenna (L1/L2) functioned as the POS/MV master antenna; the starboard side antenna functioned as the POS/MV secondary.

The AML Smart Probe SV&P sensor was deployed by hand off the starboard side of the vessel.

Offset values were applied to the data in CARIS HIPS as specified in the vessel configuration file (VCF). Vessel offsets used are shown in the following table. Note that the VCF does not contain navigation offsets because the position provided by the POS/MV is already corrected to the CRP.

Shoreline Skiff Vessel Offsets				
From	Y	Z		
CRP	IMU – POS/MV	0.000	0.00	0.00
CRP	Reson 8125 Transducer	0.085	-0.126	2.108
CRP	GPS1 – Master Antenna	-2.389	1.345	-0.963
CRP	GPS2 – Slave Antenna	-0.855	1.363	-0.970
CRP	Draft Measuring Point	-0.004	-0.148	0.161

## Table 21 - Vessel Offsets (Shoreline Skiff) Page 1

Note: All units are meters.

CRP is the top-center of the IMU.

Axis used: X positive toward Starboard

Y positive toward Bow

Z positive in to the water



Survey Launch	Shoreline Skiff
Official Number	WN6739NW
Owner	Stabbert Maritime
Year Built	2004
Length	24 ft
Beam	8.5 ft
Draft	1.42 ft
Gross Ton	
Net Ton	
Mechanical Power	(2) Suzuki 140H OB
Electrical	

# Table 22 - Vessel Specifications (Shoreline Skiff)



**Figure 11 - Shoreline Skiff** 





Figure 12 – Pole Mounted Reson 8125 (Shoreline Skiff)



Figure 13 - Differential and POS/MV Antennas (Shoreline Skiff)



R/V Davidson

The R/V Davidson (Figure 14) accommodated a survey crew, acquisition hardware, and processing equipment. The keel was cut just aft of mid-ship and Reson 8111 multibeam sonar was installed. A conical cowling protected the sonar head forward and aft by a crescent shaped skid. The accelerometer package for a POS/MV was mounted on the lower deck of the vessel just over the 8111 multibeam transducer head.

Two Trimble L1/L2 GPS antennas were mounted on the ships top deck for positioning and heading (Figure 15). The two POS/MV antennas were offset 2.0m apart fore and aft. The forward antenna functioned as the POS/MV master antenna; the aft antenna functioned as the POS/MV secondary.

The AML Smart Probe SV&P sensors and the CTD were deployed from an A-Frame on the stern using a hydraulic winch.

Offset values were applied to the data in CARIS HDCS as specified in the vessel configuration file (VCF). Vessel offsets used are shown in the following table. Note that the VCF does not contain navigation offsets because the position provided by the POS/MV is already corrected to the CRP.

Davidson Vessel Offsets				
From	То	X	Y	Z
CRP	IMU – POS/MV	0.000	0.000	0.000
CRP	Reson - 8111 Transducer	0.046	-0.342	2.047
CRP	GPS 1 - Master Antenna	-0.248	4.982	-23.478
CRP	GPS 2 - Slave Antenna	-0.318	2.993	-23.419
CRP	Draft Measuring Point, Port	-5.778	-1.599	-4.282
CRP	Draft Measuring Point, Starboard	5.672	-10.211	-5.392

## Table 23 - Vessel Offsets (Davidson)

Note: All units are meters.

CRP is the top-center of the IMU.

Axis used: X positive toward Starboard

Y positive toward Bow

Z positive in to the water



Survey Launch	<b>R/V Davidson</b>
Official Number	1066485
Owner	Davidson, LLC/Ocean Services, LLC
Year Built	1967
Length	175 ft
Beam	38 ft
Draft	17.75 ft
Gross Ton	250
Net Ton	833
Mechanical Power	1800 hp

# Table 24 - Vessel Specifications (Davidson)



Figure 14 R/V Davidson





Figure 15 Differential and POS/MV Antennas (Davidson)



Figure 16 Hull Mounted Reson 8111



## **Appendix III – Calibration Reports**

4431 Calibration Certificate.pdf 4655 Calibration Certificate.pdf 4656 Calibration Certificate.pdf 4820 Calibration Certificate.pdf 4932 Calibration Certificate.pdf 4966 Calibration Certificate.pdf 5282 Calibration Certificate.pdf 5283 Calibration Certificate.pdf 5284 Calibration Certificate.pdf 727 Calibration Certificate.pdf 8125 C SVP.pdf