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DEPARTMENT OF COMMERCE  
U. S. COAST AND GEODETIC SURVEY

State: California.

11-5613

DESCRIPTIVE REPORT.

Hydrographic Sheet No. 25

LOCALITY:

Southern California coast

San Clemente Island.

1933-34

CHIEF OF PARTY:

O. W. Swainson,

5758

DEPARTMENT OF COMMERCE  
U. S. COAST AND GEODETIC SURVEY

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HYDROGRAPHIC TITLE SHEET

The Hydrographic Sheet should be accompanied by this form, filled in as completely as possible, when the sheet is forwarded to the Office.

Field No. 25

REGISTER NO. 5758

State California

General locality Southern California Coast

Locality San Clemente Island

Scale 1:20,000 Date of survey October 24 1933  
to May 17, 1934

Vessel PIONEER

Chief of Party O. W. Swainson  
O. W. Swainson, J. M. Smook, P. L. Bernstein, R. A. Gilmore,  
Surveyed by and J. C. Ellerbe.

Protracted by H. J. Pulskamp (Draftsman) and H. J. Healy

Soundings penciled by H. J. Pulskamp and H. J. Healy.

Soundings in fathoms ~~feet~~

Plane of reference M. L. L. W.

Subdivision of wire dragged areas by

Inked by Robinson + ( )

Verified by Robinson

Instructions dated November 18, 1932

Remarks: Robinson

DESCRIPTIVE REPORT

TO ACCOMPANY

HYDROGRAPHIC SHEET, FIELD NO. 25.

AUTHORITY

The hydrography of field sheet No. 25 was done in accordance with Instructions dated November 18, 1932, for project No. 120.

LOCALITY

The sheet extends offshore of the 1933 work of Lieut. R.W. Knox, around the southern and southeastern end of San Clemente Island, Calif.

CONTROL

The control was visual fixes on triangulation stations established or recovered by Lieut. R.W. Knox in 1933, and topographic signals established by the same party.

SURVEY METHODS

The work was done on a scale of 1:20,000, using the PIONEER throughout. All soundings were taken with the fathometer, supplemented with a large number of vertical casts. These casts were taken close together off the southeast end of the island due to the irregular bottom and also to check the slope corrections as determined from the depth curves.

The lines were run parallel to the shore to allow a gradual increase in the spacing of the lines as the depth increased. Cross lines were run normal to the beach at about five mile intervals.

Bottom characteristics were usually obtained at the vertical casts and are so indicated on the sheet.

Depth curves are drawn at 50, 100 and 200 fathoms.

CURRENTS

No current observations were made, nor were any decided currents observed in the course of the hydrography.

TIDES

Tidal data was obtained from the automatic tide gages maintained by Lieut. R.W. Knox, first at Wilson Cove, San Clemente Island and later at Avalon, Catalina Island. No time or height corrections were made to the data obtained in referring them to the locality of the sheet.

MAGNETICS

No magnetic observations were made.

### FATHOMETER CORRECTIONS

Fathometer corrections were computed for sheets 12,13,14,25,26 and 27 as a group prior to November 21,1933 and then again after that date up to May 14,1934. Another set of corrections was determined for sheets 25,26 and 47 as a group for the period May 14 to May 31,1934.

For detailed tables and descriptions of the determination of the fathometer corrections see 1933 Seasons Report for the PIONEER. See also the Descriptive Report for sheet, field No.12 for the corrections up to May 14, 1934. The method of computing the fathometer correction after May 14 is explained in detail and is made a part of this report on subsequent pages.

A resume of the corrections applied to this sheet is attached to the front of Volume 1, and an abstract of the fathometer comparisons is made a part of this report.

### SLOPE CORRECTIONS

All corrections for slope were computed in accordance with Special Publication No.165. The depth curves were drawn using fathometer soundings that were corrected for salinity and temperature. A scale was made to read the percent of slope between 100 fathom depth curves. Using this scale the complete area of the sheet was investigated.

In many places the percentage of slope was taken between intermediate depth curves, for example between 250 and 350 fathoms. The corrections were all entered in the record and the soundings reduced.

Where slope corrections were applied, the final reduced sounding is shown on the smooth sheet, followed by a sounding in parenthesis, which is corrected for all other factors except slope.

In the case of the wire soundings they are shown on the sheet followed by V.C. Where ~~the~~ slope corrections were applied to the soundings in the immediate vicinity of the V.C. a correction was also applied to the reduced fathometer sounding at the V.C., so besides the wire reading there are given two other soundings in parenthesis, namely the reduced fathometer sounding and same corrected for slope. Where no slope correction has been applied only one sounding in parenthesis is given at the V.C., namely the reduced fathometer sounding.

### DANGERS

There are no dangers to navigation on this sheet.

### JUNCTION WITH OTHER SHEETS

The hydrography checked very well with the junction of the 1933 inshore work of Lieut. R.W. Knox. Where there are small discrepancies with Lieut. Knox's work, use his soundings.

This sheet joins sheet field No. 26 on the north side of the island and sheet, field No. 27 on the south side of the island. There is a discrepancy of about 2% with some of the soundings on sheet No.26 and agrees very well with sheet No.27.

#### COMPARISONS WITH PREVIOUS SURVEYS

Tracings of the surveys on sheets 1430, 4366, 4549a and 4783 were made and these were used for the comparison with the new survey. The following was noted:

Sheet 1430: There were a few discrepancies with this sheet, but most of the soundings showed fairly good agreement.

Sheet 4366: As a whole the agreement with this sheet was good except near longitude  $118^{\circ} 20'$  between latitudes  $32^{\circ} 47'$  and  $32^{\circ} 48'$ .

Sheet 4549a: The agreement of the overlapping section of this sheet with the present survey was very good except for the six soundings on a line from latitude  $32^{\circ} 53.8'$  longitude  $118^{\circ} 22.8'$  to latitude  $32^{\circ} 56'$  longitude  $118^{\circ} 24.7'$ , which are exceedingly lower than those obtained on field sheet No.25.

Sheet 4783: As a whole the agreement of the overlapping section with this sheet was very good.

In all of the above cases where the old survey and the present one do not agree, accept the present soundings. (With the exception of the area Southeast of the southeast end of the island, where the fixes were weak, as noted later, the control was very good and the fathometer soundings were supplemented with a large number of vertical casts. The last two days of work on this sheet were devoted entirely to taking vertical cast comparisons.)

#### MISCELLANEOUS

Some difficulty was encountered in obtaining good control southeast of the southeast end of the island, as on several occasions swingers were used for fixes. There was also some confusion about  $\Delta$  Guds. The fixes were plotted with this station on the boat sheet, but when check angles were taken it was noted that  $\odot$  Guds 2 had been used, and this point has been plotted as a hydrographic signal and was used in plotting the smooth sheet. Both  $\Delta$  Guds and  $\odot$  Guds 2 were used.

$\Delta$  Three was erroneously plotted on the boat sheet and this was not discovered until practically all the plotting using that station was finished. When correctly used it made a decided change in the plotting of the lines.

In view of the changes made on the smooth sheet on account of the use of  $\odot$  Guds 2 and the correct position of  $\Delta$  Three, the lines on the smooth sheet southeast and southsoutheast of the southeast end of the island do not conform to those on the boat sheet.

1. At latitude  $32^{\circ} 53' 3''$  longitude  $118^{\circ} 23' 7''$  the fathometer sounding (325) on C day is probably too deep, as it doesn't check the vertical comparisons taken nearby (positions 29F and 40F). The next fathometer sounding on position 161 C checks the vertical cast taken at position 39F.

2. At position 30F (latitude  $32^{\circ} 53' 7''$  longitude  $118^{\circ} 23' 3''$ ) the vertical cast seems to be too deep, as it doesn't check the other soundings. The fathometer sounding seems to be correct. *V.C. not plotted.*

3. At latitude  $32^{\circ} 54' 3''$  longitude  $118^{\circ} 24' 8''$  there is a discrepancy of about 4% in the crossing (408 and 420).

4. At latitude  $32^{\circ} 50' 4''$  longitude  $118^{\circ} 21' 2''$  there is a discrepancy of 22 fathoms between the fathometer sounding and the vertical cast (position 22F). The slope corrections were not applied to the line of soundings near position 22F, therefore it wasn't applied to the <sup>fathometer</sup> reading taken at the vertical cast, the reason being that the slope is less than the critical value. However, as the slope is about 7% in this case, if it were applied to the fathometer reading it would bring it up to the vertical cast. This same condition exists at position 26F (latitude  $32^{\circ} 51' 1''$  longitude  $118^{\circ} 22' 1''$ ) where the slope is about 5%. *Slope comes  $3\frac{1}{2}\%$  accord. to Sp. Pub. 165*

5. At latitude  $32^{\circ} 46' 8''$  longitude  $118^{\circ} 25' 4''$ , there is a sounding of 43 fathoms between a 32 and a 37 and at latitude  $32^{\circ} 46' 6''$  longitude  $118^{\circ} 25' 6''$  there is a sounding of 39 fathoms between a 47 and a 45. These soundings are correct. The bottom is very bumpy in this area, and the soundings were checked on sheet No. 27. *not plotted*

6. At latitude  $32^{\circ} 45' 8''$  longitude  $118^{\circ} 22' 4''$  the sounding of 153<sup>1/2</sup> fathoms between 160 and 178 looks doubtful. It is noted that the recorder marked this as a slope sounding in the record book. It probably wasn't called to the attention of the officer in charge at the time. *\* Sounding not plotted. Very probably the echo was not from point*

7. At latitude  $32^{\circ} 47' 7''$  longitude  $118^{\circ} 20' 6''$  there is a sounding of 101 fathoms just inside of 97 (discrepancy of about 4%). *directly beneath vessel.*

8. At latitude  $32^{\circ} 45' 7''$  longitude  $118^{\circ} 19' 1''$  there is a sounding of 363 fathoms near a 376 (discrepancy of about  $3\frac{1}{2}\%$ ).

9. At latitude  $32^{\circ} 48' 8''$  longitude  $118^{\circ} 20' 3''$  there is a sounding of 66 fathoms between a 48 and a 63. The bottom in this locality is very uneven and the soundings are probably all correct.

With the few exceptions noted above, the crossings on this sheet checked very well.

*J. M. Smook,*  
J. M. Smook,  
H. & G. Engineer.

## FATHOMETER CORRECTIONS

For

Field Sheets Nos. 12, ~~14~~, 25, 26, and 27.

### TABLE A

This table shows the computation of the theoretical and final fathometer correction, the latter being obtained by application to the former of index corrections computed on tables B and C.

Column 0 is the temperature scaled from a curve of temperatures taken in the areas of the sheets. (See blueprint).

Column 1 is true depth of water.

Column 2 is salinity scaled from a curve plotted with data furnished by the Scripps Institute of Oceanography. These salinities were taken west of San Miguel Island, but are believed to be of sufficient accuracy for use in the areas covered by the sheets concerned.

Column 3 is the velocity of sound through sea water as taken from the British Admiralty Tables for each depth.

Column 4 is the mean of the velocities from the surface to each succeeding depth.

Column 5 is the distance the sound traveled from the oscillator to the bottom and back to the hydrophone for the No. 3 (Navy rat) hydrophone and Big Oscillator.

Column 6 is the uniform scale reading on a fathometer, computed from the depth and mean theoretical velocity. The speed of the fathometer was 248 r.p.m., or 62/15 r.p.s. The uniform scale reading equals  $124/15 \times D \times 1.828$ . The factor, 1.828, is used to reconcile the depth in fathoms to the mean theoretical velocity in meters.

In column 7 the reading on the uniform scale is changed to the corresponding reading on the existing non-uniform scale of the fathometer. Where the existing scale is uniform, this column is left blank.

Column 8 is the computed theoretical correction, and is equal to column 1 minus column 7.

Column 9 is the final correction to fathometer soundings, obtained by applying an index correction of minus 0.9 fathom to the corresponding theoretical corrections. These final corrections apply from October 1, 1933 to November 21, 1933.

Column 10 is the final correction to the fathometer soundings, obtained by applying an index correction of plus 1.4 fathoms to the corresponding theoretical corrections. These corrections apply after November 21, 1933.

In columns 9 and 10, it is to be noted that the corrections are listed opposite true depths of water, but in order to simplify the entering of the reducers in the sounding volumes these corrections were plotted on a curve against indicated depths and the final values shown in Table D taken from this curve.

Column 11 is the distance the sound travels from the small oscillator to the bottom and back to the number 2 (tuned) hydrophone.

Column 12 is the uniform scale reading for the number 2-small oscillator combination. (See column 6 this report for method of computation)

Column 13 for the number 2-small oscillator combination is the same as column 7 for the number 3-large oscillator combination.

Column 14 is the theoretical fathometer correction and equals column 2 minus column 13.

Column 15 is the final fathometer correction and is column 14 plus an index correction of -1.8 fathoms. This column applies from October 1 to November 21, 1933.

Column 16 is the final fathometer correction that applies after November 21, 1933. This correction is column 14 plus an index correction of +1.0 fathom.

These corrections were plotted on a curve against indicated fathometer soundings and the corrections in Table D taken therefrom.

Columns 5, 6, 7, 8, 9, and 10 apply to the big oscillator-number 3 hydrophone combination; columns 11, 12, 13, 14, 15, and 16 apply to the small oscillator-number 2 hydrophone combination; columns 0, 1, 2, 3, and 4 apply to both combinations.

#### TABLE B

In table B are listed the comparison of the indicated fathometer soundings with the corresponding vertical casts to obtain an index correction (I.C.). On the left hand side of the table are the comparisons taken between October 1, and November 21, with a separate table for the long dash. On the right hand side of the table are the comparisons taken after November 21. This table is for the Number 3- Big Oscillator combination.

#### TABLE C

In table C are listed the comparisons of the number 2 hydrophone-Small Oscillator combination fathometer soundings and the corresponding vertical casts. Only a few of the comparisons taken were used, as a number were taken on a slope. Those on the left side of the table are for the



period from October 1 to November 21, and those on the right side are for the period after November 21. The long dash comparisons were so variable as to be unreliable, therefore the long dash comparisons listed on table B were used in every case where the long dash was used in sounding. This correction was taken as the difference between the average short dash I. C. and the average long dash I. C. for the number 3 hydrophone- big oscillator combination before November 21. This correction (-2.7 fathoms) is applied as an additional correction to every long dash sounding, the regular short dash correction being entered. For the number 2 hydrophone-small oscillator, this additional correction has been applied to the original curve, and the values tabulated in Table D.

TABLE D

Table D is the final table from which the reducers were entered in the sounding volumes, and is self-explanatory.

All the values are in fathoms except column 2 of Table A, which is in parts per thousand, and columns 3 and 4 of Table A, which are in meters per second.

TABLE A  
 FATHOMETER CORRECTIONS, SAN CLEMENTE ID.  
 No. 3 Hydrophone, Big Oscillator.

| Temp.<br>°C | True<br>Depth<br>Fms | Salin-<br>ity<br>o/oo | Theor.<br>Vel.<br>m/s | Mean<br>Vel.<br>m/s | D<br>Fms | Uniform<br>Scale<br>Rdg.<br>Fms | Non-unif<br>Scale<br>Rdg.<br>Fms | Theor.<br>Cor'n<br>Fms | Final<br>Cor'n<br>to 11/21<br>IC-0.9 | Final<br>Cor'n<br>after 11/21<br>IC 1.4 |
|-------------|----------------------|-----------------------|-----------------------|---------------------|----------|---------------------------------|----------------------------------|------------------------|--------------------------------------|---|
| 0           | 1                    | 2                     | 3                     | 4                   | 5        | 6                               | 7                                | 8                      | 9                                    | 10                                      |
| 16.0        | 2                    | 33.60                 | 1505.6                |                     |          |                                 |                                  |                        |                                      |   |
| 15.8        | 4                    |                       | 04.9                  | 1505.2              | 8.0      | 8.0                             | 7.7                              | -3.7                   | -4.6                                 |   |
| 15.7        | 6                    |                       | 04.7                  | 05.1                | 8.7      | 8.7                             | 8.3                              | -2.3                   | -3.2                                 |   |
| 15.4        | 8                    | .70                   | 03.9                  | 04.8                | 9.8      | 9.8                             | 9.6                              | -1.6                   | -2.5                                 | -0.2                                    |
| 14.9        | 10                   |                       | 02.4                  | 04.3                | 11.1     | 11.1                            | 11.0                             | -1.0                   | -1.9                                 | +0.4                                    |
| 14.0        | 12                   |                       | 1499.6                | 03.5                | 12.6     | 12.6                            | 12.5                             | -0.5                   | -1.4                                 | +0.9                                    |
| 13.1        | 14                   |                       | 96.6                  | 02.5                | 14.3     | 14.4                            | 14.3                             | -0.3                   | -1.2                                 | +1.1                                    |
| 12.5        | 16                   |                       | 94.7                  | 01.6                | 16.0     | 16.1                            | 16.0                             | 0.0                    | -0.9                                 | +1.4                                    |
| 12.0        | 18                   |                       | 92.9                  | 00.6                | 17.8     | 17.9                            | 17.8                             | +0.2                   | -0.7                                 | +1.6                                    |
| 11.8        | 20                   |                       | 92.2                  | 1499.8              | 19.6     | 19.8                            |                                  | 0.2                    | -0.7                                 | 1.6                                     |
| 11.5        | 24                   | .80                   | 91.5                  | 98.4                | 23.3     | 23.5                            |                                  | 0.5                    | -0.4                                 | 1.9                                     |
| 11.4        | 28                   |                       | 91.3                  | 97.4                | 27.1     | 27.4                            |                                  | 0.6                    | -0.3                                 | 2.0                                     |
| 11.4        | 32                   |                       | 91.4                  | 96.6                | 31.0     | 31.3                            |                                  | 0.7                    | -0.2                                 | 2.1                                     |
| 11.6        | 42                   | .90                   | 92.5                  | 95.6                | 40.7     | 41.1                            |                                  | 0.9                    | 0.0                                  | 2.3                                     |
| 11.5        | 52                   |                       | 92.6                  | 95.0                | 50.6     | 51.2                            |                                  | 0.8                    | -0.1                                 | 2.2                                     |
| 11.2        | 62                   |                       | 91.8                  | 94.5                | 60.5     | 61.2                            |                                  | 0.8                    | -0.1                                 | 2.2                                     |
| 10.7        | 72                   | 34.00                 | 90.5                  | 93.9                | 70.4     | 71.3                            |                                  | 0.7                    | -0.2                                 | 2.1                                     |
| 10.2        | 82                   |                       | 89.0                  | 93.3                | 80.4     | 81.4                            |                                  | 0.6                    | -0.3                                 | 2.0                                     |
| 9.8         | 92                   |                       | 87.9                  | 92.7                | 90.4     | 91.5                            |                                  | 0.5                    | -0.4                                 | 1.9                                     |
| 9.5         | 102                  |                       | 87.1                  | 92.1                | 100.3    | 101.5                           | 101.3                            | 0.7                    | -0.2                                 | 2.1                                     |
| 9.2         | 112                  | .10                   | 86.4                  | 91.6                | 110.3    | 111.8                           | 111.6                            | 0.4                    | -0.5                                 | 1.8                                     |
| 9.0         | 122                  |                       | 86.0                  | 91.1                | 120.2    | 121.9                           |                                  | 0.1                    | -0.8                                 | 1.5                                     |
| 8.5         | 142                  |                       | 84.8                  | 90.2                | 140.2    | 142.2                           |                                  | -0.2                   | -1.1                                 | 1.2                                     |
| 8.2         | 162                  | .20                   | 84.6                  | 89.5                | 160.2    | 162.5                           |                                  | -0.5                   | -1.4                                 | 0.9                                     |
| 7.9         | 182                  |                       | 84.0                  | 88.8                | 180.2    | 183.0                           |                                  | -1.0                   | -1.9                                 | 0.4                                     |
| 7.7         | 202                  |                       | 83.9                  | 88.4                | 200.2    | 203.0                           | 202.8                            | -0.8                   | -1.7                                 | 0.6                                     |
| 7.2         | 242                  | .30                   | 83.4                  | 87.6                | 240.2    | 244.1                           |                                  | -2.1                   | -3.0                                 | -0.7                                    |
| 6.7         | 282                  |                       | 82.7                  | 86.9                | 280.2    | 284.8                           |                                  | -2.8                   | -3.7                                 | -1.4                                    |
| 6.2         | 322                  |                       | 82.1                  | 86.3                | 320.2    | 325.4                           |                                  | -3.4                   | -4.3                                 | -2.0                                    |
| 5.8         | 362                  |                       | 81.8                  | 85.8                | 360.1    | 366.1                           |                                  | -4.1                   | -5.0                                 | -2.7                                    |
| 5.4         | 402                  |                       | 81.6                  | 85.4                | 400.1    | 407.0                           |                                  | -5.0                   | -5.9                                 | -3.6                                    |
| 5.1         | 442                  | .40                   | 81.7                  | 85.0                | 440.1    | 447.9                           |                                  | -5.9                   | -6.8                                 | -4.5                                    |
| 4.7         | 482                  |                       | 81.5                  | 84.7                | 480.1    | 488.9                           |                                  | -6.9                   | -7.8                                 | -5.5                                    |
| 4.4         | 522                  |                       | 81.5                  | 84.5                | 520.1    | 529.8                           |                                  | -7.8                   | -8.7                                 | -6.4                                    |
| 4.1         | 562                  |                       | 81.6                  | 84.3                | 560.1    | 570.6                           |                                  | -8.6                   | -9.5                                 | -7.2                                    |

Additional list to show correction over part of dial that is not uniform.

| Non-uniform<br>scale rdg. | Theor.<br>Cor'n. | Final Cor'n<br>to 11/21 | Final Cor'n<br>after 11/21 | Non-uniform<br>scale rdg. | Theor<br>Cor'n | Final Cor'n<br>to 11/21 | Final Cor'n<br>after 11/21 |
|---------------------------|------------------|-------------------------|----------------------------|---------------------------|----------------|-------------------------|----------------------------|
| 101                       | 0.7              | -0.2                    | 2.1                        | 201                       | -1.1           | -2.0                    | +0.3                       |
| 102                       | 0.8              | -0.1                    | 2.2                        | 202                       | -1.0           | -1.9                    | +0.4                       |
| 103                       | 0.9              | 0.0                     | 2.3                        | 203                       | -0.8           | -1.7                    | +0.6                       |
| 104                       | 1.0              | 0.1                     | 2.4                        | 204                       | -0.7           | -1.6                    | +0.7                       |
| 105                       | 1.0              | 0.1                     | 2.4                        | 206                       | -0.5           | -1.4                    | +0.9                       |
| 106                       | 1.0              | 0.1                     | 2.4                        | 208                       | -0.8           | -1.7                    | +0.6                       |
| 107                       | 0.9              | 0.0                     | 2.3                        | 209                       | -0.9           | -1.8                    | +0.5                       |
| 108                       | 0.8              | -0.1                    | 2.2                        | 210                       | -1.1           | -2.0                    | +0.3                       |
| 111.3                     | 0.4              | -0.5                    | 1.8                        | 212                       | -1.2           | -2.1                    | +0.2                       |
| 121.9                     | 0.1              | -0.8                    | 1.5                        |                           |                |                         |                            |

TABLE A CONTINUED  
 No. 2 Hydrohpane, Small Oscillator

| True Depth | D    | Uniform Scale Rdg. | Non-unif. Scale Rdg. | Theor. Cor'n. | Final Cor'n to 11/21 I.C. -1.8 | Final Cor'n after 11/21 I.C. 1.0 |
|------------|------|--------------------|----------------------|---------------|--------------------------------|----------------------------------|
| 2          | 11   | 12                 | 13                   | 14            | 15                             | 16                               |
| 4          | 2.8  | 2.8                | 2.4                  | 1.6           | -0.2                           | +2.6                             |
| 6          | 4.5  | 4.5                | 4.0                  | 2.0           | +0.2                           | 3.0                              |
| 8          | 6.3  | 6.3                | 5.7                  | 2.3           | 0.5                            | 3.3                              |
| 10         | 8.3  | 8.3                | 8.0                  | 2.0           | 0.2                            | 3.0                              |
| 12         | 10.2 | 10.3               | 10.1                 | 1.9           | 0.1                            | 2.9                              |
| 14         | 12.2 | 12.3               | 12.1                 | 1.9           | 0.1                            | 2.9                              |
| 16         | 14.1 | 14.2               | 14.1                 | 1.9           | 0.1                            | 2.9                              |
| 18         | 16.1 | 16.2               | 16.1                 | 1.9           | 0.1                            | 2.9                              |
| 20         | 18.1 | 18.2               | 18.1                 | 1.9           | 0.1                            | 2.9                              |
| 24         | 22.1 | 22.3               |                      | 1.7           | -0.1                           | 2.7                              |
| 28         | 26.1 | 26.3               |                      | 1.7           | -0.1                           | 2.7                              |
| 32         | 30.1 | 30.4               |                      | 1.6           | -0.2                           | 2.6                              |
| 42         | 40.1 | 40.5               |                      | 1.5           | -0.3                           | 2.5                              |
| 52         | 50.1 | 50.7               |                      | 1.3           | -0.5                           | 2.3                              |
| 62         | 60.1 | 60.8               |                      | 1.2           | -0.6                           | 2.2                              |
| 72         | 70.1 | 70.9               |                      | 1.1           | -0.7                           | 2.1                              |
| 82         | 80.1 | 81.1               |                      | 0.9           | -0.9                           | 1.9                              |
| 92         | 90.0 | 91.1               |                      | 0.9           | -0.9                           | 1.9                              |
| 102        | 100  | 101.3              | 101.1                | 0.9           | -0.9                           | 1.9                              |
| 112        | 110  | 111.5              | 111.4                | 0.6           | -1.2                           | 1.6                              |
| 122        | 120  | 121.7              |                      | 0.3           | -1.5                           | 1.3                              |
| 142        | 140  | 142                |                      | 0.0           | -1.8                           | 1.0                              |
| 162        | 160  | 162.3              |                      | -0.3          | -2.1                           | 0.7                              |
| 182        | 180  | 182.8              |                      | -0.8          | -2.6                           | 0.2                              |
| 202        | 200  | 203.1              | 202.9                | -0.9          | -2.9                           | 0.1                              |
| 242        | 240  | 243.9              |                      | -1.9          | -3.7                           | -0.9                             |
| 282        | 280  | 284.6              |                      | -2.6          | -4.4                           | -1.6                             |
| 322        | 320  | 325.2              |                      | -3.2          | -5.0                           | -2.2                             |
| 402        | 400  | 406.9              |                      | -4.9          | -6.7                           | -3.9                             |
| 362        | 360  | 366                |                      | -4.0          | -5.8                           | -3.0                             |
| 442        | 440  | 447.8              |                      | -5.8          | -7.4                           | -4.6                             |
| 482        | 480  | 488.8              |                      | -6.8          | -8.6                           | -5.8                             |
| 522        | 520  | 529.7              |                      | -7.7          | -9.5                           | -6.7                             |
| 562        | 560  | 570.5              |                      | -8.5          | -10.3                          | -7.5                             |

Additional list to show the corrections over part of the dial that is not uniform.

| Indicated depth (Non-uniform scale) | Theor. Cor'n. | Final Cor'n to Nov. 21; IC-1.8 | Final Cor'n after Nov. 21; IC 1.0 |
|-------------------------------------|---------------|--------------------------------|-----------------------------------|
| 101                                 | 0.9           | -0.9                           | 1.9                               |
| 102                                 | 1.0           | -0.8                           | 2.0                               |
| 103                                 | 1.1           | -0.7                           | 2.1                               |
| 104                                 | 1.2           | -0.6                           | 2.2                               |
| 105                                 | 1.2           | -0.6                           | 2.2                               |
| 106                                 | 1.2           | -0.6                           | 2.2                               |
| 108                                 | 1.0           | -0.8                           | 2.0                               |
| 110                                 | 0.7           | -1.1                           | 1.7                               |
| 111.5                               | 0.6           | -1.2                           | 1.6                               |
| 121.7                               | 0.3           | -1.5                           | 1.3                               |

TABLE B  
COMPARISON OF FATHOMETER READINGS WITH VERTICAL CASTS FOR  
INDEX CORRECTION

| No. 3 Hydrophone                         |              |              |       |        | Big Oscillator SHORT DASH      |              |              |       |        |
|--|--------------|--------------|-------|--------|--------------------------------|--------------|--------------|-------|--------|
| Before Nov. 21, 1933                     |              |              |       |        | On and after Nov. 21, 1933.    |              |              |       |        |
| Fath. Rdg.                               | Theor. Cor'n | Crt'd. Fath. | V.C.  | I.C.   | Fath. Rdg.                     | Theor. Cor'n | Crt'd. Fath. | V. C. | I.C.   |
| 25.4                                     | 0.5          | 25.9         | 25.1  | -0.8   | 9.6                            | -1.6         | 8.0          | 11.3  | (3.3)  |
| 25.4                                     | 0.5          | 25.9         | 24.9  | -1.0   | 9.5                            | -1.6         | 7.9          | 11.3  | (3.4)  |
| 40.0                                     | 0.9          | 40.9         | 39.6  | -1.3   | 35.5                           | 0.8          | 36.3         | 36.9  | 0.6    |
| 14.7                                     | -0.3         | 14.4         | 14.4  | 0.0    | 44.5                           | 0.9          | 45.4         | 46.2  | 0.8    |
| 39.3                                     | 0.9          | 40.2         | 39.1  | -1.1   | 11.5                           | -0.7         | 10.8         | 13.0  | (2.2)  |
| 17.3                                     | 0.2          | 17.5         | 16.9  | -0.6   | 9.0                            | -1.6         | 7.4          | 10.0  | (2.6)  |
| 36.3                                     | 0.8          | 37.1         | 35.8  | -1.3   | 9.8                            | -1.6         | 8.2          | 11.4  | (3.2)  |
| 45.7                                     | 0.9          | 46.6         | 45.4  | -1.2   | 12.0                           | -0.7         | 11.3         | 13.6  | (2.3)  |
| 47.0                                     | 0.8          | 47.8         | 46.4  | -1.4   | 30.5                           | 0.7          | 31.2         | 31.8  | 0.6    |
| 48.5                                     | 0.8          | 49.3         | 48.9  | -0.4   | 30.0                           | 0.7          | 30.7         | 31.5  | 0.8    |
| 60.6                                     | 0.8          | 61.3         | 63.2  | (1.9)  | 55.5                           | 0.8          | 56.3         | 57.8  | 1.5    |
| 39.2                                     | 0.9          | 40.1         | 38.6  | -1.5   | 55.0                           | 0.8          | 55.8         | 57.6  | 1.8    |
| 60.8                                     | 0.8          | 61.6         | 61.1  | -0.5   | 55.2                           | 0.8          | 56.0         | 57.5  | 1.5    |
| 60.1                                     | 0.8          | 60.9         | 60.9  | 0.0    | 45.1                           | 0.9          | 46.0         | 47.3  | 1.3    |
| 60.8                                     | 0.8          | 61.6         | 60.2  | -1.4   | 45.8                           | 0.9          | 46.7         | 47.3  | 0.6    |
| 59.8                                     | 0.8          | 60.6         | 60.0  | -0.6   | 35.0                           | 0.8          | 35.8         | 36.0  | 0.2    |
| 39.8                                     | 0.9          | 40.7         | 40.00 | -0.7   | 57.5                           | 0.8          | 58.3         | 60.0  | 1.7    |
| 40.0                                     | 0.9          | 40.9         | 39.8  | -1.1   | 42.5                           | 0.9          | 43.4         | 43.9  | 0.5    |
| 63.8                                     | 0.8          | 64.6         | 66.0  | (1.4)  | 29.8                           | 0.7          | 30.5         | 32.6  | 2.1    |
| 64.0                                     | 0.8          | 64.8         | 65.3  | (0.5)  | 30.5                           | 0.7          | 31.2         | 31.7  | 0.5    |
| 162                                      | -0.5         | 161.5        | 168.0 | (6.8)  | 24.2                           | 0.5          | 24.7         | 25.8  | 1.1    |
| 39.2                                     | 0.9          | 40.1         | 38.5  | -1.6   | 77.5                           | 0.6          | 78.1         | 79.0  | 0.9    |
| 346                                      | -3.8         | 342.2        | 345.3 | (3.1)  | 15.5                           | 0.1          | 15.6         | 16.2  | 0.6    |
| 337.5                                    | -3.7         | 333.8        | 336.5 | (2.7)  | 15.1                           | 0.1          | 15.2         | 16.1  | 0.9    |
| 49.5                                     | 0.8          | 50.3         | 49.5  | -0.8   | 18.0                           | 0.2          | 18.2         | 19.0  | 0.8    |
| 19.8                                     | 0.2          | 20.0         | 20.0  | 0.0    | 55.6                           | 0.8          | 56.4         | 57.5  | 1.1    |
| 39.8                                     | 0.9          | 40.7         | 39.3  | -1.4   | 52.5                           | 0.8          | 53.3         | 53.8  | 0.5    |
| 58.2                                     | 0.8          | 59.0         | 60.0  | +1.0   | 44.0                           | 0.9          | 44.9         | 46.4  | 1.5    |
| 159.8                                    | -0.4         | 159.4        | 168.0 | (8.6)  | 93.5                           | 0.5          | 94.0         | 91.7  | (-2.3) |
| 147.5                                    | -0.3         | 147.2        | 149.4 | (12.2) | 84.5                           | 0.6          | 85.1         | 83.2  | (-1.9) |
| 64                                       | 0.8          | 64.8         | 67.2  | (2.4)  | 30.5                           | 0.7          | 31.2         | 31.8  | 0.6    |
|  |              |              |       |        | 30.0                           | 0.7          | 30.7         | 31.5  | 0.8    |
| MEAN FOR INDEX CORRECTION -0.9           |              |              |       |        | 14.2                           | -0.3         | 13.9         | 16.0  | 2.1    |
|  |              |              |       |        | 14.0                           | -0.3         | 13.7         | 15.8  | 2.1    |
|  |              |              |       |        | 24.3                           | 0.5          | 24.8         | 25.8  | 1.0    |
|  |              |              |       |        | 24.5                           | 0.5          | 25.0         | 25.9  | 0.9    |
| -LONG DASH-                              |              |              |       |        | 11.2                           | -0.7         | 10.5         | 12.7  | 2.2    |
| 37.2                                     | 0.8          | 38.0         | 34.9  | -3.1   | 11.2                           | -0.7         | 10.5         | 12.6  | 2.1    |
| 38.0                                     | 0.8          | 38.8         | 34.9  | -3.9   | 11.5                           | -0.7         | 10.8         | 12.6  | 1.8    |
| 38.3                                     | 0.8          | 39.1         | 35.3  | -3.8   | 208                            | -1.2         | 206.8        | 208.8 | 2.0    |
| 38.8                                     | 0.8          | 39.6         | 34.4  | -4.2   | 49.5                           | 0.8          | 50.3         | 49.0  | (-1.3) |
| 28.0                                     | 0.6          | 28.6         | 25.1  | -3.1   | 114.5                          | 0.2          | 114.7        | 116.8 | 2.1    |
| 28.1                                     | 0.6          | 28.7         | 24.9  | -3.8   | 15.2                           | -0.2         | 15.0         | 17.8  | 2.8    |
| 42.6                                     | 0.9          | 43.5         | 39.6  | -3.9   | 15.5                           | -0.2         | 15.3         | 17.8  | 2.5    |
| 159.8                                    | -0.5         | 159.3        | 168.0 | (8.7)  | 59.1                           | 0.8          | 59.9         | 60.1  | 0.2    |
| 148.5                                    | -0.3         | 148.2        | 159.0 | (10.8) | 191.5                          | -1.1         | 190.4        | 191.4 | 1.0    |
| 346.0                                    | -3.7         | 342.3        | 345.3 | (3.0)  | 36.3                           | 0.8          | 37.1         | 37.8  | 0.7    |
| 337.5                                    | -3.6         | 333.9        | 336.5 | (2.6)  | 51.0                           | 0.8          | 51.8         | 53.4  | 1.6    |
| Mean for index correction 7) 25.8 (-3.6) |              |              |       |        | Mean for index correction +1.4 |              |              |       |        |
| I. C. -0.9                               |              |              |       |        |                                |              |              |       |        |
| -3.6                                     |              |              |       |        |                                |              |              |       |        |

Difference = -2.7 fms. which is to be added to all LONG DASH soundings as these comparisons are all that compare well enough for an index correction.

TABLE C.  
COMPARISON OF THE FATHOMETER READINGS WITH VERTICAL CASTS FOR INDEX CORRECTION  
SHORT DASH

| Before November 21, 1933  |              |             |       |        | On and after Nov. 21, 1933              |              |             |       |       |
|---------------------------|--------------|-------------|-------|--------|---|--------------|-------------|-------|-------|
| Fath. Rdg.                | Theor. Cor'n | Crtd. Fath. | V.C.  | I.C.   | Fath. Rdg.                              | Theor. Cor'n | Crtd. Fath. | V.C.  | I.C.  |
| 61.0                      | 1.2          | 62.2        | 61.1  | -1.1   | 52.5                                    | 1.3          | 53.8        | 53.4  | -0.4  |
| 61.2                      | 1.2          | 62.4        | 60.9  | -1.5   | 71.0                                    | 1.1          | 72.1        | 74.5  | 2.4   |
| 61.0                      | 1.2          | 62.2        | 60.2  | -2.0   | 209.0                                   | -1.2         | 207.8       | 208.8 | 1.0   |
| 60.5                      | 1.2          | 61.7        | 60.0  | -1.7   | 420.0                                   | -5.2         | 414.8       | 419.8 | (5.0) |
| 81.7                      | 0.9          | 82.6        | 81.2  | -1.4   |   |              |             |       |       |
| 97.0                      | 0.8          | 97.8        | 95.2  | -2.6   |   |              |             |       |       |
| 102.0                     | 0.7          | 102.7       | 99.9  | (-2.8) |   |              |             |       |       |
| 115.5                     | 0.4          | 114.9       | 117.9 | (2.0)  |   |              |             |       |       |
| 118.0                     | 0.3          | 118.3       | 116.3 | -2.0   |   |              |             |       |       |
|                           |              |             |       | 7)12.3 |   |              |             |       |       |
| Mean for Index Correction |              |             |       | -1.8   | 3)3.0<br>Mean for index correction +1.0 |              |             |       |       |

The following comparisons were not used for the I.C. as they were taken on a slope.

|       |      |       |       |      |
|-------|------|-------|-------|------|
| 143.5 | 0.0  | 143.5 | 148.2 | 4.7  |
| 145.0 | 0.0  | 145.0 | 147.5 | 2.5  |
| 145.8 | 0.0  | 145.8 | 147.5 | 1.7  |
| 148.0 | -0.1 | 147.9 | 148.2 | 0.3  |
| 151.0 | -0.2 | 150.8 | 159.4 | 8.6  |
| 161.5 | -0.3 | 161.2 | 168.0 | 6.8  |
| 248.0 | -1.9 | 246.1 | 248.0 | 1.9  |
| 348.9 | -3.8 | 345.1 | 353.0 | 7.9  |
| 380.0 | -4.4 | 375.6 | 376.5 | 0.9  |
| 535.0 | -7.8 | 527.2 | 550.0 | 22.8 |

LONG DASH

|                       |      |       |         |        |
|-----------------------|------|-------|---------|--------|
| 101.0                 | 0.7  | 101.7 | 95.2    | (-6.5) |
| 117.0                 | 0.3  | 117.3 | 117.9   | 0.6    |
| 148.0                 | -0.1 | 147.9 | 147.5   | -0.4   |
| 152.0                 | -0.2 | 151.8 | 159.0   | 7.2    |
| 157.0                 | -0.2 | 156.8 | 168.0   | 11.2   |
| 161.0                 | -0.3 | 160.7 | 168.0   | 7.3    |
| 228.0                 | -1.5 | 226.5 | 223.4   | -3.1   |
| 224.0                 | -1.4 | 222.6 | 223.5   | 0.9    |
| 248.0                 | -1.9 | 246.1 | 248.0   | 1.9    |
| 251.0                 | -2.0 | 249.0 | 248.0   | -1.0   |
| 265.0                 | -2.2 | 262.8 | 273.3   | 10.5   |
| 307.0                 | -3.0 | 304.0 | 306.2   | 2.2    |
| 337.0                 | -3.4 | 333.6 | 336.5   | 2.9    |
| 343.0                 | -3.6 | 339.4 | 353.0   | 13.6   |
| 345.5                 | -3.6 | 331.9 | 345.3   | 13.4   |
| 380.0                 | -4.4 | 375.6 | 376.5   | 0.9    |
| 537.0                 | -8.0 | 529.0 | 550.0   | (21.0) |
| 422.0                 | -5.2 | 416.8 | 419.8   | 3.0    |
|                       |      |       | 16)72.1 |        |
| Mean Index correction |      |       |         | 4.5    |

These Long Dash Comparisons not used. The ones on Table B are used in every case where the Long Dash was used. The difference between the Long Dash and the Short Dash was 2.7 fathoms and the Long Dash gave soundings that were too deep. Therefore, an additional correction of -2.7 fathoms must be made in each case where the Long Dash was used.

## FINAL FATHOMETER CORRECTIONS

Big Oscillator - Number 3 Hydrophone  
Before November 21, 1933

| Short Dash     |                     | Long Dash      |                     |
|----------------|---------------------|----------------|---------------------|
| Depth<br>(Fms) | Correction<br>(Fms) | Depth<br>(Fms) | Correction<br>(Fms) |
| 10 - 11        | -2                  | 11 - 15        | -4                  |
| 11.1 - 12.9    | -1 $\frac{1}{2}$    | 15.1 - 21      | -3 $\frac{1}{2}$    |
| 13 - 17        | -1                  | 21.1 - 32      | -3                  |
| 17.1 - 25.9    | -1 $\frac{1}{2}$    | 32.1 - 57      | -2 $\frac{1}{2}$    |
| 26.0 - 80      | 0                   | 58 - 102       | -3                  |
| 80.1 - 100     | -1 $\frac{1}{2}$    | 103 - 108      | -2 $\frac{1}{2}$    |
| 100 - 109      | 0                   | 109 - 112      | -3                  |
| 110 - 112      | -1 $\frac{1}{2}$    | 113 - 140      | -3 $\frac{1}{2}$    |
| 113 - 150      | -1                  | 141 - 172      | -4                  |
| 151 - 210      | -2                  | 173 - 210      | -4 $\frac{1}{2}$    |
| 211 - 260      | -3                  | 211 - 222      | -5                  |
| 261 - 322      | -4                  | 223 - 275      | -6                  |
| 323 - 379      | -5                  | 276 - 345      | -7                  |
| 380 - 425      | -6                  | 346 - 390      | -8                  |
| 426 - 470      | -7                  | 391 - 435      | -9                  |
| 471 - 515      | -8                  | 436 - 479      | -10                 |
| 516 - 560      | -9                  | 480 - 525      | -11                 |
| 561 - 605      | -10                 |                |                     |

After November 21, 1933. *to May 14 1934*

|            |                  |
|------------|------------------|
| 9.5 - 10   | 0                |
| 10.1 - 11  | +1 $\frac{1}{2}$ |
| 11.1 - 14  | +1               |
| 14.1 - 21  | +1 $\frac{1}{2}$ |
| 21.1 - 102 | +2               |
| 103 - 166  | +1               |
| 167 - 224  | 0                |
| 225 - 278  | -1               |
| 279 - 343  | -2               |
| 344 - 389  | -3               |
| 390 - 435  | -4               |
| 436 - 480  | -5               |

NONE

Note: For sheet 13, +1.4 fms. was used up to 25 fms. See attached abstract of vertical casts.

Note: For LONG DASH soundings after November 21, apply an additional correction of minus (-) 2.7 fms. Long dash was too deep by this amount.

For FRX6 soundings throughout the period covered by these corrections, apply an additional correction of plus (+) 7.0 fms.

FINAL FATHOMETER CORRECTIONS  
Small Oscillator - Number 2 Hydrophone.

Before November 21, 1933.

| Short Dash     |                | Long Dash.     |            |
|----------------|----------------|----------------|------------|
| Depth<br>(Fms) | Correction     | Depth<br>(Fms) | Correction |
| 10 - 34        | 0              | 50 - 125       | -4         |
| 35 - 70        | $-\frac{1}{2}$ | 126 - 180      | -5         |
| 71 - 102       | -1             | 181 - 237      | -6         |
| 103 - 107      | $-\frac{1}{2}$ | 238 - 293      | -7         |
| 108 - 111      | -1             | 294 - 350      | -8         |
| 112 - 165      | -2             | 351 - 402      | -9         |
| 166 - 220      | -3             | 403 - 454      | -10        |
| 221 - 277      | -4             |                |            |
| 278 - 335      | -5             |                |            |
| 336 - 388      | -6             |                |            |
| 389 - 442      | -7             |                |            |
| 443 - 482      | -8             |                |            |
| 483 - 518      | -9             |                |            |

After November 21, 1933.

|           |                  |           |     |    |
|-----------|------------------|-----------|-----|----|
| 10 - 21   | +3               | ---       | 115 | -1 |
| 22 - 52   | +2 $\frac{1}{2}$ | 116 - 170 |     | -2 |
| 53 - 109  | +2               | 171 - 225 |     | -3 |
| 110 - 125 | +1 $\frac{1}{2}$ | 226 - 282 |     | -4 |
| 126 - 154 | +1               | 283 - 338 |     | -5 |
| 155 - 181 | + $\frac{1}{2}$  | 339 - 390 |     | -6 |
| 182 - 212 | 0                |           |     |    |
| 213 - 267 | -1               |           |     |    |
| 268 - 323 | -2               |           |     |    |
| 324 - 377 | -3               |           |     |    |
| 378 - 428 | -4               |           |     |    |
| 429 - 472 | -5               |           |     |    |
| 473 - 510 | -6               |           |     |    |
| 511 - 558 | -7               |           |     |    |

Note: For FRx6 soundings throughout the period covered by these corrections, apply an additional correction of plus (+) 7.0 fathoms.

## FATHOMETER CORRECTIONS

For period from May 14th to May 31st, 1934.

Sheets Nos. 25, 26, and 47.

The temperature and salinity curves used to obtain the theoretical fathometer corrections are attached to this report. The temperatures were obtained during the period and in the area for which they are applied. The data for the salinity curves was obtained in adjacent areas during the previous season. It has been found that there is not enough seasonal change in salinity to affect the results appreciably.

Table 1 shows the method of computation of average velocities to various depths. Depths are listed in column 7. Salinities and temperatures corresponding to the depths of column 7 are shown in columns 5 and 6 respectively and are taken from the accompanying curves. The velocities in column 1 are taken from table 2 of the British Admiralty Tables of the Velocity of Sound in Sea Water. The pressure corrections in column 2 and the salinity corrections in column 3 were taken from tables 4 and 3 of the same publication. In column 4 are the algebraic sums of columns 1, 2, and 3, which are the velocities corresponding to the depths in column 7. In column 8 are the average velocities from the surface to the depth in column 7. The average velocities at the bottom of the table for depths less than 100 fathoms were obtained by linear interpolation in the first part of the table.

Table 2 shows the method of computation of the theoretical fathometer corrections for the two base lines-- hydrophone to the big oscillator and hydrophone to the small oscillator. The theoretical corrections are obtained as follows. Let the distance between hydrophone and oscillator be  $2b$  and the depth from surface to the floor of ocean be  $d$ . The hydrophones on oscillators are all 2 fathoms below the water line. Then the distance traveled by the sound from oscillator to the floor of the ocean is

$(d-2)^2 + b^2$ , neglecting the progress of the ship. (This is the hypotenuse of the right triangle whose two legs are half the length of the base line and the depth of the ocean below the base line.) The time  $t$  taken by the sound to travel from oscillator to bottom to hydrophone is then

$$t = \frac{2 \sqrt{(d-2)^2 + b^2}}{V}$$

when  $V$  is the average velocity (col. 2)

If the fathometer makes  $n$  revolutions per second, then the fathometer reading is given by  $100nt$  since the dial is graduated into 100 divisions. The values of  $(d-2)^2 + b^2$  are given in column 3 of table 2 for the big oscillator, and in column 6 for the small oscillator, with the fathometer readings in columns 4 and 7 respectively. Since the average velo-



cities in column 2 are expressed in meters and the distances are in fathoms, the conversion factor enters. The fathometer speed was 247.6 revolutions per minute when the

$$\text{Fathometer reading} = \frac{2 \sqrt{(d-2)^2 + b^2}}{V} \quad 1.8288 \frac{247.6}{60} 100 =$$

$$1509 \frac{\sqrt{(d-2)^2 + b^2}}{V} .$$

The difference between the actual depth and the fathometer reading is the theoretical correction and is shown in columns 5 and 8. The Theoretical corrections are plotted on an accompanying graph.

Non-uniformity of the fathometer scale does not enter as no soundings less than 15 fathoms were made during the period, and for depths greater than 100 fathoms the error is less than 1%.

Index corrections were obtained from vertical cast comparison under 150 fathoms. The data are shown in tables 3 and 4.

The final fathometer correction is then the algebraic sum of the theoretical and index corrections.



TABLE 2.

Sheet 25, 26, 47

After May 14th, 1934.

| 1                  | 2                            | 3                                  | 4                         | 5                               | 6                                  | 7                         | 8                                |
|--------------------|------------------------------|------------------------------------|---------------------------|---------------------------------|------------------------------------|---------------------------|----------------------------------|
| Depth (d)<br>(Fms) | Average<br>Velocity<br>m/sec | #3 Hydro.                          | Big Oscillator            |                                 | #2 Hydro.                          | Small Oscillator          |                                  |
|                    |                              | $\frac{1}{2}$ Distance<br>Traveled | Fath.<br>Reading<br>(Fms) | $\pi$ . Fath.<br>Corr.<br>(Fms) | $\frac{1}{2}$ Distance<br>Traveled | Fath.<br>Reading<br>(Fms) | $\pi$ . Fath.<br>C orr.<br>(Fms) |
| 2                  |                              | 8.00                               | 7.97                      | -5.97                           |                                    |                           |                                  |
| 27                 | 1507                         | 26.3                               | 26.3                      | +0.7                            | 25.1                               | 25.1                      | +1.9                             |
| 52                 | 1501                         | 50.6                               | 50.9                      | +1.1                            | 50.04                              | 50.3                      | +1.7                             |
| 77                 | 1498                         | 75.5                               | 76.0                      | +1.0                            | 75.03                              | 75.6                      | +1.4                             |
| 102                | 1495                         | 100.4                              | 101.3                     | +0.7                            | 100.02                             | 101.0                     | +1.0                             |
| 127                | 1493                         | 125.4                              | 126.7                     | +0.3                            | 125                                | 126.3                     | +0.7                             |
| 152                | 1492                         | 150.3                              | 152.0                     | 0                               | 150                                | 151.7                     | +0.3                             |
| 177                | 1491                         | 175.3                              | 177.5                     | -0.5                            | 175                                | 177.2                     | -0.2                             |
| 202                | 1490                         | 200.2                              | 202.7                     | -0.7                            | 200                                | 202.5                     | -0.5                             |
| 252                | 1488                         | 250                                | 253.7                     | -1.7                            | 250                                | 253.6                     | -1.6                             |
| 302                | 1488                         | 300                                | 304.4                     | -2.4                            | 300                                | 304.4                     | -2.4                             |
| 352                | 1488                         | 350                                | 355.4                     | -3.4                            | 350                                | 355.4                     | -3.4                             |
| 402                | 1487                         | 400                                | 406.3                     | -4.3                            | 400                                | 406.3                     | -4.3                             |
| 452                | 1486                         | 450                                | 457.3                     | -5.3                            | 450                                | 457.3                     | -5.3                             |
| 502                | 1486                         | 500                                | 508.2                     | -6.2                            | 500                                | 508.2                     | -6.2                             |
| 552                | 1486                         | 550                                | 559                       | -7                              | 550                                | 559                       | -7                               |
| 602                | 1486                         | 600                                | 610                       | -8                              | 600                                | 610                       | -8                               |
| 652                | 1486                         | 650                                | 660.4                     | -8.4                            | 650                                | 660.4                     | -8.4                             |
| 702                | 1486                         | 700                                | 711.4                     | -9.4                            | 700                                | 711.4                     | -9.4                             |
| 752                | 1486                         | 750                                | 762.3                     | -10.3                           | 750                                | 762.3                     | -10.3                            |
| 802                | 1486                         | 800                                | 813                       | -11                             | 800                                | 813                       | -11                              |
| 852                | 1486                         | 850                                | 864                       | -12                             | 850                                | 864                       | -12                              |
| 902                | 1486                         | 900                                | 914                       | -12                             | 900                                | 914                       | -12                              |
| 7                  | 1513                         | 9.43                               | 9.41                      | -2.41                           |                                    |                           |                                  |
| 12                 | 1512                         | 12.81                              | 12.78                     | -0.78                           |                                    |                           |                                  |
| 17                 | 1510                         | 17.0                               | 17.0                      | 0                               | 15.15                              | 15.14                     | +1.86                            |
| 22                 | 1508                         | 21.6                               | 21.6                      | +0.4                            | 20.1                               | 20.1                      | +1.9                             |
| 32                 | 1506                         | 31.1                               | 31.2                      | +0.8                            | 30.1                               | 30.16                     | +1.84                            |
| 42                 | 1503                         | 40.9                               | 41.1                      | +0.9                            | 40.0                               | 40.2                      | +1.8                             |
| 62                 | 1500                         | 60.6                               | 61.0                      | +1.0                            | 60.03                              | 60.4                      | +1.6                             |
| 72                 | 1499                         | 70.5                               | 71.0                      | +1.0                            | 70.03                              | 70.5                      | +1.5                             |
| 82                 | 1497                         | 80.5                               | 81.1                      | +0.9                            | 80.03                              | 80.7                      | +1.3                             |
| 92                 | 1496                         | 90.5                               | 90.2                      | +0.8                            | 90.02                              | 90.8                      | +1.2                             |

COMPUTATION OF INDEX CORRECTION  
FOR SHEETS 25, 26, and 47.

AFTER MAY 14, 1934.

TABLE 3

| NO. 3 Hyd. Big Oscillator - F. R. - Short Dash |          |       |            |                   |                  |
|--|----------|-------|------------|-------------------|------------------|
| Sheet  | Position | V° C. | Fathometer | Theor. Correction | Index Correction |
| 25   | 1E       | 141.1 | 141.5      | + 0.1             | - 0.5            |
| 25   | 5E       | 50.0  | 50.3       | + 1.0             | - 1.3            |
| 25   | 21E      | 50.5  | 50.5       | + 1.0             | - 1.0            |
| 25   | 23E      | 41.8  | 41.6       | + 0.9             | - 0.7            |
| 25   | 57E      | 131.1 | 131.5      | + 0.3             | - 0.7            |

Average I. C. = - 1.0 fathoms (.84)

TABLE 4

| No. 2 Hyd. Small Oscillator - F. R. - Short Dash |          |       |            |                   |                  |
|--|----------|-------|------------|-------------------|------------------|
| Sheet  | Position | V° C. | Fathometer | Theor. Correction | Index Correction |
| 25   | 1E       | 141.1 | 143.0      | + 0.4             | - 2.5            |
| 25   | 5E       | 50.0  | 51.0       | + 1.7             | - 2.7            |
| 25   | 23E      | 41.8  | 43.0       | + 1.8             | - 2.0            |
| 25   | 52E      | 29.9  | 72.5       | + 1.5             | - 4.1 R          |
| 25   | 53E      | 107.0 | 107.0      | + 1.0             | - 1.0            |
| 26   | 74H      | 50.0  | 50.5       | + 1.7             | - 2.2            |

Average I. C. = - 2.0 fathoms (rejecting the - 4.1)

No. 2 Hyd. Small Oscillator - F. R. - Long Dash

Average of 9 comparisons on Sheet 47 of No. 2 Small, Short Dash, and No. 2 Small, Long Dash, show the long dash reads 1-1/2 fathoms higher than short dash. See abstract of vertical cast comparisons.

Average I. C.  $2\frac{1}{2}$  fathoms.

No. 2 Hyd. Small Oscillator - F.R.x6

Average of 30 comparisons (Sheets 25 and 47) of No. 2 Small, Long Dash, and No. 2 Small, F.R.x6 show the F.R.x6 reads  $1\frac{1}{2}$  fathoms higher than the Long Dash. Two differences of the 30 rejected. Sheet 26 average: 0 but if ~~the~~ 7 of the 23 comparisons on Sheet 26 are rejected, the average for Sheet 26 is also  $1\frac{1}{2}$ . See abstract of vertical cast comparisons.

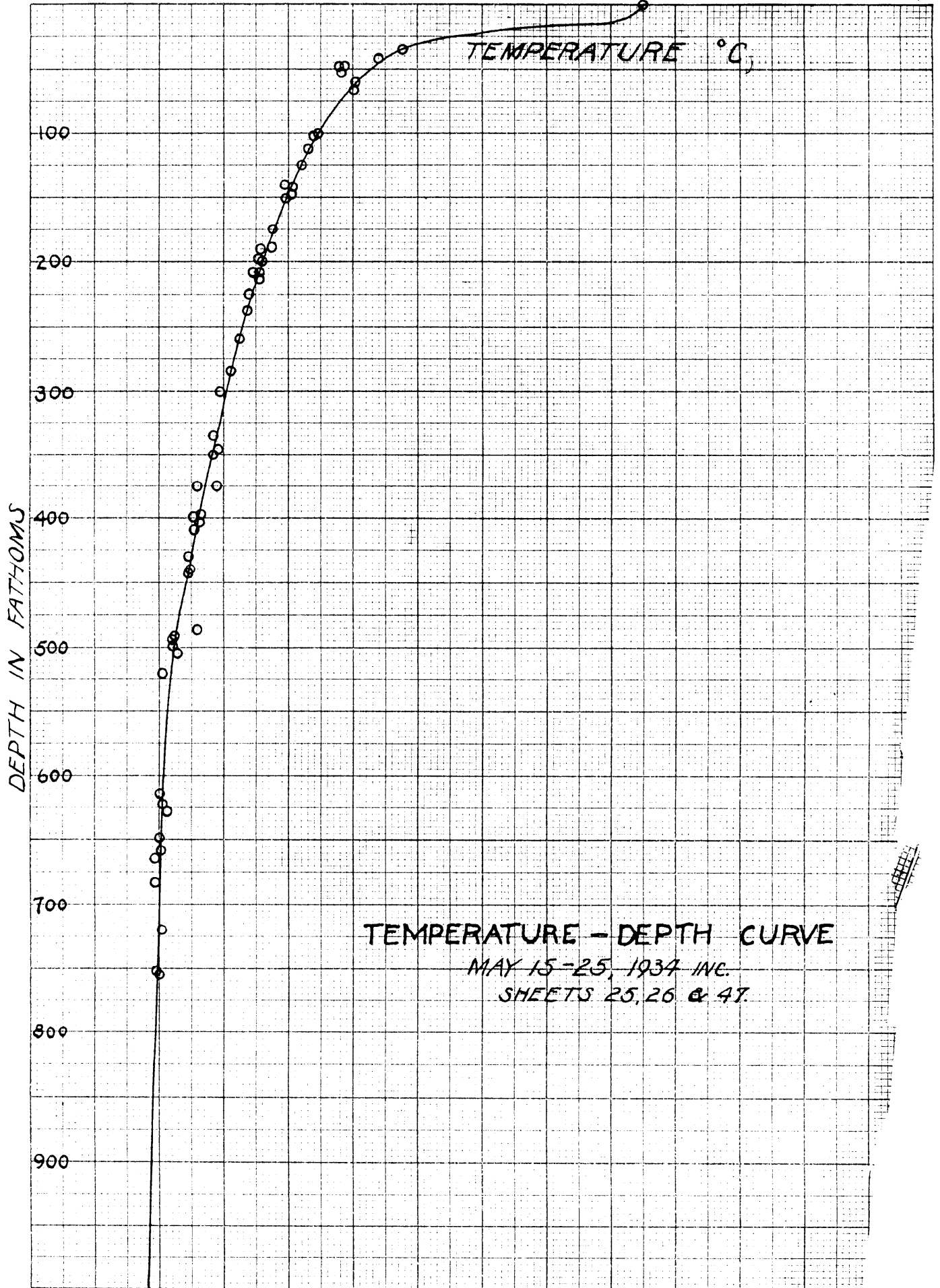
Average I. C. = - 4 fathoms.

FATHOMETER CORRECTIONS - AFTER MAY 16, 1934.

Sheets Nos 25, 26, & 47.

| No. 3 Hyd. Big Osc.    |                 | No. 2 hydrophone Small Oscillator |       |                        |                 |                                     |                  |
|------------------------|-----------------|-----------------------------------|-------|------------------------|-----------------|-------------------------------------|------------------|
| Short Dash             |                 | F.R. x 6                          |       | Short Dash             |                 | Long Dash                           |                  |
| Depth                  | Corr.           | Depth                             | Corr. | Depth                  | Corr.           | Depth                               | Corr.            |
| 18 - 31 $\frac{1}{2}$  | - $\frac{1}{2}$ | 104 - 120                         | -4    | 15 - 40                | 0               | 15 - 40                             | -1 $\frac{1}{2}$ |
| 32 - 92                | 0               | 121 - 165                         | -5    | 40 $\frac{1}{2}$ - 90  | - $\frac{1}{2}$ | 40 $\frac{1}{2}$ - 87 $\frac{1}{2}$ | -2               |
| 93 - 100 $\frac{1}{2}$ | - $\frac{1}{2}$ | 166 - 235                         | -6    | 90 $\frac{1}{2}$ - 120 | -1              | 88 - 100 $\frac{1}{2}$              | -2 $\frac{1}{2}$ |
| 101 - 165              | -1              | 236 - 285                         | -7    | 121 - 165              | -2              | 101 - 155                           | -3               |
| 166 - 235              | -2              | 286 - 345                         | -8    | 166 - 235              | -3              | 156 - 210                           | -4               |
| 236 - 285              | -3              | 346 - 400                         | -9    | 236 - 285              | -4              | 211 - 264                           | -5               |
| 286 - 345              | -4              | 401 - 450                         | -10   | 286 - 345              | -5              | 265 - 319                           | -6               |
| 346 - 400              | -5              | 451 - 505                         | -11   | 346 - 400              | -6              | 320 - 370                           | -7               |
| 401 - 450              | -6              | 506 - 565                         | -12   | 401 - 450              | -7              | 371 - 424                           | -8               |
| 451 - 505              | -7              | 566 - 625                         | -13   | 451 - 505              | -8              | 425 - 475                           | -9               |
| 506 - 565              | -8              | 626 - 685                         | -14   | 506 - 565              | -9              | 476 - 534                           | -10              |
| 566 - 625              | -9              | 686 - 750                         | -15   | 566 - 625              | -10             | 535 - 595                           | -11              |
| 626 - 685              | -10             |                                   |       | 626 - 685              | -11             | 596 - 659                           | -12              |
| 686 - 750              | -11             |                                   |       | 686 - 750              | -12             | 660 - 715                           | -13              |
|                        |                 |                                   |       |                        |                 | 716 - 780                           | -14              |

0 2 4 6 8 10 12 14 16 18 20



TEMPERATURE - DEPTH CURVE

MAY 15-25, 1934 INC.

SHEETS 25, 26 & 47.

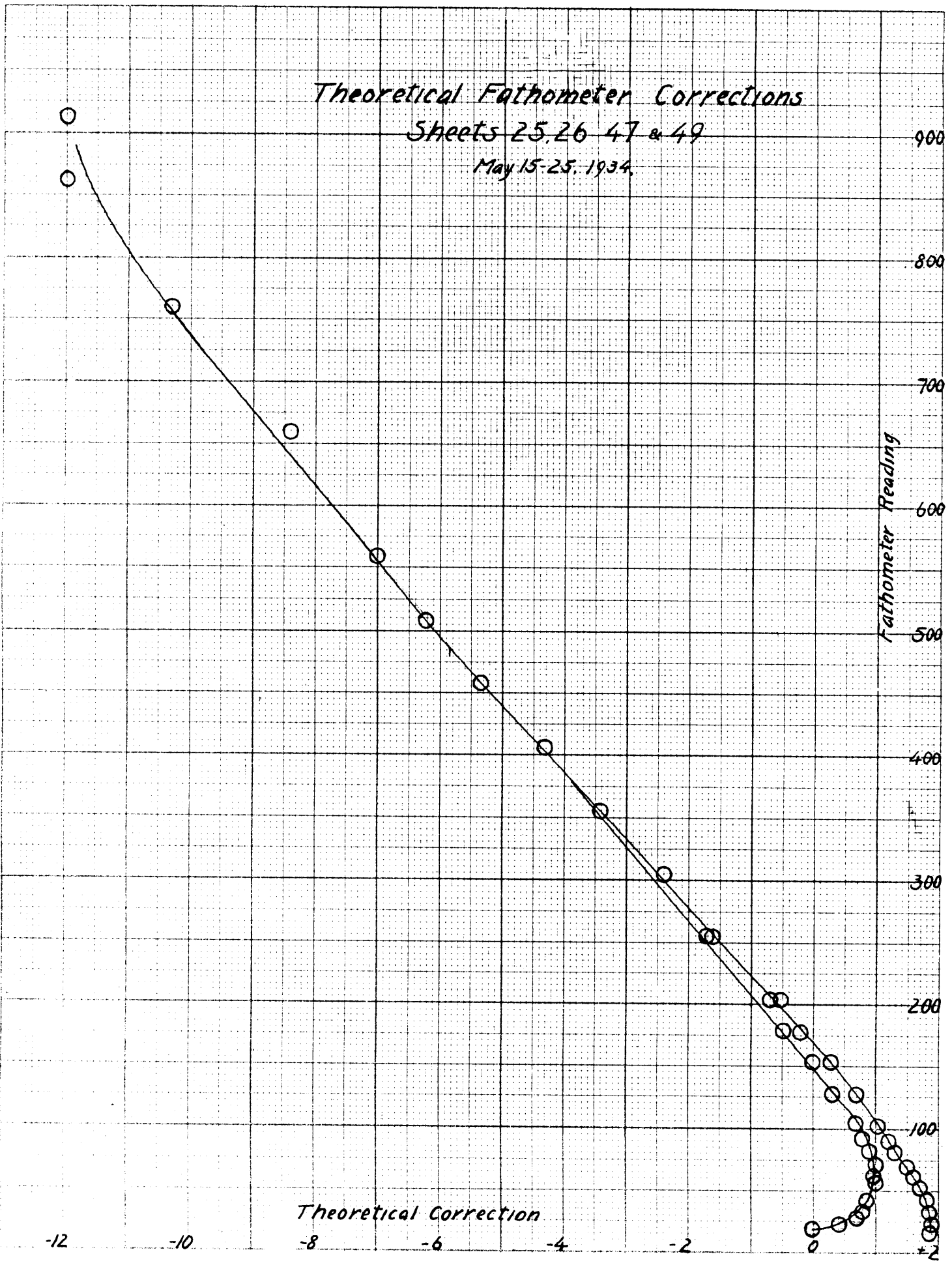
# Theoretical Fathometer Corrections

Sheets 25, 26, 47 & 49

May 15-25, 1934.

Fathometer Reading

Theoretical Correction



ABSTRACT OF VERTICAL CASTS WITH APPLICATION OF SLOPE CORRECTION  
Sheet No. 25.

| Date 1933 | Pos.  | Hydrophone & Oscillator used. | Fath. Rng. | Fath. Cor'n.    | Crt'd. Fath. Sndg. | Slope Cor'n. | Crt'd. Fath. Sdg. + Slope Cor'n. | V. C. | *  |
|-----------|-------|-------------------------------|------------|-----------------|--------------------|--------------|----------------------------------|-------|----|
| 10/24     | 1A    | #3 Big FRSD                   | 45.7       | 0               | 45.7               | 0            | 45.7                             | 45.4  |    |
|           | 2A    | " "                           | 47         | 0               | 47                 | 0            | 47                               | 46.4  |    |
| 1/4/34    | 54B   | #2 Sml "                      | 261        | -1              | 260                | 0(+3%)       | 260                              | 272   | 12 |
|           | 54B   | " FRx6                        | 255        | +6              | 261                | 0(+3%)       | 261                              | 272   | 12 |
|           | 100B  | " SD                          | 171.5      | + $\frac{1}{2}$ | 172                | 0            | 172                              | 171.6 |    |
| 1/5       | 152C  | " "                           | 439        | -5              | 434                | +17          | 451                              | 450   | 8  |
|           | 152C  | " LD                          | 441        | -7              | 434                | +17          | 451                              | 450   | 8  |
|           | 152C  | " FRx6                        | 435        | +2              | 437                | +17          | 454                              | 450   | 8  |
|           | 190C  | " SD                          | 366        | -3              | 363                | +7           | 370                              | 368   | 8  |
|           | 190C  | " LD                          | 366        | -6              | 360                | +7           | 367                              | 368   | 8  |
|           | 190C  | " FRx6                        | 360        | +4              | 364                | +7           | 371                              | 368   | 8  |
| 1/6       | 28D   | " SD                          | 504        | -6              | 498                | 0            | 498                              | 504   |    |
|           | 28D   | " LD                          | 507        | -9              | 498                | 0            | 498                              | 504   |    |
|           | 28D   | " FRx6                        | 502        | +1              | 503                | 0            | 503                              | 504   |    |
|           | 55D   | " SD                          | 554        | -7              | 547                | 0            | 547                              | 547   |    |
|           | 55D   | " LD                          | 556        | -10             | 546                | 0            | 546                              | 547   |    |
|           | 55D   | " FRx6                        | 548        | 0               | 548                | 0            | 548                              | 547   |    |
|           | 102D  | " SD                          | 150        | +1              | 151                | 0            | 151                              | 149   |    |
|           | 102D  | " LD                          | 153        | -2              | 151                | 0            | 151                              | 149   |    |
|           | 102D  | " FRx6                        | 143        | +8              | 151                | 0?           | 151                              | 149   |    |
|           | 102+D | " SD                          | 150        | +1              | 151                | 0?           | 151                              | 158   |    |
|           | 102+D | " LD                          | 151        | -2              | 149                | 0?           | 149                              | 158   |    |
|           | 102+D | " SD                          | 141        | +1              | 142                | 0?           | 142                              | 155   |    |
|           | 102+D | " LD                          | 142        | -2              | 140                | 0?           | 140                              | 155   |    |
|           | 102+D | " FRx6                        | 136        | +8              | 144                | 0?           | 144                              | 155   |    |
|           | 101D  | " SD                          | 127        | +1              | 128                | 0(+10%)      | 128                              | 141   | 31 |
|           | 101D  | " LD                          | 129        | -2              | 127                | 0(+10%)      | 127                              | 141   | 31 |
| 5/15      | 1E    | " SD                          | 143        | -2              | 141                | 0            | 141                              | 141   |    |
|           | 1E    | #4 Big "                      | 142        | -1              | 141                | 0            | 141                              | 141   |    |
|           | 5E    | #2 Sml "                      | 51         | - $\frac{1}{2}$ | 50.5               | 0            | 50.5                             | 50    |    |
|           | 5E    | #4 Big "                      | 50.3       | 0               | 50.3               | 0            | 50.3                             | 50    |    |
|           | 5+E   | #2 Sml "                      | 51         | - $\frac{1}{2}$ | 50.5               | 0            | 50.5                             | 50    |    |
|           | 9E    | " "                           | 104        | -1              | 103                | 0(+2%)       | 103                              | 107   | 32 |
|           | 21E   | #4 Big "                      | 50.5       | 0               | 50.5               | 0            | 50.5                             | 50.5  |    |

\* Difference between V. C. and fathometer sounding for critical slope at which correction for slope ~~is~~ first applied.

*would be*



ABSTRACT OF VERTICAL CASTS WITH APPLICATION OF SLOPE CORRECTION  
 Sheet No. 25. C ontinued

| Date<br>1934 | Pos.          | Hydrophone<br>&<br>Oscillator<br>used. | Fath.<br>Rdng. | Fath.<br>Cor'n. | Crt'd.<br>Fath.<br>Sndg. | Slope<br>Cor'n. | Crt'd.<br>Fath. Sdg.<br>+ Slope<br>Cor'n. | V. C.           | *   |
|--------------|---------------|--|----------------|-----------------|--------------------------|-----------------|---|-----------------|-----|
| 5/15         | 23E           | #2 Sml FRSD                            | 42             | - $\frac{1}{2}$ | 41.5                     | 0               | 41.5                                      | 41.8            |     |
|              | 23E           | #4 Big "                               | 41.6           | 0               | 41.6                     | 0               | 41.6                                      | 41.8            |     |
|              | 35E           | #2 Sml "                               | 388            | -6              | 382                      | 0               | 382                                       | 377             |     |
|              | 35E           | #4 Big "                               | 390            | -5              | 385                      | 0               | 385                                       | 377             |     |
|              | 43E           | #2 Sml "                               | 234            | -3              | 231                      | 0(+2%)          | 231                                       | 238             | 16  |
|              | 43E           | " LD                                   | 238            | -5              | 233                      | 0(+2%)          | 233                                       | 238             | 16  |
|              | 43E           | #4 Big SD                              | 233            | -2              | 231                      | 0(+2%)          | 231                                       | 238             | 16  |
|              | 52E           | #2 Sml "                               | 72.5           | - $\frac{1}{2}$ | 72                       | 0               | 72  | 69.9            |     |
|              | 53E           | " "                                    | 107            | -1              | 106                      | 0               | 106                                       | 107             |     |
|              | 54E           | " "                                    | 245            | -4              | 241                      | +14             | 256                                       | 244             | 16  |
|              | 54E           | #4 Big "                               | 246            | -3              | 243                      | +15             | 258                                       | 244             | 16  |
|              | 55E           | #2 Sml "                               | 223            | -3              | 220                      | +9              | 229                                       | 220             | 18  |
|              | 55E           | #4 Big "                               | 220            | -2              | 218                      | +9              | 227                                       | 220             | 18  |
|              | 56E           | #2 Sml "                               | 116            | -1              | 115                      | 0               | 115                                       | 118             |     |
|              | 57E           | " "                                    | 130            | -2              | 128                      | 0               | 128                                       | 131             |     |
|              | 57E           | #4 Big "                               | 132            | -1              | 131                      | 0               | 131                                       | 131             |     |
|              | 62E           | #2 Sml "                               | 181            | -3              | 178                      | +20             | 198                                       | 202             | 20  |
|              | 62E           | #2 Sml FRx6                            | 175            | -6              | 169                      | +20             | 189                                       | 202             | 20  |
|              | 62E           | #5 Big SD                              | 176            | -2              | 174                      | +20             | 194                                       | 202             | 20  |
|              | 63E           | #2 Sml "                               | 254            | -4              | 250                      | +17             | 267                                       | 250             | 16  |
|              | 63E           | #5 Big "                               | 251            | -3              | 248                      | +17             | 265                                       | 250             | 16  |
|              | 67E           | #2 Sml "                               | 274            | -4              | 270                      | +14             | 284                                       | 271             | 12  |
|              | 70E           | " "                                    | 274            | -4              | 270                      | +17             | 287                                       | 278             | 12  |
|              | 70E           | " LD                                   | 240            | -5              | 235                      | +17             | 253                                       | 278             | 12  |
|              | 70E           | " "                                    | 272            | -6              | 266                      | +17             | 283                                       | 278             | 12  |
|              | 73E           | " "                                    | 305            | -6              | 299                      | +16             | 315                                       | 313             | 9   |
|              | 76E           | " "                                    | 522            | -10             | 512                      | 0               | 512                                       | 514             |     |
|              | 76E           | " FRx6                                 | 525            | -12             | 513                      | 0               | 513                                       | 514             |     |
|              | 80E           | " "                                    | 548            | -11             | 537                      | 0               | 537                                       | $\frac{565}{0}$ | 8   |
|              | 1/16          | 1F                                     | " LD           | 289             | -6                       | 283             | 0   | 283             | 290 |
| 1F           |               | " FRx6                                 | 293            | -8              | 285                      | 0               | 285                                       | 290             |     |
| 2F           |               | No fathometer                          | sounding       |                 |                          |                 |   | 341             |     |
| 6F           |               | #2 Sml FRx6                            | 396            | -9              | 387                      | 0               | 387                                       | 389             |     |
| 7F           | No fathometer | sounding                               |                |                 |                          |                 | 333                                       |                 |     |

\* Difference between B. C. and fathometer sounding for critical slope at which correction for slope ~~is~~ first applied.

*would be*

ABSTRACT OF VERTICAL CASTS WITH APPLICATION OF SLOPE CORRECTION

Sheet No. 25.

Continued

3.

| Date<br>1934 | Pos. | Hydrophone<br>&<br>Oscillator<br>used. | Fath.<br>Rdng. | Fath.<br>Cor'n. | Crt'd.<br>Fath.<br>Sdg. | Slope<br>Cor'n.       | Crt'd.<br>Fath. Sdg.<br>+ Slope<br>Cor'n. | V. C . | *  |
|--------------|------|--|----------------|-----------------|-------------------------|-----------------------|---|--------|----|
| 1/16         | 8F   | No fathometer sounding                 |                |                 |                         |                       |   | 276    |    |
|              | 9F   | " "                                    | " "            |                 |                         |                       | 196                                       |        |    |
|              | 11F  | #2 Sml FRLD                            | 506            | -10             | 496                     | 0                     | 496                                       | 507    |    |
|              | 11F  | " FRx6                                 | 512            | -12             | 500                     | 0                     | 500                                       | 507    |    |
|              | 14F  | " LD                                   | 371            | -8              | 363                     | +18                   | 381                                       | 404    | 8  |
|              | 14F  | " FRx6                                 | 373            | -9              | 364                     | +18                   | 382                                       | 404    | 8  |
|              | 15F  | " LD                                   | 295            | -6              | 289                     | +9                    | 298                                       | 295    | 10 |
|              | 15F  | " FRx6                                 | 300            | -8              | 292                     | +9                    | 301                                       | 295    | 10 |
|              | 15F  | " SD                                   | 292            | -5              | 287                     | +9                    | 296                                       | 295    | 10 |
|              | 16F  | " LD                                   | 328            | -7              | 321                     | +6                    | 327                                       | 320    | 10 |
|              | 16F  | " FRx6                                 | 322            | -8              | 314                     | +6                    | 320                                       | 320    | 10 |
|              | 17F  | " SD                                   | 392            | -6              | 386                     | +12                   | 398                                       | 399    | 8  |
|              | 17F  | " FRx6                                 | 392            | -9              | 383                     | +12                   | 395                                       | 399    | 8  |
|              | 18F  | " LD                                   | 368            | -7              | 361                     | 0                     | 361                                       | 362    | 8  |
|              | 19F  | " "                                    | 398            | -8              | 390                     | +15                   | 405                                       | 397    | 8  |
|              | 19F  | " FRx6                                 | 397            | -9              | 388                     | +15                   | 403                                       | 397    | 8  |
|              | 20F  | " LD                                   | 271            | -6              | 265                     | +18                   | 283                                       | 312    | 10 |
|              | 20F  | " FRx6                                 | 273            | -7              | 266                     | +18                   | 284                                       | 312    | 10 |
|              | 21F  | " LD                                   | 314            | -6              | 308                     | +15                   | 323                                       | 336    | 10 |
|              | 21F  | " FRx6                                 | 321            | -8              | 313                     | +15                   | 328                                       | 336    | 10 |
|              | 22F  | " LD                                   | 220            | -5              | 215                     | 0(+7%)                | 215                                       | 250    | 16 |
|              | 22F  | " FRx6                                 | 234            | -6              | 228                     | 0(+7%)                | 228                                       | 250    | 16 |
|              | 23F  | " LD                                   | 304            | -6              | 298                     | +12                   | 310                                       | 320    | 10 |
|              | 23F  | " FRx6                                 | 298            | -8              | 290                     | +12                   | 302                                       | 320    | 10 |
|              | 24F  | " LD                                   | 386            | -8              | 378                     | 0                     | 378                                       | 375    |    |
|              | 24F  | " FRx6                                 | 387            | -9              | 378                     | 0                     | 378                                       | 375    |    |
|              | 25F  | " LD                                   | 459            | -9              | 450                     | 0                     | 450                                       | 453    |    |
|              | 25F  | " FRx6                                 | 458            | -11             | 447                     | 0                     | 447                                       | 453    |    |
|              | 26F  | " SD                                   | 222            | -3              | 219                     | 0(+5%)                | 219                                       | 232    | 16 |
|              | 26F  | " FRx6                                 | 220            | -6              | 214                     | 0(+5%)                | 214                                       | 232    | 16 |
|              | 27F  | " SD                                   | 176            | -3              | 173                     | 0(+6 $\frac{1}{2}$ %) | 173                                       | 193    | 16 |
|              | 27F  | " FRx6                                 | 178            | -6              | 172                     | 0(+6 $\frac{1}{2}$ %) | 172                                       | 193    | 16 |

\* Difference between V. C. and fathometer sounding for critical slope at which correction for slope ~~is~~ first applied.

*would be*

V  
4.

ABSTRACT OF VERTICAL CASTS WITH APPLICATION OF SLOPE CORRECTION  
Sheet No. 25. Continued

| Date 1934 | Pos. | Hydrophone & Oscillator used. | Fath. Rdnng. | Fath. Cor'n. | Crt'd. Fath. Sndg. | Slope Cor'n.          | Crt'd. Fath. Sdg. + Slope Cor'n. | V. C. | *  |
|-----------|------|-------------------------------|--------------|--------------|--------------------|-----------------------|----------------------------------|-------|----|
| 1/16      | 28F  | #2 Sml FRSD                   | 324          | -5           | 319                | 0                     | 319                              | 321   |    |
|           | 28F  | " FRx6                        | 328          | -8           | 320                | 0                     | 320                              | 321   |    |
|           | 29F  | " SD                          | 288          | -5           | 283                | 0                     | 283                              | 287   |    |
|           | 29F  | " FRx6                        | 290          | -8           | 282                | 0                     | 282                              | 287   |    |
|           | 30F  | " LD                          | 402          | -8           | 394                | 0(+3 $\frac{1}{2}$ %) | 394                              | 430   | 8  |
|           | 30F  | " FRx6                        | 400          | -9           | 391                | 0(+3 $\frac{1}{2}$ %) | 391                              | 430   | 8  |
|           | 31F  | " LD                          | 434          | -9           | 425                | 0(+1%)                | 425                              | 445   | 8  |
|           | 31F  | " FRx6                        | 448          | -10          | 438                | 0(+1%)                | 438                              | 445   | 8  |
|           | 32F  | " LD                          | 376          | -8           | 368                | 0                     | 368                              | 375   |    |
|           | 32F  | " FRx6                        | 378          | -9           | 369                | 0                     | 369                              | 375   |    |
|           | 33F  | " LD                          | 323          | -7           | 316                | +17                   | 333                              | 341   | 10 |
|           | 33F  | " FRx6                        | 325          | -8           | 317                | +17                   | 334                              | 341   | 10 |
|           | 34F  | " LD                          | 424          | -8           | 416                | 0                     | 416                              | 414   |    |
|           | 34F  | " FRx6                        | 426          | -10          | 416                | 0                     | 416                              | 414   |    |
|           | 35F  | " LD                          | 466          | -9           | 457                | 0                     | 457                              | 458   |    |
|           | 35F  | " FRx6                        | 468          | -11          | 457                | 0                     | 457                              | 458   |    |
|           | 36F  | " "                           | 538          | -12          | 526                | 0                     | 526                              | 528   |    |
|           | 37F  | " LD                          | 475          | -9           | 466                | 0                     | 466                              | 461   |    |
|           | 38F  | " FRx6                        | 430          | -10          | 420                | 0                     | 420                              | 421   |    |
|           | 39F  | " LD                          | 301          | -6           | 295                | 0                     | 295                              | 302   |    |
|           | 39F  | " FRx6                        | 294          | -8           | 286                | 0                     | 286                              | 302   |    |
|           | 40F  | " LD                          | 295          | -6           | 289                | 0                     | 289                              | 292   |    |
|           | 40F  | " FRx6                        | 298          | -8           | 290                | 0                     | 290                              | 292   |    |
| 1/17      | 1G   | " LD                          | 522          | -10          | 512                | +5                    | 517                              | 520   | 8  |
|           | 1G   | " FRx6                        | 512          | -12          | 500                | +5                    | 505                              | 520   | 8  |
|           | 2G   | " LD                          | 568          | -11          | 557                | 0                     | 557                              | 558   |    |
|           | 2G   | " FRx6                        | 571          | -13          | 558                | 0                     | 558                              | 558   |    |
|           | 3G   | " LD                          | 623          | -12          | 611                | 0                     | 611                              | 615   |    |
|           | 3G   | " FRx6                        | 624          | -13          | 611                | 0                     | 611                              | 615   |    |
|           | 4G   |                               |              |              |                    |                       |                                  | 557   |    |
|           | 5G   | " LD                          | 563          | -11          | 552                | 0                     | 552                              | 550   |    |
|           | 5G   | " FRx6                        | 564          | -12          | 552                | 0                     | 552                              | 550   |    |

\* Difference between V. C. and fathometer sounding for critical slope at which correction for slope ~~is~~ first applied.

*would be*

STATISTICS - SHEET NO. 25

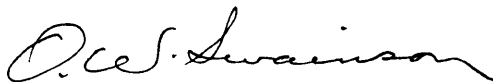
| Day    | Date    | No.Pos. | No. Sdgs. | Stat. Miles<br>of Soundings | Vol. | Wire Soundings |
|--------|---------|---------|-----------|-----------------------------|------|----------------|
| A      | Oct. 24 | 149     | 925       | 156.4                       | 1    |                |
| B      | Jan. 4  | 143     | 634       | 81.2                        | 1    |                |
| C      | Jan. 5  | 190     | 675       | 120.0                       | 2    |                |
| D      | Jan. 6  | 112     | 575       | 58.0                        | 2    |                |
| E      | May 15  | 80      | 218       | 22.0                        | 2    |                |
| F      | May 16  | 40      | 74        | 28.0                        | 3    | 37             |
| Totals |         | 714     | 3101      | 465.6                       | 3    | 37             |

CHIEF OF PARTY'S REPORT  
ON INSPECTION OF RECORDS AND SHEETS.

Lieutenant H.J. Healy examined the records and sheet carefully. He went through the records and inspected the boat sheet to see that all hydrographic features mentioned in the records were plotted on the smooth sheet. The smooth sheet plotting was then checked by placing a tracing of the smooth sheet positions over the boat sheet and replotting the questionable positions.

The sheet was then turned over to Lieutenant J.M. Smook for a review. He checked the crossings and the junctions with the adjacent sheets. He also made a comparison of the sheet with the old surveys. Points of doubt or discrepancy were called to my attention for action.

The descriptive report was written by Lieutenant J.M. Smook.



O.W. Swainson,  
Chief of Party,  
Commanding Str. PIONEER.

## TIDE NOTE FOR HYDROGRAPHIC SHEET

May 18, 1935

Division of Hydrography and Topography:

✓ Division of Charts: Attention Mr. E. P. Ellis

Tide Reducers are approved in  
3 volumes of sounding records for

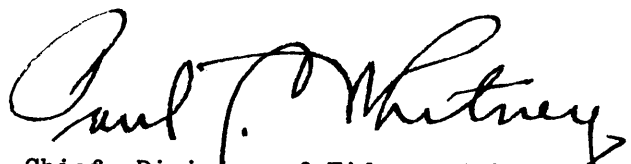
HYDROGRAPHIC SHEET      5758

Locality      San Clemente Island, California

Chief of Party:      O. W. Swainson in 1933-1934  
Plane of reference is      mean lower low water reading  
3.6 ft. on tide staff at      Santa Barbara  
16.5 ft. below B.M.      1

Height of mean higher high water above plane of reference is 5.4 ft.

Condition of records satisfactory except as noted below:

  
Chief, Division of Tides and Currents.

Date May 8, 1935

**GEOGRAPHIC NAMES**  
**California**

Survey No. H5758

Chart No. 5102

Diagram No. 5102-3

Approved by the Division of Geographic Names, Department of Interior. ✕

Referred to the Division of Geographic Names, Department of Interior. R

Under investigation. Q

| Status | Name on Survey | Name on Chart   | New Names<br>in local use | Names assigned<br>by Field | Location |
|--------|----------------|---|---------------------------|----------------------------|----------|
|        | -----          | <u>San Clemente Island</u> ✓                          |                           |                            |          |
|        |                | <u>Pyramid Head</u> ✓                                 |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                | APPROVED NAMES<br>UNDERWRITTEN IN ALL<br>H. L. Flemer |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |
|        |                |   |                           |                            |          |

Field Records Section (Charts)

HYDROGRAPHIC SHEET NO. ...5758

The following statistics will be submitted with the  
cartographer's report on the sheet:

|   |        |
|---|--------|
| Number of positions on sheet                            | .714.  |
| Number of positions checked                             | ..27.. |
| Number of positions revised                             | ..x2   |
| Number of soundings recorded                            | .3101. |
| Number of soundings revised                             | ..200. |
| Number of signals erroneously<br>plotted or transferred | ..0... |

Date: -6-11-35

Verification by *Michael Robinson*

Review by *S. Prigari*

Time: 30 hrs.

Time: 32 <sup>3</sup>/<sub>4</sub> hrs.



Smooth Sheet 1

Boat Sheet 1

Sounding Records 3 Vols. \_\_\_\_\_

Descriptive Report Yes

Title Sheet Yes

List of Signals \_\_\_\_\_

Landmarks for Charts (Form 567) \_\_\_\_\_

Statistics Yes

Approved by Chief of Party O. W. Swainson

Recoverable Station Cards (Form 524) \_\_\_\_\_

Special Chart for Lighthouse Service \_\_\_\_\_  
(Circular Nov. 30, 1933)

Remarks \_\_\_\_\_

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

6-11-35

## Verifier's Report on H-5758.

- 1- The Records conform to Hydrographic Manual instructions in the main. ~~Sounding Records read in fathoms and tenths and are so shown on H-5758.~~
- 2- ~~Considering the depth of soundings shown it is deemed that areas have been sufficiently developed to show depth curves completely.~~ <sup>can be</sup>
- 3- ~~Reference to protracted positions and soundings between those positions were well covered in the Descriptive Report and were accepted with but little checking, as long as its numerical values were as recorded. See (6) "Remarks."~~
- 4- ~~Due to the reworking of the Smooth Sheet by the Plotter as covered in the Descriptive Report, Positions were accepted on authority of Report without change, except Pos. 190c which plotted considerably off the point shown on the Smooth Sheet. It was deemed fair to assume that Ep @ 33°-40' as recorded was erroneously put down for Ep @ 40°-33' as it plotted in that Position. Pos. 44 B and Pos. 190c were erroneously plotted \* found by reviewer.~~
- 5- There are four (4) adjacent Sheets H-5600, H-5474 both scale 1:20,000 are transferred to H-5758. H-5601, scale: 20,000 will have part of H-5758 transferred on to it and H-5459, scale: -10,000 will also have part of H-5758 transferred on to it. <sup>see Remark. 3</sup>
- 6- ~~Remarks:—Since the Smooth Sheet was reworked on account of erroneous location of Signals, mentioned in the Descriptive Report, some of the positions first plotted were left on the Sheet unknowingly, thus the same Position appeared twice in different locations; it was only by thorough verifying that these positions were discovered and eliminated.~~  
 As many as 130 Sndgs. were changed in the records (due to tide corrections)  
 → The field party failed to erase erroneously plotted positions due to wrong use of sig Guds and Guds 2 (See, Report p. 3)

25-1178

What the verifier has in mind here is that  
where rejections <sup>in positions</sup> are noted in the Edg. volumes  
the corresponding numbers thus rejected should be  
used with the succeeding accepted work. He  
believes that the gap created by the omission  
of several rejected position numbers on a sheet  
would tend to confuse and cause one to look  
for the missing numbers, particularly where  
there is a break in the line.

after the Smooth Sheet was plotted. These soundings <sup>some</sup> had to be corrected <sup>were corrected</sup> while verifying; soundings omitted due to erasures <sup>were plotted where</sup> when replotted were supplied from Records. In some cases the respacing of soundings to conform to time became necessary.

Where V.C.s. were taken:- Soundings were invariably <sup>plotted thus:</sup> given <sup>Corrected Sndg (Echo Sndg)</sup>

These were made to read  $\left\{ \begin{array}{l} \text{Sndg VC} \\ \text{Corrected Sndg (Echo Sndg)} \end{array} \right.$  (by authority) \*

~~The usual field procedure of renumbering Positions when rejection are made were not followed in the Records. When Positions were rejected, the following position read on:- thus:- i.e. 10A 11A 12A 13A 14A 15A 16A etc. this would tend to increase the chances of confusion in plotting and future reference.~~

~~In a number of cases where the line broke off and moved to a new Position some distance away, the new Position wasn't geographically located, these were supplied. to aid the reviewer in expediting his work.~~

Due to fathometer method of sounding, there seems to be a conspicuous lack of Bottom Characteristics for H, B, C and D days, regrettably so, because on E, F and G days when a number of V.C. soundings were taken, the bottom showed interesting characteristics. ✓

Respectfully submitted

Michael Robinson

\* What the verifier is stating here is that the echo soundings were not plotted on the line.

On echo work the usual procedure is to plot the echo sdg. on line and offset the vertical casts as an offset.

Section of Field Records

REVIEW OF HYDROGRAPHIC SURVEY NO. 5758 (1933-34) - FIELD NO. 2

San Clemente Island, California  
Surveyed in October 24, 1933, to May 17, 1934  
Instructions dated November 18, 1932 (PIONEER)

Fathometer Soundings.

3 Point Fixes on Shore Signals.

Chief of Party - O. W. Swainson.

Surveyed by - O. W. S., J. M. Smook, P. L. Bernstein, R. A. Gilmore,  
J. C. Ellerbe.

Protracted by - H. J. Pulskamp, H. J. Healy.

Soundings penciled by - H. J. P., H. J. H.

Verified and Inked by - M. Robinson.

1. Condition of Records.

The records are neat and legible and conform to the requirements of the Hydrographic Manual except as follows:

- a. More bottom characters should have been taken along the eastern limit and also at the southern portion between long's.  $118^{\circ}20'$  and  $118^{\circ}26'$ , where none have been shown.
- b. Evidence that the plotting of Hydrographic Signals was checked in the field was lacking, since the initials of the checker were omitted on the sheet. This was accomplished in the office.
- c. A number of cuts to hydrographic signals were not entered on the index page of the record volumes.
- d. The Descriptive Report is complete and comprehensive and satisfactorily covers all items of importance.

2. Compliance with Instructions for the Project.

The survey complies with the instructions for the project.

3. Sounding Line Crossings.

With a few exceptions noted in the Descriptive Report, page 4, the agreement in depths at crossings is good.

4. Depth Curves.

The usual depth curves may be satisfactorily drawn.

5. Junctions with Contemporary Surveys.

- a. Satisfactory junction is made with H-5600 (1934) on the north.

b. Junction with H-5474 (1933) on the west is satisfactory, but in the portion south of lat.  $32^{\circ}52'$  and east of San Clemente I., the agreement in the overlapping depths is not good in a number of places. The steep slopes in this vicinity are no doubt contributing factors to the discrepancy. Since sheet H-5474 (1933) covers the area with wire soundings, the 1933 survey should be given preference for charting.

c. Satisfactory junction is made with H-5459 (1934) on the south inshore limits.

6. Comparison with Prior Surveys.

a. H-1429 (1878-79).

This survey on a scale of 1:20,000, covers sections of the western and southern portions of the present survey with relatively few soundings which are not in good agreement.

Comparison of the soundings in the southern portion indicates a general deepening has occurred since the date of the old survey, bringing the 50 fathom curve approximately 500 meters nearer shore.

The soundings in the western section from the 100 fathom curve, seaward, are shoaler than those of the present survey.

The present survey adequately covered this area and a large number of excellent comparisons between the wire and the fathometer soundings were obtained.

The old work should not be used for charting.

b. H-1430 (1879).

This survey on a scale of 1:20,000 covers the eastern portion of the present survey with widely spaced soundings. The agreement in the depths is in general very good.

The 331 fathom sounding charted in lat.  $32^{\circ}56.1'$ , long.  $118^{\circ}25.6'$  was found to be erroneously plotted on the old survey and should be 531.

Since the present survey covers the area adequately, the old survey should be disregarded for charting purposes.

c. H-4265a (1922-23).

This survey on a scale of 1:100,000 overlaps the present survey at the south limit with four soundings which are in fair agreement with the depths of the later survey. For charting purposes the present survey should be given preference.

d. H-4366 (1924-1928).

This survey on a scale of 1:160,000 covers the area of the present survey with widely spaced soundings. The agreement in most places is very good, except for a few soundings southeasterly of signal Guds.

The 482 fathom shoal sounding charted in lat.  $32^{\circ}52'$ , long.  $118^{\circ}19'$  falls on the present survey among deeper soundings, of which 493 is the shoalest, and since the surrounding depths are in agreement with the present ones, the 482 is being carried forward.

The present survey should supersede the old survey as the area has been adequately covered.

e. H-4549a (1925).

This survey on a scale of 1:140,000, overlaps the present survey with two lines of soundings off the east coast and several soundings off the south coast. With the exception of a very few soundings, the agreement in the depths is in general satisfactory.

The old survey has nothing outstanding to be carried forward and should be superseded by the present survey which covers the area very satisfactorily.

f. H-4504 (1925).

This survey on a scale of 1:120,000, overlaps the present survey at its southeastern portion with widely spaced soundings.

The agreement in depths in general is satisfactory. The old survey adds nothing of particular value to the present work and should not be used for charting.

g. H-4782 (1928).

This survey on a scale of 1:80,000, covers a portion of the present survey on the south and the agreement in depths in general is very good.

An outstanding 28 fathom sounding charted in lat. 32°45.7', long. 118°24.6' falls in an area where the present survey found a least depth of 26 fathoms.

There are no features on the old survey which the present has not adequately developed. The present survey should be given preference for charting.

7. Comparison with Charts No's. 5101, 5126.

Within the area of the present survey the chart is based on surveys discussed in the foregoing paragraphs and contains no additional information that needs consideration in this review.

Attention is called to the erroneous sounding 331 in approximate lat. 32°56', long. 118°25.6', which should be 531 (par. 6b, this review).

8. Field Plotting.

The protracting of positions and the plotting of soundings is good.

9. Additional Field Work Recommended.

No additional work is required.

10. Superseding Old Surveys.

Within the area covered, the present survey, with the indicated additions from previous surveys, supersedes the following surveys for charting purposes:

|         |              |          |
|---------|--------------|----------|
| H-1429  | (1878-79)    | in part. |
| H-1430  | (1878)       | " "      |
| H-4265a | (1922-23)    | " "      |
| H-4366  | (1924, 1928) | " "      |
| H-4549a | (1925)       | " "      |
| H-4504  | (1925)       | " "      |
| H-4783  | (1928)       | " "      |

11. Reviewed by - G. Risegari, July 1, 1935.

Supervised by - A. L. Shalowitz.

Examined and approved:

*C. K. Green*  
C. K. Green,  
Chief, Section of Field Records.

*L. O. Pollock*  
Chief, Division of Charts.

*F. S. Borden*  
Chief, Section of Field Work.

*G. Stude*  
Chief, Division of H. & T.

*applied to drawing of Chart 5111 - Sept 9, 1935 - J.W.*



25 Jan 7 1936  
END

5758

Additional work

Form 504  
Rev. Dec. 1933  
DEPARTMENT OF COMMERCE  
U.S. COAST AND GEODETIC SURVEY  
R. S. PATTON, DIRECTOR

**DESCRIPTIVE REPORT**

~~TOPOGRAPHIC~~ }  
Hydrographic } Sheet No. 10-1

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Additional work

---

State California

LOCALITY

South of San Clemente Island

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1935

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CHIEF OF PARTY

R. R. Moore

5758

Additional work

POST-OFFICE ADDRESS: P. O. Box 530, Long Beach, California.

*etc chief*  
*22*  
*25*  
*80*

TELEGRAPH ADDRESS:

EXPRESS ADDRESS:

1935 NOV 22 AM 11:56

DEPARTMENT OF COMMERCE

U. S. COAST AND GEODETIC SURVEY

*20*  
*80*

*NOV 22 11 56 AM '35*

U.S.C. & G.S.S. PIONEER,

November 16, 1935.

To: The Director,  
U. S. Coast and Geodetic Survey,  
Washington, D. C.

From: The Commanding Officer,  
U.S.C. & G.S.S. PIONEER.

Subject: Investigation of reported shoal.

An examination of the shoaling reported south of San Clemente Island by the Commanding Officer of the U. S. S. BUCHANAN in the Hydrographic Office Notice to Mariners dated October 24, 1935, was made while the PIONEER was in that vicinity last Monday.

The attached tracing, <sup>being forwarded</sup> shows the result of the examination.

This area is also covered by Field Sheet No. 25, of the 1934 season of the PIONEER which has been sent to the Office.

The sounding record is being forwarded to the Office.

*R. R. Moore*  
R. R. Moore,  
H. & G. Engineer,  
Commanding PIONEER.

### TIDE NOTE FOR HYDROGRAPHIC SHEET

December 18, 1935.

Division of Hydrography and Topography:

✓ Division of Charts: Attention: Mr. E. P. Ellis

Tide Reducers are approved in  
1 volumes of sounding records for

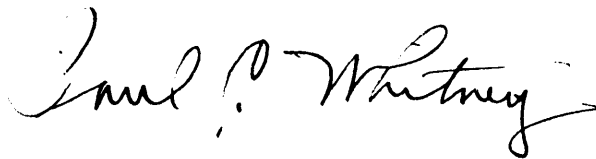
HYDROGRAPHIC SHEET 5758 Additional Work

Locality South of San Clemente Island, Coast of Southern Calif.

Chief of Party: R. R. Moore in 1935  
Plane of reference is mean lower low water reading  
3.6 ft. on tide staff at Los Angeles  
14.0 ft. below B.M. 8

Height of mean high water above plane of reference is 4.7 feet.

Condition of records satisfactory except as noted below:



Chief, Division of Tides and Currents.

Field Records Section (Charts.)

HYDROGRAPHIC SHEET NO. ....

The following statistics will be submitted with the cartographer's report on the sheet:

|  |         |
|--|---------|
| Number of positions on sheet                         | .....18 |
| Number of positions checked                          | .....18 |
| Number of positions revised                          | .....   |
| Number of soundings recorded                         | .....83 |
| Number of soundings revised                          | .....0  |
| Number of signals erroneously plotted or transferred | .....   |

Date: Jan. 22, 1936

Verification by James McCormick

Time: 4 hr.

Review by

Time:

Verifier's Report on H-5758 (Additional Work)

Records: Records are complete.

Drafting: Tracing of additional work was submitted by field party on a scale of 1:10,000. It was carefully done and served as a check on the verifier's plotting of work on scale of 1:20,000.

Remarks: Topo signal Gros was obtained from T-4857. Pyramid Point L.H. (1934) was obtained from Division of Geodesy. It checked the hydrographic signal Lite within 4 meters so verifier did not ink it on sheet.

4 soundings of the additional work fell in the overlap with H-5459. They were transferred to that sheet and inked in the same color as the rest of the overlap.

January 22, 1936.

Submitted,



J. A. McCormick.

Section of Field Records

REVIEW OF HYDROGRAPHIC SURVEY NO. 5758 (Additional Work 1935)

Off Pyramid Head, San Clemente Island, California  
Surveyed in Nov. 1935  
Instructions dated H. O. Notice to Mariners, Oct. 24, 1935.

Fathometer Soundings.

3 Point Fixes on shore signals.

Chief of Party - R. R. Moore.  
Surveyed by - R. R. Moore.  
Protracted by - J. A. McCormick.  
Soundings penciled by - J. A. McCormick.  
Verified and inked by - J. A. McCormick.

1. Purpose of Survey.

The purpose of the additional work was to determine the existence of the reported 25 fathom shoaling in latitude  $32^{\circ}48'06''$ , longitude  $118^{\circ}21'30''$ , mentioned in the H. O. Notice to Mariners, No. 43 of 1935.

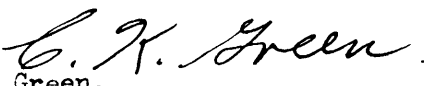
2. Results of Survey.

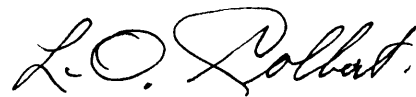
The extent of development in the additional work and the work on H-5758 (1933-34) appears sufficient to satisfactorily disprove the existence of the reported 25 fathom shoaling. This depth falls on H-5758 (1933-34) in depths of 51 fathoms with no indication of a shoaling and in a generally sandy bottom area. It is not believed to exist in the reported position and should not be charted.

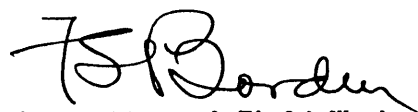
3. Reviewed by - G. Risegari, Jan. 28, 1936.


Inspected by - A. L. Shalowitz.

Examined and approved:

  
C. K. Green,  
Chief, Section of Field Records.

  
L. O. Lobbat,  
Chief, Division of Charts.

  
J. S. Borden,  
Chief, Section of Field Work.

  
G. Hude,  
Chief, Division of H. & T.

25 Jan 1936  
EAB

Applied to Chart 5101 - May 4, 1936 L.M.Z.

Applied to Chart 5117 June 4, 1937 G.H.S.