

7973

Diag. Chrt. Nos. 8861-2, 8862, 8863-3, 8864-2,

9000-1, 9302

Form 504

C9-343

U. S. COAST AND GEODETIC SURVEY

DEPARTMENT OF COMMERCE

DESCRIPTIVE REPORT

Type of Survey HYDROGRAPHIC

Field No. PI-502-52 Office No. H-7973

LOCALITY

State ALASKA

General locality BERING SEA

Locality SOUTH CENTRAL BERING SEA

1952

CHIEF OF PARTY

THOS. B. REED C. Pierce

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DATE JAN 23 1953

B-1870-1 (1)

DEPARTMENT OF COMMERCE  
U. S. COAST AND GEODETIC SURVEY

HYDROGRAPHIC TITLE SHEET

The Hydrographic Sheet should be accompanied by this form, filled in as completely as possible, when the sheet is forwarded to the Office.

REGISTER No. H-7973

Field No. PI-502-52 and PF-502-52

State Alaska

General locality Bering Sea

Locality South Central Bering Sea

Scale 1:500,000 Date of survey May - September 1952

Instructions dated Project CS-343 dtd. 6 March 1951, 28 May 1951, 21 March 1952

Vessel Ships PIONEER & PATHFINDER

Chief of party Thos. B. Reed C. Pierce

Surveyed by Ships' Officers of PIONEER & PATHFINDER

Soundings taken by fathometer, ~~graph recorder, hand lead line~~

Fathograms scaled by Fathometer Operators

Fathograms checked by Ships' Officers

Protracted by A.R.B. Benton, Jr., P.O. Reimer, Jr., and G.E. Cook

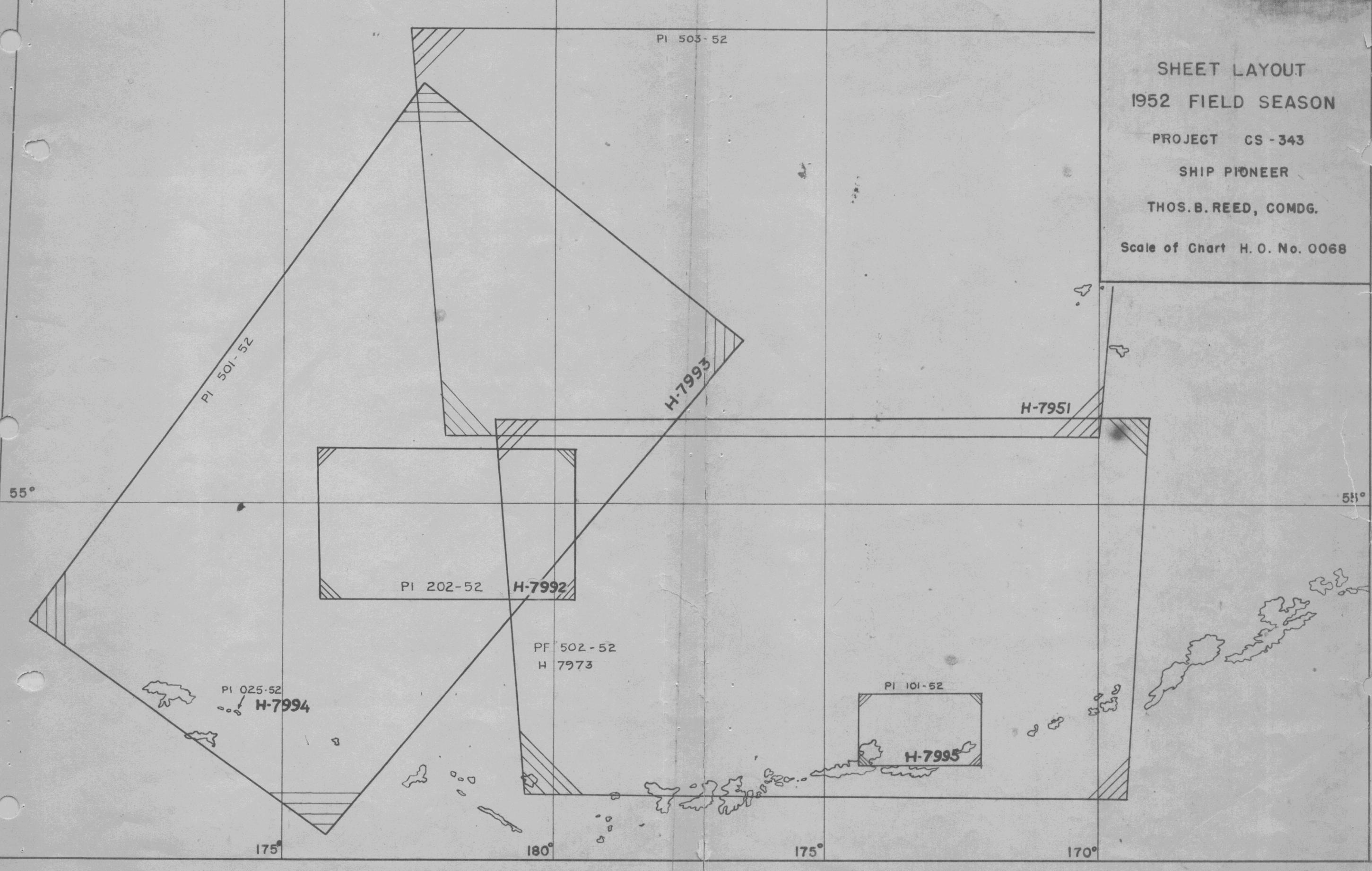
Soundings penciled by H.C. Applequist, A.R.B. Benton, Jr., and G.E. Cook

Soundings in fathoms ~~feet~~ MLLW

REMARKS: Note: 1 or 2 Bot. characteristics can be added to this sheet from Spec. Report of Bainbridge (1953) No. 162  
JAD.

SHEET LAYOUT  
1952 FIELD SEASON  
PROJECT CS - 343  
SHIP PIONEER  
THOS.B.REED, COMDG.

Scale of Chart H. O. No. 0068



DESCRIPTIVE REPORT TO ACCOMPANY HYDROGRAPHIC SURVEY

REGISTER NO. H-7973

FIELD NO. PI & PF-502-52

SOUTH CENTRAL BERING SEA, ALASKA  
1952

Project No. CS-343  
Ships PIONEER & PATHFINDER  
Scale 1:500,000

THOS. B. REED, CHIEF OF PARTY  
CHARLES PIERCE, CHIEF OF PARTY  
Surveyed by: Ships' Officers

A. PROJECT:

This survey was executed in accordance with the Director's Instructions, Project CS-343, dated 6 March 1951, 28 May 1951, 21 June 1951, and 21 March 1952.

B. SURVEY LIMITS AND DATES:

This survey covers the offshore area north of the Aleutian Islands to Latitude 56° North from approximately 170°W. Longitude to approximately 179°W. Longitude. The entire area was not completed and there is an unsurveyed area in the northeast part of the sheet.

This sheet joins prior surveys H-6573, H-6700 and H-6701 at the southeastern part; contemporary survey H-7995 on a scale of 1:100,000 in the vicinity of Amlia Island; prior survey H-6850, in the vicinity of Atka Island; contemporary sheet EX-401-52 of the Ship EXPLORER in the vicinity of Tanaga and Kanaga Islands; prior survey H-7806 north of Gareloi Island; contemporary survey H-7972 by the PATHFINDER on a scale of 1:200,000 to the west; contemporary survey H-7993 to the northwest and contemporary survey H-7951 to the north. The last two surveys are on a scale of 1:500,000.

Field work was begun by the Ship PATHFINDER on 12 May 1952 and ended 23 June 1952. The Ship PIONEER began field work on 1 June 1952 and ended on 14 September 1952.

C. VESSELS AND EQUIPMENT:

The Ships PIONEER and PATHFINDER surveyed the area. The Ship PIONEER used fathometers NMC No. I-766 and NMC-2 No. 117. The PATHFINDER used fathometers 808 J No. 130-S, NJ 3 No. 22 and NMB No. 106.

D. CONTROL STATIONS:

EPI stations ATtu, AMchitka, and SEguam were located by the personnel of the Ship PIONEER and their locations are discussed in a separate report. EPI station TANAGA was established and the location furnished by the Ship EXPLORER. The stations in the Aleutian Islands are all on the N.A. 1927 Datum. The St. Paul datum was tied to the N.A. 1927 Datum by EPI in 1951. The EPI station at St. Paul was established and the location furnished by the Ship PATHFINDER.

E. SOUNDINGS:

Most of the PIONEER soundings were taken with the NMC fathometer. The NMC2 was used in depths under 800 fathoms. During rough weather the fathometer would not record soundings and at these times the soundings were taken by audio. All soundings recorded on the fathograms were scanned and verified.

The area in which the PIONEER worked was all in deep water and no tide corrections were applied.

In accordance with the Director's letter, dated 21 June 1951, 21/mek, S-1-PI, no velocity corrections were applied. The calibrated velocity of the fathometers used is 800 fathoms per second.

*Verifier: Apply vel. corr. in area of overlap  
with inshore surveys  
where necessary*

F. CONTROL OF HYDROGRAPHY:

The hydrography was controlled by EPI. On the last day only one EPI station was available during the last four hours of hydrography and Loran Rate 1-L-6 was used in conjunction with EPI SE-guam. This portion of the line crossed four other lines and the agreement was good. In the area between St. Paul Island and Se-guam Island the system of lines crossed the bisectrix. The positions at the ends of these lines were held and the positions in between adjusted in accordance with the log readings.

G. ADEQUACY OF SURVEY:

The survey is believed complete over that part covered. However, the northeast corner of the sheet, from Longitude  $175^{\circ}$  W eastward and between Latitudes  $54^{\circ} 50'$  and  $55^{\circ} 50'$ , was not completed. The area directly east of this area is unsurveyed and it can probably be surveyed at the same time with the same control stations.

Junctions with adjacent surveys appear satisfactory.

H. CROSSTRAIGHTS:

The crossings in general are satisfactory except at depths in the vicinity of 2000 fathoms. During the latter part of the season the NMC fathometer was not operating very satisfactorily being badly in need of a complete overhaul after nearly continuous use during the season. The fathogram was extremely difficult to read during rough weather and much of the sounding was by audio, which is not very satisfactory in the vicinity of 2000 fathoms. On the cross-line on DA Day, the soundings from position 43 to 52 were rejected. Due to rough weather the soundings were not recording and the fathometer operator apparently read the initial. There are a considerable number of crossings with discrepancies of 30 fathoms due to the above conditions. The crossings at lesser depths are good.

J. COMPARISONS WITH PRIOR SURVEYS AND CHARTS:

There are no prior surveys in this area. H. O. Chart No. 0068 covers this area. West of Longitude 175°W. the soundings on the chart are generally deeper than those obtained on this survey.

K. DANGERS AND SHOALS:

There are no dangers to surface navigation within the limits of this survey.

L. DATA INCLUDED WITH THIS REPORT:

1. Summary of EPI corrections.
2. Abstract of Statistics.
3. Computations of Arc Points.
4. Approval Sheet.

M. TABULATION OF APPLICABLE DATA:

1. Report of EPI Calibration.
2. Triangulation Report on Location of EPI Stations.

N. MISCELLANEOUS:

The Ship PATHFINDER's work was plotted by personnel of the Ship PIONEER. The reports of the Ship PATHFINDER covering EPI Calibration, Corrections to Soundings, and Locations of Stations were not furnished this party. The sounding volumes were received completed and ready for plotting.

An overlay was made for the area between Latitudes 52° 00' and 52° 40' and Longitudes 176° 15'E and 176° 40'E, just north of Adak. Too many sounding lines were run in this area to show all the soundings on the smooth sheet.

Respectfully submitted

*H. C. Applequist*  
H. C. Applequist  
CMDR. USC&GS

Approved and forwarded:

*Thos. B. Reed*

Thos. B. Reed  
CAPT., USC&GS  
Comdg., Ship PIONEER

SUMMARY OF EPI CORRECTIONS

Survey H-7973

Field No. PI-502-52

Shore Equipment

Period

Correction

EPI ATtu

T-7 C-6	Prior to 16 June	-5.0
T-7 C-6	After 16 June	-3.5
T-4 C-6	Prior to 16 June	-3.6
T-4 C-6	After 16 June	-2.6

EPI AMchitka

T-3 C-2	Entire Period	-5.0
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EPI TAnaga

T-8 C-7	Prior to 16 June	-4.2
T-8 C-7	After 16 June	-4.9
T-8 C-8	Prior to 16 June	-4.8
T-8 C-8	After 16 June	-6.3

EPI SEguam

T-4 C-6	Prior to 1200 29 August	-1.8
T-4 C-6	After 1200 29 August	-4.0
T-4 C-4	Prior to 1200 29 August	-2.7
T-4 C-4	After 1200 29 August	-3.7
T-7 C-6	Prior to 1200 29 August	-4.6
T-7 C-6	After 1200 29 August	-3.6
T-7 C-4	On 14 Sept. only time used	-4.3

EPI PAUL

C-2 T-5	Entire Period	-5.3
C-3 T-5	Entire Period	-6.3

ABSTRACT OF STATISTICS FOR HYDROGRAPHIC SURVEY  
Register No. H-7973 Field No. PI-502-52

Ship PIONEER

DAY BLUE	VOL. NO.	DATE	NO. OF POS.	STATUTE MILES
A	1	1 June	32	147.0
B	1	2 June	14	55.6
C	1	4 June	42	249.8
D	1	17 June	36	215.0
E	1 & 2	18 June	74	446.2
F	2	19 June	13	54.0
G	2	22 June	33	179.4
H	2	23 June	75	425.6
J	2	24 June	25	147.2
K	3	19 August	6	37.7
L	3	20 August	63	381.8
M	3	24 August	31	195.5
N	3	25 August	72	450.8
P	4	26 August	30	172.5
Q	4	28 August	43	257.6
R	4	29 August	56	326.6
S	4 & 5	30 August	72	445.1
T	5	31 August	72	435.2
U	5	1 September	72	441.6
V	5 & 6	2 September	72	457.7
W	6	3 September	72	446.2
X	6 & 7	4 September	71	400.2
Y	7	5 September	67	395.6
Z	7	6 September	72	427.8
AA	7 & 8	7 September	72	291.0
BA	8	8 September	72	392.0
CA	8 & 9	9 September	72	358.9
DA	9	10 September	72	373.8
EA	9	11 September	24	146.0
FA	9	12 September	28	176.6
GA	9 & 10	13 September	72	396.8
HA	10	14 September	40	198.9
		TOTAL	1,667	9,525.8

ABSTRACT OF STATISTICS FOR HYDROGRAPHIC SURVEY  
Register No. H-7973      Field No. PI-502-52

Ship PATHFINDER

DAY BROWN	VOL. NO.	DATE	NO. OF POS.	STATUTE MILES
A	1	14 May	4	29.0
B	1	15 May	19	141.5
C	1	19 May	33	145.9
D	1	24 May	21	99.4
E	1	25 May	10	40.2
F	1	28 May	2	9.5
G	1	29 May	35	51.1
H	1	8 June	51	141.5
J	1	11 June	5	26.1
K	1	12 June	27	126.5
L	2	20 June	30	145.5
M	2	21 June	21	93.0
N	2	23 June	16	77.0
P	3	12 May	8	41.0
Q	3	29 May	7	31.4
R	3	30 May	13	61.0
S	3	16 June	10	22.9
T	3	20 June	7	29.3
			TOTALS	1,311.8

COMBINED TOTALS, PIONEER AND PATHFINDER

POSITIONS	1986
STATUTE MILES	10837.6
SQUARE STATUTE MILES	39200

ARC POINTS

Survey H-7973

Field No. PI-502-52

DISTANCE	AZIMUTH °	LATITUDE °   °   "   N	LONGITUDE °   °   "   E
<u>EPI ATtu</u>		52 56 31.30 N	173 15 02.52 E
3200 ms	255	53 51 06.32 N	179 42 00.78 W
4000 ms	255	54 00 46.76 N	177 53 43.75 W
4800 ms	255	54 08 48.98 N	176 04 39.57 W
3200 ms	235	55 15 33.37 N	179 26 04.12 E
3200 ms	275	52 21 24.63 N	179 43 38.05 W
<u>EPI TANaga</u>		51 39 59.64 N	178 05 17.57 W
1000 ms	180	53 00 47.48 N	178 05 17.57 W
2000 ms	180	54 21 34.20 N	178 05 17.57 W
3000 ms	180	55 42 19.83 N	178 05 17.57 W
2000 ms	150	53 58 39.06 N	179 37 41.77 E
2000 ms	240	52 57 04.08 N	174 13 31.43 W
<u>EPI AMchitka</u>		51 25 01.17 N	179 17 33.06 E
	PATHFINDER FINAL	01.19	33.04
	Arcs computed from top position		
1200 ms	225	52 32 42.08 N	178 49 59.73 W
2400 ms	225	53 38 29.83 N	176 51 42.58 W
3600 ms	225	54 42 13.82 N	174 47 13.45 W
2400 ms	187	54 37 21.27 N (GP with PI-501-52 Reg No. H-7993)	179 58 14.39 E
2400 ms	250	52 25 08.09 N	175 44 12.83 W
<u>EPI ST. PAUL</u>		57 07 31.45 N	170 15 54.97 W
1200 ms	30	55 43 06.57 N	171 41 44.80 W
3600 ms	30	52 51 32.30 N	174 16 04.98 W
2400 ms	30	54 17 44.71 N	173 01 35.29 W
2400 ms	60	55 24 36.89 N	175 11 08.35 W
2400 ms	00	53 53 42.87 N	170 15 54.97 W
<u>EPI SEguam</u>		52 23 09.35 N	172 24 19.36 W
1400 ms	150	54 00 28.38 N	174 00 18.31 W
2800 ms	150	55 36 23.03 N	175 44 00.80 W

POSITION COMPUTATION, FIRST-ORDER TRIANGULATION  
(For calculating machine computation)

$\alpha$	2	to 3				$\alpha$	3	to 2			
$2d\angle$		$\delta$		+		$3d\angle$	$\delta$		-		
$\alpha$	$2E^{\rho_1} AT$	to 1 Arc Point 4800 $y$		$+10$		$\alpha$	$3E^{\rho_1} AT$	to 1 Arc Point 3200 $y$	$-235^\circ$		
$\Delta\alpha$						$\Delta\alpha$					
$\alpha'$	1	to 2				$\alpha'$	1	to 3			
First Angle of Triangle											
$\phi$	52° 56' 31.30"	2 $E^{\rho_1} AT$	$\lambda$	173° 15' 02.525"	$\phi$	52° 56' 31.30"	3 $E^{\rho_1} AT$	$\lambda$	173° 15' 02.525"		
			$s = 719.254.56$	$\Delta\lambda$	+ 10	40° 17.91		$s = 479.503.04$	$\Delta\lambda$	+ 11	01.60
$\phi'$	54° 06' 48.98"	1 Arc Point 4800 $y$	$x'$	176° 04' 39.57 w	$\phi'$	53° 15' 33.37	1 Arc Point 3200 $y$	$x'$	179° 26' 04.12 E		
	151° 46.29					1032.0					
$\Delta\phi$											
$\sin \alpha$	0.965 - 925.83										
$\cos \alpha$	0.258 819.05										
$x = s \sin \alpha$	- 694.746.558										
$y = -s \cos \alpha + 186.156.782$	H . 055° 090.570										
$a = (x'/10,000)^2$	$Hx' = (\text{approx. } \Delta\lambda'')$										
$y \text{ cor.} = +fa$	$3946.53599$										
$y \text{ cor.} = +fa$	$3946.464.688.5^{(734.66)}$										
$y_0$	5° 867.951.377	$\sin \phi$				$y_0$	5° 867.951.377	$\sin \phi$			
$y'$	+ 186 891.444	$\sin \phi'$				$y'$	+ 275.378.467	$-\sin \phi'$			
$y_1$	6 054 842.821	$1 + \cos \Delta\phi$				$y_1$	6 143.329.844	$1 + \cos \Delta\phi$			
$V_a$	- 53° 149.341	$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta\phi}$				$V_a$	- 17 491.169	$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta\phi}$			
$y_2$	6 00 054 719	$-\Delta\lambda''(\text{approx.})$				$y_2$	6 125.834.692	$-\Delta\lambda''(\text{approx.})$			
$V$	11. 014.59	$+ F(\Delta\lambda'')^3$				$V$	11. 344.25° (40.011)	$+ F(\Delta\lambda'')^3$			
$K(V_B/1,000)^2 + 1277 \times 284.455$	$- \Delta\alpha''$					$K(V_B/1,000)^2 + 1208 \times 305.941$	$- \Delta\alpha''$	$\text{Copy } \sim K4M$			

POSITION COMPUTATION, FIRST-ORDER TRIANGULATION  
(For calculating machine computation)

$\alpha$	2	to 3						$\alpha$	3	to 2			
$2d\angle$		&		+				$3a\angle$	&	-			
$\alpha$	$2 E\rho/AT$	to 1 Arc $\rho/14740024$		$255^{\circ}$				$\alpha$	$3 E\rho/AT$	to 1 Arc $\rho/14740024$	$255^{\circ}$		
$\Delta\alpha$								$\Delta\alpha$					
$\alpha'$	1	to 2						$\alpha'$	1	to 3			
First Angle of Triangle													
$\phi$	$52^{\circ} 56' 31.30$	$2 E\rho/AT$	$\lambda$	$173^{\circ} 15' 02.52 E$	$\phi$	$52^{\circ} 56' 31.30$	$3 E\rho/AT$	$\lambda$	$173^{\circ} 15' 02.52 E$	$b = (\gamma/10,000)^2$	$154.0193$	$b = (\gamma/10,000)^2$	$240.6552$
			$s = 479503.04$	$\Delta\lambda$	$+0.7^{\circ} 02.32$					$\sin \alpha$	$0.965^{\circ} 925^{\circ} 83^{\circ} 4$	$\sin \alpha$	$0.965^{\circ} 925^{\circ} 83^{\circ} 4$
$\phi'$	$53^{\circ} 51' 06.32$	$1 Arc Point$ $255^{\circ} 0$	$\lambda'$	$179^{\circ} 42' 00.78 W$	$\phi'$	$54^{\circ} 00' 46.76$	$1 Arc Point$ $255^{\circ} 0$	$\lambda'$	$177^{\circ} 53' 43.75 W$	$x cor. = -\frac{1}{2} fb$	$629.5311$	$x cor. = -\frac{1}{2} fb$	$984.1113$
										$\cos \alpha$	$0.258819059$	$\cos \alpha$	$0.258819059$
										$x'$	$-463^{\circ} 135.200$	$x'$	$-578^{\circ} 899.489$
										$H$	$.054913480$	$H$	$.054913480$
										$y = -s \sin \alpha$	$-463^{\circ} 164.372$	$y = -s \cos \alpha + 155^{\circ} 130.652$	$Hx' = (approx. \Delta\lambda') 25334.525^{\circ}$
										$\Delta\lambda''$	$25334.525^{\circ}$	$\Delta\lambda''$	$25334.525^{\circ}$
										$Arc-\sin = +\frac{V(Va)}{15}$	$16645.5122$	$Arc-\sin = +\frac{V(Va)}{15}$	$84.39^{\circ}$
										$a = (x'/10,000)^2$	$3144.9421$	$a = (x'/10,000)^2$	$3351.2346$
										$y cor. = +fa$	$17542.6235$	$y cor. = +fa$	$27408.4073$
										$\Delta\lambda''$	$-25376.696$	$\Delta\lambda''$	$-31873.727$
										$y_0$	$5867951.322$	$y_0$	$5867951.322$
										$y'$	$+155^{\circ} 555.840$	$y'$	$+155^{\circ} 555.840$
										$\sin \phi$		$\sin \phi$	
										$y_1$	$6023507.217$	$y_1$	$6023507.217$
										$V_a$	$-34531.5C7$	$V_a$	$-34531.5C7$
										$\sin \phi + \sin \phi'$	$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta\phi}$	$\sin \phi + \sin \phi'$	$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta\phi}$
										$y_2$	$5987975.7145^{\circ} 145^{\circ} 198^{\circ} 27.0$	$y_2$	$5987975.7145^{\circ} 145^{\circ} 198^{\circ} 27.0$
										$V$	$10.76913$	$V$	$10.76913$
										$K(Va/1,000)^2 + .12C(x535.557)$	$K(Va/1,000)^2 + .12C(x535.557)$	$K(Va/1,000)^2 + .12C(x535.557)$	$K(Va/1,000)^2 + .12C(x535.557)$
										$\Delta\alpha''$	$-\Delta\alpha''$	$\Delta\alpha''$	$-\Delta\alpha''$

POSITION COMPUTATION, FIRST-ORDER TRIANGULATION  
(For calculating machine computation)

$\alpha$	2	to 3											
$2d\angle$		&			+								
$\alpha$	$2 E \rho_1 A T$	to 1 $A \rho_1 \rho_2 \sin \Delta \alpha$			$275^\circ$								
$\Delta \alpha$													
$\alpha'$	1	to 2											
First Angle of Triangle													
$\phi$	$5^{\circ} 2'$	$54'$	$31.30$	$2 E \rho_1 A T$	$\lambda$	$173$	$15'$	$02.524$	$\phi$			$3$	
					$s = 479.503.04$	$\Delta \lambda$	$+07$	$01$				$s =$	
	$\phi'$	$5^{\circ} 21'$	$24.63$	$1 \text{ Arc } \rho_1 \sin \frac{275^\circ}{32004}$	$\lambda'$	$179$	$43'$	$38.054$	$\phi'$			$\Delta \lambda$	
												$1$	
					$\gamma_{61.3}$							$\lambda'$	
$\Delta \phi$													
$\sin \alpha$	$0.996$	$19.470$	$4$		$(\log s =$				$\Delta \phi$			$b = (\gamma/10,000)^2$	
$\cos \alpha$	$0.087$	$153.74$	$+$		$17.465^2$				$\sin \alpha$			$\sin \alpha$	
$\mathbf{x} = s \sin \alpha$	$-477.674.387$				$x = -\frac{1}{2} f_b$	$71.4204$	$(3.412)$		$\cos \alpha$			$\mathbf{x}'$	
$\mathbf{y} = -s \cos \alpha$	$-477.674.387$				$\mathbf{H}$	$.052$	$837$	$884$	$\mathbf{x} = s \sin \alpha$			$\mathbf{H}$	
$\mathbf{a} = (x/10,000)^2$	$22.51$	$73.38$			$Hx' = (\text{approx. } \Delta \lambda'')$	$-25$	$239$	$335$	$\mathbf{y} = -s \cos \alpha$			$Hx' = (\text{approx. } \Delta \lambda'')$	
$\mathbf{y cor.} = +f_a$	$18.661.388$	$(77.999)$			$\text{Arc}-\sin = +\frac{V(Va)}{15}$	$15.884.1565$	$(40.091)$		$\mathbf{a} = (x/10,000)^2$			$\text{Arc}-\sin = +\frac{V(Va)}{15}$	
$\mathbf{y}_o$	$5^{\circ} 867$	$951.377$			$\mathbf{y cor.} = +f_a$				$\mathbf{y}$			$\mathbf{y}$	
$\mathbf{y}'$	$-41$	$869$	$431$		$\Delta \lambda''$				$\mathbf{y}'$			$\mathbf{y}'$	
$\mathbf{y}_1$	$5^{\circ} 866$	$081.946$			$1 + \cos \Delta \phi$				$\mathbf{y}_1$			$\mathbf{y}_1$	
$\mathbf{y}_2$	$5^{\circ} 802$	$431.615$			$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta \phi}$				$\mathbf{y}_2$			$\mathbf{y}_2$	
$\mathbf{v}$	$10.21969$				$-\Delta \alpha''$ (approx.)				$\mathbf{v}$			$\mathbf{v}$	
$\mathbf{K} (Va/1,000)^2 +$	$12(4 \times 543.65)$				$+ F(\Delta \lambda'')^3$	$\frac{K}{1 + \cos \Delta \phi}$			$\mathbf{K} (Va/1,000)^2 +$			$\mathbf{K} (Va/1,000)^2 -$	
					$- \Delta \alpha''$								

POSITION COMPUTATION, FIRST-ORDER TRIANGULATION

**U. S. COAST AND GEODETIC SURVEY  
DEPARTMENT OF COMMERCE**  
**(Ed. Sept. 1945)**

POSITION COMPUTATION, FIRST-ORDER TRIANGULATION  
(For calculating machine computation)

$\alpha$	2	to 3					$\alpha$	3	to 2				
$2^d \angle$		&		+			$3^d \angle$		&		—		
$\alpha$	$2 \bar{\Sigma} \rho / TA$	to 1 Arc Point 2000 $y$		150			$\alpha$	$3 \bar{\Sigma} \rho / TA$	to 1 Arc Point 2000 $y$	240			
$\Delta \alpha$							$\Delta \alpha$						
$\alpha'$	1	to 2					$\alpha'$	1	to 3				
First Angle of Triangle													
$\phi$	51° 39' 52.64	2 $\bar{\Sigma} \rho / TA$	$\lambda$	178° 05' 17.57 w	$\phi$	51° 39' 59.64	3 $\bar{\Sigma} \rho / TA$	$\lambda$	178° 05' 17.57 e				
			$s = 299.689.40$	$\Delta \lambda$	+ 02° 17' 00.66		$s = 299.689.40$	$\Delta \lambda$	- 03° 51' 46.14				
$\phi'$	53° 58' 39.00	1 Arc Point 2000 $y$	$\lambda'$	179° 37' 44.77 E	$\phi'$	52° 57' 04.08	1 Arc Point 2000 $y$	$\lambda'$	174° 13' 31.43 w				
1202.4													
$\Delta \phi$			$(\log s = b/(5/10,000)^2 \cdot 673.6030)$		$\Delta \phi$		$(\log s = b/(5/10,000)^2 \cdot 224.5343)$						
$\sin \alpha$	0.500 000 00	+	$\mathbf{x} \text{ cor.} = -\frac{1}{2} fb \cdot 2755.3731$	$(44.28\frac{1}{2})$	$\sin \alpha$	0.500 000 00	$\mathbf{x} \text{ cor.} = -\frac{1}{2} fb \cdot 914.4576$	$(23.83\frac{1}{2})$					
$\cos \alpha$	0.866 025 40	n	$\mathbf{x}' + 149.803.41$		$\cos \alpha$	0.500 000 00	$\mathbf{x}' - 259.514.735$						
$\mathbf{x} = s \sin \alpha$	+ 149.844.700		$\mathbf{H} . 054.866.827$		$\mathbf{x} = s \sin \alpha - 259.538.633$		$\mathbf{H} . 053.554.209$						
$\mathbf{y} = -s \cos \alpha + 259.538.633$			$\mathbf{Hx}' = (\text{approx. } \Delta \lambda') + 8219.238$		$\mathbf{y} = -s \cos \alpha + 149.844.700$		$\mathbf{Hx}' = (\text{approx. } \Delta \lambda') - 13.899.407$						
$\mathbf{a} = (\mathbf{x}'/10,000)^2 \cdot 224.4104$			$\text{Arc-sin cor} = +\frac{V(Va)}{15} \cdot 1733.8810 \cdot 1.425$		$\mathbf{a} = (\mathbf{x}'/10,000)^2 \cdot 673.4793$		$\text{Arc-sin cor} = +\frac{V(Va)}{15} \cdot 4842.9144 \cdot 6.731$						
$\mathbf{y} \text{ cor.} = +fa$	1835.9031	(47.649)	$\Delta \lambda'' + 8220.66$		$\mathbf{y} \text{ cor.} = +fa \cdot 5509.7341 \cdot (82.360)$	$\Delta \lambda''$	$13.906.138$						
$\mathbf{y}_o$	5° 22' 025.97		$\sin \phi$		$\mathbf{y}_o$	5° 22' 025.97	$\sin \phi$						
$\mathbf{y}'$	+ 259.586.28		$\sin \phi'$		$\mathbf{y}'$	149.927.26	$\sin \phi'$						
$\mathbf{y}_1$	5° 985.12.25		$1 + \cos \Delta \phi$		$\mathbf{y}_1$	5° 875.953.23	$1 + \cos \Delta \phi$						
$\mathbf{v}_a$	- 2 415.89		$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta \phi}$		$\mathbf{v}_a$	- 6 994.57	$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta \phi}$						
$\mathbf{y}_2$	5° 983.19.09		$-\Delta \alpha'' \text{ (approx.)}$		$\mathbf{y}_2$	5° 868.956.66	$-\Delta \alpha'' \text{ (approx.)}$						
$\mathbf{v}$	10.765.48	(0.73)	$+ F(\Delta \lambda')^3$		$\mathbf{v}$	10.385.34	$+ F(\Delta \lambda')^3$	$\frac{\text{comp } 9.99}{\text{cor } 2.54}$					
$K(Va/1,000)^2 + .1267 K 5.836.5$			$-\Delta \alpha''$		$K(Va/1,000)^2 + .1228 K 48.9240$		$-\Delta \alpha''$	$\text{corr } KAM$					

**Form 26 a**

**U. S. COAST AND GEODETIC SURVEY  
DEPARTMENT OF COMMERCE**  
**(Ed. Sept. 1945)**

POSITION COMPUTATION, FIRST-ORDER TRIANGULATION

(For calculating machine computation)

POSITION COMPUTATION, FIRST-ORDER TRIANGULATION  
(For calculating machine computation)

$\alpha$	2	to 3					$\alpha$	3	to 2			
$2d\angle$		&		+			$3d\angle$		&		-	
$\alpha$	2 EPI AM	to 1 Arc Point 12004		225°			$\alpha$	3 EPI AM	to 1 Arc Point 36004	225°		
$\Delta\alpha$							$\Delta\alpha$					
$\alpha'$	1	to 2					$\alpha'$	1	to 3			
First Angle of Triangle												
$\phi$	51° 25' 01.17'	2 EPI AM	$\lambda$	179° 17' 33.06 E	$\phi$	51° 25' 01.17'	3 EPI AM	$\lambda$	179° 17' 33.06 E	$\phi$	51° 25' 01.17'	
$\sin \alpha$	0.707 106 78 47		$\Delta\lambda$	+ 01 52 27.21			$\sin \alpha$	0.707 106 78 47		$\Delta\lambda$	+ 05 55 13.49	
$\cos \alpha$	0.707 106 78 47		$\lambda'$	178° 49' 59.73 W	$\phi'$	51° 42 13.82	1 Arc Point 36004	$\lambda'$	174° 47 13.45 W	$\phi'$	51° 42 13.82	
$b = (\gamma/10,000)^2$	161.6647		$(\log s =$	$b = (\gamma/10,000)^2$	141.6647		$(\log s =$	$b = (\gamma/10,000)^2$	143.4825			
$x$ cor. = $-\frac{1}{2}fb$	661.3703	(8.41)	$x$ cor. = $-\frac{1}{2}fb$	5952.3374	227.647		$x$ cor. = $-\frac{1}{2}fb$	5952.3374	227.647			
$\cos \alpha$	.707 106 78 47		$x'$	- 122° 139.04			$x'$	- 381 215.285				
$x = s \sin \alpha$	- 122 147.444		H	.053 063 553			H	.055 842 565				
$y = -s \cos \alpha + t_{fa}$	122 147.444		$Hx' = (\text{approx. } \Delta\lambda')$	- 6746.449			$Hx' = (\text{approx. } \Delta\lambda')$	- 21288.047				
$s = (x/10,000)^2$	161.66433		$\text{Arc-sin } \frac{V(V_B)}{\text{cor}} = + \frac{V(V_B)}{15}$	1124.7829	.759		$\text{Arc-sin } \frac{V(V_B)}{\text{cor}} = + \frac{V(V_B)}{15}$	11953.2930	.25496			
$y \text{ cor.} = +t_{fa}$	1322.5255	(14.616)	$\Delta\lambda'$	- 6747.21			$\Delta\lambda'$	21313.49				
$y_0$	5° 698 238.47		$\sin \phi$				$\sin \phi$					
$y'$	+ 122 147.26		$\sin \phi'$				$\sin \phi'$					
$y_1$	5° 625 422.73		$1 + \cos \Delta\phi$				$1 + \cos \Delta\phi$					
$V_A$	- 1651.43		$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta\phi}$				$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta\phi}$					
$y_2$	5° 823 771.30		$-\Delta\lambda''$ (approx.)				$-\Delta\lambda''$ (approx.)					
$V$	10.21649		$+ F(\Delta\lambda')^3$				$+ F(\Delta\lambda')^3$					
$K(V_B/1,000)^2$	+ 2.7272 x 1214	(0.35)	$-\Delta\lambda''$				$-\Delta\lambda''$					

POSITION COMPUTATION, FIRST-ORDER TRIANGULATION  
(For calculating machine computation)

$\alpha$	2	to 3					$\alpha$	3	to 2			
$2^d \angle$		&		+			$3^d \angle$		&		-	
$\alpha$	2 EPI AM	to 1 Arc Point 2400 <sub>4</sub>	250				$\alpha$	3 EPI AM	to 1 Arc Point 2400 <sub>4</sub>	225		
$\Delta\alpha$							$\Delta\alpha$					
$\alpha'$	1	to 2					$\alpha'$	1	to 3			
First Angle of Triangle												
$\phi$	51	25	01.17	2 EPI AM	$\lambda$	179 17 33.06 E	$\phi$	51	25	01.17	3 EPI AM	$\lambda$
					$\Delta\lambda$	04 58 14.11					$\Delta\lambda$	3 50 44.36
$\phi'$	52	25	08.09	1 Arc Point 2400 <sub>4</sub>	$\lambda'$	175 44 12.83 W	$\phi'$	53	38	29.83	1 Arc Point 2400 <sub>4</sub>	$\lambda'$
												176 51 42.58 W
$\Delta\phi$							$\Delta\phi$					
$\sin \alpha$	- 0.93969262						$\sin \alpha$	- 0.70710678				
$\cos \alpha$	- 0.34202014						$\cos \alpha$	- 0.70710678				
$x = s \sin \alpha$	- 337.939.10	H					$x = s \sin \alpha$	- 254.294.89	H			
$y = -s \cos \alpha$	122.999.77	Hx' = (approx. $\Delta\lambda''$ )	- 17.873.94				$y = -s \cos \alpha$	+ 254.294.89	Hx' = (approx. $\Delta\lambda''$ )	- 13.837.60		
$s = (x'/10,000)^2$	1 141.8870	$\text{Arc-sin } = + \frac{V(V_a)}{15}$	+ 14.17°				$s = (x'/10,000)^2$	646.3168	$\text{Arc-sin } = + \frac{V(V_a)}{15}$	6.76		
$y \text{ cor.} = +f_a$	9 342.9194	$\Delta\lambda''$	- 17.894.11				$y \text{ cor.} = +f_a$	5 288.1614	$\Delta\lambda''$	- 13.844.36		
$y_o$	5 698 258.47	$\sin \phi'$					$y_o$	5 698 258.47	$\sin \phi'$			
$y'$	123 114.64						$y'$	+ 254.429.37	$\sin \phi'$			
$y_1$	5 821 373.16	$1 + \cos \Delta\phi$					$y_1$	5 952 687.84	$1 + \cos \Delta\phi$			
$V_a$	- 11 650.76	$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta\phi}$					$V_a$	- 6 883.02	$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta\phi}$			
$y_2$	5 809 722.46	$-\Delta\alpha''$ (approx.)					$y_2$	5 945 804.82	$-\Delta\alpha''$ (approx.)			
$V$	10.20308	$+ F(\Delta\lambda'')^3$					$V$	10.64960	$+ F(\Delta\lambda'')^3$	$\frac{\text{Comp Sec}}{\text{H.A}}$		
$K(V_a/1,000)^2 + 135.742$	16.45	$-\Delta\alpha''$					$K(V_a/1,000)^2 + .1250x47.376$	5.92	$-\Delta\alpha''$	$\frac{\text{Comp Sec}}{\text{H.A}}$		

$$f = 8.182 \quad K = 0.1212$$

# POSITION COMPUTATION, FIRST-ORDER TRIANGULATION (For calculating machine computation)

U. S. COAST AND GEODETIC SURVEY  
DEPARTMENT OF COMMERCE  
(Vol. Sent 1946)

POSITION COMPUTATION, FIRST-ORDER TRIANGULATION  
(For calculating machine computation)

$\alpha$	2	to 3					$\alpha$	3	to 2			
$2d\angle$		&		+			$3d\angle$		&			
$\alpha$	<b><math>^2EPI</math></b>	<b>PAUL</b>	to <b><math>^1ARC</math></b> Point <b>Z400μ</b>	<b><math>00</math></b>			$\alpha$	<b>3</b>	to <b>1</b>			
$\Delta\alpha$							$\Delta\alpha$					
$\alpha'$	<b>53</b>	<b>53</b>	<b>42.87</b>	<b><math>^1ARC</math></b> Point <b>Z400μ</b>	<b><math>00</math></b>	<b>180</b>	<b>00</b>	<b>00.00</b>	<b>180</b>	<b>00</b>	<b>00.00</b>	
$\alpha'$	1	to 2					$\alpha'$	1	to 3			
First Angle of Triangle												
$\phi$	<b>57</b>	<b>07</b>	<b>31.45</b>	<b><math>^2EPI</math></b>	<b>PAUL</b>	<b><math>\lambda</math></b>	<b>170</b>	<b>15</b>	<b>54.97</b>	<b><math>\phi</math></b>	<b>3</b>	<b><math>\lambda</math></b>
				<b><math>s = 359.627.28</math></b>		$\Delta\lambda$	—	—	—		<b><math>s =</math></b>	$\Delta\lambda$
$\phi'$	<b>53</b>	<b>53</b>	<b>42.87</b>	<b><math>^1ARC</math></b> Point <b>Z400μ</b>	<b><math>00</math></b>	<b><math>\lambda'</math></b>	<b>170</b>	<b>15</b>	<b>54.97</b>	$\phi'$	1	$\lambda'$
<b>1325.384 —</b>												
$\Delta\phi$												
$\sin \alpha$	0.0	—										
$\cos \alpha$	1.000	—										
$x = s \sin \alpha$	0	—										
$y = -s \cos \alpha$	<b>-359.627.28</b>	—										
$a = (x/10,000)^2$	—	—										
$y \text{ cor.} = +f_a$	—	—										
$y_0$	<b>6333.666.584</b>	—										
$y'$	<b>-359.627.28</b>	—										
$y_1$	<b>5914.039.30</b>	—										
$V_a$	—	—										
$y_2$	<b>5914.039.30</b>	—										
$V$	—											
$K (V_a/1,000)^2 +$	—											
$f = 8.170$												

POSITION COMPUTATION, FIRST-ORDER TRIANGULATION  
(For calculating machine computation)

First Angle of Triangle									
$\alpha$	2	to 3							
$2d\angle$		&	+				$3d\angle$		
$\alpha$	2 EPI PAUL	to 1 Arc Point 2400 $\mu$	30				$\alpha$	3 EPI PAUL	to 1 Arc Point 2400 $\mu$
$\Delta\alpha$							$\Delta\alpha$		
$\alpha'$	1	to 2					$\alpha'$	1	to 3
$\phi$	57 07 31.45	2 EPI PAUL	$\lambda$	170 15 54.97	$\phi$	57 07 31.45	3 EPI PAUL	$\lambda$	170 15 54.97
					b = 359 627.28			b = 359 627.28	
$\phi'$	54 17 44.71	1 Arc Point 2400 $\mu$	$\Delta\lambda$	+ 2 45 40.32	$\Delta\lambda$	+ 2 45 40.32		$\Delta\lambda$	+ 4 55 13.38
			x'	173 01 35.29	x'	173 01 35.29		x'	175 11 08.35
	13 82.422			1 140.904		1 140.904		1 140.904	
$\Delta\phi$		(log b = (y/10,000) <sup>2</sup> )			$\Delta\phi$		(log b = (y/10,000) <sup>2</sup> )		
$\sin \alpha$	0.500			969.9883	$\sin \alpha$	0.500		323.3295	
$\cos \alpha$	0.866 025 40		x cor.	- 71.258	$\cos \alpha$	0.866 025 40	x cor.	- 41.141	
$x = s \sin \alpha$	179 813.640		x'	3962.8872	$x = s \sin \alpha$	311 496.359	x'	1320.9627	
$y = -s \cos \alpha$	- 311 496.359		H	.055 289 019	$y = -s \cos \alpha$	179 813.640	H	.056 834 489	
$s = (x'/10,000)^2$	323.0132		$Hx' = (\text{approx. } \Delta\lambda'')$	+ 9 937.780	$y = -s \cos \alpha$	- 17 913.384	$Hx' = (\text{approx. } \Delta\lambda'')$	+ 17 698.556	
$y \text{ cor.} = +f_a$	2.639.8311		$\Delta\lambda''$	+ 82.21	$s = (x'/10,000)^2$	969.7321	$\Delta\lambda''$	14.828	
$y_o$	6 333 666.584				$y \text{ cor.} = +f_a$	7 923.6810		8 317.8678	
$y'$	- 311 528.576		$\sin \phi$		$y_o$	6 333 666.584	$\sin \phi$		
$y_1$	6 022 138.008				$y'$	- 179 956.119	$\sin \phi$		
$V_a$	- 3 520.199		$1 + \cos \Delta\phi$		$y_1$	6 153 710.465	$1 + \cos \Delta\phi$		
$y_2$	6 018 617.809		$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta\phi}$		$V_a$	- 11 039.217	$\frac{\sin \phi + \sin \phi'}{1 + \cos \Delta\phi}$		
$V$	10.895 98		$-\Delta\alpha''$ (approx.)		$y_2$	(e) 142 671.248	$-\Delta\alpha''$ (approx.)		
	1.574		$+ F(\Delta\lambda'')^3$		$V$	11.383 80	$+ F(\Delta\lambda'')^3$	Comp GEN	
			K (Va/1,000) <sup>2</sup> + .1276 x 12.3918					HCN	
			- $\Delta\alpha''$					Copy ✓	

POSITION COMPUTATION, FIRST-ORDER TRIANGULATION  
(For calculating machine computation)

$\alpha$	2	to 3				$\alpha$	3	to 2		
$2d \angle$		&		+		$3d \angle$	&		-	
$\alpha$	2EPI SEGMENT to 1 Arc Point 1400'					$\alpha$	3EPI SEGMENT to 1 Arc Point 2800'			
$\Delta\alpha$						$\Delta\alpha$				
$\alpha'$	1	to 2					180	00	00.00	
						$\alpha'$	1	to 3		

First Angle of Triangle

$\phi$	52	23	09.35	2 EPI SEGMENT	$\lambda$	172	24	19.36' W	$\phi$	52	23	09.35	3 EPI SEGMENT	$\lambda$	172	24	19.36' W
$\sin \alpha$	0.500 000 00			$s=209.782.58$	$\Delta\lambda$	+ 1	35	58.95	$\phi'$	55	36	23.03	1 Arc Point 2800'	$\Delta\lambda$	+ 3	19	40.44
$\cos \alpha$	0.866 025 40			$x' = s \sin \alpha + 104.877.13$													
$y = -s \cos \alpha + 181.677.043$				$Hx' = (\text{approx. } \Delta\lambda'')$													
$\mathbf{a} = (x'/10,000)^2$	109.9921	$^{16.346}$	$^{16.346}$	$\text{Arc } -\sin = + \frac{V(Va)}{15}$													
$y \text{ cor.} = +f_a$	899.7134			$851.0441$													
$y_0$	5 806 068.493			$\Delta\lambda''$													
$y'$	+ 181.693.389			$y = -s \cos \alpha + 36.3.364.086$													
$y_1$	5 987.761.882			$Hx' = (\text{approx. } \Delta\lambda'') + 11.975.842$													
$V_a$	- 1 184.956			$\mathbf{a} = (x'/10,000)^2$	439.6122				$\text{Arc } -\sin = + \frac{V(Va)}{15}$	4.597							
$y_2$	5 986.576.926	$^{7.102}$	$^{7.102}$	$y \text{ cor.} = +f_a$	3595.9399	$^{130.660}$	$^{130.660}$	$\Delta\lambda''$									
$V$	10.7352			$y_0$	5 806 068.493				$\text{Arc } -\sin = + \frac{V(Va)}{15}$	3838.5865							
$K(Va/1,000)^2 + .1259 \times 1.4044$	$^{+ 0.176}$			$y'$	+ 363.484.746												
				$y_1$	6 169.553.137				$\sin \phi + \sin \phi'$	$^{1}$	$^{1}$	$^{1}$	$1 + \cos \Delta\phi$				
				$V_a$	- 5 031.137												
				$y_2$	6 164.522.102	$^{5.433}$			$- \Delta\alpha''$ (approx.)								
				$V$	11.444.50	$^{49}$			$+ F(\Delta\lambda'')^3$								
				$K(Va/1,000)^2 + .1316 \times 153.123$	$^{3.331}$				$- \Delta\alpha''$								
									$\text{Comp. } GBC$								
									$\frac{\text{MC}}{\text{PC}}$								

$$f = 8.4882^2 \cdot 17.842 = 4580$$

$$\text{U. S. GOVERNMENT PRINTING OFFICE 16-34867-3}$$

$$f = 8.1760$$

APPROVAL SHEET TO ACCOMPANY

Survey H-7973

Project CS-343

The field work was supervised closely and the boat sheet inspected daily.

The records and smooth sheet have been inspected and are approved.

The survey is considered adequate.



Thos. B. Reed  
CAPT., USC&GS  
Comdg. Ship PIONEER

RHC

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## TIDE NOTE FOR HYDROGRAPHIC SHEET

~~Division of Coastal Surveys~~

2 February 1953

Division of Charts: R. H. Carstens

Plane of reference approved in 13  
volumes of sounding records for

HYDROGRAPHIC SHEET 7973

Locality South Bering Sea, Alaska

C. Pierce )  
Chief of Party: T. B. Reed ) in 1952  
Plane of reference is mean lower low water, reading  
3.0 ft. on tide staff at Sweeper Cove  
19.8 ft. below B. M. 16 (1951)

Height of mean high water above plane of reference is  
3.7 feet.

Condition of records satisfactory except as noted below:

E. C. McKay  
Section of Tides

Chief, Division of Tides and Currents.

GEOGRAPHIC NAMES  
Survey No. H-7973

Name on Survey	A On Chart No.	B On previous survey No.	C On U. S. quadrangle Maps	D From local information	E On local Maps	F P. O. Guide or Map	G Rand McNally Atlas	H U. S. Light List	K
Alaska									1
<u>Bering Sea</u>		(for title)							2
									3
									4
									5
									6
									7
									8
									9
									10
									11
									12
									13
									14
									15
									16
									17
									18
									19
									20
									21
									22
									23
									24
									25
									26
									27

Names underlined in  
~~red~~ are approved

1-30-53  
L. Heck

Hydrographic Surveys (Chart Division)

HYDROGRAPHIC SURVEY NO. H-7973..

Records accompanying survey:

Boat sheets ...2..; sounding vols. 13...; wire drag vols. ....;  
bomb vols. ....; graphic recorder rolls 5 Envs.;  
special reports, etc. 1. Smooth Sheet; 1. Descriptive Report; ....  
.....

The following statistics will be submitted with the cartographer's report on the sheet:

Number of positions on sheet	.....
Number of positions checked	.....
Number of positions revised	.....
Number of soundings revised (refers to depth only)	.....
Number of soundings erroneously spaced	.....
Number of signals erroneously plotted or transferred	.....
Topographic details	Time .....
Junctions	Time .....
Verification of soundings from graphic record	Time .....
Verification by.....	Total time ..... Date .....
Reviewed by.....	Time ..... Date .....

VERIFIER'S REPORT OF HYDROGRAPHIC SURVEY NO. H- 7973

The verifier should deal with the present hydrographic survey only, as the reviewer considers its relation to previous surveys and published charts. He should be thoroughly familiar with Chapters 3, 7 and 9 of the Hydrographic Manual.

1. The descriptive report was consulted and appropriate notes were made in soft pencil regarding action taken.
2. Soundings originating with the survey and mentioned in the descriptive report have been verified, including latitude and longitude.
3. All reference to survey sheets mentioned in the descriptive report include the registry number and year.
4. Geographic names of hydrographic features if on sheet are in slanting lettering and of topographic features in vertical lettering.
5. All items affecting the plotting of the survey which are entered in the remarks columns of the sounding records were noted and check marked. In all cases appropriate action was taken.
6. All positions verified instrumentally were check marked in the sounding records.
7. All critical soundings are clear and legible and are a little larger than the adjacent soundings.
8. The metal protractor has been checked within the last three months.
9. The protracting and plotting of all bad crossings were verified.
10. All detached positions locating critical soundings, rocks or buoys were verified.
11. The boat sheet was compared with the smooth sheet.

12. The spacing of soundings as recorded in the records was closely followed.
13. The bottom characteristics were shown on outstanding shoals.
14. The reduction and plotting of doubtful soundings were checked.
15. The transfer of contemporary topographic information was carefully examined.
16. All junctions were transferred and overlapping curves made identical.
17. The notation "JOINS H- (19--)" was added in ink for all contemporary adjoining or overlapping sheets now registered. Those not verified are shown in pencil.
18. The depth curves have been inspected before inking.
19. All triangulation stations and transfer of topographic and hydrographic signals were checked.
20. Heights of rocks were checked against range of tide.
21. Rocks transferred from topographic surveys have a dotted curve where shown thereon. Rocks located accurately by hydrographer are encircled by dotted red curve.
22. Unnecessary pencil notes have been removed.
23. Objects on which signals are located and which fall outside of the low water line have been described on the sheet.
24. The low water line and delineation of shoal areas have been properly shown.
25. Degree and minutes values and symbols have been checked.
26. Questionable soundings have been checked on the fathograms.

27. Source of shoreline and signals (when not given in report).
28. All notes on sheet are in accordance with figure 171 in the Hydrographic Manual.
29. All aids located, with those on contemporary topographic sheets, have been shown on survey.
30. Depth curves were satisfactory except as follows:
  
  
  
  
  
  
31. Sounding line crossings were satisfactory except as follows:
  
  
  
  
  
  
32. Junctions with contemporary surveys were satisfactory except as follows:
  
  
  
  
  
  
33. Condition of sounding records was satisfactory except as follows:
  
  
  
  
  
  
34. The protracting was satisfactory except as follows:
  
  
  
  
  
  
35. The field plotting of soundings was satisfactory except as follows:
  
  
  
  
  
  
36. Notes to reviewer:

Verified by

Date

# NAUTICAL CHARTS BRANCH

SURVEY NO. H-7973

## Record of Application to Charts

DATE	CHART	CARTOGRAPHER	REMARKS
1/17/55	8862	D.H. Benson	Fully applied Before <del>After</del> Verification and Review
2/10/55	9102	D.H. Benson	Before <del>After</del> Verification and Review Fully applied subject to corrections after V+R.
4/17/55	9302	D.H. Benson	Before <del>After</del> Verification and Review Fully applied subject to corrections after V+R.
4/28/55	9000	D.H. Benson	Before <del>After</del> Verification and Review Fully applied subject to corrections after V+R.
3/30/55	8802	GTE	Partially applied Before <del>After</del> Verification and Review
Jan 20/56	8865	H.D. Stegman	Before <del>After</del> Verification and Review in part thru 8862 cat
12-8-58	8861	J. Heaton	Partially applied Before <del>After</del> Verification and Review Partly
12/23/58	8863	J.P. Walker	Before <del>After</del> Verification and Review Completely
Dec. '61	8864	L.V.E.	Before <del>After</del> Verification and Review
12/29/77	8863	KANIS	Before After Verification and Review
2/15/80	(16500) 8861	Sager	Consider as a Fully Applied CAT I Survey Before Verification -
2/19/80	(16011) 8802	Sager	Consider as final application of CAT I Survey Before Verification consider as final application of CAT I Survey
<del>4/18/96</del>	16001	D.M. Kalinchen	CONSIDERED <del>AS</del> FULLY APPLIED CAT I

M-2168-1

A basic hydrographic or topographic survey supersedes all information of like nature on the uncorrected chart.  
 Give reasons for deviations, if any, from recommendations made under "Comparison with Charts" in the Review.