

NOAA FORM 77-28 SUPERSEDES FORM C&GS-537

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Acronyms and Abbreviations

ARP – Antenna Reference Point **CO-OPS –** Center for Operational Oceanographic Products and Services **CORS –** Continuously Operating Reference Station **DGPS –** Differential Global Positioning System **Dn –** Julian Day Number **ERS –** Ellipsoidally-Referenced Survey **FPM –** Field Procedures Manual **GPS –** Global Positioning System **HSSD –** Hydrographic Surveys Specifications and Deliverables **IAKAR –** Inertially Aided Kinematic Ambiguity Resolution **ITRF –** International Terrestrial Reference Frame **kHz –** kilo Hertz **MHW** – Mean High Water **MLLW –** Mean Lower Low Water **NAD83 –** North American Datum of 1983 **NAVD88 –** North American Vertical Datum of 1988 **NGS –** National Geodetic Survey **NOAA –** National Oceanic and Atmospheric Administration **NOS –** National Ocean Service **NWLON –** National Water Level Observation Network **POS/MV –** Position and Orientation System for Marine Vessels **PPK** – Post Processed Kinematic **RTK** – Real-Time Kinematic **SBET –** Smoothed Best Estimate of Trajectory **TPU –** Total Propagated Uncertainty **USCG –** United States Coast Guard **UTC –** Coordinated Universal Time **UTM –** Universal Transverse Mercator **WGS84** – World Geodetic System 1984

OPR-D304-FH-12 Horizontal and Vertical Control Report Approaches to Chesapeake Bay, Virginia July 2012 – December 2012 NOAA Ship Ferdinand R. Hassler (S250) Chief of Party: LCDR Benjamin K. Evans, NOAA

INTRODUCTION

This report applies to surveys D00173, H12423, H12424, H12501, H12502, H12503, H12504 and H12505 located in the Approaches to Chesapeake Bay, Virginia. These surveys were performed by the crew of the NOAA Ship Ferdinand R. Hassler under project OPR-D304-FH-12 Approaches to Chesapeake Bay, as specified in the Hydrographic Survey Project Instructions (March 2, 2012) and Change 1 of these instructions (September 18, 2012).

This supplemental report to survey project OPR-D304-FH-12 outlines methods used for collection, processing and application of three-dimensional position and water level correctors on bathymetric data. The format and content of this report varies from traditional Horizontal and Vertical Control Reports outlined in section 8.1.5.2 of the HSSD.

PROJECT PARAMETERS

- 1. Datum: North American Datum of 1983, Zone 18
- 2. Chart Datum: Soundings reduced to MLLW
- 3. Differential Correctors for real-time navigation: United States Coast Guard DGPS beacon, Driver, Virginia (289kHz)
- 4. Filing naming structure: In order to differentiate attitude data recorded by the Internal Motion Unit (IMU) from the ship's two hulls, positioning data file names followed the YYYY-DDD-S250* naming convention (where * is either "S" or "P", signifying data from the starboard or port hull, respectively).

Smooth Best Estimate Trajectory Solution

To improve horizontal and vertical positioning, Applanix POSPac MMS software v.6.1 was used during postprocessing to produce Smoothed Best Estimate of Trajectory (SBET) solutions using an Inertially Aided Kinematic Ambiguity Resolution (IAKAR) solution relative to ITRF00.

The POSPac Smart Base processing method was used to produce the SBET solutions over the course of the entire project. The SmartSelect option was used, which manually computes and downloads a network based on available data.

All surveys in this project are at least 10 nautical miles offshore and could only be encompassed in the Smart Base network by using baselines outside of the 100 km maximum, specified in Section 9.1.1.1 of the NOS HSSD. No other correction procedure yielding similar accuracy (such as Single Base) was possible in this area. As a result, a virtual base station was developed.

The OCS limit of 100 kilometers was exceeded to allow the network to encompass the survey area. Applanix has determined that encompassing the survey area with distant stations is preferable to limiting the network to closer stations that do not fully encompass the survey area. Figure 1shows an example of a network used, including Continuously Operating Reference Stations (CORS), baselines and project survey grounds.

Figure 1: Example of Smart Base network geometry for OPR-D304-FH-12

After a QC process to ensure data reliability, SBET and error files were exported to NAD83 datum using POSPac MMS export function. SBET and error files are given .sbet and .smrmsg extensions, respectively.

METHODOLOGY

Two separate vertical control methods were used in project OPR-D304-FH-12 to reduce data to Mean Lower Low Water (MLLW) levels. Vertical Datum Transformation (VDatum) was used to transform from ellipsoid referenced soundings to MLLW when acceptable 3-D GPS-derived solutions existed. When reliable GPS derived heights were not available, Discrete Zoning was used. CO-OPS provided zoning files and verified tide station values were used for zoned tide reduction. The OPR-D304-FH-12 VDatum Evaluation report, submitted under Appendix I of this report, outlines the comparison techniques and results performed for this project. Appendix I also includes the signed memorandum, approving the recommendations put forth in the VDatum Evaluation report.

Table 1outlines the use of VDatum and Discrete zoning methods.

Table 1: Project sheets and primary mode of deriving waterline

GPS Tides

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VDatum was the primary method used to compute water levels for sheets D00173, H12502, H12503 and H12504.

The Load Attitude and Navigation tool in CARIS HIPS was used to load the navigation, height and attitude data from the SBET files. GPS Tides were processed using the VDatum separation file provided by HSD OPS¹ with CARIS HIPS Compute GPS Tide tool. After SBET files and GPS tides were computed, CARIS HDCS lines were Sound Velocity Corrected (to apply attitude) and Merged (to apply navigation). Specific settings are shown in Figure 2. For surveys reduced to MLLW using ERS methods, the Apply GPS Tide box was selected during the Merge process. After the application of GPS Tides, the vertical solutions were examined for errors or artifacts.

¹ Rev1 applied to surveys H12504 and H12505 per D304-FH-12_revised_SEP.pdf submitted with individual survey's project correspondence folder.

Figure 2: CARIS SBET Application Options. Merge dialog shows "Apply GPS Tide" button checked, this was done only on data being referenced to MLLW via ellipsoidal processing techniques

Post-processed uncertainty estimates (SMRMSG files) for position, height and attitude were applied using the CARIS HIPS Load Error tool and used during the calculation of TPU by checking Error Data for the uncertainty source in the HIPS Compute TPU tool. Figure 3 shows specific options chosen during CARIS application of SMRMSG data:

Figure 3: CARIS SMRMSG error loading parameters

For all data reduced to MLLW using VDatum, a zoning uncertainty value of 0.081 meters was used in the CARIS HIPS Compute TPU process in accordance with the project instructions.

Verified Tides

Discrete zoning is the primary method for vertical control for sheets H12423, H12424, H12501 and H12505. The active NWLON station at Duck, North Carolina (865-1370) is the reference station. This station was damaged during Hurricane Sandy (October 29, 2012) and taken offline for repairs. The station remained offline until the end of November. *Hassler* did not acquire any data on this project during this outage. The station was operating normally when operations resumed in December 2012.

After receiving the final tide notes from CO-OPS, verified tides were downloaded and applied using the CARIS HIPS Load Tide tool. The preliminary zoning file was accepted as final for all sheets within this project. The zoning uncertainty to be applied during Compute TPU was not provided by CO-OPS due to lack of available water level time series data. The value from the previous year adjoining project (OPR-D304-FH-11), 0.09 meters, was used for this project.

CASE-BY-CASE DATA MODIFICATIONS

Interpolation of GPS Tide Errors Using SBETs

In limited areas throughout the survey, errors in the GPS-derived vertical position solution led to vertical errors in the associated soundings. These altitude errors were located by examining the surface for areas of high standard deviation. CARIS Subset Editor and Attitude Editor were used to isolate the error in these cases to a GPS height error.

These errors are most apparent in the "GPS Tide" record generated in CARIS. This record is calculated during the "Calculate GPS Tide" process by removing the inertial generated heave record (Trueheave) from the postprocessed GPS height solution (from the applied SBET) and applying the datum-ellipsoid transformation model. The resultant record should contain both the tidal signal and any loading or dynamic draft effects. In cases where there was both an apparent vertical error in the corrected soundings and the GPS Tide record had physically unreasonable jumps or anomalies, the GPS Tide anomalies were rejected in CARIS Attitude Editor and the resultant gap linearly interpolated. For short duration anomalies contained wholly within the line, this rejection and interpolation could be done simply in Attitude Editor.

For lines where GPS tide anomalies extended beyond the end of the line, this simple interpolation approach was not feasible because the heave record, and thus the derived GPS height record, does not extend beyond the end of the line. In these cases, the SBET attitude was reapplied with a buffer beyond each end of the line. The GPS height was smoothed through application of a 60 second moving average (effectively removing heave without reliance on the inertial data) and the GPS height re-calculated with the smoothed GPS height shown in Figure 4. These extended GPS tide records were then interpolated in a similar fashion as described above.

Figure 4: Compute GPS Tide - Interpolated Options

GPS Height Interpolated Lines							
Survey	Vessel	Dn	Line	Survey	Vessel	Dn	Line
H12502	Port	253	052534	H12503	Port	267	050830
			060806			268	131439
		256	175640			269	142919
			183429		Starboard	268	041818
		257	165620				120524
		271	114027				131439
	Starboard	252	010824				152117
		253	064636			269	161909
		256	001107				181746
			183429	H12504	Starboard	286	185218
		257	140950			345	225301
			145000			346	183719
			165619				
		266	183542				
		271	114026				

Table 2: Project sheets and lines which the GPS height was interpolated

Applanix True Heave

Experimentation was conducted during the field season on the reliability of internally logged Trueheave files in the POS M/V. Downloading these files while concurrently logging the internal file, which is required for 24 hour operation, causes data gaps.

Some of these data gaps were corrected by applying the concurrently logged Ethernet files when available. In few cases it was necessary to completely remove the TrueHeave record from the CARIS HDCS directory and apply real time heave correctors. Table 3 outlines the primary Trueheave file format used and any exceptions.

Table 3: Project sheets and associated Trueheave files used. NOTE: i, e, n = Internal, Ethernet, None

LETTER OF APPROVAL

The letter of approval for this report and all accompanying data follows on the next page.

UNITED STATES DEPARTMENT OF COMMERCE National Oceanic and Atmospheric Administration NOAA Marine and Aviation Operations NOAA Ship *Ferdinand R. Hassler* S-250 439 West York Street Norfolk, VA 23510

March 20, 2013

As Chief of Party, I have ensured that standard field surveying and processing procedures were adhered to during acquisition and processing of horizontal and vertical control data in accordance with the Hydrographic Manual, Fourth Edition; Field Procedures Manual, April 2012; and the NOS Hydrographic Surveys Specifications and Deliverables, as updated for April 2012. Additional guidance was provided by applicable Hydrographic Technical Directives. All data and reports are respectfully submitted to Atlantic Hydrographic Branch.

I acknowledge that all of the information contained in this report is complete and accurate to the best of my knowledge.

In addition, the following individuals were responsible for oversight of acquisition and processing of this data:

> LT Madeleine M. Adler, NOAA Field Operations Officer

____________________________________ LT Samuel F. Greenaway, NOAA Executive Officer (Field Operations Officer during acquisition)

